

FORT PIERCE INTERCHANGE AQUIFER TEST REPORT

BY: GEORGE W. HILL

I. Summary

- A. Location. -- St. Lucie County, Florida, Township 35 South,  
Range 39 East, NE $\frac{1}{4}$  Section 26. Jupiter Field  
Headquarters Office.
- B. Dates. -- August 23-25, 1979
- C. Length. -- Pumping: 22.7 hours; recovery 18.3 hours.
- D. Discharge. -- 163 GPM
- E. Hydraulic Coefficients. -- Transmissivity -- 1,600 ft<sup>2</sup>/d (rounded)  
Storage Coefficient -- See Page 5
- F. Analytical Model. -- Hantush-Jacob (Leaky artesian, nonsteady flow)
- G. Remarks. -- T values computed from three observation wells  
were virtually the same and at the same time,  
in the same range with values computed using  
Boulton's delayed yield model (1,700 ft<sup>2</sup>/d, rounded).

## II. Narrative

### A. Introduction

1. Test Purpose. -- To determine the transmissivity and if possible, determine the storage coefficient of the best producing zone of the so-called shallow aquifer. This test is part of a reconnaissance study of the aquifer properties as a part of Project FL-268, called The Upper East Coast Planning Area which includes Martin and St. Lucie Counties and the eastern edge of Okeechobee County, Florida.

2. Personnel. -- The test was conducted by Ralph Wilcox, Bill Long, Mike Dooley and Jay Wendorf - all on the Jupiter Field Office staff. Test analysis, computation and report were done by George W. Hill and reviewed by Fred Meyer of the South Florida Subdistrict.

### B. Physical Aspects

1. Site Location. -- The test site is in Township 35 South, Range 39 East, in the northeast quarter of Section 26, about five miles southwest of downtown Fort Pierce in southwest corner of the intersection of the Florida Sunshine Parkway and State Road 70 (Exhibit I).

2. Test Drilling and Geophysical Logging. -- Prior to the installation of the well network, a test well was drilled to the base of the shallow aquifer; cuttings were logged and examined. Geophysical logs, including spontaneous potential, resistivity and gamma, were run (Exhibit III).

3. Aquifer Description. -- The so-called shallow aquifer is mainly composed of sand, clay, silt and shell of Pleistocene and Pliocene epochs. Sediments forming the aquifer system are components of the Fort Thompson and Anastasia Formations overlain by Pamlico Sand (W. Miller, 1979). Shell and sand lenses in the Caloosahatchee Marl are also present. Many facies changes appear. Generally the aquifer system is unconfined and under water-table conditions, but localized artesian conditions have been noted by other investigators (Parker 1955) in the vicinity of Fort Pierce and Indiantown where discontinuous clay lenses act as confining units.

The production well and all observation wells except one were screened in a zone consisting mainly of slightly cemented to cemented sand, shell, and sandstone, with some clay streaks near the top and bottom of the screened zone. The screened zone is overlain with sand and shell mixed with clay lenses (54-67 feet) and is underlain with green, dry clay (Exhibit III). The gamma logs seem to indicate the pumped zone to have much less clay than the beds above and below.

4. Well Descriptions. -- The production well was finished with a 6-inch ID PVC pipe to a depth of 110 feet and screened from 70 to 110 feet with wire wrapped underbar construction PVC screen with 0.030 slots.

Four 2-inch ID PVC wells were installed and used in the test for observation wells. Pertinent well data is shown in the table below.

<u>Well No.</u>	<u>Radius, in Feet</u>	<u>Drilled Depth in Feet</u>	<u>Screened Interval in Feet</u>
60N	60	123	70-110
200W	200	111	70-110
30S	30	123	72-112
100S	100	117	72-112
300S	300	113	72-112
30SH	30	30	Open Hole

See Exhibit II

5. Instrumentation. -- Four Keck/Stevens water-level recorders for recording drawdown data on analog charts. Steel tapes were used for collecting water-level data from other wells. A Weather Measure, Model B201 barograph was used to record barometric pressure during the test.

6. Pump. -- The production well was pumped with a 4-inch centrifugal pump.

7. Measurement of Drawdown. -- Chart records are good with only minor adjustments of pen trace to taped measurements. The recorder on well 60S malfunctioned at the beginning of the test, but was made functional after 40 minutes into the test. The drawdown for the early time was measured with a tape. No adjustments were made to the water-level data for barometric pressure or water-level fluctuations. Please see Exhibit VII.

Shallow well 30SH was jetted in several hours before the beginning of the test by the use of approximately 600 gallons of water to a depth of 30 feet. Water levels taken before, during and after the test show a steady decline. If this decline were the result of pumping, then it should show recovery after the pump stopped. The falling W-L was probably the result of discontinuation of injecting water in the hole construction process. (Exhibit VII, Item 6).

8. Discharge. -- The production well was pumped at approximately 163 GPM. Discharge steadily declined from 194 GPM at the beginning of the test to 157 GPM at the end. The pumping rate was measured with a circular orifice weir (6-9 inch pipe, 2-inch orifice) with a piezometer mounted in the side of the weir. Pumping data is shown in Exhibit V.

A 6-inch aluminum pipeline was used to route the pumped water 600 feet south into a ditch draining into Ten Mile Creek below the saltwater barrier in the southeast quarter of Section 26 about 1700 feet from the pumped well.

9. Potential Recharge Boundaries. -- Ten Mile Creek, which is elevated by a control structure (see above), is located within 2000 feet on the west side and 1700 feet on the south side of the production well. A small pond is located about 1000 feet northeast of the production well and another is located about 1200 feet to the west. No staff gages or recording equipment were installed at these sites and no water-level data was recorded.

### C. Computations

1. Computations are included in Exhibit VIII. Three solution methods were considered - Hantush-Jacob solution for a leaky confined aquifer with vertical movement; the Boulton solution for delayed yield in an unconfined aquifer with vertical movement and the Bound Aquifer Method after Stallman.

2. Type Curve Solutions. -- Transmissivity values computed using all three of the afore mentioned methods are in the same general range. Log-log plots of drawdown versus time (or  $\frac{t}{r^2}$  when applicable) can be fitted to each of the three families of type curves reasonably well. The average T value computed for each of the three methods are shown below.

<u>Method</u>	<u>No. of Wells</u>	<u>T Value, ft<sup>2</sup>/day</u>
Hantush-Jacob	3	1,630
Delayed Yield	3	1,700
Image Well Theory	4	1,860

The test was too short to verify a delayed yield response.

The following image well computations were done to determine the existance of a recharge boundary from adjacent surface water bodies:

<u>Obs. Well</u>	<u>s-ft.</u>	<u>t<sub>R</sub>-min.</u>	<u>t<sub>i</sub>-min.</u>	<u>r-ft.</u>	<u>r<sub>i</sub>-ft.</u>
100S	2.0	1.1	600	100	2335
200W	2.0	5.6	600	200	1922
300S	1.0	6.5	300	300	2038

These calculations indicate the image well location to be approximately 2000 feet from the pumped well. Therefore the boundary would be estimated at half this distance which does reach the nearest surface water body located about 700 ft. northeast of the pumped well.

Although no water-level data was obtained on the pond to the northeast, it is possible for recharge to affect the test. The type curve fits are good for wells 100S, 200W and 300W.

On the other hand, the lithologic and geophysical logs indicate the presence of, at least a semiconfining bed above the pumped zone. This suggests a leaky artesian situation that seems prevalent in the study area. It is unfortunate that the shallow well (30SH) did not function properly (continued to recede after pump stopped).

3. Transmissivity. -- Use the average of the Hantush-Jacob method which is  $1,630 \text{ ft}^2/\text{day}$ . If the image well theory is correct, then the T value would be  $1,860 \text{ ft}^2/\text{day}$ .

4. Storage Coefficient. -- Storage Coefficient computed on the basis of Hantush-Jacob Method (leaky artesian, nonsteady flow) are as follows:

<u>Well No.</u>	<u>Storage Coefficient</u>
100S	$7.1 \times 10^{-5}$
200W	$1.1 \times 10^{-4}$
300S	$3.6 \times 10^{-4}$

5.  $Leakance = 6.0 \times 10^{-4}$

Identification No. 272427 0802403.02 Sheet No. FP-1

County St. Lucie Lat-Long 272427 N0802403.02

Twp 35S Rg 39E Sec 26 ad ad Date 7/17/79

Location Pumped Well - Turnpike Test Ft. Pierce  
 LS = 17 ft.

Driller P&W Drilling Owner USGS Log by W.A. Long

Depth	Time	Hardness	Description of Formation
0-2	1050	Soft	Sand, fine, light gray.
2-16		Soft	Sand, fine to medium - tan to brown.
16-19		Soft	Sand, fine to coarse, 20% (silica quartz).
19-22	1107	Soft	Muck, black, fine sandy with coarse quartz 10%.
22-25	1118	Soft	Muck, black, fine to coarse sand, clayey, tough.
25-32		Soft	Shell, broken to small whole, gray black to brown with fine to coarse silica sand.
32-42	1140	Med.	Limestone, with broken shell and sand, loosely cemented.
42-51	1150	Med.	As above.
51-54		Med.	As above with small whole shell and clayey sand.
54-62	1205	Med-Soft	Sand and shell mixed with gray clay streaks (50%) Stopped - mixed mud.
62-67	1330	Soft	As above with very few thin clay streaks.
67-82	1346	Med.	Sand and shell slightly cemented with 30% clay streaks.
82-85	1350	Med.	As above.
85-92		Med with hard streaks	Sand and shell cemented - no clay.
92-102	1418	Med w/hard streaks	Sand and shell cemented - a little clay (gray, sandy).
102-112	1424	Same	Sand, shell and sandstone streaks, gray, sand is very fine to fine, sandstone is same, shell small, broken.
112-115	1434 1438	Same	Clay, sandy, greenish, dry.

Identification No. \_\_\_\_\_ Unit No. FP-60 W

County St. Lucie Lat-Long 272427 0802403.05

Twp 35S Rg 39E Sec 26 aad Date 7/19/79

Location Near SSP interchange in Ft. Pierce

Driller P&W Drilling Owner USGS Log by W.A. Long

Depth	Time	Hardness	Description of Formation
0-3	0835	Soft	Sand, fine to medium, gray white.
3-7		Soft	Sand, fine to medium, orange (yellow rust).
7-20		Soft	Sand, fine to coarse, brown, organic layer at 13 to 14 feet.
20-21	0845	Soft	Clay, black fine sandy 30% (muck).
21-25	0852	Soft	Clay, black, fine to coarse sand.
25-41	0858	Med.	Loose, cemented shell and sand, gray dark.
41-47	0904	Med.	As above - a "dirty looking formation". Formation turned to tan at 39 feet.
47-62	0907	Soft	Sand and shell, small broken shell, fine to med. sand 50% drilled real fast, loose.
62-82	0924	Med. to	Sand and shell as above, slightly cemented from 63' to 67' then loose shell small to large broken.
	0928	Soft	As above.
82-89	0932	Soft	Sand and small shell, cemented.
89-91		Hard	Sand and broken shell, slightly cemented drilled nice (good formation).
91-102	0940	Med.	As above, a little marly clay light gray.
102-110	0948	Med.	Clay, sandy, greenish.
110-119	0955	Soft	Sandstone, clay, dark green.
119-121		V. Hard	Sandy clay, green.
121-125	1015	Med.	

Identification No. \_\_\_\_\_ Office No. FP-100 S

County St. Lucie Lat-Long 272427 0802403.03

Twp 35S Rg 39E Sec 26 aad Date 7/18/79

Location On Gordy Rd. nearest Turnpike Interchange at Ft. Pierce

Driller P&W Drilling Owner USGS Log by W.A. Long

Depth	Time	Hardness	Description of Formation
0-3	1130	Soft	Sand fine, white.
3-8		Soft	Sand, clayey, yellow rust.
8-14		Soft	Sand, fine.
14-15		Soft	Muck layer.
15-19		Soft	Sand, fine to very coarse 20% (clear quartz sand).
19-20	1137	Soft	Muck, black with sand.
20-23	1141	Soft	Muck, black with sand.
23-36		Soft	Shell, broken small (Beach deposits dark to tan).
36-42	1150	Med.	Limestone, sandy tan to gray.
42-53	1208	Med.	Shell, broken to small whole, tan to gray, little fine gray sand.
53-58		Med.	Clay, blue gray light, mushy but smooth.
58-62	1220	Med.	Shell, broken to small whole, cream to light gray, little sand.
	1225		
62-82	1223	Med	Sand and shell, tan.
82-102	1258	Med.	Shell, fine, broken, with some sand, tan to gray, increasing in cemented nodules dark gray and large broken shell.
	1306		
102-112	1311	Med.	As above.
112-117	1318	Med.	Silt and sandy clay, light green-gray (dry).



Identification No. \_\_\_\_\_ UCHL NO. FP-200 W

County St. Lucie Lat-Long 272427 0802403.06

Twp 35S Rg 39E Sec 26aad Date 7/20/79

Location Near SSP Interchange in Ft. Pierce

Driller P&W Drilling Owner USGS Log by W.A. Long

Depth	Time	Hardness	Description of Formation
0-2	0910	Soft	Sand, fine white.
2-6		Soft	Sand, fine to medium, yellow orange.
6-17		Soft	Sand, clayey, light gray to tan.
17-20		Soft	Sand, fine to coarse, brown.
20-21	0915	Soft	Sand, clayey, dark gray to black.
21-26	0921	Soft	Sand, clayey, dark gray to black.
26-31		Med. Hard	Limestone sandy, dark gray to brown.
21-42	0930	Soft to Med.	Sand and shell, loose to slightly cemented with 6" to 1 ft. sandy clay lenses alternating with 2 ft. sand and shell beds.
42-63	0940	Soft	Shell and sand, thin layers of clay, gray.
	0948		
63-84	1010	Soft	Shell and sand, thin layers of brown to light gray clay.
	1015		
84-88	1023	Soft	As above.
88-90		V. Hard	Sandstone, real hard, olive color.
90-104	1037	Soft	Shell, broken and sand, fine to med. with small gray nodules (a few).
104-109	1055	Med. Soft	Sandstone, silty, (salt and pepper look).
109-111	1100	Soft	Sand, fine and clay, sandy; light green.

Identification No. \_\_\_\_\_ Object No. FP-300 S

County St. Lucie Lat-Long 272427 0802493.04

Twp 35S Rg 39E Sec 26 aad Date 7/19/79

Location Near SSP Interchange in Ft. Pierce.

Driller P&W Drilling Owner USGS Log by W.A. Long

Depth	Time	Hardness	Description of Formation
0-12	1435	Soft	Sand, clayey, light gray.
12-13		Med.	Sand, clayey, light gray, black with organic.
13-17		Med.	Sand, clayey, brown.
17-20	1445	V. Soft	Sand, fine to coarse, light gray.
20-22		Soft	Clay, sandy, black, tough.
22-25	1450	Med.	Shell, cemented sandy, gray to tan.
25-37		Med. Hard	Shell, cemented, sandy, brown to tan.
37-42	1500	Med. Soft	Shell and sand, loose.
42-50	1508	Med. Soft	Same as above.
50-56	1513	Soft	Clay, sandy, blue green.
56-62		Med.	Shell 60% and sand, fine to med; shell small to med. whole, tan and gray.
62-74	1516	Med.	Shell and sand with clay layers, shell is broken large to small, whole and broken, sand is fine to medium.
74-79	1523	Soft	Clay, fine sandy.
79-85	1526	Soft	Shell fine broken to small whole loose.
85-87		Soft	Sand and shell slightly cemented but drills.
87-89		Med.	As above cemented very hard streaks 87-88.
89-102	1535	Hard	Loose, with sandstone layers thin and very thin clay, lenses light gray.
102-105	1540		Loose as above, also dark gray.
105-109			Silty sand and loose, murky.
109-113	1545		Clay sandy, green.

