CHRis Swenzy

EVALUATION OF PUMPING TEST RESULTS CHULUOTA WELL SITE

SEMINOLE COUNTY, FLORIDA

JAMMAL & ASSOCIATES, INC. Consulting Engineers

MEMBER

Associated Soil and Foundation Engineers, Inc. American Consulting Engineers Council National Society of Professional Engineers Florida Institute of Consulting Engineers American Society for Testing and Materials American Concrete Institute

1675 Lee Road, 32789 📕 P.O. Box 339, Winter Park, Florida 32790 📕 Telephone (305) 645-5560

TABLE OF CONTENTS

| | <u>Page</u> |
|---------------------------------------|-------------|
| LIST OF FIGURES | i |
| LIST OF TABLES | i |
| EXECUTIVE SUMMARY | ii |
| INTRODUCTION Purpose and Scope | 2 |
| GEOLOGIC AND HYDROLOGIC CONDITIONS | • |
| Geology | 4 5 |
| FIELD INVESTIGATIONS | |
| Well Construction. | 7 |
| Area Well Inventory | 8 8 |
| Water Quality Tests. | 9 |
| RESULTS | |
| Water Quality Tests | 10 |
| Aquifer Performance Test | ĩi |
| Model Simulation | 13 |
| CONCLUSIONS | 14 |
| REFERENCES | |
| APPENDICES Adjacent Floridan Users | |

Aquifer Performance Test Data Water Quality

÷

 $\mathbf{\Lambda}$

LIST OF FIGURES

| 50 | 1.1 | LOW | с р | > A - | GE |
|----|-----|-----|-----|-------|-----|
| τv | | -vn | υr | · H I | ac. |

| Figure #1 | : Site Location, Chuluota Well Field | 3 |
|------------|--|----|
| Figure #2 | : Location of Adjacent Floridan Users | 8 |
| Figure #3 | Chlorides and Total Alkalinity Concentrations During the 72-Hour Pump Test | 10 |
| Figure #4: | Calcium and Sodium Concentrations During the 72-Hour Pump Test | 10 |
| Figure #5: | Sulfate, Magnesium and Potassium Concentrations During the 72-Hour Pump Test | 10 |
| Figure #6: | Time/Drawdown in Observation Well #2 | 11 |
| Figure #7: | Time/Recovery in Observation Well #2 | 11 |
| Figure #8: | Simulated Drawdown Associated with Pumpage at 500 gpm, Chuluota Well Field | 13 |
| | LIST OF TABLES | |
| | | |

| Table 1: | Water Sampling Intervals | 9 |
|----------|--------------------------------|----|
| Table 2: | Aquifer Performance Parameters | 12 |

EXECUTIVE SUMMARY

Southern States Utilities (SSU) has proposed to install and operate a back-up potable supply well to the existing supply wells currently servicing residents within SSU's service area in Chuluota, Florida. An investigation was performed to evaluate the potential impacts of groundwater withdrawals from the proposed Well #1 located at the corner of Brumley Road and The investigation included installation of two (2) Avenue H. wells, conducting a test 72-hour aquifer pumping test. laboratory analysis of collected water samples and interpretation of the resultant hydrologic data.

Analysis of water samples collected at selected time intervals during the 72-hour pumping test indicated that water produced from the well is of the transitional water type (TW) as defined by Frazee (1982). Time-related samples were collected to detect changes in water quality with time during the test. Sample analysis showed that the concentration levels of most ions decreased during the 72-hour period of the pump test suggesting that the pumped aquifer was receiving freshwater recharge from overlying hydrologic units.

Analysis of the pump test data indicates that the upper portion of the Floridan aquifer behaves as a leaky artesian aquifer. Observations made in the field indicate that a drawdown of approximately 14 feet may be expected within the pumping well at a discharge of 500 gpm. Subsequent model simulations of pumpage from the well indicate that less than one (1) foot of drawdown of the potentiometric surface of the Floridan aquifer will be seen at distances greater than 600 feet from the well.



-ii-

A well inventory did not locate individuals using the same aquifer within this 600 foot radius. The model simulation indicates that a maximum drawdown of 0.3 feet is expected in the well of the nearest adjacent user as a result of the proposed pumpage from Southern States Utilities Well #1.

Based upon the results of the aquifer performance test and analysis of the resultant hydrologic data, Jammal & Associates, Inc., concludes the following: [Groundwater of suitable quality for drinking purposes is available from Southern States Utilities Well #1 at the design pumping rate of 500 gpm. 2 Time-dependent water quality test results strongly suggest that pumpage from Southern States Utilities Well #1 at the design pumping rate will not have an adverse impact on water quality in the Floridan aquifer or on adjacent water wells.

Ζ

-iii-

INTRODUCTION

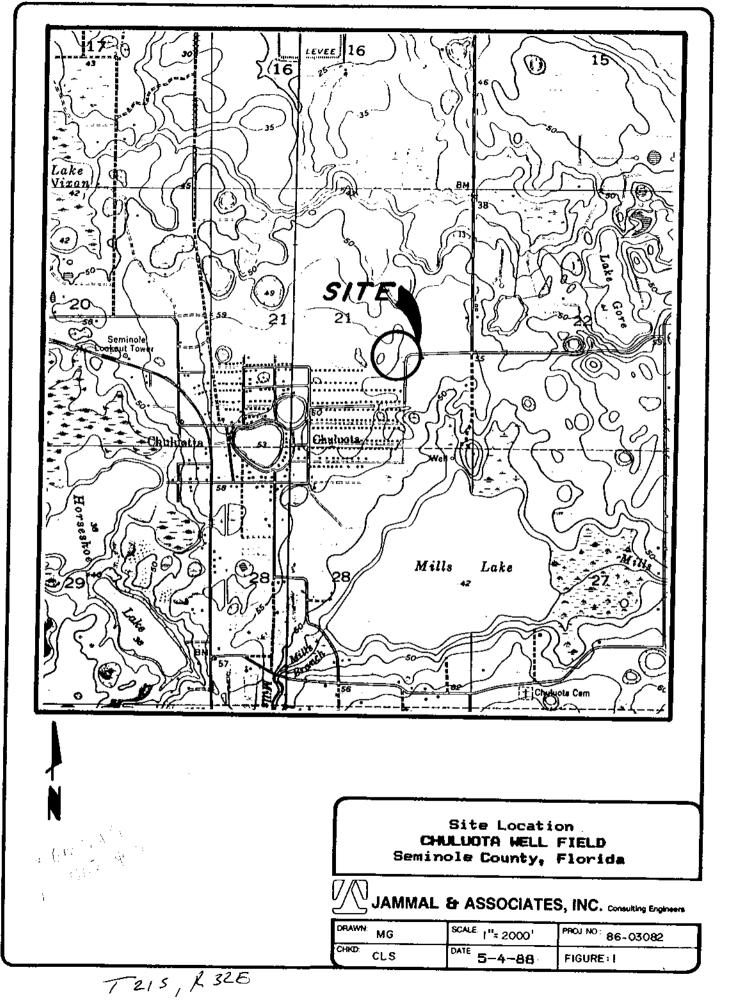
Purpose and Scope

A drinking water supply facility proposed for construction by Southern Utilities, State Inc.. is located in an area designated as a special condition zone by the St. Johns River Water Management District (SJRWMD) because of its proximity to an area where water quality in the upper Floridan aquifer has characteristics of relict sea water. The facility exists in an area labeled as a transitional zone where water quality for the upper Floridan indicates mixing of fresh water recharge with more mineralized water. Published literature indicates that water quality in the Floridan aquifer generally deteriorates towards the east, in the direction of the St. Johns River.

Two test/production wells were constructed at the proposed Chuluota Well Field to provide a means of collecting certain hydrologic data in the immediate vicinity of the proposed well site. One of the wells will be designated as a stand-by well to the existing Southern States Utilities Chuluota water supply facility while the other well will be used as a permanent observation well, providing an avenue to obtain hydrologic information from the upper Floridan aquifer.

An aquifer performance test was conducted to estimate aquifer hydraulic characteristics in the vicinity of the proposed wells. The aquifer coefficients determined from the pump tests were employed to construct a model to simulate the effects of withdrawals from the proposed back-up well.

-2-



Water samples were collected at selected intervals during the course of the aquifer performance test and submitted to an independent chemical laboratory for analysis. A geochemical pattern analysis was conducted on each of the collected samples in order to isolate trends in water stability with time.

Based upon collected geologic and hydrologic information, conclusions regarding the availability and quality of potable water from the proposed site are presented.

Project Location and Site Description

The proposed Chuluota Well site is located approximately one mile east of S.R. 419 in southeast Seminole County. Figure 1 shows the location of the proposed site. Well #1, designated as stand-by well, is a 10-inch well located approximately 75 feet west of the intersection of Brumley Road and Avenue H. Well #2, designated as an observation well, is a 10-inch well located 200 feet west of Well #1.

The surficial land surface features surrounding the proposed well site are characterized by low relief with an estimated 1% to 2% grade toward a depression located approximately 300 feet to the north. Residential housing exists approximately 700 feet to the south and west and approximately one-quarter of a mile to the east.

GEOLOGIC AND HYDROLOGIC CONDITIONS

<u>Geology</u>

The regional geology for the site consists of thick marine limestone and dolostone deposits overlain by sand, clays and silts (Lichtler. 1972). Far below those units are the crystalline rocks of the basement complex. In the site vicinity, wells typically penetrate only the upper 200 feet of stratum.

Geologic logs from wells drilled in the area typically contain sections including deposits from Eocene Age limestones to Recent Age fine sands. Penetrated Eocene limestone deposits consist of soft, cream colored, shelly limestones known as the Ocala Formation. Geologic logs from the completed test/production wells indicate that the top of the Ocala is at a depth of approximately 160 feet.

Unconformably overlying the Ocala Formation are deposits of silt, clay and limestones collectively known as sand. the Hawthorn Formation. The clayey sands of the Miocene Age Hawthorn deposits effectively retard the vertical movement of water into the lower Floridan aquifer. Lower portions of the Hawthorn Formation many times contain limestone sections that when in direct hydraulic contact with the lower Eocene limestones are considered part of the Floridan aquifer

(Lichtler, et al, 1968). Geologic logs from the constructed test/production wells indicate that the Hawthorn is approximately 140 feet thick in the site vicinity.

Overlying the Hawthorn are more recent Pleistocene to Recent undifferented deposits. These deposits generally make up the upper 20 feet of sediments as shown by the geologic logs of the on-site wells. These deposits are composed of layers of fine sands differentiated only by color and minor trace constituents.

<u>Hydrogeology</u>

Within the project area, principal aquifer systems exist under artesian and non-artesian conditions. The non-artesian or unconfined aquifer in Seminole County is composed of a series of sand and clay deposits varing in thickness from 75 to over 150 feet thick (Barraclough 1972). Collective deposits of the Hawthorn Formation and overlying Pleistocene to Recent sands compose portions of non-artesian aquifer. Groundwater within this aquifer exists under atmospheric conditions and is. directly affected by climatic factors such as rainfall and evapotranspiration. In the areas of the proposed well field. the non-artesian aquifer yields relatively small amounts of water.

The primary aquifer in Seminole County is the artesian, or Floridan aquifer. In the area of the proposed well field, the Floridan consists of the Eocene limestone and dolostone deposits as well as the lower limestone deposits of the

overlying Hawthorn Formation which are in direct hydraulic contact with the lower Eocene units. The geologic logs from the test wells suggest the top of the Floridan is approximately 120 feet below land surface (bls). The constructed test/production wells tap approximately the upper 90 feet of this aquifer.

Existing fresh groundwater supplies are derived primarily from rain that falls in recharge areas of Polk and Orange Counties (Barraclough, 1962). However, it is suspected that considering the numerous occurrence of sinkholes and depressions surrounding the proposed well site, that local recharge is also significant. Maps presented by Barraclough, 1962 suggest a moderately effective recharge area located directly south of the well field. Lichtler, 1972, suggests that the well field may be included in the recharge areas.

Surface soils consist of Blanton, Lakewood and Plummer fine sands which are typically moderately well drained. Average rainfall is approximately 7.0 inches per month in summer and 2.5 inches per month in the winter. Annual totals approximate 53 inches during an average year. Although rainfall and surface soil conditions are conducive to vertical infiltration, numerous clay layers within the underlying Hawthorn Formation retard downward movement locally.

Water quality in the upper Floridan aquifer in the vicinity of the wells is termed transitional, meaning that water quality data show characteristics of both fresh recharge and connate waters (Barraclough, 1962). These characteristics may be the result of the mixing of fresh water recharge with connate water. The connate water is believed to exist as a reminant of the Pleistocene Epoch interglacial period or by the entrapment of sea water during the formation of the rock unit. The source for the poorer quality water is likely the lower portion of the Floridan aquifer.

Analysis of water from wells tapping the upper Floridan aquifer north and eastward from the proposed well field indicate increasingly poor water quality in those directions. Maps presented by Barraclough, (1962), show water with total dissolved solids and chloride concentrations in excess of Florida drinking water standards from wells tapping the upper Floridan aquifer 2 to 3 miles east of the proposed well field. This area is generally comparable to areas of artesian flow.

FIELD INVESTIGATIONS

Well Construction

During the construction of Well #1, Jammal & Associates, Inc., was present to conduct on-site geologic logging of rock cuttings from the well. Field tests for chlorides, pH and hydrogen sulfide were completed during construction of Well #1 to monitor water quality with depth. Based upon the field tests and analysis of the well cuttings retrieved during

-7-

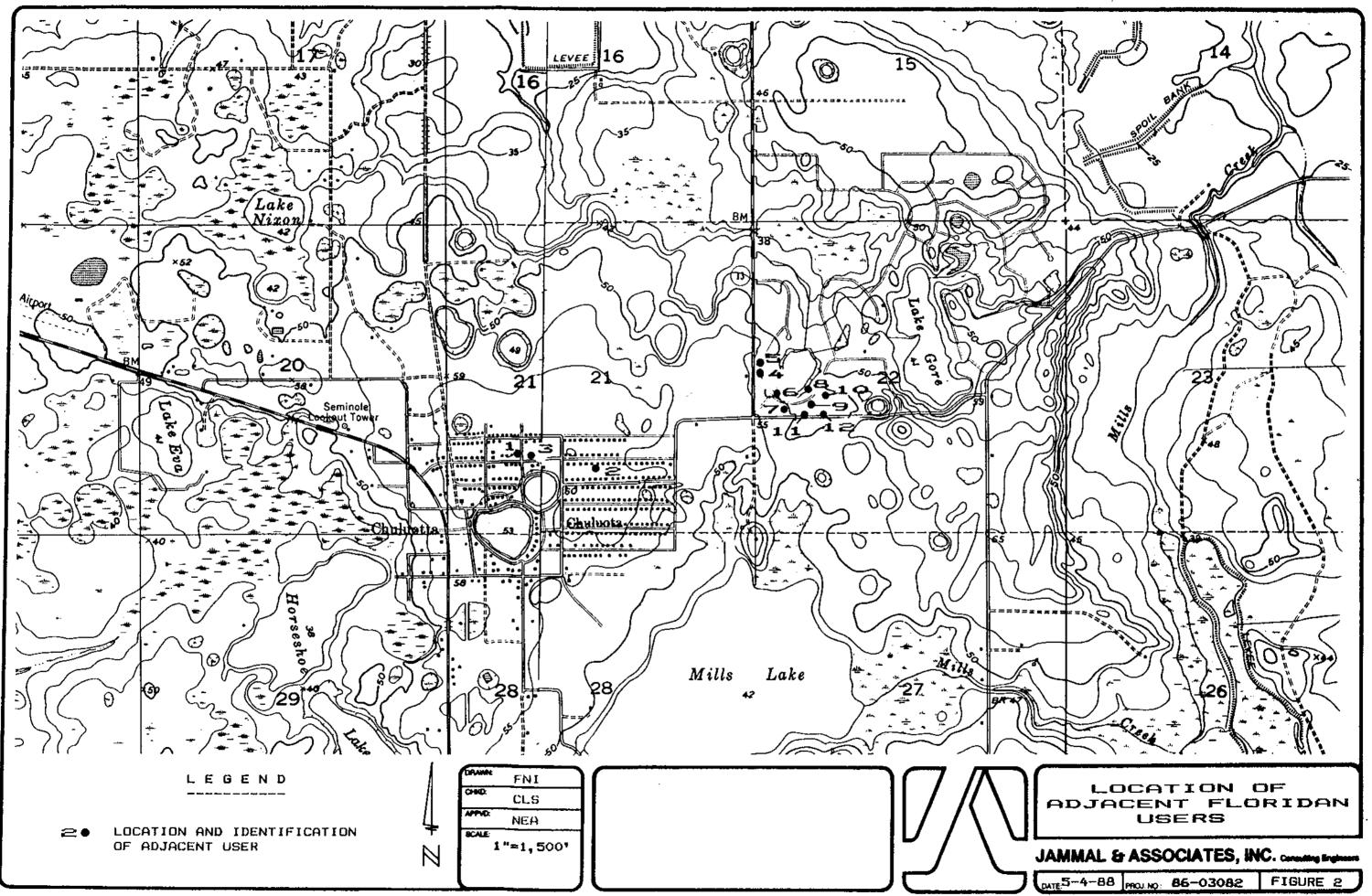
drilling, a completion depth of 218 was determined for Well #1. Casing in this well was set to a depth of 122 feet bls. Well #2 was completed in a similar manner to Well #1.