Identification No. \_\_\_\_\_ Object No. FP-30S

County St. Lucie Lat-Long 272427 0802403.01

Twp 35S Rg 39E Sec 26 aad Date 5/22/79

Location Near Ft. Pierce SSP Interchange.

Driller P&W Drilling Owner USGS Log by W.A. Long

Depth	Time	Hardness	Description of Formation
0-2	1556	Soft	Sand, fine, light gray.
2-6		Soft	Sand, clayey, rust colored, fine, little gray mottled.
6-10		Soft	Sand, fine clayey, pink to gray mottled.
10-14		Soft	Sand, fine brown.
14-19	1605	Soft	Sand, fine clayey.
19-27	1608	Soft	Black organic layer, sandy (hard pan).
27-36		Med. to hard streaks	Shell fragments, tan to gray cemented in sandy matrix (quartz sand 20%).
36-40	1614	Med. Soft	Shell 70%, broken with fine sand 30%, brown.
40-44	1616	Med. Soft	Shell, broken with clayey sand (gray) lenses (using a little water).
44-51	1630	Med. Soft	Shell, broken with fine sand, brown to tan.
51-66	1633	Med. Soft	Same as above with clay lenses greenish gray, smooth.
66-71	1638	Med. Soft	Same as above, no clay.
71-81	1642	Med. Soft	Same as above with tan clay, a little very fine sand.
81-85	1652	Med. Soft	Shell, broken with very fine sand, tan with thin cemented streaks.
85-88		Med.	
88-96	1711	Med.	Sand 70%, very fine to medium with broken shell, gray.
96-99	1714	Med.	As above.
99-104	1725	Hard	Sand fine, and shell, broken with a little clay in streaks.
104-110		Hard	Sandstone, fine grained gray (calcite cemented).
110-116		Soft	Sand 70% very fine to medium with fine broken shell.
116-120	1734	Med.	Sandy clay, with broken large shell 10% greenish gray (salt and pepper look) phosphatic (Tamiami).
120-126	1740	Med.	Clay, sandy dark green (balls in sieve).
	1745		

# Fort Pierce Interchange

## U. S. GEOLOGICAL SURVEY - WELL LOG

WELL NUMBER 27 2427 080240305 LOCAL COUNTY ST. Lucie  
(latitude-longitude)

OWNER OR NAME \_\_\_\_\_

LOCATION T 35s R 39E SEC 26, SE 1/4 NE 1/4 NE 1/4

WELL DEPTH 125 ft., CASING 122 ft., DIAMETER 2 in.

DEPTH LOGGED 120 ft., TOP \_\_\_\_\_ ft., DATE COMPLETED 7-19-79  
 BOTTOM \_\_\_\_\_ ft.

FORMATION \_\_\_\_\_, FORMATION TOP reference to LSD \_\_\_\_\_

AQUIFER \_\_\_\_\_, WATER LEVEL reference to LSD \_\_\_\_\_

ELEVATION LSD 18 ft. MSL SPEED OF LOGGING 20 ft/min.

TOP OR START OF LOG 4 ft. above LSD  
below

OPERATOR Wm Hopkins

### TYPE LOG

- |   |  |   |
|---|--|---|
| <input type="checkbox"/> DRILLING TIME                    | <input type="checkbox"/> MAGNETIC                | <input type="checkbox"/> PHOTOGRAPHIC (TV, still, movie)  |
| <input type="checkbox"/> CASING-COLLAR                    | <input type="checkbox"/> INDUCTION               | <input type="checkbox"/> RADIOACTIVE-TRACER               |
| <input type="checkbox"/> CALIPER (diameter)               | <input checked="" type="checkbox"/> GAMMA-RAY    | <input type="checkbox"/> RADIATION                        |
| <input type="checkbox"/> DRILLER'S                        | <input type="checkbox"/> DIPMETER (inclinometer) | <input type="checkbox"/> SONIC                            |
| <input checked="" type="checkbox"/> ELECTRIC              | <input type="checkbox"/> LATER                   | <input type="checkbox"/> TEMPERATURE                      |
| <input type="checkbox"/> FLUID-CONDUCTIVITY (RESISTIVITY) | <input type="checkbox"/> MICRO                   | <input type="checkbox"/> TEMPERATURE (FLUID-CONDUCTIVITY) |
| <input checked="" type="checkbox"/> GEOLOGIST OR SAMPLE   | <input type="checkbox"/> MICROLATER              | <input type="checkbox"/> FLUID-VELOCITY                   |
|   | <input type="checkbox"/> NEUTRON                 |   |

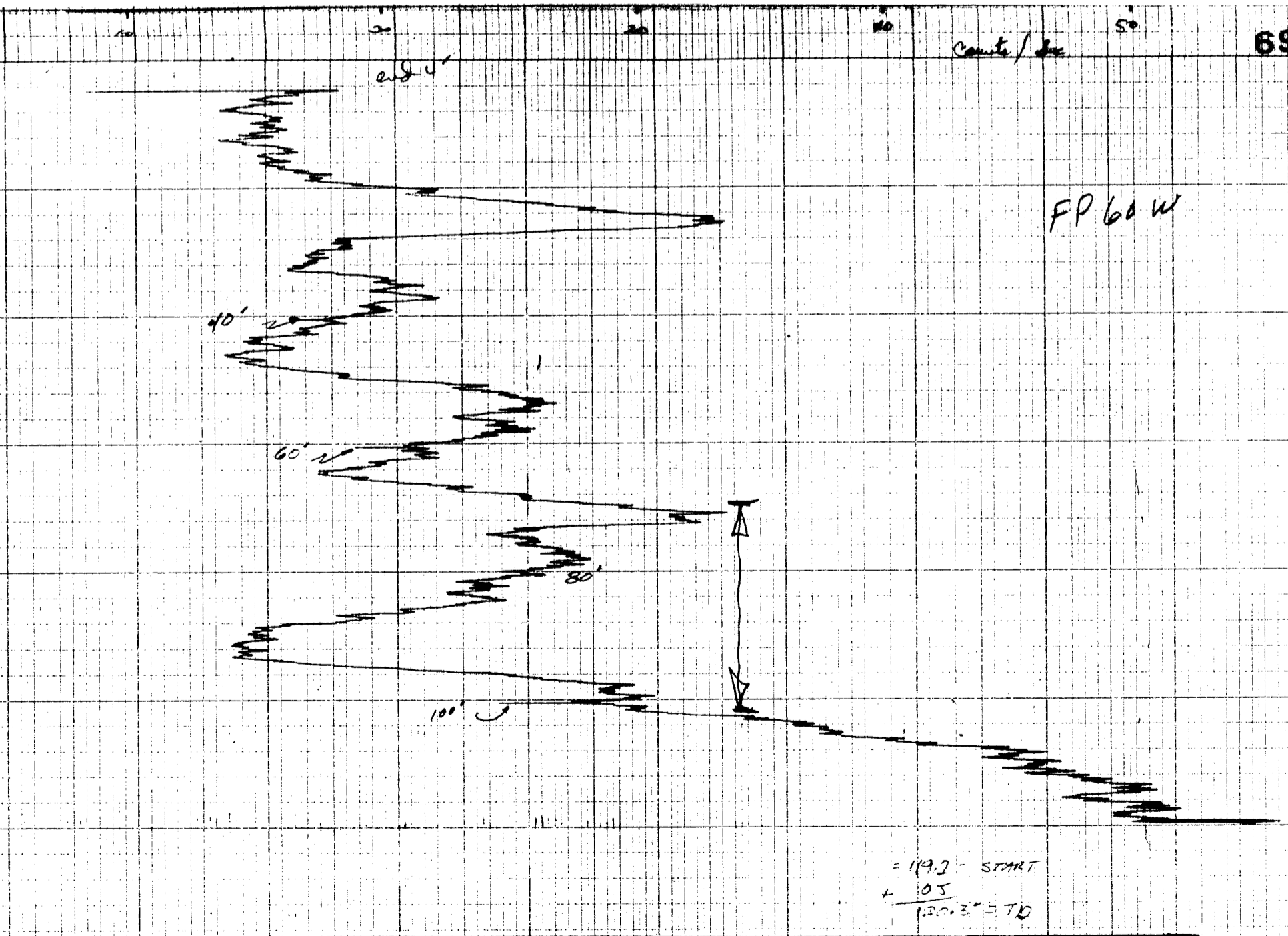
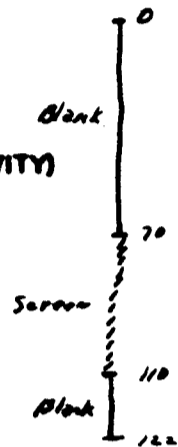
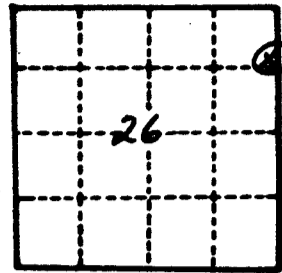
### USE OF WELL

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| <input type="checkbox"/> DRAINAGE  | <input type="checkbox"/> OIL-GAS                | <input type="checkbox"/> WITHDRAWAL |
| <input type="checkbox"/> DESTROYED | <input type="checkbox"/> RECHARGE               | <input type="checkbox"/> WASTE      |
|                                    | <input checked="" type="checkbox"/> TEST        |                                     |

QW SAMPLE  NO  YES DATE SAMPLED \_\_\_\_\_ DEPTH(S) SAMPLED \_\_\_\_\_

LOG SCALES HORIZ 50 cps = 9.7", VERT 1" = 20' LOGGED  UP  DOWN

S.P. \_\_\_\_\_ [DEPTH] RESISTIVITY \_\_\_\_\_



FP 60-W

July 19, 1979

Gamma log up @ 20' / min  
Chart Scale = 20' / in

Rate = 50 cps  
TC = 8

# Fort Pierce Interchange

## U. S. GEOLOGICAL SURVEY - WELL LOG

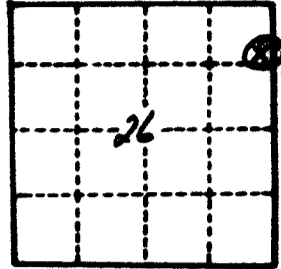
WELL NUMBER 272427 0802403.05 LOCAL # \_\_\_\_\_ COUNTY ST. Lucie

OWNER OR NAME U.S.G.S.

LOCATION T 35S R 39E SEC 26, SE 1/4 NE 1/4 NE 1/4

WELL DEPTH 125 ft., CASED 122 ft., DIAMETER 2 in.

DEPTH LOGGED 125 ft., TOP \_\_\_\_\_ ft., DATE COMPLETED 7-19-79  
 BOTTOM \_\_\_\_\_ ft.



FORMATION \_\_\_\_\_, FORMATION TOP reference to LSD \_\_\_\_\_

AQUIFER \_\_\_\_\_, WATER LEVEL reference to LSD \_\_\_\_\_

ELEVATION LSD 18 ft. MSL SPEED OF LOGGING 30 ft/min.

TOP OR START OF LOG 6.5 ft. above LSD  
 below

OPERATOR W. Hopkins

### TYPE LOG

- |   |  |   |
|---|--|---|
| <input type="checkbox"/> DRILLING TIME                    | <input type="checkbox"/> MAGNETIC              | <input type="checkbox"/> PHOTOGRAPHIC (TV, still, movie)  |
| <input type="checkbox"/> CASING-COLLAR                    | <input type="checkbox"/> INDUCTION             | <input type="checkbox"/> RADIOACTIVE-TRACER               |
| <input type="checkbox"/> CALIPER (diameter)               | <input checked="" type="checkbox"/> GAMMA-RAY  | <input type="checkbox"/> RADIATION                        |
| <input type="checkbox"/> DRILLER'S                        | <input type="checkbox"/> DIPMETER (inclinator) | <input type="checkbox"/> SONIC                            |
| <input checked="" type="checkbox"/> ELECTRIC              | <input type="checkbox"/> LATER                 | <input type="checkbox"/> TEMPERATURE                      |
| <input type="checkbox"/> FLUID-CONDUCTIVITY (RESISTIVITY) | <input type="checkbox"/> MICRO                 | <input type="checkbox"/> TEMPERATURE (FLUID-CONDUCTIVITY) |
| <input checked="" type="checkbox"/> GEOLOGIST OR SAMPLE   | <input type="checkbox"/> MICROLATER            | <input type="checkbox"/> FLUID-VELOCITY                   |
|   | <input type="checkbox"/> NEUTRON               |   |

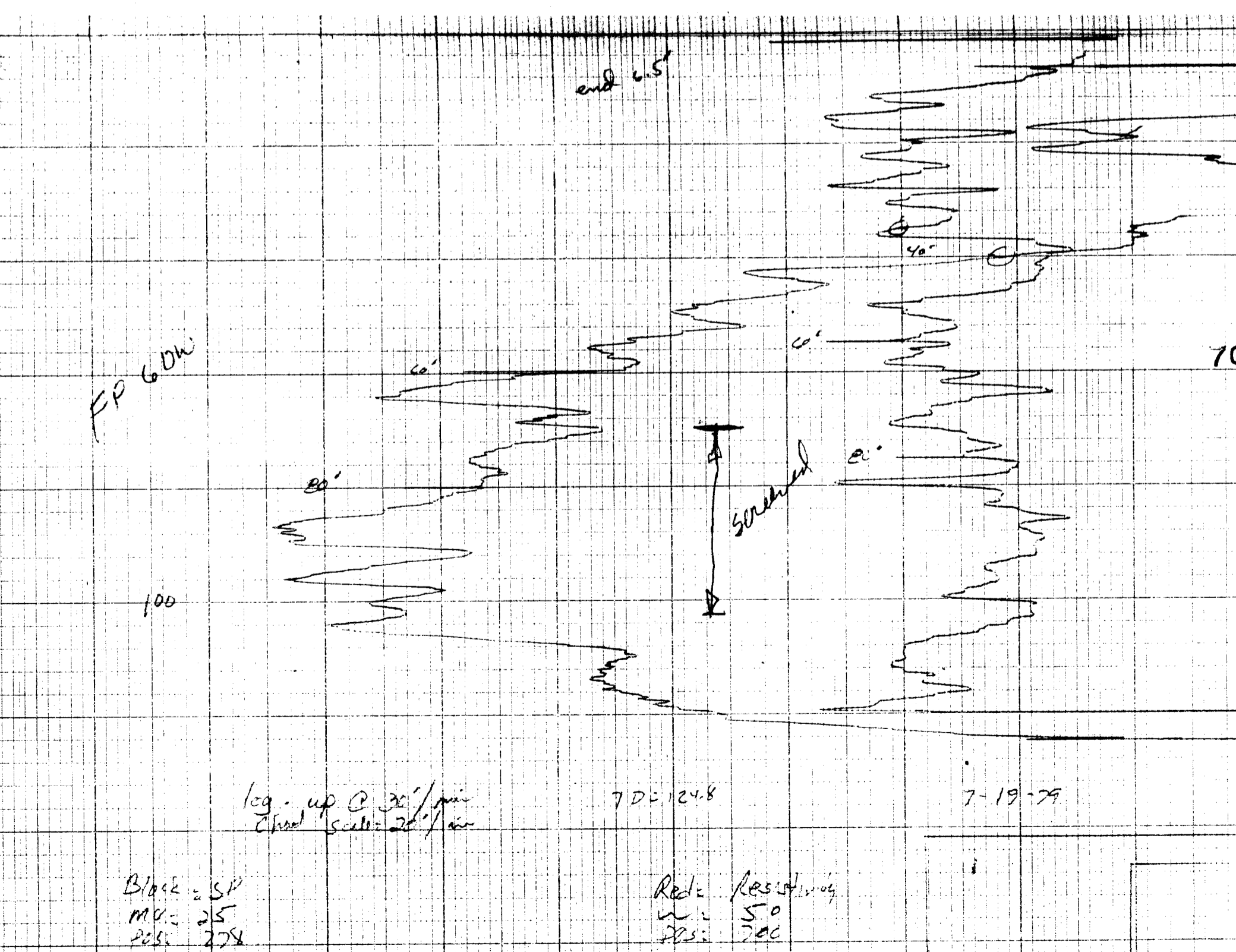
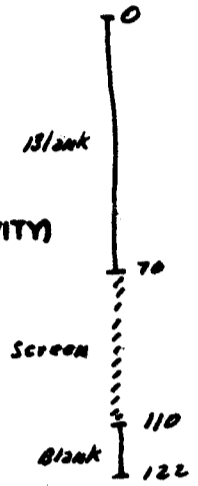
### USE OF WELL

- |                                    |   |                                     |
|------------------------------------|---|-------------------------------------|
| <input type="checkbox"/> ANODE     | <input checked="" type="checkbox"/> OBSERVATION | <input type="checkbox"/> UNUSED     |
| <input type="checkbox"/> DRAINAGE  | <input type="checkbox"/> OIL-GAS                | <input type="checkbox"/> WITHDRAWAL |
| <input type="checkbox"/> DESTROYED | <input type="checkbox"/> RECHARGE               | <input type="checkbox"/> WASTE      |
|                                    | <input checked="" type="checkbox"/> TEST        |                                     |

QW SAMPLE  NO  YES DATE SAMPLED \_\_\_\_\_ DEPTH(S) SAMPLED \_\_\_\_\_

LOG SCALES HORIZ \_\_\_\_\_, VERT 1" = 20' LOGGED  UP  DOWN

S.P. MV = 25 [DEPTH] RESISTIVITY Ohms = 50



Site Fort Pierce

Date of test 8-23-79

Well No 300 S actual r 300

m.p. elevation 17.93'  
 m.p. elev only valid with respect to other wells in suite.

1160  
 312/45

Item # 9

time	min since start of test	depth to water (ft)	draw-down (ft)	$t/r^2$ day ft <sup>2</sup>
8-23-79 1440	0	7.49	0	
1518	3	7.72	0.23	$2.31 \times 10^{-8}$
1520	5	8.17	0.68	3.86
1522	7	7.57	1.08	5.40
1525	10	8.98	1.49	$7.72 \times 10^{-8}$
1535	20	9.71	2.22	$1.5 \times 10^{-7}$
1545	30	10.11	2.62	2.3
1600	45	10.51	3.02	3.5
1609	54	10.71	3.22	4.2
1636	81	11.09	3.60	6.3
1649	94	11.19	3.70	$7.3 \times 10^{-7}$
1725	130	11.45	3.96	$1.0 \times 10^{-6}$
1809	174	11.68	4.19	1.34
1908	234	11.86	4.37	1.81
1943	269 ✓	11.94	4.45	2.08
2008	294 ✓	11.95	4.46	2.27
2110	356 ✓	12.10	4.61	2.75
2212	418 ✓	12.16	4.67	3.23
2306	486 <sup>474</sup>	12.22	4.73	3.66
8-24-79 0057	555 <sup>533</sup>	12.27	4.79	4.11
0141	649 <sup>627</sup>	12.33	4.84	4.84
0209	677 <sup>655</sup>	12.36	4.87	5.05
0257	735 <sup>713</sup>	12.37	4.88	$5.50 \times 10^{-6}$

Site Ft Pierce date of test \_\_\_\_\_

Well No 300 S actual r 300 m.p. elevation \_\_\_\_\_

time	min since start of test	depth to water (ft)	drawdown (ft)	$T/r^2 \text{ day ft}^{-2}$
0356	<del>778</del> 762	12.39	4.90	$5.88 \times 10^{-6}$
0520	<del>862</del> 846	12.41	4.92	6.53
0608	<del>910</del> 894	12.43	4.94	6.90
0711	<del>973</del> 957	12.46	4.97	7.38
0810	<del>1032</del> 1016	12.49	5.00	7.84
0910	<del>1092</del> 1076	12.51	5.02	$8.3 \times 10^{-6}$
1004	<del>1146</del> 1130	12.53	5.04	$8.72 \times 10^{-6}$
1104	<del>1206</del> 1190	12.55	5.06	$9.18 \times 10^{-6}$
1204	<del>1266</del> 1250	12.57	5.08	$9.65 \times 10^{-6}$
1303	<del>1325</del> 1309	12.58	5.09	$1.00 \times 10^{-5}$
1404	<del>1386</del> 1370	12.58	5.09	$1.06 \times 10^{-5}$
1504	<del>1446</del> 1430	12.59	5.10	$1.10 \times 10^{-5}$
1516	min since shutdown	12.59	5.10	
429	1	12.42	4.93	
	3	11.73	4.24	
	<del>5</del>	11.78	<del>4.29</del>	
	10	11.37	3.88	
	16	10.94	3.45	
	22	10.64	3.15	
	27	10.43	2.94	
	48	9.93	2.44	
	65	9.60	2.11	
-25-79 1047		7.72	0.23	

Site Fort Pierce

date of test 8-23#24-79

Well No 100S actual r 99 ft m.p. elevation 18.90'  
 m.p. elev. only valid with respect to other wells in suite.

Item # 3

time	min since start of test	depth to water (ft)	drawdown (ft)	$T/r^2$ day ft <sup>-2</sup>
1505	0	8.30	0	
	1	10.27	1.97	$6.94 \times 10^{-8}$
	2	11.17	2.87	$1.4 \times 10^{-7}$
	3	11.68	3.38	$2.1 \times 10^{-7}$
	4	12.02	3.72	2.8
	5	12.27	3.98	3.5
	7	12.71	4.41	4.9
	10	13.15	4.85	6.9
	13	13.45	5.15	$9.0 \times 10^{-7}$
	15	13.62	5.32	$1.04 \times 10^{-6}$
	20	13.95	5.65	1.39
	25	14.18	5.88	1.74
	30	14.37	6.07	2.08
	40	14.66	6.36	2.78
	50	14.85	6.55	3.47
	60	15.02	6.72	4.17
	75	15.22	6.92	5.21
	90	15.37	7.07	6.25
	120	15.58	7.28	$8.33 \times 10^{-6}$
1801	166	15.80	7.50	$1.15 \times 10^{-5}$
1849	213	15.96	7.66	1.48
2003	280	16.10	7.80	2.0
2103	348	16.19	7.89	2.42



Site At Pierce date of test \_\_\_\_\_

Well No 100N actual r 100 m.p. elevation \_\_\_\_\_

time	min since start of test	depth to water (ft)	drawdown (ft)	$T/r^2$ drawdown <sup>-2</sup>
2206	411	16.28	7.98	$2.85 \times 10^{-5}$
2303 8-21-71	468	16.33	8.03	3.25
05014	529	16.36	8.08	3.67
8129	614	16.42	8.12	4.26
0207	652	16.43	8.13	4.53
0304	709	16.44	8.14	4.92
0358	763	16.45	8.15	5.30
0511	836	16.47	8.17	5.81
606	891	16.48	8.18	6.19
709	954	16.50	8.20	6.62
759	1004	16.52	8.22	6.97
830	1035	16.55	8.25	7.19
908	1073	16.57	8.27	7.45
102	1127	16.58	8.28	7.83
03	1188	16.60	8.30	8.25
00	1245	16.61	8.31	8.65
01	1306	16.62	8.32	9.07
58	1363	16.62	8.32	$9.46 \times 10^{-5}$
500	1425	16.63	8.33	
	1447	15.27	6.97	
	1448	14.59	6.29	
	1449	14.18	5.88	
	1450	13.88	5.58	

min since shutdown

1  
2  
3  
4

Site Ft Pierce date of test \_\_\_\_\_

Well No 1005 actual r 100 m.p elevation \_\_\_\_\_

time	min since start of test	depth to water (ft)	drawdown (ft)	$T/r^2$ dayft <sup>-2</sup>
	1451	5	13.64	5.34
	1453	7	13.25	4.95
	1455	9	12.75	4.65
	1458	12	12.60	4.30
	1461	15	12.30	4.00
	1466	20	11.97	3.67
	1472	25	11.64	3.34
	1476	30	11.46	3.16
	1506	60	10.68	2.38
1630	1515	69	10.53	2.23
1700	1545	99	10.20	1.90
1800	1605	159	9.72	1.42
1900	1665	219	9.43	1.13
2000	1725	279	9.25	0.95
2100	1785	339	9.12	0.82
2200	1845	399	9.05	0.75
2300	1905	459	8.98	0.68
2400	1965	519	8.92	0.62
0100	2025	579	8.85	0.55
0200	2085	639	8.80	0.50
0400	2205	759	8.72	0.42
0600	2325	879	8.66	0.36
0000	2565	1119	8.58	0.28

Site Fort Pierce

date of test 8-23+24-79

Well No 200W actual r 200 ft

m. p elevation 18.49'

M.P. elev only valid with respect to other wells in suite.

Item # 5

time	min since start of test	depth to water (ft)	drawdown (ft)	$T/r^2$ draw <sup>2</sup>
8-23-79 1515	0	7.67	0	
	1	7.98	0.31	$1.74 \times 10^{-8}$
	2	8.52	0.85	$3.5 \times 10^{-8}$
	3	8.93	1.26	5.2
	4	9.27	1.60	6.9
	5	9.55	1.88	$8.7 \times 10^{-8}$
	7	9.98	2.31	$1.2 \times 10^{-7}$
	10	10.50	2.83	$1.7 \times 10^{-7}$
	13	10.89	3.22	2.3
	15	11.10	3.43	2.6
	20	11.52	3.85	3.5
	25	11.78	4.11	4.3
	30	12.03	4.36	5.2
	40	12.40	4.73	6.9
	50	12.63	4.96	8.7
	60	12.84	5.17	$1.0 \times 10^{-6}$
	75	13.07	5.40	1.3
	90	13.25	5.58	1.6
1715	120	13.41	5.72	2.1
1804	169	13.73	6.06	2.9
1900	225	13.92	6.25	3.9
1951	284	14.05	6.38	4.9
2059	344	14.15	6.48	6.0

Site Ft Pierce date of test 8-23, 24-79

Well No 200 W actual r 200 m.p. elevation \_\_\_\_\_

time	min since start of test	depth to water (ft)	drawdown (ft)	$T/r^2 \text{ dayft}^{-2}$
2200	405	14.23	6.56	7.0
2300	465	14.30	6.63	8.1
2400	525	14.35	6.68	9.1
0124	609	14.40	6.73	$1.1 \times 10^{-5}$
0200	645	14.42	6.75	1.12
0257	703	14.43	6.76	1.22
0402	767	14.45	6.78	1.33
0515	840	14.48	6.81	1.46
0557	982	14.49	6.82	1.53
0702	947	14.50	6.83	1.64
0804	1009	14.52	6.85	1.75
0905	1070	14.54	6.87	1.86
1000	1125	14.56	6.89	1.95
1102	1187	14.57	6.90	2.1
1156	1243	14.60	6.93	2.3
1300	1305	14.61	6.94	2.3
1354	1359	14.62	6.95	2.4
1500	1425	14.64	6.97	
	1446.5	14.55	6.88	
	1447	14.43	6.76	
	1448	14.03	6.36	
	1449	13.72	6.05	
	1450	13.42	5.75	

min since start hour

Site Ft Pierce date of test \_\_\_\_\_

Well No 200w actual r 200 m.p elevation \_\_\_\_\_

time	min since start of test	depth to water (ft)	drawdown (ft)	$T/r^2$ day ft <sup>-2</sup>
	1451	5	13.25	5.58
	1453	7	12.88	5.21
	1455	9	12.57	4.90
	1458	12	12.20	4.53
	1461	15	11.90	4.23
	1466	20	11.53	3.86
	1472	26	11.18	3.51
	1476	30	10.99	3.32
	1491	45	10.47	2.80
	1506	60	10.10	2.43
1630	1515	69	9.93	2.26
1700	1545	99	9.53	1.86
1700	1605	159	9.09	1.42
1700	1665	219	8.83	1.16
2000 3-25-79 0930	1725	279	8.65	0.98
	2535	1089	7.94	0.27

Site Fort Pierce date of test 8-23-79

Well No 60 W actual r 60 ft m.p. elevation 18.79'

M.P. elev only valid with respect to other wells in suite

Item # 2

time	min since start of test	depth to water (ft)	drawdown (ft)	$T/r^2 \text{ dayft}^{-2}$
1515	0	8.08	0	
	3	12.40	4.32	$5.8 \times 10^{-7}$
	4	13.31	5.23	$7.7 \times 10^{-7}$
	5	13.60	5.52	$9.6 \times 10^{-7}$
	7	14.05	5.97	$1.35 \times 10^{-6}$
	10	14.40	6.32	$1.93 \times 10^{-6}$
	13	14.83	6.75	2.51
	16	15.09	7.01	3.09
	20	15.38	7.30	3.86
	25	15.63	7.55	4.82
	30	15.83	7.75	5.79
	40	16.10	8.02	7.72
	50	16.31	8.23	$9.65 \times 10^{-6}$
1615	60	16.47	8.39	$1.16 \times 10^{-5}$
	77	16.67	8.59	1.48
	90	16.80	8.72	1.74
1715	120	16.99	8.91	2.32
1803	168	17.20	9.12	3.24
1901	226	17.36	9.28	4.36
2001	286	17.47	9.39	5.52
2158	403	17.63	9.55	7.77
2259	464	17.68	9.60	$8.95 \times 10^{-5}$
2359	524	17.73	9.65	$1.01 \times 10^{-4}$

9.78  
6.32  
2.46

-5  
4

Site Fort Pierce date of test 8-23, 24-79

Well No 60W actual r 60 m.p. elevation \_\_\_\_\_

time	min since start of test	depth to water (ft)	drawdown (ft)	$T/r^2$ day <sup>-2</sup>
0125	610	17.77	9.69	1.18 - 4
0201	646	17.78	9.70	$1.25 \times 10^{-4}$
0258	703	17.78	9.70	1.36
0401	766	17.79	9.71	1.47
0514	839	17.81	9.73	1.62
0557	882	17.82	9.74	1.70
0704	949	17.84	9.76	1.83
0802	1007	17.86	9.78	1.94
0904	1069	17.90	9.82	2.06
0959	1124	17.93	9.85	2.17
1101	1186	17.94	9.86	2.25
1157	1242	17.95	9.87	2.40
1258	1303	17.96	9.88	2.51
1358	1363	17.96	9.88	$2.63 \times 10^{-4}$
1500	1425	17.96	9.88	$2.75 \times 10^{-4}$
	1446.5	16.17	8.09	
	1447	15.67	7.59	
	1448	14.90	6.82	
	1449	14.13	6.35	
	1450	14.08	6.00	
	1451	13.81	5.73	
	1453	13.37	5.29	
	1455	13.03	4.95	

Site Fort Pierce

date of test 8.23.24-79

Well No 60W actual r 60 m.p. elevation \_\_\_\_\_

time	min since start of test	depth to water (ft)	drawdown (ft)	$T/r^2 \text{ dayft}^{-2}$
	1451	12	12.64	4.56
	1461	15	12.29	4.21
	1466	20	11.94	3.86
	1472	26	11.58	3.50
	1476	30	11.38	3.30
	1491	45	10.86	2.78
	1506	60	10.50	2.42
1530	1515	61	10.36	2.28
1700	1545	99	9.96	1.88
1800	1605	159	9.46	1.40
1900	1665	219	9.22	1.14
2000	1725	279	9.03	0.95
2100	1785	339	8.90	0.82
2200	1845	399	8.82	0.74
2300	1905	459	8.74	0.66
2400	1965	519	8.68	0.60
0100	2025	579	8.62	0.54
0200	2085	639	8.57	0.49
0300	2145	699	8.53	0.45
0400	2205	759	8.49	0.41
0600	2325	879	8.43	0.35
0800	2445	999	8.39	0.31
0140	2545	1099	8.35	0.27