Area Well Inventory

A field survey was conducted to identify permitted and/or non-permitted Floridan aquifer wells within the predicted radius of influence caused by pumpage from the proposed well. Figure 2 shows the locations of identified adjacent users within a 1/4 mile to 1/2 mile radius from the proposed well. The identification of the adjacent users was limited by the availability and cooperation of the individual homeowners. A table listing the names, addresses, depth of well, map identification and use of each well is presented as an Appendix.

Aquifer Performance Test

In order to determine estimates for the aquifer coefficients in the area adjacent to the proposed back-up supply well, a constant rate discharge test was conducted utilizing the two (2) recently constructed test/production wells. The test consisted of pumping Well #1 at a constant rate of 514 gallons per minute (gpm) for a period of 72-hours. Prior to the start of the test, a Stephens F-Type water level recorder was installed on the observation well (Well #2) to monitor changes in the water level before, during and after the constant discharge test. Water levels were recorded for a period of one (1) week prior to the start of the test to observe natural



RAPHIX #24

fluctuations of the potentiometric surface over time. The first four hours of drawdown and recovery were measured manually. The time/drawdown and time/recovery data obtained during the course of the test are presented in the tables attached in the Appendix to this report.

Water Quality Tests

During the course of the aquifer performance test water samples were collected and taken to an independent chemical laboratory for analysis. A total of 8 samples were collected during the 72-hour period that the test was conducted. Seven of the collected samples were analyzed for cations and anions necessary for the completion of a geochemical pattern eighth sample, collected after 72-hours of analysis. The pumpage, was analyzed for National Interim Primary and State of Florida Secondary Drinking Water Standards. The table below indicates the time since the start of pumpage that each of the samples was collected.

TABLE 1

<u>Water Sampling Intervals</u>

| SAMPLE IDENTIFICATION | SAMPLING TIME (HOURS)* |
|-----------------------|------------------------|
| Sample 1 | 0.2 |
| Sample 2 | 3.9 |
| Sample 3 | 8.2 |
| Sample 4 | 20.7 |
| Sample 5 | 29.7 |
| Sample 6 | 44.9 |
| Sample 7 | 54.7 |
| Sample 8 | 72.0 |

*Time since start of pumpage on 72-hour test.



-9-

RESULTS

Water Quality Testing

Water samples collected during the aquifer performance test (APT) were analyzed by Bionomics Laboratory, Inc. of Orlando, Florida. Results of the tests indicate that all analyzed parameters are within standards for potable water as stipulated in Chapter 17-22, F.A.C.. The results of the laboratory analyses are presented in the Appendix.

A geochemical pattern analysis was completed on each of the eight (8) water samples collected during the aquifer performance test. Analysis of the samples indicated that Well #1 is withdrawing water of the transitional water type (TW) as described by Frazee (1982).

The time-related results of the analyzed water samples show that water quality over the course of the test was stable. Figures 3, 4 and 5 show the progression of concentrations for selected indicator ions during the course of the 72-hour pump test. Examination of these figures and the laboratory data from which they were constructed suggests that in general, the concentration of minerals in the water withdrawn from Well #1 decreased slightly with time of pumpage.

Aquifer Performance Test

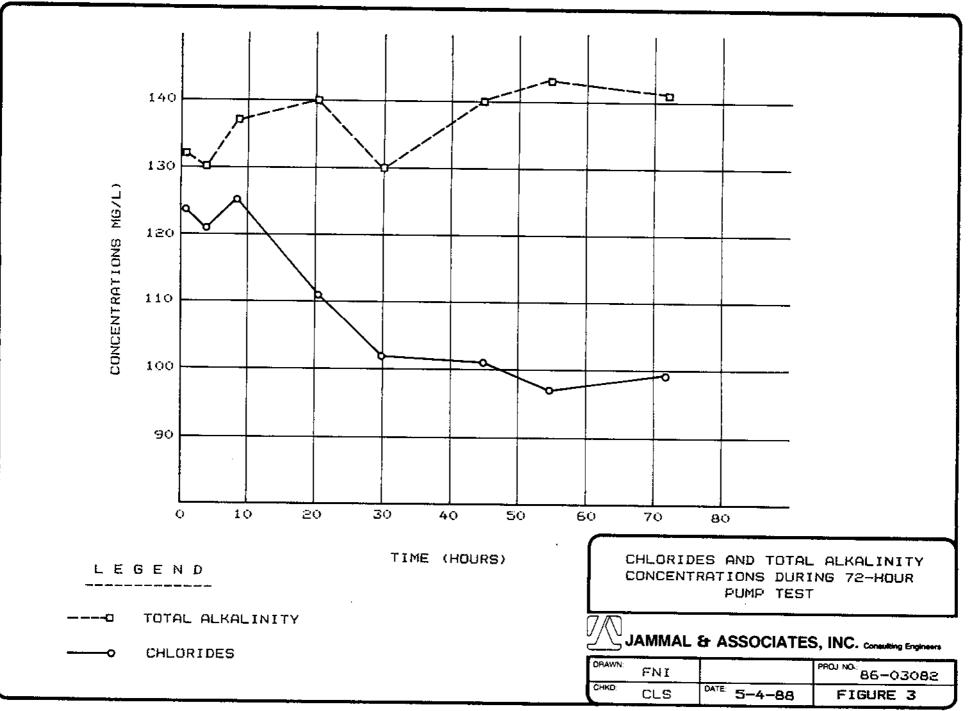
Time/drawdown and time/recovery data collected during the 72-hour constant rate test were evaluated to determine estimates