9-194  
November 1949

UNITED STATES  
DEPARTMENT OF THE INTERIOR  
GEOLOGICAL SURVEY  
WATER RESOURCES DIVISION

Sh 30

WATER LEVEL MEASUREMENTS (Field)

Measured by Wilcox, Long, Wendert

Location of Project Fort Pierce Pumping test

DATE	HOUR	WELL NO.	TAPE READING AT—		DEPTH TO WATER	REMARKS
			Meas. point	Water level		
8-23-79	1445		8.00	3.69	4.31	
	1507		8.00	3.63	4.37	
	1514		9.00	4.62	4.38	
	1517	2 MIN	8.00	3.61	4.39	
		3 MIN	8.00	3.61		
		14 MIN	8.00	3.59		
		30 MIN	6.00	1.56	4.44	
	1524		7.00	2.52	4.47	
	1525		7.00	2.52	4.49	
	1615	65 MIN	6.00	1.49	4.51	
	1630		5.00	.47	4.53	
	1646		5.00	.44	4.56	
	1703		6.00	1.44	4.56	
	1716		5.00	.41	4.59	
	1802		5.50	.24	4.66	
	1859		5.00	.22	4.74	
	1902		5.00	.16	4.84	
	2103		14.00	9.06	4.94	* 2
	2204		6.00	.97	5.03	
	2302		6.00	0.90	5.10	
8-24-79	0004		6.00	.83	5.17	
	127		6.00	.73	5.27	
	204		6.00	.68	5.32	

Item 6

9-194  
November 1949

UNITED STATES  
DEPARTMENT OF THE INTERIOR  
GEOLOGICAL SURVEY  
WATER RESOURCES DIVISION

WATER LEVEL MEASUREMENTS (Field)

Measured by \_\_\_\_\_

Location of Project \_\_\_\_\_

DATE	HOUR	WELL NO.	TAPE READING AT—		DEPTH TO WATER	REMARKS
			Meas. point	Water level		
8/24/79	0302		6.00	.61	5.39	
	0400		6.00	.52	5.48	
	0510		6.00	.46	5.54	
			6.00	.38	5.62	
	0707		6.00	0.32	5.68	
	0802		6.00	0.26	5.74	
	0906		6.00	0.18	5.82	
	1000		7.00	0.13	5.87	
	1101		7.00	1.08	5.92	
	1159		7.00	1.02	5.98	
	1259		7.00	0.97	6.03	
	1354		7.00	0.91	6.09	
	1500		7.00	0.85	6.15	
	1518		7.00	.84	6.16	
	1 MIN		7.00	.81	6.19	
	7'30"		7.00	.83	6.17	
	9'30"		7.00	.83	6.17	
	11 MIN		7.00	.83	6.17	
	20 MIN		7.00	.81	6.19	
	29 MIN		7.00	.79	6.21	
	45 MIN		9.00	.79	6.21	
1627	6 51 AM		7.00	.77	6.23	

Site Fort Pierce

date of test 8-23+24-79

Well No 305 actual r 30 ft

m.p. elevation 19.97  
 m.p. elev only valid with respect to other wells in suite.

Item #4

time	min since start of test	depth to water (ft)	drawdown (ft)	$T/r^2$ dayft <sup>-2</sup>
1515	0	9.29	0	
	1	15.44	6.15	$7.7 \times 10^{-7}$
	2	16.36	7.07	$1.54 \times 10^{-6}$
	3	16.85	7.56	$2.31 \times 10^{-6}$
	4	17.17	7.88	$3.09 \times 10^{-6}$
	5	17.42	8.13	$3.86 \times 10^{-6}$
	7	17.79	8.50	$5.40 \times 10^{-6}$
	10	18.19	8.90	$7.72 \times 10^{-6}$
	13	18.45	9.16	$1.00 \times 10^{-5}$
	15	18.60	9.31	$1.16 \times 10^{-5}$
	20	18.88	9.59	$1.54 \times 10^{-5}$
	25	17.08	9.79	$1.93 \times 10^{-5}$
	30	19.24	9.95	$2.32 \times 10^{-5}$
	40	19.48	10.19	$3.09 \times 10^{-5}$
	50	19.64	10.35	$3.86 \times 10^{-5}$
1615	60	19.29	10.00	$4.63 \times 10^{-5}$
1630	75	19.93	10.64	$5.79 \times 10^{-5}$
1645	90	20.06	10.77	$6.94 \times 10^{-5}$
1716	100 121	20.23	10.94	$9.34 \times 10^{-5}$
1801	166	20.42	11.13	$1.28 \times 10^{-4}$
1859	224	20.56	11.27	$1.73 \times 10^{-4}$
2002	287	20.65	11.36	$2.21 \times 10^{-4}$
2102	347	20.73	11.44	$2.68 \times 10^{-4}$

Site Fort Pierce

date of test 8-23, 24-79

Well No 303 actual r 30 m.p. elevation         

time	min since start of test	depth to water (ft)	drawdown (ft)	$T/r^2$ days <sup>-2</sup>
2202	407	20.80	11.51	3.14 -4
2301 8-24-79	466	20.85	11.56	3.60 -4
0002	527	20.88	11.59	4.07 -4
0126	611	20.90	11.61	4.71 -4
0202	647	20.90	11.61	4.99 -4
0259	704	20.91	11.62	5.43 -4
0356	763	20.92	11.63	5.68
0509	834	20.94	11.65	6.44
0601	886	20.95	11.66	6.84
0705	950	20.96	11.67	7.33
0701	1006	20.98	11.69	7.76
0805	1070	21.02	11.73	8.26
0959	1124	21.04	11.75	8.67
1101	1186	21.05	11.76	9.15
1158	1243	21.06	11.77	9.59
1258	1303	21.06	11.77	$1.00 \times 10^{-3}$
1356	1361	21.06	11.77	1.05
1457	1422	21.05	11.76	$1.11 \times 10^{-3}$
	1447	16.80	7.51	
	1448	15.99	6.70	
	1449	15.50	6.21	
	1450	15.15	5.86	
	1451	14.85	5.56	

Site Fort Pierce

date of test 8-23, 24-79

Well No 305 actual r 30 m.p. elevation       

time	min since start of test	depth to water (ft)	drawdown (ft)	$T/r^2$ day ft <sup>-2</sup>
	1453 7	14.44	5.15	
	1455 9	14.11	4.82	
	1458 12	13.74	4.45	
	1461 15	13.42	4.13	
	1466 20	13.07	3.78	
	1472 26	12.73	3.44	
	1476 30	12.54	3.25	
	1491 45	12.06	2.77	
	1506 60	11.72	2.43	
1630	1515 69	11.54	2.25	
1700	1545 99	11.21	1.92	
1800	1605 159	10.75	1.46	
1900	1665 219	10.47	1.18	
2000	1725 279	10.26	0.97	
2100	1785 339	10.13	0.84	
2200	1845 399	10.04	0.75	
2300	1905 459	9.98	0.69	
2400	1965 519	9.91	0.62	
8-25-79 0100	2025 579	9.85	0.56	
0200	2085 639	9.79	0.50	
0400	2205 759	9.70	0.41	
0600	2325 879	9.65	0.36	
0950	2555 1109	9.58	0.29	

//

UNITED STATES  
DEPARTMENT OF THE INTERIOR  
GEOLOGICAL SURVEY  
WATER RESOURCES DIVISION

300 S

Stat 1516 \*

WATER LEVEL MEASUREMENTS (Field)

Measured by \_\_\_\_\_

Location of Project

Fort Pierce (pumping test)

DATE	HOUR	WELL NO.	TAPE READING AT—		DEPTH TO WATER	REMARKS
			Mens. point	Water level		
8-23-79	1440		9.00	1.51	7.49	
	1518		9.00	1.28	7.72	
	1520		9.00	0.83	8.17	
	1522		12.00	3.43	8.57	
	1525		10.00	1.02	9.97	
	1535		10.00	0.29	9.71	
	1545		11.00	0.89	10.11	
	1600		11.00	0.49	10.51	
	1609		12.00	1.29	10.71	
	1636		12.00	0.91	11.09	
	1649		12.00	0.81	11.19	
	1725		12.00	0.55	11.45	
	1809		14.00	2.32	11.68	
	1908		13.00	1.14	11.86	
	1925		13.00	1.06	11.94	
	2008		13.00	1.05	11.95	
	2110		13.00	0.90	12.10	
	2212		13.00	0.84	12.16	
	2308		13.00	0.78	12.22	
8/24/79	0007		13.00	0.72	12.28	
	0111		13.00	0.67	12.33	
	0209		13.00	0.64	12.36	
	2:07		13.00	0.58	12.42	

Item 9

9-194  
November 1948

UNITED STATES  
DEPARTMENT OF THE INTERIOR  
GEOLOGICAL SURVEY  
WATER RESOURCES DIVISION

WATER LEVEL MEASUREMENTS (Field)

Measured by \_\_\_\_\_

Location of Project \_\_\_\_\_

DATE	HOUR	WELL NO.	TAPE READING AT—		DEPTH TO WATER	REMARKS
			Mens. point	Water level		
	350		13.00	0.61	12.39	
	0520		13.00	0.59	12.41	
	0707		13.00	0.57	12.43	
	0711		13.00	0.54	12.46	
	0715		13.00	0.53	12.47	
	0910		13.00	0.49	12.51	
	1004		13.00	0.47	12.53	
	1104		13.00	0.45	12.55	
	1204		13.00	0.43	12.57	
	1303		13.00	0.42	12.58	
	1404		13.00	0.42	12.58	
	1504		13.00	0.41	12.59	
	1516		13.00	0.41	12.59	
	1 min		13.00	0.58	12.42	Pump off
	3 min		13.00	1.27	11.73	
	5 min		12.00	0.22	11.78	← ?
	10 min		12.00	0.63	11.37	
	16 min		12.00	1.06	10.94	
	22		12.00	1.36	10.64	
	27		12.00	1.57	10.43	
	48 min		11.00	1.07	9.93	
	55 min		11.00	1.40	9.60	
8-25-79	1047		9.00	1.68	7.72	

Fort Pierce Test  
August 23-24, 1979

Obs. Well 305

100  
Δ Bounded Aquifer (9)

WELL 305

$$\Sigma W(u) = 1.0$$

$$T = \frac{163 \times 1.0}{4\pi \times 1.20}$$

$$S = \frac{4 \times 2080 \times 3.6}{900 \times 1440 \times 1000}$$

$$r = 30$$

$$\frac{1}{u} = 1000$$

$$= 15,600$$

$$= 1.000023 (2.3 \times 10^{-5})$$

$$Q = 163$$

$$t = 3.6$$

$$= 2,080$$

$$s = 1.20$$

10

Theris ---  
K = 125

1.0

$$\Delta \cdot 0$$

$$H(u, \beta) = 1.0$$

$$T = \frac{163 \times 1.0}{4\pi \times 1.40}$$

$$S = \frac{4 \times 1780 \times 6.0}{900 \times 1440 \times 1000}$$

$$\frac{1}{u} = 10^3$$

$$t = 6.0$$

$$= 13,340$$

$$= .000033 (3.3 \times 10^{-5})$$

$$s = 1.4$$

$$= 1,780$$

⊙ Hantush Modified

1.1

10

100

1000

10000

Fort Pierce Test  
August 23-24, 1979

Superconduct

Bounded Aquifer (Plate 9)

Obs. Wells 100 S & 200 W

Well 100 S

$$\Delta \Sigma W(u) = 1.0 \quad T = 163 \times 1.0$$

$$\frac{1}{u} = 10 \quad 4\pi r^2 \times 1.40$$

$$t = 8.2 \quad = 13,340$$

$$S = 1.40 \quad = 1,780$$

$$k = 20$$

Well 200 W

$$\Delta \Sigma W(u) = 1.0 \quad T = 163 \times 1.0 \quad S = 4 \times 1710 \times 9.0 \quad 200 W \quad 100 S$$

$$\frac{1}{u} = 10 \quad 4\pi r^2 \times 1.46 \quad 200^2 \times 1440 \times 10 \quad r = 200 \quad r = 100$$

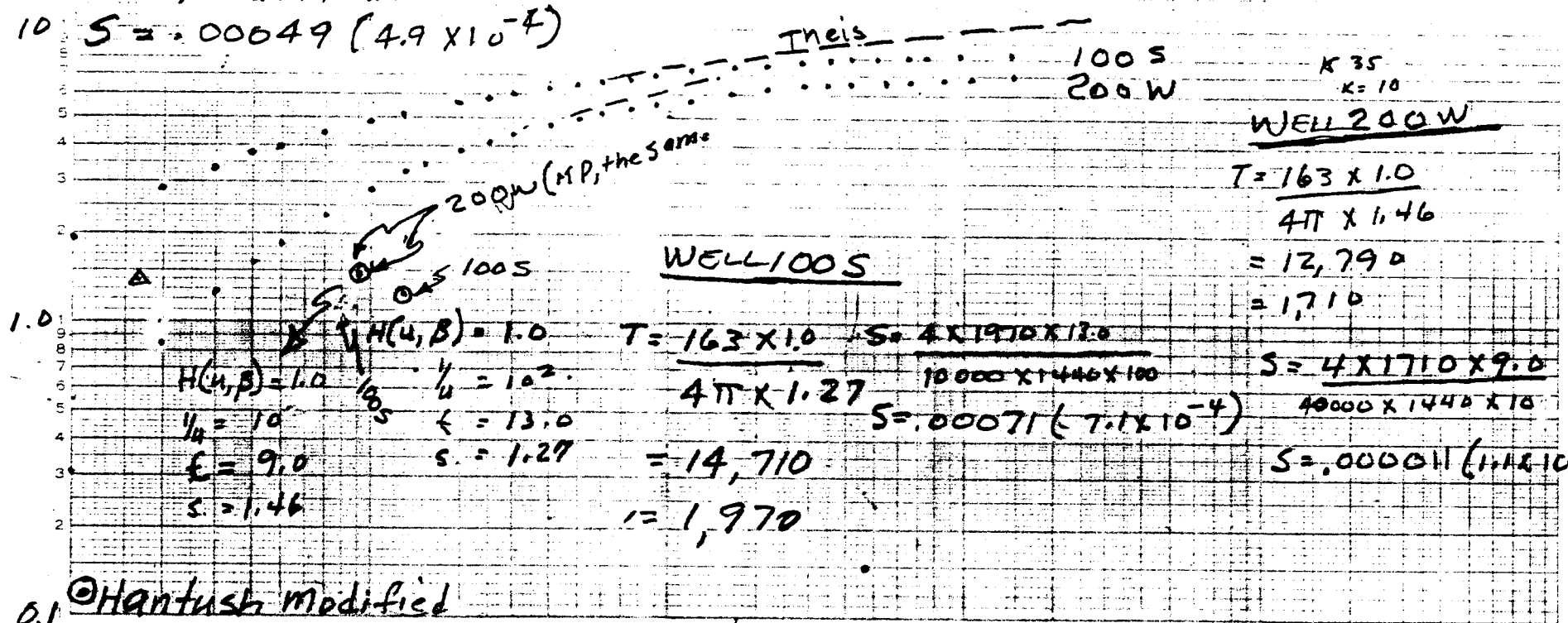
$$t = 9.0 \quad = 12793 \quad S = 1.1 \times 10^{-4} \quad Q = 163 \quad Q = 16$$

$$S = 1.46 \quad = 1710$$

$$k = 10$$

$$S = \frac{4 \times 2,153 \times 8.2}{100^2 \times 1440 \times 10}$$

$$S = .00049 \quad (4.9 \times 10^{-4})$$



WELL 200 W

$$T = 163 \times 1.0$$

$$4\pi r^2 \times 1.46$$

$$= 12,790$$

$$= 1,710$$

WELL 100 S

$$T = 163 \times 1.0 \quad S = 4 \times 1710 \times 9.0$$

$$4\pi r^2 \times 1.27 \quad 10000 \times 1440 \times 10$$

$$S = .00071 \quad (7.1 \times 10^{-4})$$

$$= 14,710$$

$$= 1,970$$

$$S = 4 \times 1710 \times 9.0$$

$$40000 \times 1440 \times 10$$

$$S = .000011 \quad (1.1 \times 10^{-4})$$

0.1 © Hantush Modified

Comp by GWH

Fort Pierce Aquifer Test

August 23-24, 1979

by: GWHill 1/6/80

Estimation of Image well radius, PL 9

$r = 60$

$K = 25$

$r_i = 1500$

$r/2 = 30$   $r_i/2 = 750$

$r = 100$

$K = 20$

$r_i = 2000$

$r/2 = 50$   $r_i/2 = 1000$

$r = 200$

$K = 10$

$r_i = 2000$

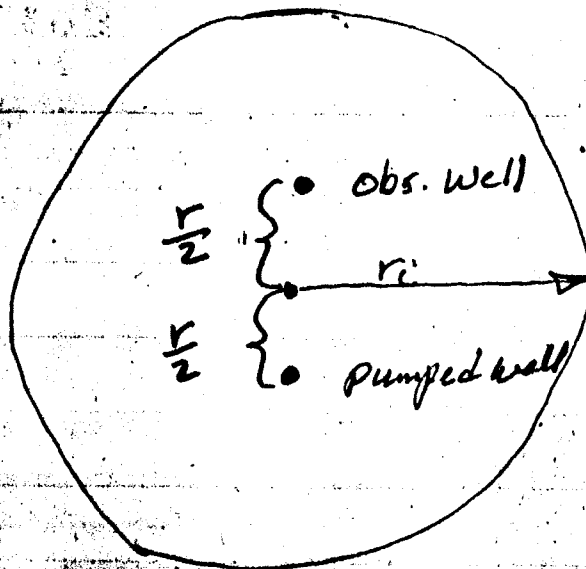
$r/2 = 100$   $r_i/2 = 1000$

$r = 300$

$K = 7$

$r_i = 2100$

$r/2 = 150$   $r_i/2 = 1050$



This checks results of the Log-log Method shown in the test report on page 4.



# Fort Pierce Test

## August 23-24, 1979

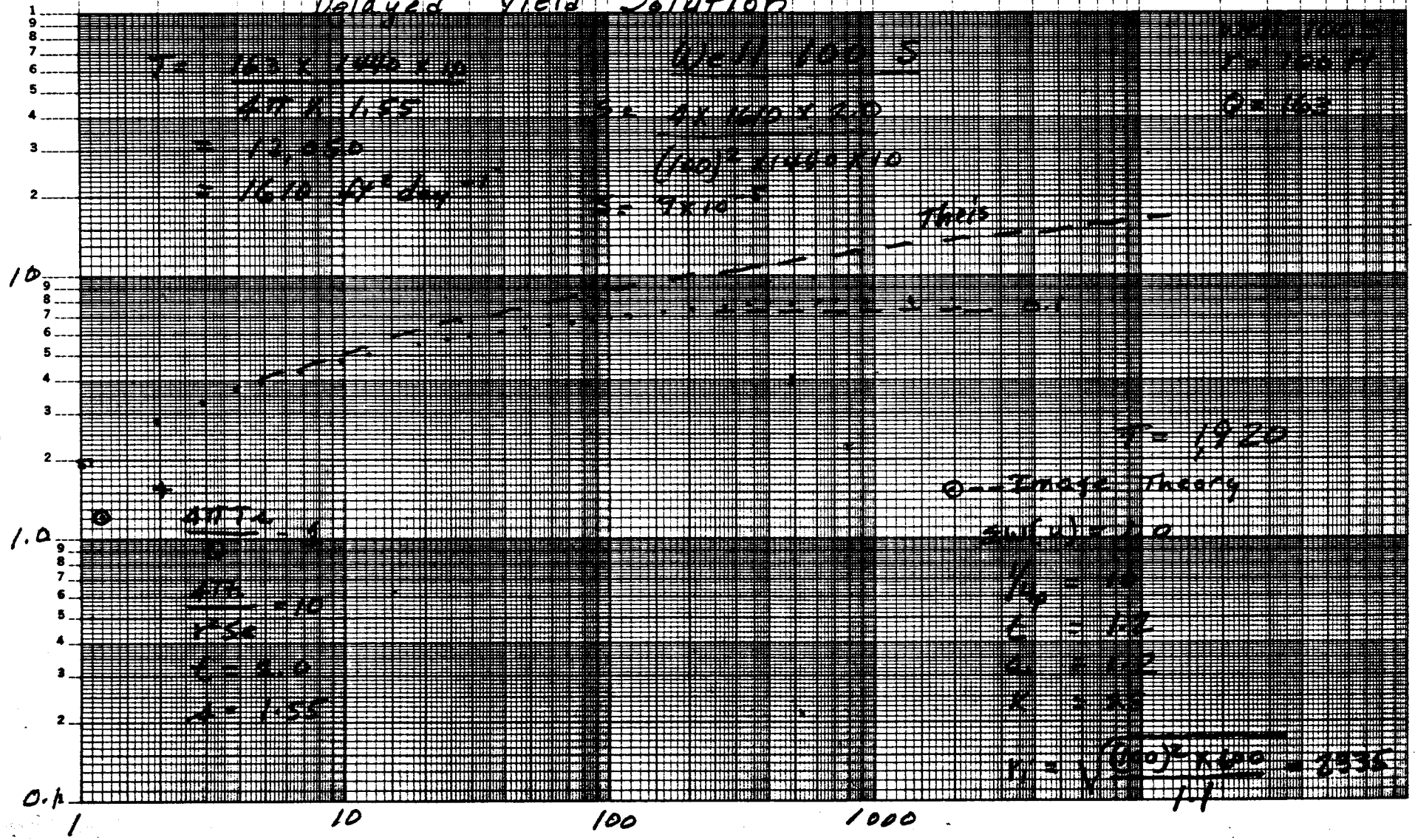
Comp. by GWH

### Delayed Yield Solution

$T = 16.2 \times 10^4 \times 10$   
 $h = 1.55$   
 $\mu = 12,000$   
 $\sigma = 16.10 \times 10^4 \text{ day}^{-1}$

Well 100 S  
 $\mu = 12,000 \times 10$   
 $(100)^2 \times 10^4 \times 10$   
 $\sigma = 9 \times 10^4$

$\mu = 12,000$   
 $\sigma = 16.10$



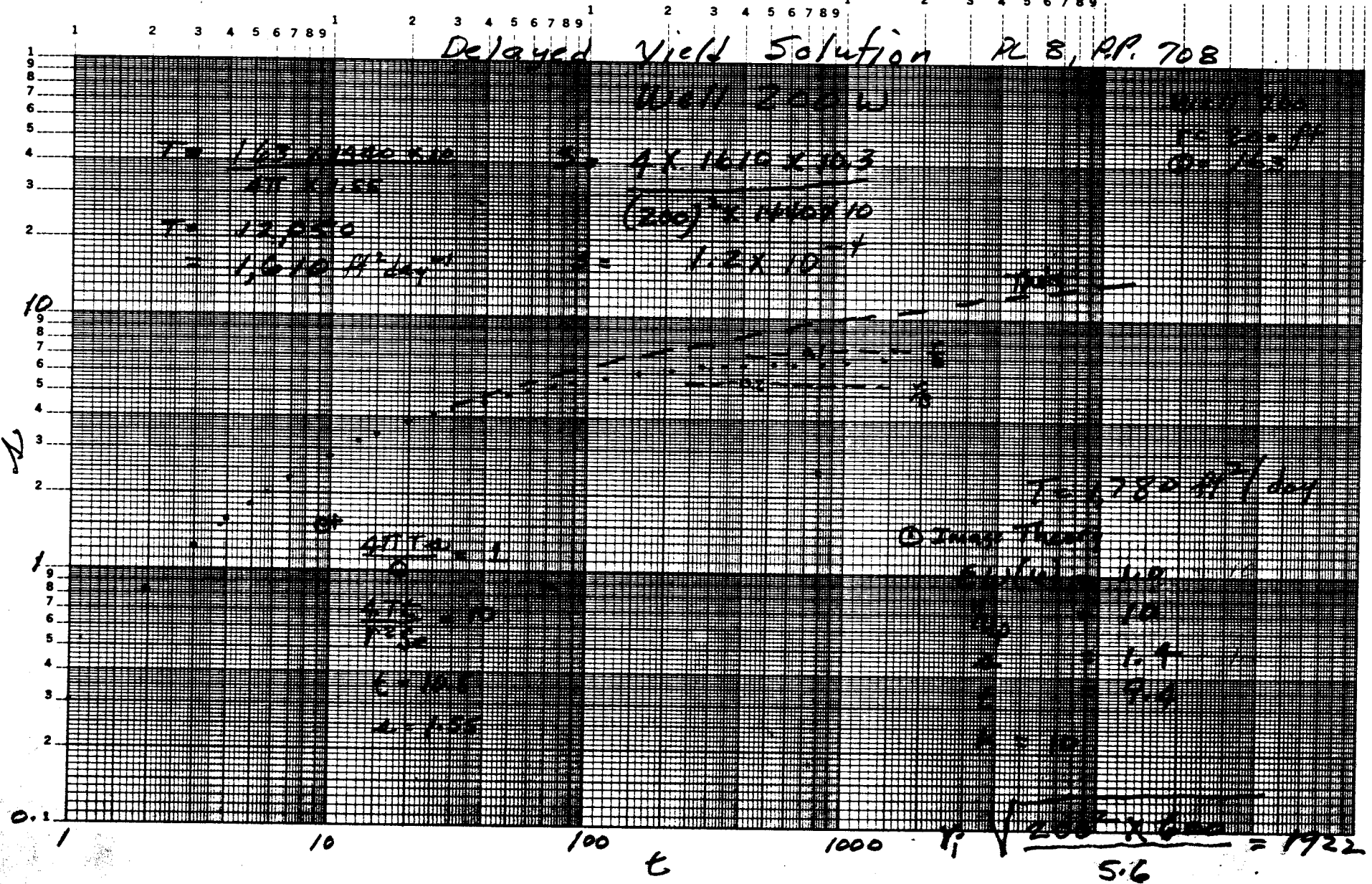
$\frac{h}{r} = 1.55$   
 $\frac{h}{r} = 10$   
 $\mu = 12,000$   
 $\sigma = 16.10$   
 $\lambda = 1.55$

$T = 1920$   
 Image Theory  
 $\mu = 12,000$   
 $\sigma = 16.10$   
 $\lambda = 1.55$   
 $\mu = \sqrt{(100)^2 \times 10^4} = 2530$

Fort Pierce Test  
August 23-24, 1979

Comp. by GWH

Delayed Yield Solution PL 8, RP. 708



$T = 1.8 \times 10^5$  sec  
 $S = 4 \times 10^{19} \times 10^{-3}$   
 $T = 12,000$   
 $S = 1.2 \times 10^{-4}$

$S = 4 \times 10^{19} \times 10^{-3}$   
 $(200)^2 \times 60 = 10$   
 $1.2 \times 10^{-4}$