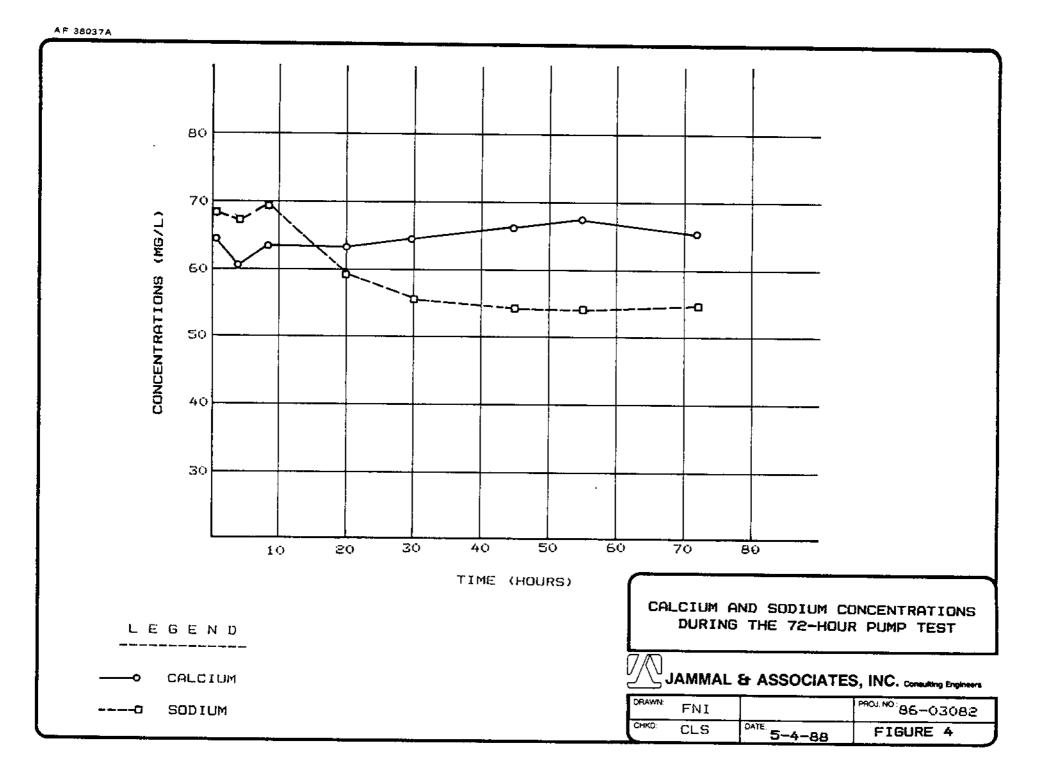
÷,

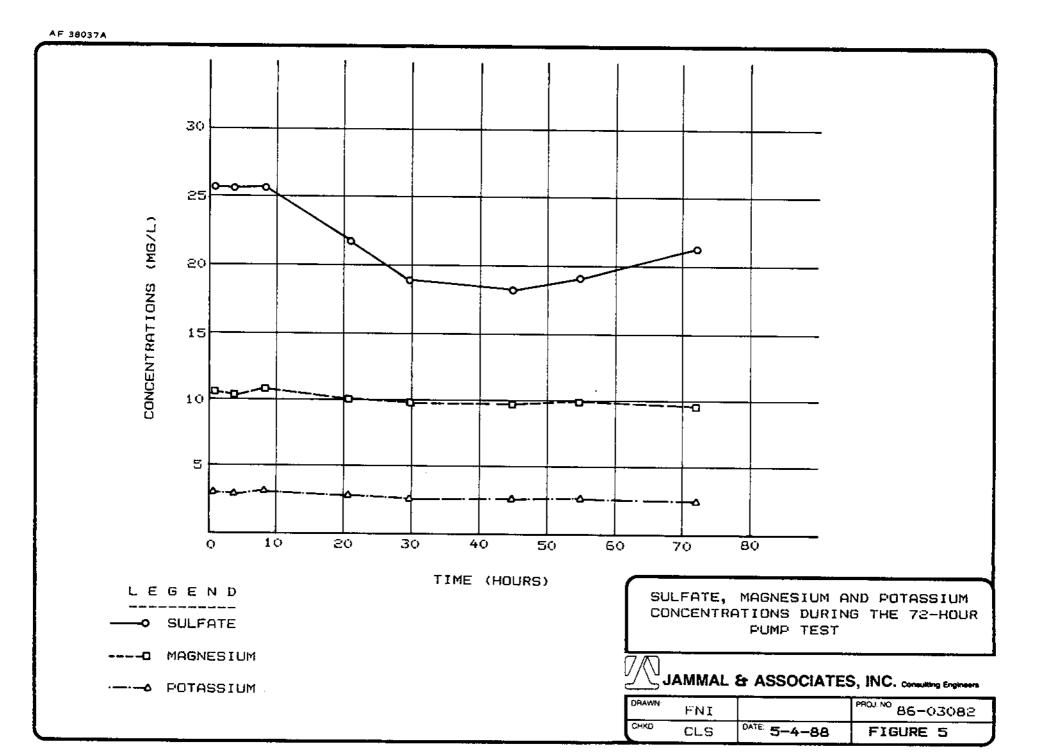
3

Z









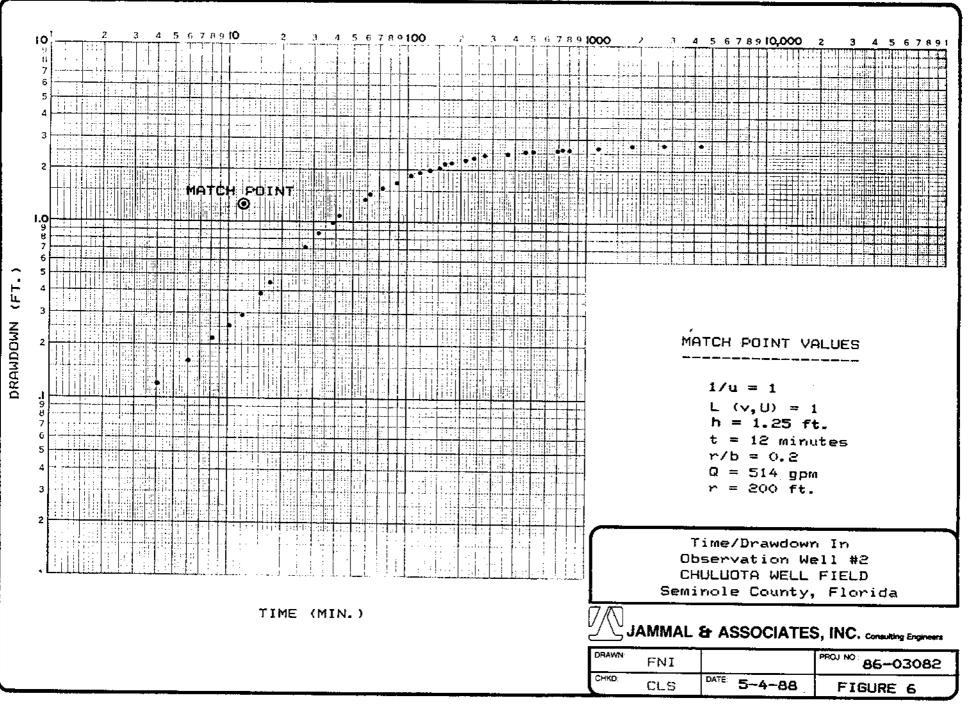
for certain hydraulic parameters necessary to assess the impacts of withdrawals from proposed Southern States Utilities Production Well #1. The data were evaluated using graphical and computer-simulated curve-matching techniques for a leaky artesian aquifer. Figures 6 and 7 graphically present the drawdown and recovery curves used for the type curve analysis described by Hantush and Jacob (Lohman, 1972). This method assumes that the aquifer is a homogenous, isotropic, semi-confined aquifer of infinite aerial extent with recharge from adjacent hydrologic units.

The basis of the curve matching technique requires matching the recorded time/drawdown and time/recovery data to a set of pre-defined "type" curves. Upon a match of the two curves, a match point is selected. The match points selected for each curve are shown on Figures 6 and 7. The values associated with each match point are applied to calculations which yield values for transmissivity, storage and leakance.

In addition to the manual curve-matching technique, a computer automatch technique was used. The computer simulated automatch works on much the same principle as the manual curve matching technique, however, the curves are matched by a mathematical least-squares fit to determine the hydraulic parameters.

Analysis of the drawdown and recovery data produced the results presented in Table 2.





| 10 | | | | 2 | | | 3 | | 4 | 5 | _ | ß | 7 | 8.9 | • 1• | 0 | | | : | 2 | | 3 | | 4 | 5 | 6 | 7 1 | ήo | 10 | ∞ | | | | | | з | | л | ς, | ÷. | 7 | я q |) IC | ∞ |) | | 2 | | 3 | | 4 | 5 | 6 | 7 A | I Q | 10 | ,00 | იი | | 7 | | з | | a | 5 | 6 | 7 | яq | . 1 |
|---------------|-----|-------|------|------|------------|------|-----|---------|-----------|-------------|-------|-----------|----------|---------|------------|-----------------|----------|-------|---|------|-------------|---------|----------|------|---------------|----------|----------|----|----|----------|--|-----------------|-----|-----------|--------------|-----|----------|---------|-------------|-----------|-------------|----------|------|----------|----------|------|-----------|----|-----|----------|----------|------------|-----|---------|-----|-----|----------|-----|------|----|------|-----|---------------|-------------|-----------|------------|------|------|-----|
| 10 11 7 | | | | | | ••• | | İ | | | | | ſ | | | | | | | | | - - | Ţ | [. |]. | | | İİ | ļ | | | | • | | | ľ | | | 1 | ; . . | | 1 | | - | | | 1. | | | | | 17 | 1 | | | Ţ | | T | | Ī | · | | | | | <u> </u> | Ť. | | |
| 6 | | | | | | | | - | | - | | | | | - | | | 1 | | | - | | | | - | | + | | - | + - | | • | | | | + | | | | | - | -+ | - ' | | - | · · | | | | - | | | | | | | | | | - | | | | | | | | | |
| 5 | | | | | - | | Ĺ | i. | | | | | | | Ì | : | | | | | | | | | - | <u>-</u> | | | 1 | - | | ; | . : | | | | 1 | | | | İ | | | | | | | | | | | | - | | | | · | | | ┢ | | | | | | | | | |
| | | | • | | | | - | - | | | ! | | | | | | | | | | | | | | | | | - | | | | | • | | | | - | | | | | | | | | | | | 1 | | | | | | - | | | | | | | | | | | | | | |
| 2 | | | ••• | | | | | | | | | | | | | | • | | | | | | | | | | | | | | | | • | • | | | • | • | • | • | | • • | | | | | | | | | | | | | | | | | | | - | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | | | | | l. | | • | | • | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | li | | | | 1 | | | | | 11 |
| 1.0 | | | | | | | M | | | 1 | · · · | F | D | I | N | T | | | | | | | | | | | 1.1221.1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| LO | | Ŀ | | | | | | ተነ | | | 6 |) | | | | | | | | | | | | | | | | | | | | | | | | | - | | | 1 | - | | | | | | | | | | | | | | | | | | | - | | | | | | | + | | |
| 7 6 | | | | | | | | 1. | | | | | | | | ÷• !• | | ļ | | ¦: → | - - - | | | | : | | | | | • • | · · · | <u></u> | ÷ | | - | | | | - - - | | | | | • | <u> </u> | ···· | <u> -</u> | | • | | | | | | - | | <u> </u> | | | | | | : · . · | | | | - | | |
| 5 | | | | | | | | | | | ÷ | ; ; | - | | : | • | •- | | | | - | - | | ÷ | | | - | | | | ii | ļ.: | | + | | | | · :: | | - | <u> </u> _, | ·-+ | | | | | | - | | | | - | + | | · | | | - | | | - | | | | | | + | H | |
| 3 | | | | | | | | | | | | | | | | с. 1 1 | | | | | | | | | | | | | | | 4 4 4 4 | i 1 i - | | · · · · · | | | | | | - | | | | • • | . : . | : | I | Ι. | Ъ., | . ! | . | . [| | - I | | 4 - | | | | ! | . i. | . 1 | ÷. | .ł.,. | <u>1.</u> | . . | 4 | ł t | 1 |
| 1 | | - | | | | | | | | | | | | | Ţ | | | | | | | | | | | | | | | | | Ħ | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 2 | | + | | - | | | | | | | | | | | | : | +- | 15 | | | | | | | | - | | | | <u> </u> | | | - | | | | | - | 1 | | - - - | | | | | | | | | | M | AT | гс | н | F | PO | 11(| דע | • | v | 31 | | FC | 2 | | | | | |
| | | | | | | | | - | | | | | | | - | H | 1: | | | | | | | :::: | | • | | | | 1 | | | | | | | | · • | | | | | | | | | | | | | | | | | | | | | | | | | | - | • | | | | |
| | : : | | | | | | | | | !: · | | ۰ ۰.۰ | Ŀ | | | | ! ;) | li | | | | | | | | | | | | : | | | , | | | | | | | | | | | | | | | | | | | 1 | | | = | = | 1 | | | | | | | | | | | | |
| 9 | | ╈ | | t | | | | | +++- | - | | 1.1 | | | + | | | | | | + | + | | | - | | | | | | ÷ | ∔ <u>-</u> } | | | | | | | | | | | - | | | | | | | | | | | | | | • | | 1 | | | | | | | | | | |
| 7 - | | ┥┥ | | | | | | | | | | | | | +- | | | | | | | - | | - | 1 | | | | | | | | | | | | <u> </u> | | | - | | | | | | | | | | | | ŀ | ר | = | C | ٥. | 82 | 2 | f | t, | | | | | | | | | |
| 5 | | | | | | | | 1. | | | - | - <u></u> | | | - | | | +-+ | ÷ | | | - | | ÷ | $\frac{1}{2}$ | | | | | | | | | | | ŀ÷ | _ | | - | : | | ┥┯╸┝╴ | | | | | | | | | | t | | | | | 82 0. | | | iı | ทบ | ıt | ë: | 5 | | | | | |
| 4 | - | | | - | | - | | | | | : | | | ••••••• | | | | | | | | - | . | | | | | | | | | <u>;</u> ; | - | | | | | | | | - | | | | | | | | | | | | | | | | 4 | | | 'n | | | | | | | | | |
| 3 | | | | | | •••• | | | | | 4 | ia :. | | | - | 1 1 - 1 1 | | | | | | | | | | | | | | ; | | • : • : • | : | i: | | | | | | | | | | | | | | | | | | ٣ | • | = | 8 | 20 | Ó | f | t. | • | | | | | | | | | |
| 2 | | | | | | | | . - | | | | | | | | | | | | | 1. | | | | | | | | | • | •••••••••••••••••••••••••••••••••••••• | | ŀ | | | | | | | | | •- | | 1 | _ | | | | | | _ | _ | | | | _ | | | | | | | _ | | | | | | |
| | | | 1 | | | | | 加加二 | | | :. | | | 1 | | 1 ! | ' ' | [: T | | | 1 | | | | | | | ļ | | | | | | | | | | | | | | | | ļ | | | | | | | 01 | | | | | | ec ic | | | | | | | | | | | | |
| ۱L | | ulul. | نلمل | لمال | <u>. </u> | 111 | En: | Ŀ | <u>Fi</u> | <u>u1</u> : | | | <u>.</u> | | L . | · | • | | i | | • | .1. | ! | ••• | 1. | | | • | | | | <u> ; '</u> | Ц | : P | <u> :'''</u> | 100 | Li | تلنا | <u>l'.</u> | | ! | <u> </u> | - | | | | | | | | Cł | ΗU | 11_ | UC | ЭТ | Ά | ٢ | ΙE | L. (| _ | F | I | ΞL | D | | | | | |
| | | | | | | | | | | | | | | | | | - | ТI | M | ΙĒ | (| M | 11 | ٧. | , | | | | | | | | | | | | | | | | | | | ļ | ~~~ | | | | 9 | 3e | m: | in | iCi | 16 | 2 | С | 00 | (r) | t | γ, | | F | 10 | ۰۲ ۰ | íc | a | | | |
| | | | | | | | | | | | | | | | | | | | - | | | | | | - | | | | | | | | | | | | | | | | | | | |]/ | Ŋ | J | Al | MI | MA | ٩L | 8 | t | AS | SS | 60 | C | IA | T | ES | 5, | ١N | IC | . c | one | uitir | ng E | ingk | nee |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | L | ORA | | ľ | F | ۳N | r | | Ţ | | | | _ | | | | | PF | iOi | NO | 8 | 6- | -0 | 3 | 08 | 93 |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | 1 | СНЯ | ¢D. | | ~ | Ľ | C | | | DAT | ε. Ε | - | | _ | - | | | | | | | | | 7 | | |

.

K

}⊒

TABLE 2

Aquifer Performance Test Results

| | Grap | hic | Autom | atch | |
|--|----------|----------|----------|----------|----------|
| Parameter | Drawdown | Recovery | | Recovery | Average |
| Transmissivity | 47,125 | 71,830 | 68,020 | 64,770 | 62,940 |
| (gpd/ft) Storage (dimensionless) | 5X10-3 | 4X10-3 | 4X10-3 | 5X10-3 | 4.5X10-3 |
| (gpd/ft3) | 1.9X10-1 | 7X10-2 | 1.0X10-1 | 1.0X10-1 | 1.1X10-1 |

The average value calculated for aquifer transmissivity determined from the APT appears reasonable considering the depths of the open hole sections of the two (2) test wells and the apparent specific capacity of Well #1. This value is not considered representative of the entire thickness of the Florida aquifer as only a small percentage of the aquifer is penetrated by the Southern States Utilities test/production wells.

The range of storage coefficients determined from the APT data and the calculated average value appear reasonable for a semi-confined, artesian aquifer. The leakance values presented above suggest that significant quantities of water recharge the portion of the Floridan tested when the potentiometric surface is lowered by well withdrawals.