$T = 780$  sec/day

Other Theory  
C  
1.8  
10  
1.4  
9.8

$\sqrt{200 \times 60} = 112.2$   
5.6

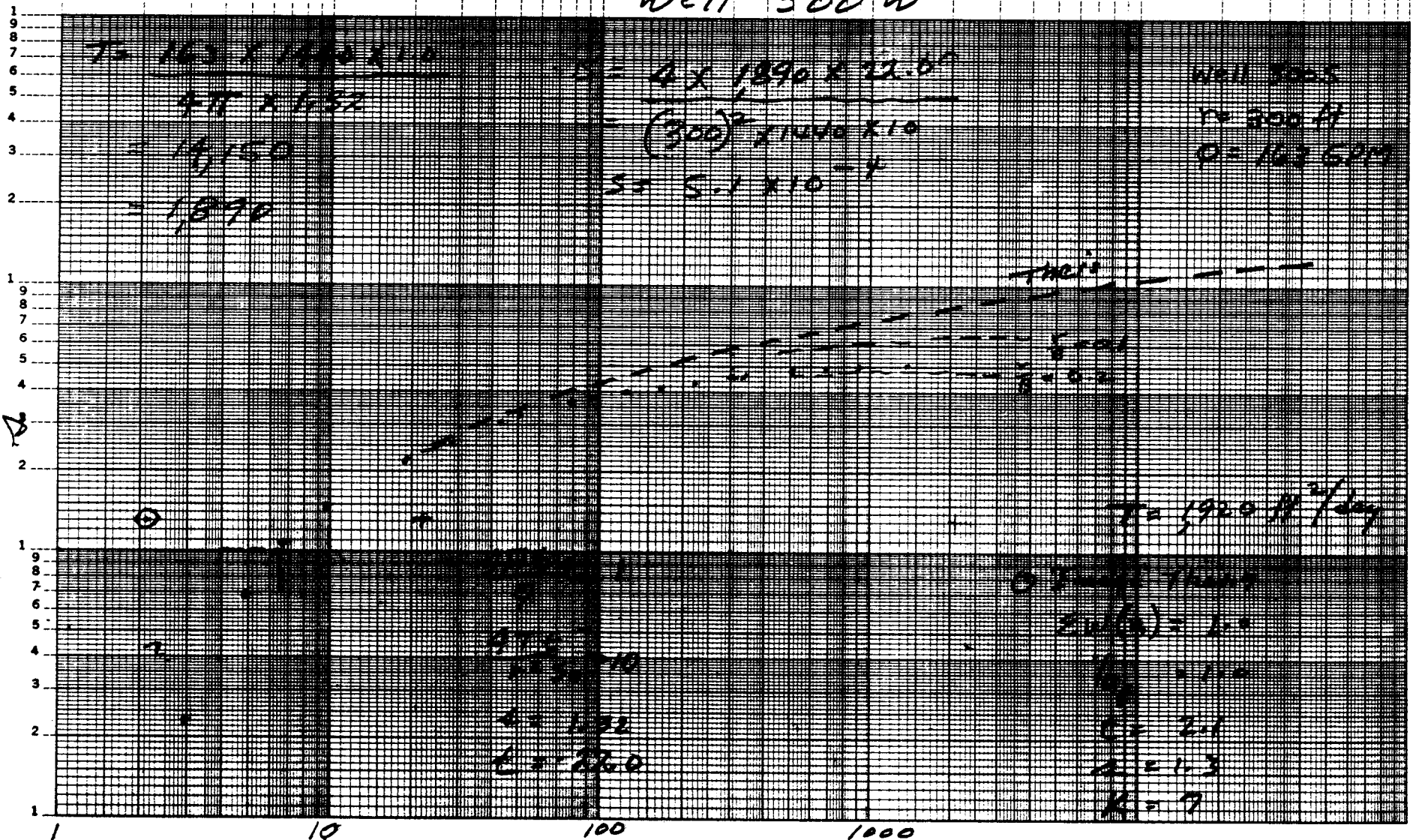


Fort Pierce Test  
August 23-24, 1979

Comp. by GWH

Delayed Yield Solutions

Well 300 W

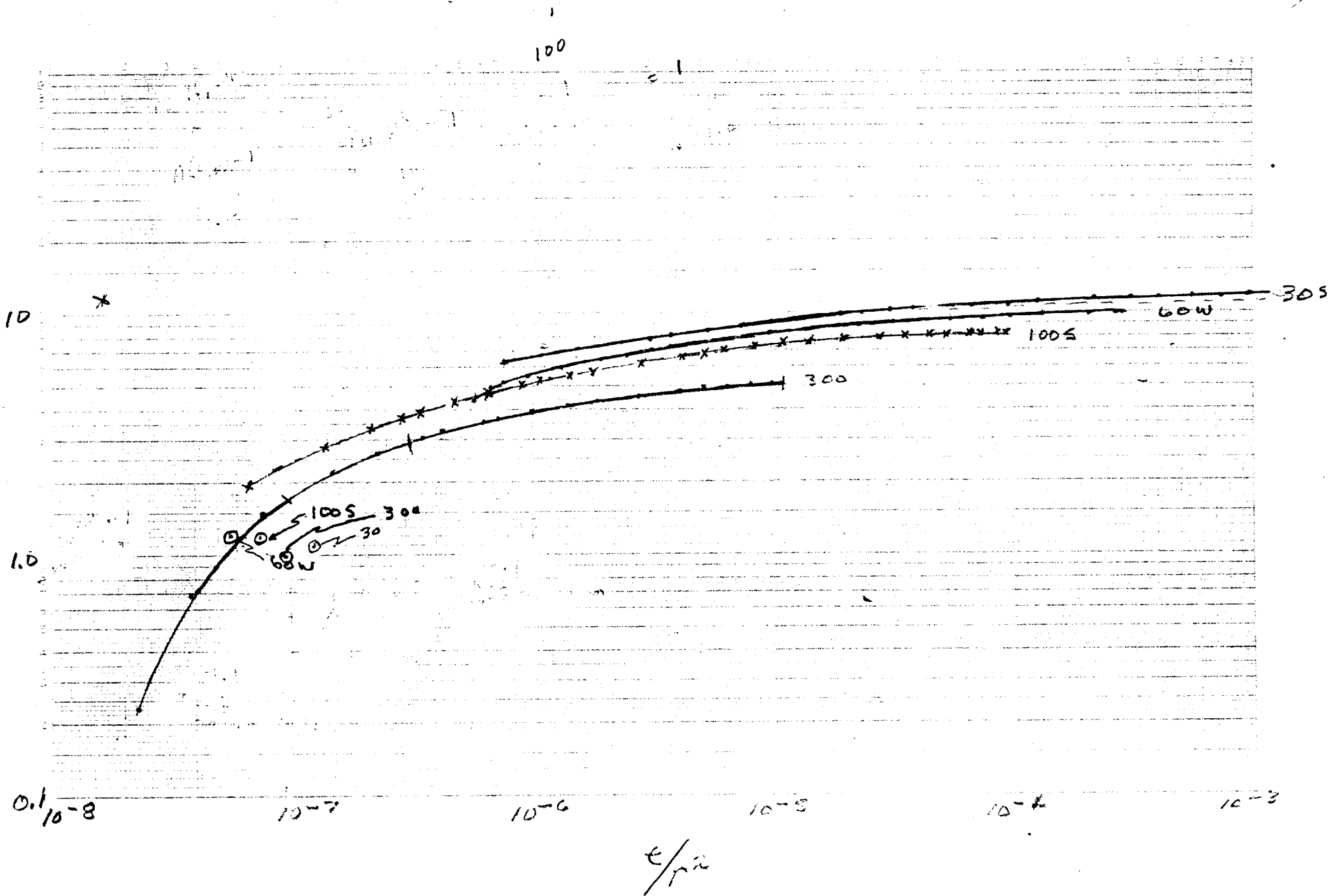


$$r_i \sqrt{\frac{(300)^2 \times 300}{6.5}} = 2038$$

# Fort Pierce Test

August 23, 24, 1979

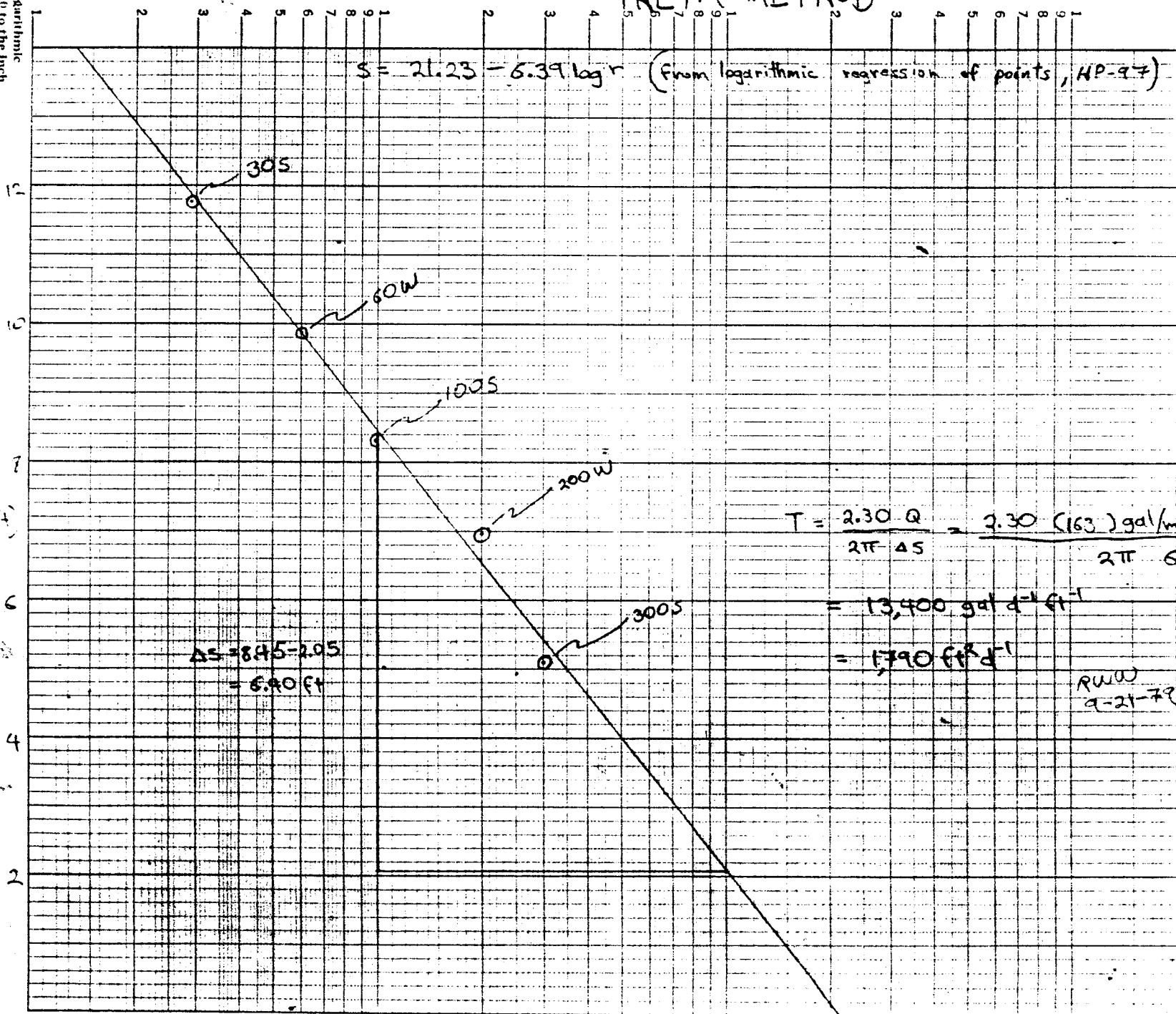
Drawdown, in feet



8-23424-79

# THEIM METHOD

$S = 21.23 - 6.39 \log r$  (from logarithmic regression of points, HP-97)



coefficients  
 $r^2 = 0.99$   
 $a = 21.23$   
 $b = -6.39$

$$T = \frac{2.30 Q}{2\pi M S} = \frac{2.30 (163) \text{ gal/min} (1440) \text{ min/d}}{2\pi (6.40) \text{ ft}}$$

$$= 13,400 \text{ gal d}^{-1} \text{ ft}^{-1}$$

$$= 1,790 \text{ ft}^2 \text{ d}^{-1}$$

RWW  
 $a = 21 - 7?$

50.00  
 10.00  
 50.00  
 9.00  
 50.00  
 8.00  
 100.00  
 6.00  
 300.00  
 5.00

Fort Pierce Test August 23-24, 1979  
 computed by George Hill

Delayed Yield Solution PL 8; PP. 708

<u>well No.</u>	<u>Transmissivity</u>	<u>S</u>
100 S	1,610 ft <sup>2</sup> /d	
200 W	1,610 ft <sup>2</sup> /d	1.2 x 10 <sup>-4</sup>
300 S	1,890 ft <sup>2</sup> /d	5.1 x 10 <sup>-4</sup> 9.0 x 10 <sup>-5</sup>

Hantush - Jacob PL 3; PP. 708

USE

<u>well No</u>	<u>Transmissivity</u>	<u>S</u>
100 S	1,780 ft <sup>2</sup> /d	7.1 x 10 <sup>-5</sup>
200 W	1,560 ft <sup>2</sup> /d	1.1 x 10 <sup>-4</sup>
300 S	1,560 ft <sup>2</sup> /d	3.6 x 10 <sup>-4</sup>

Then

$$T = 1,790 \text{ ft}^2/\text{d}$$

all in same ball park

Image Well Theory

<u>well No.</u>	<u>Transmissivity</u>	<u>S</u>
60 W	1,650 ft <sup>2</sup> /d	4.2 x 10 <sup>-4</sup>
100 S	2,153 ft <sup>2</sup> /d	4.9 x 10 <sup>-4</sup>
200 W	1,710 ft <sup>2</sup> /d	1.1 x 10 <sup>-4</sup>
300 S	1,920 ft <sup>2</sup> /d	1.3 x 10 <sup>-4</sup>

# Discharge Measurements

3" orifice 6" pipe

Location

Fort Pierce pumping test

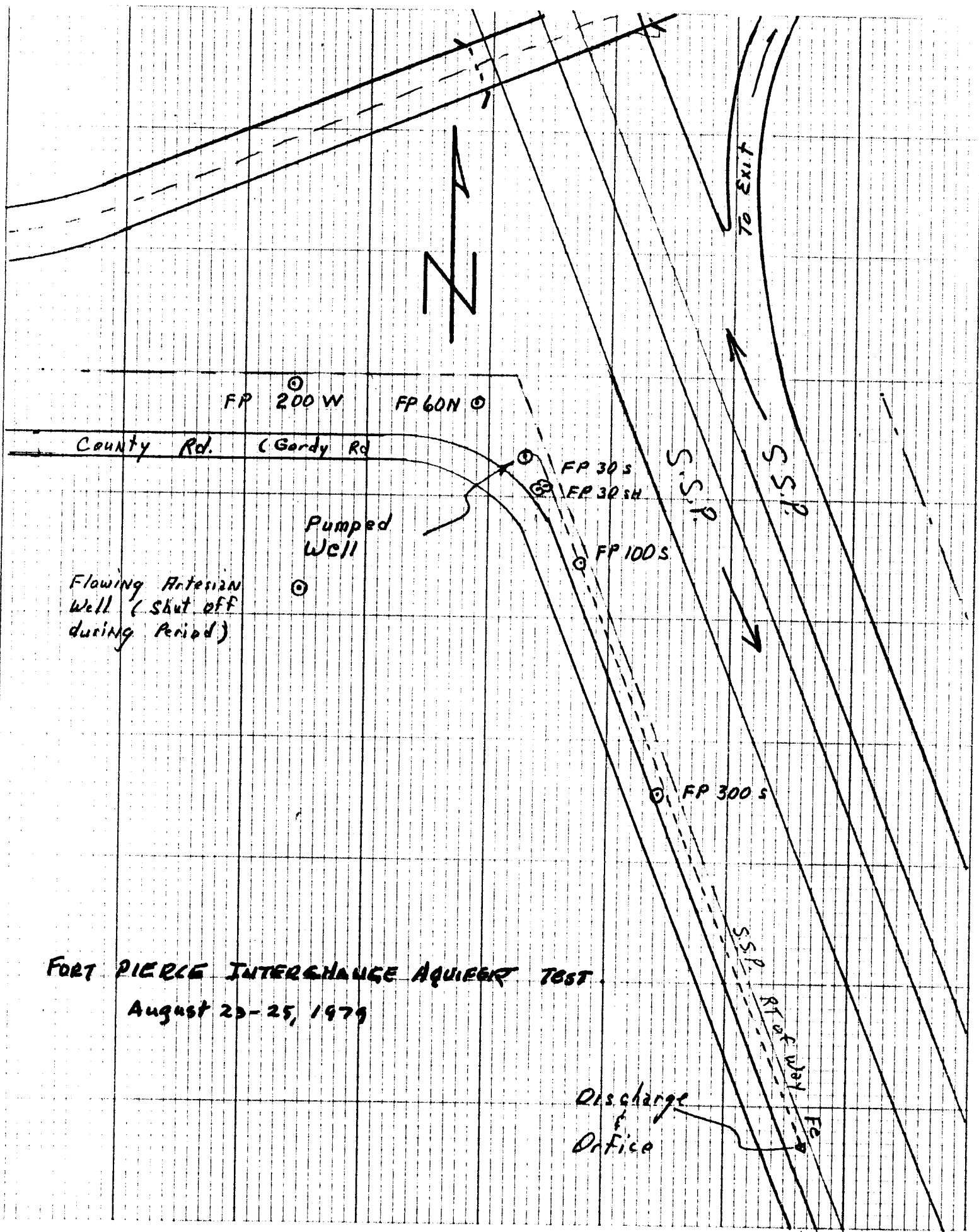
Party - Wilcox, Long, Wendorf, Cook

Date

8-23-79 & 8-24-79

LINE	time	head	discharge gpm	time	head	discharge	Rainfall	REMARKS
1							.09	Just prior to test
2	1525	33 1/2	194	1005	22 1/2	158		
3	1531	31 1/2	188	1104	22 3/8	158		
4	1544	30	183	1205	22 3/8	158		
5	1557	28 7/8	180	1304	22 1/4	157		
6	1608	28	177	1405	22 1/4	157		
7	1634	26 1/2	173	1506	22 1/4	157		
8	1650	26	171	1517	22 1/4	157		
9	1724	25 1/8	167					
10	1800	25"	167					
11	1906	24 1/8	164					weighted ave. Q = 163 gpm
12	1942	24	164					
13	2006	23 3/4	163					
14	2108	23 5/8	163					
15	2212	23 1/2	162					
16	2306	23 3/8	160					
17	0008	23 1/2	160					
18	141	22 7/8	160					
19	210	22 7/8	160					
20	308	22 7/8	160					
21	342	22 3/4	159					
22	355	22 3/4	159					
23	523	22 3/8	159					
24	0612	22 5/8	157					
25	0714	22 5/8	157					
	0813	22 1/2	156					