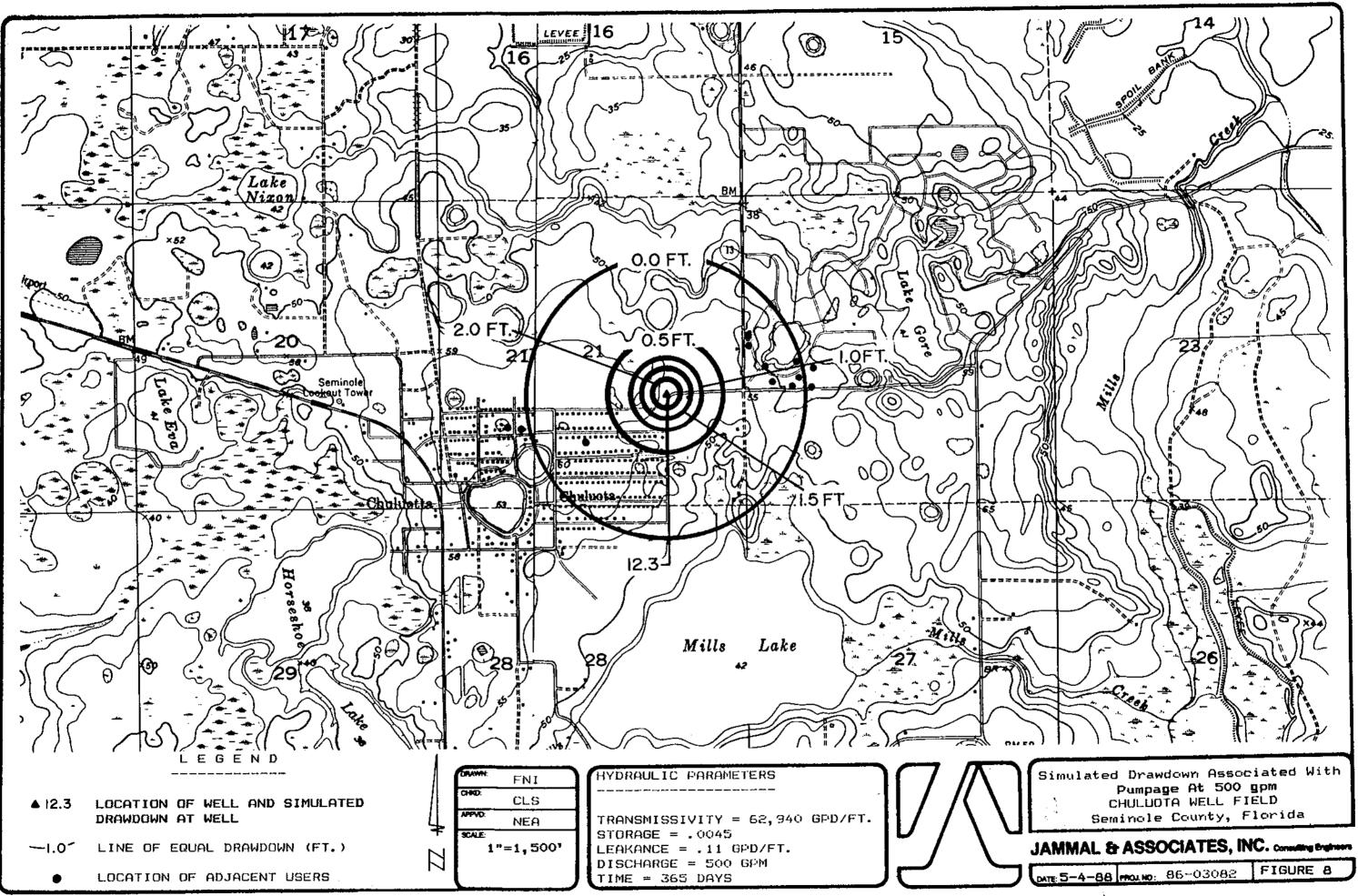
Model Simulation

Using the aquifer characteristics determined from the curve matching exercise, a model was created to simulate the impacts of withdrawals from Well #1 at the design discharge rate of 500 gpm. The model used for the simulation utilizes the Hantush-Jacob (1955) solution for a leaky artesian aquifer. Assumptions for this model are similar to those described earlier for the curve matching technique.

The model was first run and calibrated to match head conditions seen in the field during the APT. The model required no modification of the parameters determined by the curve matching exercise to produce conditions similar to those seen in the field. After the calibration run, the model was adjusted to simulate withdrawals at a rate of 500 gpm. The results of this model simulation are graphically depicted on Figure 8.

Figure 8 illustrates the predicted drawdown resulting from pumpage of Well #1 at a rate of 500 gpm continuously for 365 days, given the determined aquifer characteristics. The location of identified adjacent Floridan aquifer users is also presented on this figure to illustrate the relative impact to each. The model simulation indicates that drawdowns of less than one foot on the potentiometric surface can be expected by the residential units to the south and east of the proposed well site. It is anticipated that the largest impact to an identified local Floridan user is approximately 0.3 feet.

-13-



VPHIX #2470

LAND

Anticipated impacts to other users will be substantially less. The drawdown shown at the pumping well on Figure 8 reflects drawdown directly adjacent to the well. Recorded water levels in the pumping well during the APT suggests that drawdown in the well at 500 gpm will be on the order of 14 feet.

CONCLUSIONS (SEE GRAATA PGS)

The pumping test performed for this investigation indicates that the upper portion of the Floridan aquifer in the site vicinity behaves as a leaky artesian aquifer. Estimates of aquifer transmissivity determined from the pumping test indicate low to moderate values, most likely a direct function of partial penetration of the aquifer by the Southern States Utilities test/production wells.

Observations of the drawdown during the aquifer performance test indicate that expected drawdown at the pumping well (Well #1) will be approximately 14 feet at the design discharge rate of 500 gpm. The top of casing elevation for Well #1 was estimated from U.S.G.S. topographic maps at about 57 feet MSL. The static water level in the discharge well prior to the start of the APT was 28.1 feet below top of casing. The anticipated water level during pumping from Well #1 at 500 gpm is expected to be approximately 15 feet above MSL.

Analysis of collected water samples from Well #1 during the APT indicate that water produced from the well is of the transitional water type (TW) as described by Frazee (1982). The time related sampling indicates stable water quality during the course of the test. Concentration levels of most ions decreased slightly with time. Chloride concentrations decreased from 124 mgl to below 100 mgl for samples collected 72-hours apart. Similar decreases were noted for several other ions.

Analyses of time/drawdown and time/recovery data collected during the 72-hour pump test and subsequent model simulations indicate that drawdowns of less than one foot will be seen in the potentiometric surface at a radius greater than 600 feet from the discharge well. A field intensive well inventory indicated that no adjacent Floridan aquifer wells were located within this 600 foot radius. The model simulations indicate that approximately 0.3 feet of drawdown will occur in the nearest adjacent Floridan aquifer well as a result of the proposed pumpage from Southern States Utilities Well #1.

REFERENCES

- Barraclough, J.T, 1962, <u>Groundwater Resources of Seminole</u> <u>County, Florida</u>. Report of Investigation No. 27, U.S. Geological Survey, Florida Geological Survey.
- Frazee, J.M., Jr., 1982, <u>Geochemical Pattern Analysis: Method</u> of <u>Describing the Southeastern Limestone Regional Aquifer</u> <u>System</u>. St. Johns River Water Management District.
- Hantush, M.A. and Jacob, C.E., 1955, <u>Non-Steady Radial Flow In</u> <u>An Infinite Leaky Aquifer</u>, TRANS. AM. GEOPHY. UNION, Vol. 37, No. 6.
- Lichtler, W.F., Anderson, W. and Joyner, B.F., 1968, <u>Water</u> <u>Resources of Orange County, Florida</u>: Report of Investigation No. 50, U.S. Geological Survey, Florida Board of Conservation, Board of County Commissioners of Orange County, Florida.
- Lichtler, W.F., 1972, <u>Appraisal of Water Resources in the East</u> <u>Central Florida Region</u>: U.S. Geological Survey Report of Investigation No. 61.
- Lohman, W.S., 1972, <u>Groundwater Hydraulics</u>, U.S. Geological Survey Professional Paper, U.S. Government Printing Offices, Washington, D.C., Pages 30 - 34.
- SOIL SURVEY OF SEMINOLE COUNTY, FLORIDA, 1966, U.S. Department of Agriculture, University of Florida Agricultural Experiment Station, Land Photograph 29, Pages 6, 13 and 17.

APPENDICES

. . . 1

•

ADJACENT FLORIDAN USERS

Δ

ADJACENT FLORIDAN USERS

| Map <u>Identification</u> | Owner* | Well Depth (ft) bls | Use | Comments |
|------------------------------|---|------------------------|----------|--|
| l | Mr. Cross, corner of Ave. E and 2nd Street | Unknown | Domestic | |
| 2 | Unknown 300 2nd Street | Unknown | Unknown | |
| 3 | Mr. & Mrs. Bishop 321 2nd Street | 225 | Domestic | Good Tasting Water |
| 4 | Doug Wilson 285 Snow Hill Road | 160 | Domestic | Complaints of iron and bacteria |
| 5 | Hazel Johnson 293 Snow Hill Road | Unknown | Domestic | |
| 6 | Mr. Killen 163 Overlook Drive | 178 | Domestic | Complaints of bad taste |
| 7 | Mr. & Mrs. Diest 156 Overlook Drive | Unknown | Unknown | |
| 8 | Tate Buntz 153 Overlook Drive | Unknown | Domestic | Complaints of darkened color with extended use |
| 9 | Mr. Rancourt 160 Overlook Drive | Unknown | Domestic | |
| 10 | Unknown 152 Overlook Drive | Unknown | Unknown | |
| 11 | Unknown 900 Brumley Road | Unknown | Unknown | |
| 12 | Unknown 930 Brumley Road | Unknown | Unknown | |

AQUIFER PERFORMANCE TEST DATA

TIME/RECOVERY DURING THE CONSTANT RATE PUMP TEST

| • | TIME | MINUTES/SINCE START | DEPTH TO WATER*(ft) | th(FT) |
|-----|-------|---------------------|---------------------|--------|
| 4/7 | 12:09 | 9 | 34.9 | . 33 |
| | 12:11 | 11 | 34.81 | . 42 |
| | 12:13 | 13 | 34,74 | . 49 |
| | 12:15 | 15 | 34.66 | .57 |
| | 12:17 | 17 | 34.60 | .63 |
| | 12:20 | 20 | 34.50 | . 73 |
| | 12:22 | 22 | 34.45 | . 78 |
| | 12:25 | 25 | 34.37 | . 86 |
| | 12:30 | 30 | 34.24 | . 99 |
| | 12:35 | 35 | 34.16 | 1.07 |
| | 12:40 | 40 | 34.05 | 1.18 |
| | 12:51 | 51 | 33.90 | 1.33 |
| | 1:00 | 60 | 33.77 | 1.46 |
| | 1:12 | 72 | 33.63 | 1.60 |
| | 1:21 | 87 | 33.56 | 1.67 |
| | 1:30 | 90 | 33.48 | 1.75 |
| | 1:45 | 105 | 33.39 | 1.84 |
| | 1:55 | 115 | 33.33 | 1.90 |
| | 2:00 | 120 | 33.30 | 1.93 |
| | 2:30 | 150 | 33.15 | 2.08 |
| | 3:00 | 180 | 33.05 | 2.18 |
| | 3:30 | 210 | 32.98 | 2.25 |
| | 4:00 | 240 | 32.91 | 2.32 |
| | 4:30 | 270 | 32.85 | 2.38 |
| | 5:00 | 300 | 32.81 | 2.41 |
| | 6:00 | 360 | 32.75 | 2.46 |
| | 7:30 | 450 | 32.70 | 2.51 |
| | 8:30 | 510 | 38.68 | 2.54 |
| | 9:30 | 570 | 32.67 | 2.56 |
| | 11:30 | 690 | 32.64 | 2.60 |
| 4/8 | 1:15 | 795 | 32.60 | 2.63 |
| | 2:15 | 855 | 32,58 | 2.65 |
| | 3:00 | 900 | 32.57 | 2.66 |
| | 4:00 | 960 | 32.56 | 2.67 |
| | 4:30 | 990 | 32.56 | 2.67 |

* Initial Depth to Water= 35.23 Feet

TIME/DRAWDOWN DURING THE CONSTANT RATE PUMP TEST

| | TIME | MINUTES/SINCE START | DEPTH TO WATER*(ft) | Ah(FT) |
|-----|----------|---------------------|---------------------|--------------|
| 4/4 | 11:50 AM | 2 | 32.46 | 0 |
| | 11:52 | 4 | 32.58 | . 12 |
| | 11:54 | 6 | 32.62 | .16 |
| | 11:56 | 8 | 32.67 | .21 |
| | 11:58 | 10 | 32.71 | . 25 |
| | 12:00 PM | 12 | 32.75 | . 29 |
| | 12:03 | 15 | 32.84 | . 38 |
| | 12:05 | 17 | 32.90 | . 44 |
| | 12:15 | 27 | 33.18 | .72 |
| | 12:20 | 32 | 33.32 | . 86 |
| | 12:25 | 37 | 33.45 | . 99 |
| | 12:30 | 42 | 33.54 | 1.08 |
| | 12:45 | 57 | 33.81 | 1.35 |
| | 12:50 | 62 | 33.88 | 1.42 |
| | 1:00 | 72 | 34.00 | 1.54 |
| | 1:15 | 82 | 34.15 | 1.69 |
| | 1:31 | 103 | 34.27 | 1.81 |
| | 1:45 | 117 | 34.36 | 1.90 |
| | 2:00 | 132 | 34.45 | 1.99 |
| | 2:30 | 162 | 34.57 | 2.11 |
| | 2:46 | 178 | 34.62 | 2.16 |
| | 3:15 | 207 | 34.70 | 2.24 |
| | 3:45 | 237 | 34,76 | 2.30 |
| | 4:00 | 25 2 | 34.78 | 2.32 |
| | 4:30 | 282 | 34.82 | 2.36 |
| | 5:00 | 312 | 34.87 | 2.41 |
| | 6:00 | 372 | 34.91 | 2.45 |
| | 7:00 | 432 | 34.96 | 2.50 |
| | 8:00 | 492 | 34.99 | 2.53 |
| | 9:00 | 552 | 35.03 | 2.57 |
| | 10:00 | 612 | 35.07 | 2.61 |
| . – | 11:00 PM | 672 | 35.09 | 2.63 |
| /5 | 12:15 AM | 747 | 35.11 | 2.65 |
| | 2:00 | 852 | 35.13 | 2.67 |
| | 3:30 | 942 | 35.13 | 2.67 |
| | 6:30 | 1122 | 35.14 | 2.68 |
| | 8:30 | 1242 | 35.15 | 2.69 |
| | 12:30 PM | 1482 | 35.17 | 2.71 |
| | 3:30 | 1662 | 35.18 | 2.7 2 |
| | 5:34 | 1786 | 35.19 | 2.73 |
| | 6:30 | 1842 | 35.20 | 2.74 |
| | 9:30 | 2022 | 35.22 | 2.76 |
| /6 | 12:30 AM | 2202 | 35.23 | 2.77 |
| | 3:30 | 2382 | 35.24 | 2.78 |
| | 6:30 | 2562 | 35.24 | 2.78 |
| | 8:40 | 2688 | 35.22 | 2.76 |
| /7 | 9:10 AM | 4158 | 35.25 | 2.79 |

* Static water level prior to test = 32.46 ft DTW. ** Change in water level.

.

WATER QUALITY

 $\mathbf{\Lambda}$



Bionomics Laboratory, Inc.

4310 EAST ANDERSON ROAD P.O. BOX 8011 ORLANDO, FLORIDA 32806 (305) 851-2560 RICHARD ALT, PRESIDENT

April 20, 1988

FOR: Jammal & Associates, Inc. 1675 Lee Road Winter Park, FL 32789

ATTN: Chris Sweazy

RE: Samples Received 4/5/88, submitted by client

LABORATORY REPORT

| Lab I.D. No. Marks | 881565 Chulwota #1 | 881566 Chulwcta #2 | | 881568 Chulwcta #4 |
|---|------------------------------|------------------------------|----------------------------------|------------------------------|
| pH, lab | 7.32 | 7.34 | 7.48 | 7.30 |
| Alkalimity, total as CaCO3, mg/l | 132 | 130 | 137 | 146 |
| Chlorides as Cl, mg/l | 124 | 121 | 125 | 111 |
| Sulfates as SO4, mg/l | 25, 7 | 25.6 | 25.6 | 21,2 |
| Total dissolved solids, mg/l | 396 | 400 | 413 | 372 |
| Hetals | | | | |
| Calcium as Ca, mg/l Magnesium as Mg, mg/l Portassium as K, mg/l Sodium as Na, mg/l | 64.5 10.6 2.99 68.1 | 60.3 10.4 2.32 67.4 | 63, 8 10, 9 3, 08 69, 9 | 63.4 10.1 2.82 53.4 |
| Total hardness as CaCO3, mg/l | 205 | 194 | 204 | 200 |
| Carbonate hardness as CaCO3, mg/l | 132 | 130 | 137 | 148 |
| Non-carbonate hardness as CaCO3, mg/l | 73 | 64 | 67 | 50 |
| Bicarbomate alkalimity as CaCO3, mg/l | 132 | 130 | 137 | 148 |
| Carbonate alkalinity as CaCO3, mg/l | Q. 41 | 8. 77 | 0, 32 | 0.26 |
| Hydroxide alkalinity as CaCO3, mg/l | 0, 1* | 0.1* | 8.1 * | 0.1* |
| • • • • | | | | |

* Less than

Signed

Richard Alt, Chemist



Bionomics Laboratory, Inc.