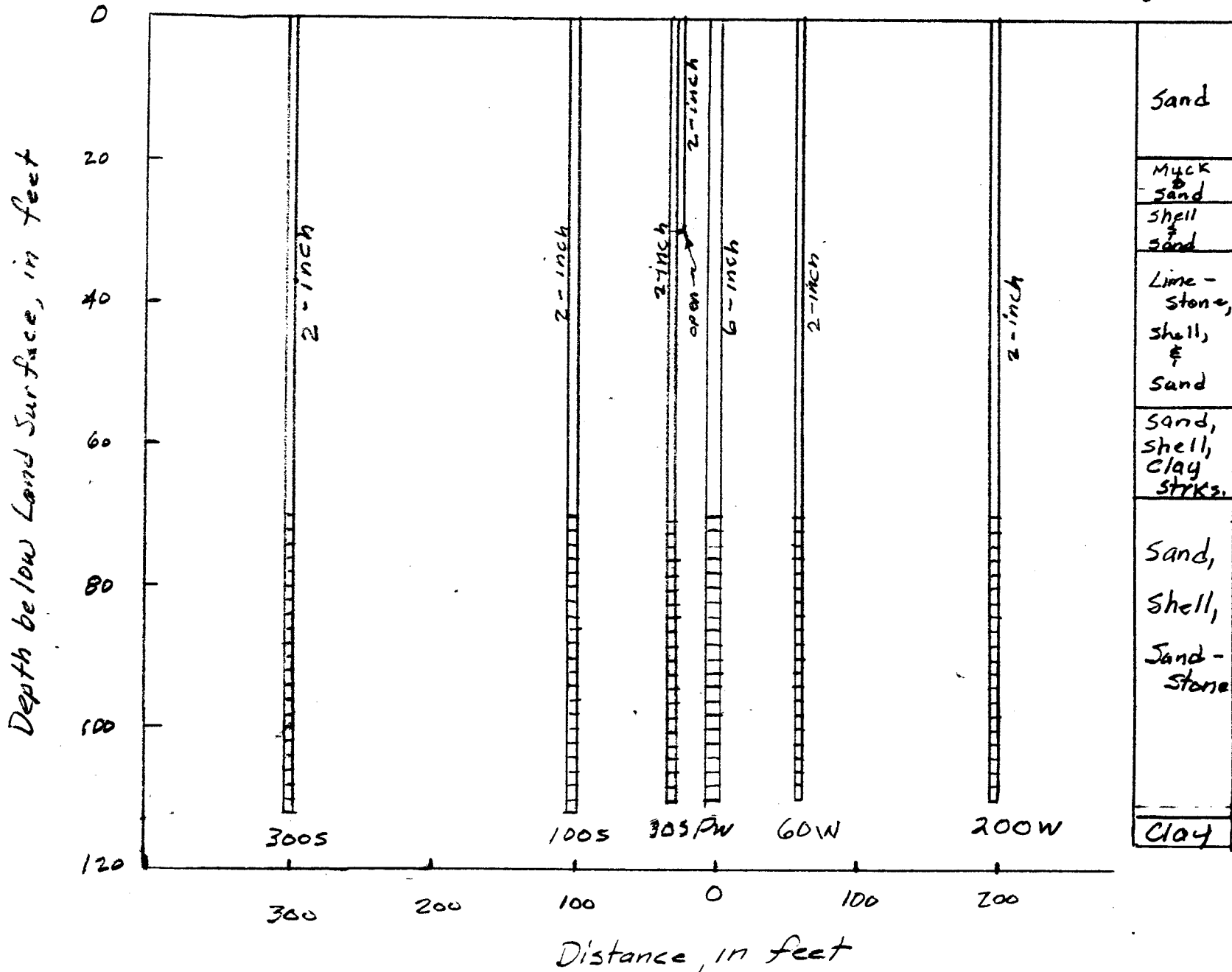


**FORT PIERCE INTERCHANGE AQUIFER TEST**  
 August 23-25, 1979

# Fort Pierce Turnpike Interchange Test

## SECTION SKETCH

Lithology  
summary (FP-1 log)



Location

SSP &amp; SA70 on Gandy Rd - Ft Pierce Exchange

Party

Long Wilcox

Date

8/25/79

LINE	Station	BS	HI Elev. Avg	HI	FS	Avg	Elev.	REMARKS
1								
2		3.77	23.77				20.00	Start Arb. Datum 20ft top of Conc RW MK. Cur. Fc line SWant inside cur of Inter Change @ FT Pierce
3								
4								
5	200				-5.28	@ 5.28	18.49	Well FP 200 W
6						6.28		LS 17.5
7	60				-4.98	@ 4.98	18.79	Well FP 60 W
8						6.11		LS 17.7
9	0				-3.68		20.09	Pumped Well FP-1 (NW cur cap)
10						6.07		LS 17.70
11	28.5				-3.80	@ 3.80	19.97	Well FP 30 so
12						6.35		LS 17.4
13	28.5				-4.08		19.69	Shallow Well FP 30 so
14						6.0		LS 17.8
15	99.2				-4.87		18.90	Well FP 102s
16						6.44		LS 17.3
17	300				-5.84	@ 5.837	17.93	Well FP 300 s
18						5.90		LS = 17.9
19								
20								
21			23.77		-3.77		20.00	Check back to start
22								
23								
24								
25								

after running levels, <sup>after</sup> adjusted m.p. by addi<sup>+0.13</sup> a coupling to 305

Location

Ft Pierce Pump Test @ SSP of SR 70

Party

Long

Date

July, 1979

Line	Station	Drill Depth	Csg Avg	Screen HI	Set Screen	Develop Avg	Standby Elev.	Remarks	REMARKS
1	Pump Well	115	73	70-110	1 hr	4 hrs		6 in well	
2									
3	<del>FP</del>	1150	438 <sup>00</sup>						
4									
5	FP-60W	123	80	70-110	1/2 hr	2 hrs	1 1/2 hrs	2 in	
6									
7	FP 200W	111	70	70-110	1/2 hr	3 hrs			
8									
9	FP -100s	117	75	72-112	1/2 hr	3 hrs			
10									
11	FP-300s	113	75	72-112	1/2	3 hrs			
12									
13									
14									
15									
16									
17									
18		2,320	450 <sup>00</sup>		300 <sup>00</sup>	125 <sup>00</sup>	82.50		
19		1150 <sup>00</sup>	438 <sup>00</sup>	<del>70-110</del>	75 <sup>00</sup>				
20									
21									
22									
23									
24									
25									

tot 1393.50



# Piped well recovery

8/24/77

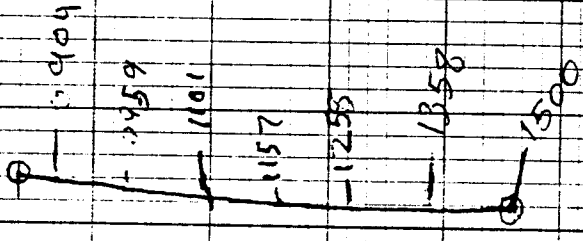
Time	H	R	DTW
2' 30 sec	19	3.15	15.85
4' 30"	15	.13	14.87
6 min	15	.28	14.72
8 min	15	.64	14.36
10	15	.90	14.1
15 min	14	.48	13.52
21	14	.85	13.15
31 min	14	1.37	12.63
46 min	14	1.80	12.14
66 min	13	1.28	11.72

(2)

D/O 60W

Fort Pierce Site  
60W RWV  
WT 0880

8-24-79  
held 19.00  
read 10.11  
d.w. 17.89



RWV  
8-24-79  
WT 1595  
held 18.50  
read 2.54  
d.w. 17.96

17.5

18

RECORDING CHARTS GRAPHIC CONTROLS CORPORATION BUFFALO, NEW YORK

FT PIERCE SITE 1005  
MAN 8/2/79  
WT 1505  
HT 10.00  
RT 1.71  
DITS 8.29

scale?