4310 EAST ANDERSON ROAD P.O. BOX 8011 ORLANDO, FLORIDA 32806 (305) 851-2560 RICHARD ALT, PRESIDENT

April 20, 1988

- FOR: Jammal & Associates, Inc. 1675 Lee Road Winter Park, FL 32789
- ATTN: Chris Sweazy

RE: Samples Received 4/6-7/88, submitted by client

LABORATORY REPORT

| Lab I.D. No. Marks | Chulucta #5 | 881575 Chulucta #6 | | |
|---------------------------------------|----------------|--------------------------|--------------|-------|
| | | | | |
| pH, lab | 7.40 | 7.25 | 7.40 | 7.30 |
| Alkalimity, total as CaCO3, mg/l | 130 | 140 | 143 | 141 |
| Chlorides as Cl, mg/l | 162 | 191 | 37 | 33 |
| Sulfates as SO4, mg/l | 18.3 | 18.3 | 19,2 | 21.3 |
| Total dissolved solids, mg/l | 369 | 344 | 348 | 348 |
| Metals | | | | |
| Calcium as Ca, mg/l | 64.8 | 66.3 | 67.5 | 65. 5 |
| Magnesium as Mg, mg/l | 9.75 | 9.61 | 3. 91 | 9.63 |
| Potassium as K, mg/l | 2.51 | 2.47 | 2.49 | 2.43 |
| Sodium as Na, Mg/l | 55.5 | 54,4 | 54,1 | 54.6 |
| Total hardness as CaCO3, mg/l | 202 | 203 | 203 | 203 |
| Carbonate hardness as CaCO3, mg/l | 130 | 140 | 143 | 141 |
| Non-carbonate hardness as CaCO3, mg/l | 72 | 63 | 66 | 62 |
| Bicarbomate alkalimity as CaCO3, mg/l | 130 | 140 | 143 | 141 |
| Carbonate alkalimity as CaCD3, mg/l | 0, 31 | 8. 24 | 9. 34 | 0.25 |
| Hydroxide alkalinity as CaCO3, mg/l | Ø. 1* | 0.1* | Q. 1* | 8, 1* |
| | | | | • |

* Less than

Richard Alt, Chemist

Signed



÷.,

Bionomics Laboratory, Inc.

4310 EAST ANDERSON ROAD P.O. BOX 8011 ORLANDO, FLORIDA 32806 (305) 851-2560 RICHARD ALT, PRESIDENT

April 27, 1988

FOR: Jammal & Assoc. 1765 Lee Road Winter Fark, FL 32789

ATTN: Chris Sweary

RE: Sample received 4/7/88 for analysis.

LABORATORY REPORT

| LAB I.D. ND. MARKS | | MCL FDER 17-22 | METHOD | 881626 Chuluota No. (|
|-----------------------|---|-------------------|-------------------|--------------------------|
| I. | Secondary Parameters | | | |
| | Chlorides as Cl, mg/l | 250 | EPA 325.3 | 33 |
| | Color, Ft/Co units | 15 | EFA 110,2 | 5* |
| | Copper as Cu, mg/1 | 1 | EPA 228.1 | 0.005* |
| | Corrosivity (Langelier Saturation Index) | -0.2/+0.2 | Std. Mtd 203 | -0.19 |
| | Foaming Agents, MBAS, mg/1 | 0.5 | EPA 425.1 | 8.85× |
| | Iron as Fe, mg/1 | 0.3 | EPA 236.1 | 0.03* |
| | Manganese as Mr., mg/l | 0.05 | EPA 243.1 | 0.03* |
| | Oden, 7.0.N. | 3 | EPA 140.1 | 2 |
| | pH | 6.5(min) | EPA 150.1 | 7.30 |
| | Sulfate as 504, mg/l | 250 | EPA 375,4 | 21.4 |
| | Total Dissolved Solids, 180 C, mg/1 | 500 | EFA 160.1 | 348 |
| | Zinc as In, mg/l | 5 | EPA 289.1 | 0, 03* |
| 1. | Primary Inorganics | | | |
| | Arsenic as As, mg/l | ø. 05 | EPA 206.2 | 0.005* |
| | Barium as Ba, mg/l | 1.0 | EFA 208.2 | 0.024 |
| | Cadmium as Cd, mg/1 | 0.010 | EPA 213.2 | 0.0005* |
| | Chromium as Cr, mg/l | 0.05 | EPA 218.2 | 0.005+ |
| | Lead as Pb, mg/l | 0. 05 | EPA 239.2 | 0.005* |
| | Mercury as Hg, mg/l | 6.062 | EPA 245.1 | 0,0005* |
| | Nitrate as N, mg/l | 10 | EPA 352.1 | 0.023 |
| | Selevium as Se, mg/l | 0, 01 | EPA 270.2 | 0,005* |
| | Silver a Ag, mg/l | 0.05 | EPA 272.1 | 0.03* |
| | Sodium as Na, mg/l | 160 | EPA 273.1 | 54.6 |
| | Fluceride as F, mg/l | 1.4-2.4 | EPA 340.2 | 0.16 |
| | Turbidity as N.T.U. | 5.0 | EPA 180.1 | 0,26 |
| | Total Coliform per 100 ml (MF) | | Std. Meth. 909 A. | 23 |

LABORATORY REPORT

Jammal & Assoc. Page two

| LAB I.D. NO. MARKS | | MCL FDER 17-22 | METHODS | 881626 Chuluata No. 8 |
|-----------------------|------------------------------|-------------------|-----------------|--|
| 111. | Primary Organic Parameters | | | |
| | Erdrin, mg/l | 0.0002 | EPA 608 | 0. 00001 × |
| | Lindane, mg/l | 0.004 | EFA 608 | &, &&&&&= |
| | Methoxychlor, mg/l | Ø. 1 | EFA 6 08 | Q. QQQ2* |
| | Toxaphere, mg/l | 0.005 | EPA 608 | Ø. ØØØ4 * . |
| | 2,4,D, mg/1 | 0.1 | EPA | 0. 00005* |
| | 2,4,5, TP Silvex, mg/l | 0.01 | EFA | 0. 00001 * |
| IV. | Volatile Organics | | | |
| | Trichloroethylene, ug/l | 3. 0 | EPA 601 | <u>1+</u> |
| | Tetrachlorcethylene, up/l | 3.0 | EPA 601 | 1* |
| | Carbon Tetrachloride, ug/l | 3.0 | EPA 601 | 1* |
| | Vinyl Chloride, ug/l | 1.0 | EPA 601 | 1* |
| | 1,1,1 -Trichloroethene, ug/1 | 200.0 | EPA 601 | 1* |
| | 1,2 -Dichlorcethame, ug/l | 3.0 | EPA 601 | 1* |
| | Benzene, ug/1 | 1.0 | EPA 602 | 1.0* |
| | Ethylene Dibromide, ug/l | 0.02 | DER | 0, 02* |
| v. | Radiology | | | |
| | Gross Alpha pCi/l | 15 | EPA 900 | "e fallen 3.6 ±1.2 pci/l |

٠

* less than

Signed Turney US Richard Alt, Chemist ----

-15-

CONCLUSIONS

The pumping test performed for this investigation indicates that the upper portion of the Floridan aquifer in the site vicinity behaves as a leaky artesian aquifer. Estimates of aquifer transmissivity determined from the pumping test indicate low to moderate values, most likely a direct function of partial penetration of the aquifer by the Southern States Utilities test/production wells.

Observations of the drawdown during the aquifer performance test indicate that expected drawdown at the pumping well (Well #1) will be approximately 14 feet at the design discharge rate of 500 gpm. The top of casing elevation for Well #1 was estimated from U.S.G.S. topographic maps at about 57 feet MSL. The static water level in the discharge well prior to the start of the APT was 28.1 feet below top of casing. The anticipated water level during pumping from Well #1 at 500 gpm is expected to be approximately 15 feet above MSL.

Analysis of collected water samples from Well #1 during the APT indicate that water produced from the well of the is transitional water type (TW) as described by Frazee (1982). The time related sampling indicates stable water quality during the course of the test. Concentration levels of most ions decreased slightly with time. Chloride concentrations decreased from 124 mg1 to below 100 mg1 for samples collected 72-hours apart. Similar decreases were noted for several other ions.

Analyses of time/drawdown and time/recovery data collected during the 72-hour pump test and subsequent model simulations indicate that drawdowns of less than one foot will be seen in the potentiometric surface at a radius greater than 600 feet from the discharge well. A field intensive well inventory indicated that no adjacent Floridan aquifer wells were located within this 600 foot radius. The model simulations indicate that approximately 0.3 feet of drawdown will occur in the nearest adjacent Floridan aquifer well as a result of the proposed pumpage from Southern States Utilities Well #1.

Based upon the results of the aquifer performance test and analysis of the resultant hydrologic data, Jammal & Associates, Inc., concludes the following:

- Groundwater of suitable quality for drinking purposes is available from Southern States Utilities Well #1 at the design pumping rate of 500 gpm.
- 2. Time-dependent water quality test results strongly suggest that pumpage from Southern States Utilities Well #1 at the design pumping rate will not have an adverse impact on water quality in the Floridan aquifer or on adjacent water wells.

-16-