Background  
water level  
well 1005

X.09

Fort Pierce Site  
1005 RWV  
8-23-79 WT 1127  
WT 9.00  
WT 0.57  
DITS 8.33



X.09

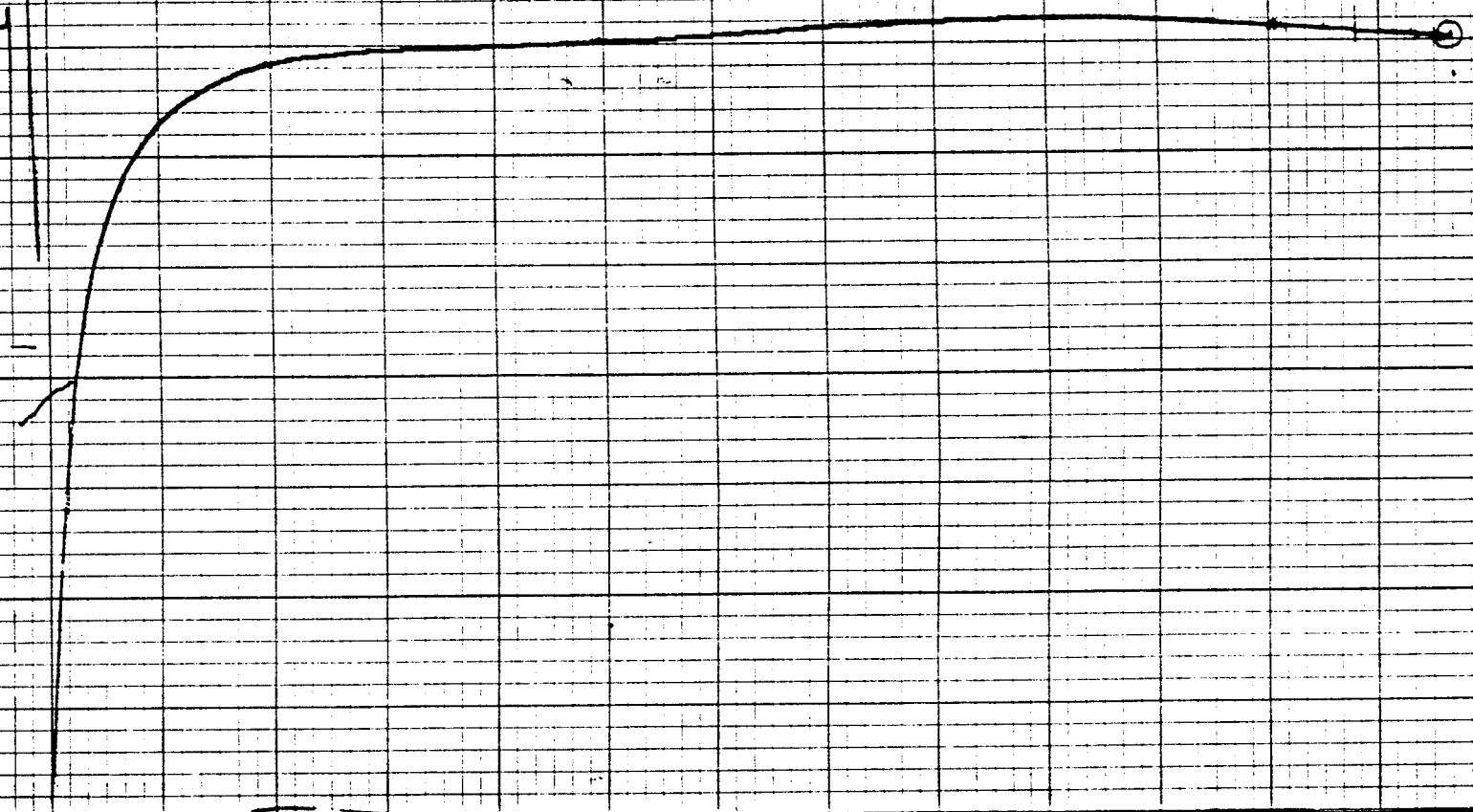


Water Well 100

X.09

Fort Pierce Site  
 1005 P.W.W.  
 8-23-79 W.I.H.A.  
 9.00  
 0.54  
 8.33

X.09



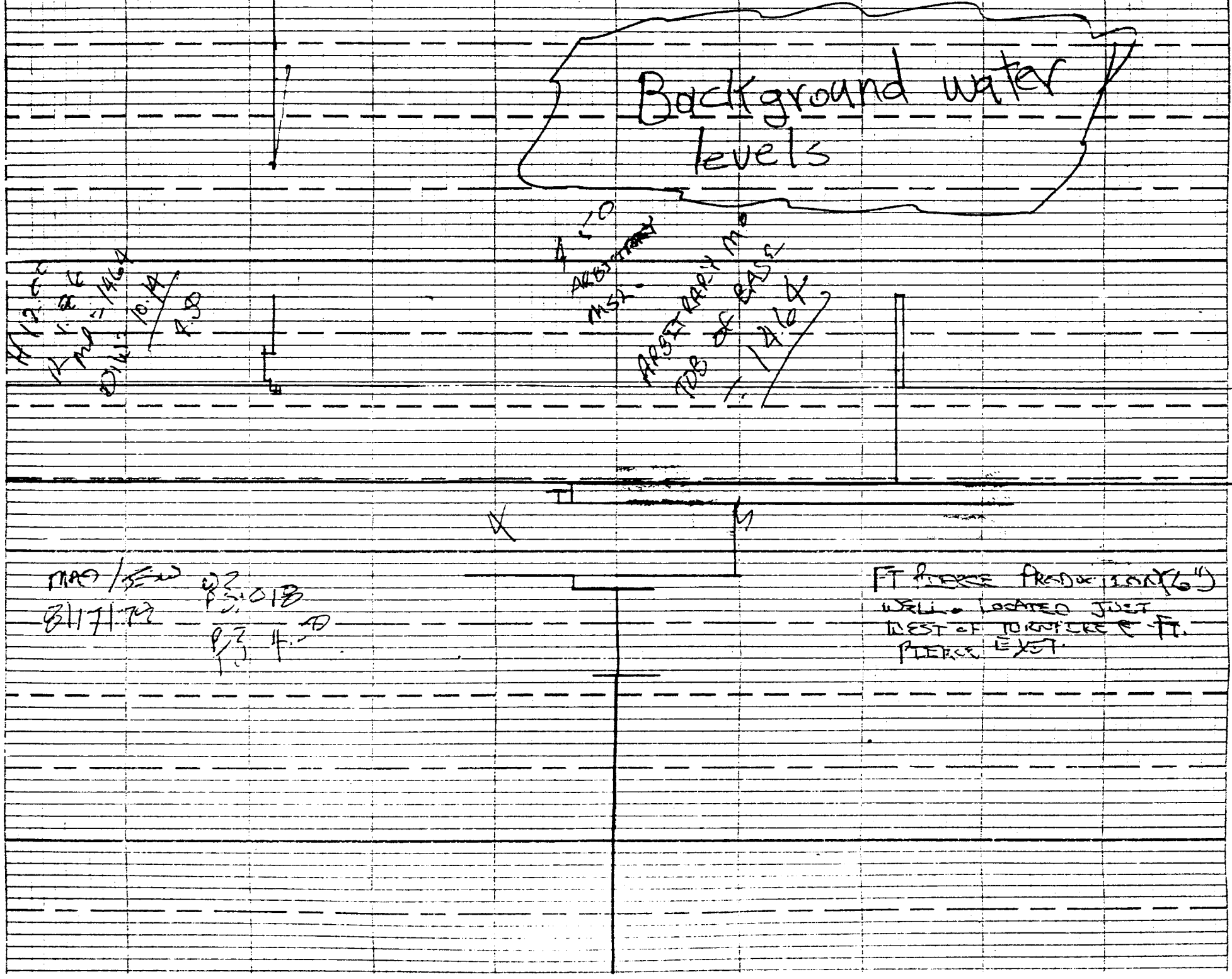
Background water levels

12.00  
1.00  
10.00  
10.00  
1.00

ASST. GRAY M.  
TDS OF BASE  
1.00

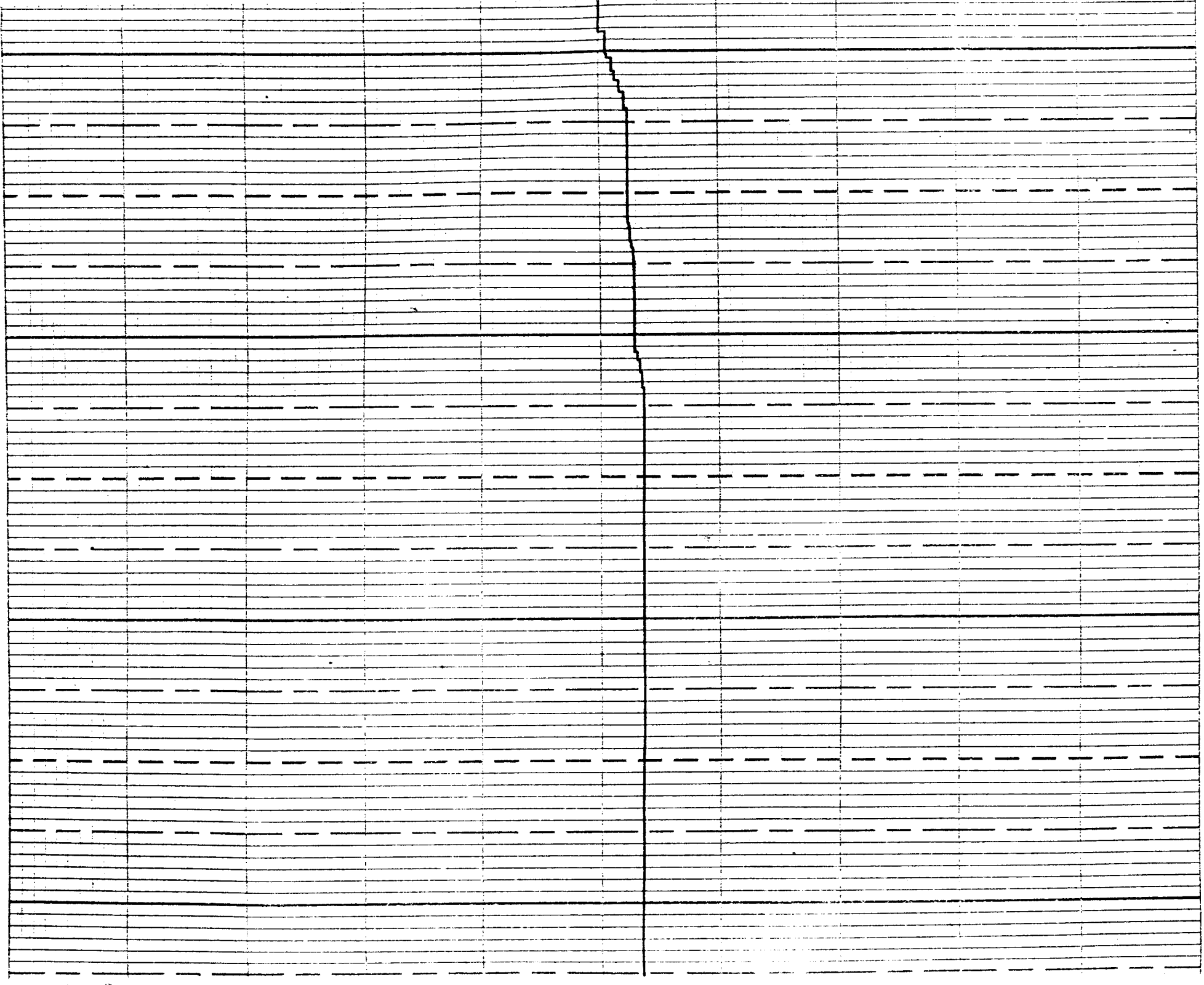
11.00  
11.00  
11.00  
11.00

FT PIERCE PRODUCTION (6")  
WELL LOCATED JUST  
WEST OF TURNPIKE & FT.  
PIERCE EXST.



8-22-79  
WT 1400

upset by 1/2  
lead  
Murt



FP 60W 8-24-79 WT-1510

15 min

17.5

12 min

9 min

5 min

4 min

3 min

2 min

held 16.00  
read 2.129  
ATW 13.871

held 2.00  
read 1.052  
ATW 10.948

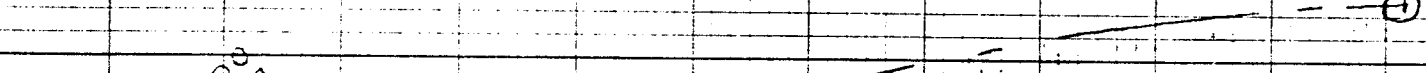
Well 60W

3

RWY/WAL 60W 8-25-79  
WT 0940

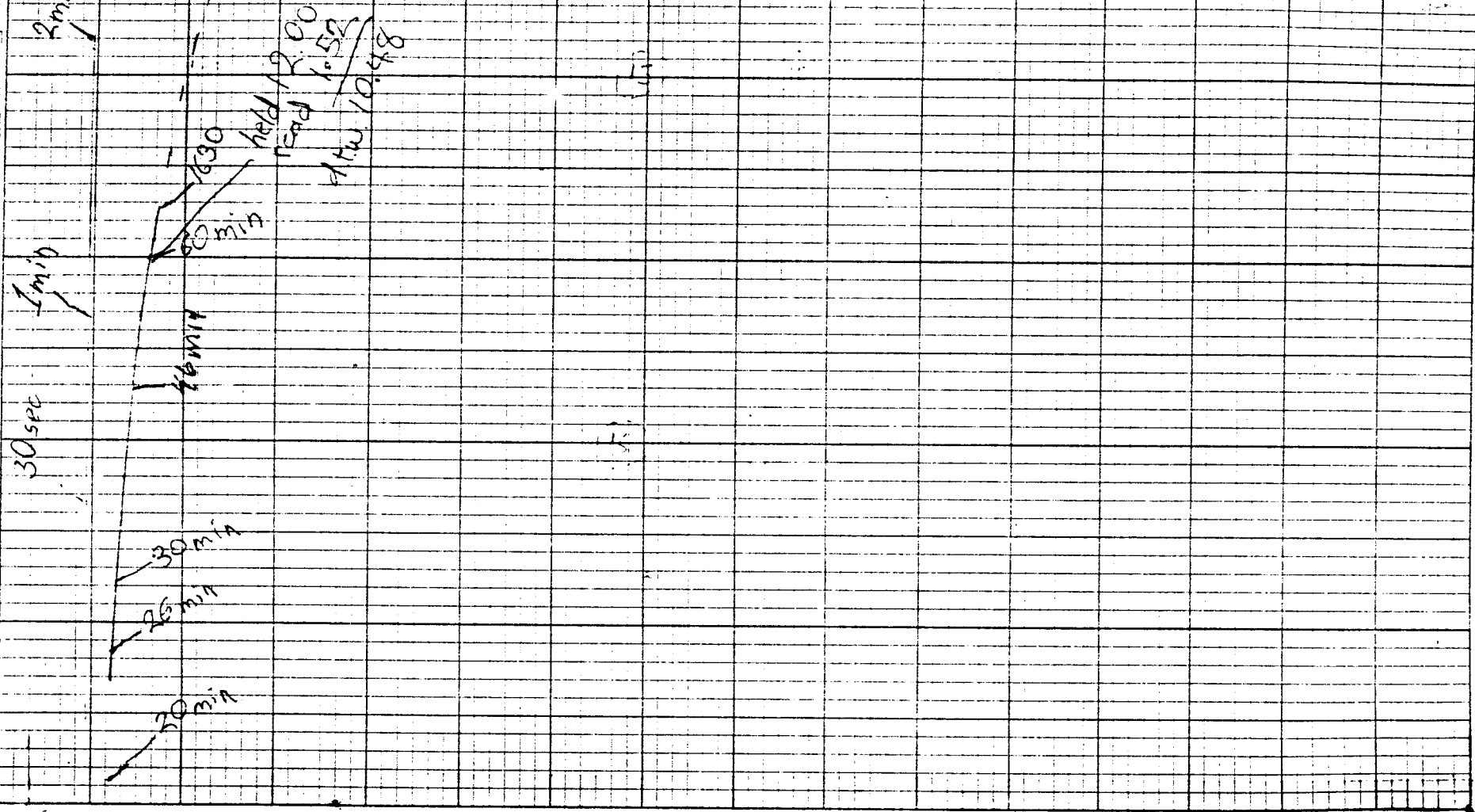
held 10.00  
read 1.05  
ATW 8.35

①



LDS-R (F-1)

RECORDING CHARTS



S. P. 8 11 10

WATER LEVEL RECORDER

Foot Point Sta

Location

Ft Pierce Pump Test @ SSP of SR 70

Party

L. J. [unclear]

Date

July, 1979

LINE	Station	Drill Depth	Csg Avg	Screen HI	Set Screen FS	Develop Avg	Standby Elev.	Remarks	REMARKS
1	Pump Well	115	73	70-110	1 hr	4 hrs		6 in well	
2									
3	<del>FP</del>	1150	438 <sup>00</sup>						
4									
5	FP-60W	123	80	70-110	1/2 hr	2 hrs	1 1/2 hrs	2 in	
6									
7	FP 200W	111	70	70-110	1/2 hr	3 hrs			
8									
9	FP -100s	117	75	72-112	1/2 hr	3 hrs			
10									
11	FP-300s	113	75	72-112	1/2	3 hrs			
12									
13									
14									
15									
16									
17									
18		2,320	900 <sup>00</sup>		300 <sup>00</sup>	1125 <sup>00</sup>	82.50		
19		1150 <sup>00</sup>	438 <sup>00</sup>	<del>75</del>	75 <sup>00</sup>				
20									
21									
22									
23									
24									
25									

Tot 6,393.50

Location

SSP &amp; SR70 on Candy Rd - Ft Pierce Exchange

Party

Long Wilcox

Date

8/25/79

LINE	Station	BS	HI Elev. Avg	HI	FS	Avg	Elev.	REMARKS
1								Start Lev. Datum 20ft top of
2		3.77	23.77				20.00	Conc R-W MK. Cur Fe pipe set inside cur of Inta Change @ FT Pierce
3								
4								
5	200				-5.28	② 5.28	18.49	Well FP 200 W
6						6.28		LS 17.5
7	60				-4.98	② 4.98	18.79	Well FP 60 W
8						6.11		LS 17.7
9	0				-3.68		20.09	Pumped Well FP-1 (NW cur cap)
10						6.07		LS 17.70
11	28.5				-3.80	② 3.80	19.97	Well FP 30 so
12						6.35		LS 17.4
13	28.5				-4.08		19.69	Shallow Well FP 30 so
14						6.0		LS 17.8
15	99.2				-4.87		18.90	Well FP 100s
16						6.44		LS 17.3
17	300				-5.84	② 5.837	17.93	Well FP 300 S
18						5.90		LS = 17.9
19								
20								
21			23.77		-3.77		20.00	Check back to start
22								
23								
24								
25								

after running levels, <sup>of test</sup>  
adjusted m.p. by addin  
a coupling to 305



# Discharge Measurements 3" orifice 6" pipe

Location Fort Pierce pumping test

Party — Wilcox, Long, Wendorf, Cook

Date 8-23-79 & 8-24-79

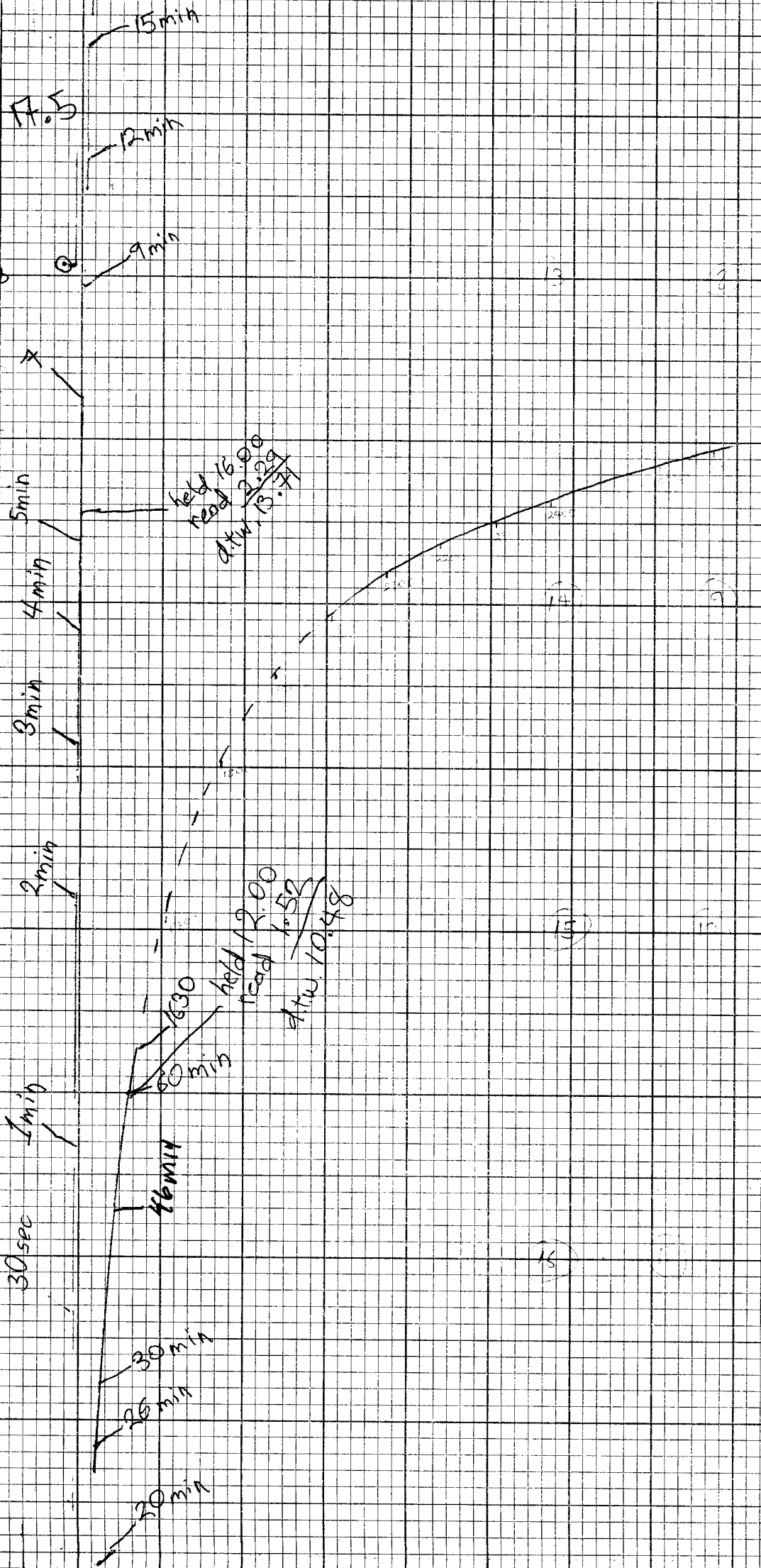
MC	time	head	discharge gpm	time	head	discharge	Rainfall	REMARKS
							.09	Just prior to test
2	1525	33 1/2	194	<sup>8/24/79</sup> 1005	22 1/2	158		
3	1531	31 1/2	188	1104	22 3/8	158		
4	1544	30	183	1205	22 3/8	158		
5	1557	28 7/8	180	1304	22 1/4	157		
6	1608	28	177	1405	22 1/4	157		
7	1634	26 1/2	173	1506	22 1/4	157		
8	1650	26	<del>171</del>	1517	22 1/4	157		
9	1724	25 1/8	168					
10	1800	25	167					weighted ave. Q = 163 gpm
11	1906	24 1/8	164					
12	1942	24	164					
13	2006	23 3/4	163					
14	2108	23 5/8	163					
15	2212	23 1/2	162					
16	2306	23 3/8	160					
17	0008	23 1/8	160					
18	141	22 7/8	160					
19	210	22 7/8	160					
20	308	22 3/4	160					
21	502	22 3/4	159					
22	355	22 1/4	159					
23	503	22 1/4	158					
24	0612	21 3/4	158					
25	0714	22 5/8	158					
			158					
	0912	22 1/2	158					



LD5-R (F-1) RECORDING CHARTS GRAPHIC CONTROLS CORPORATION BUFFALO, NEW YORK WT-1510 X 17.96 PRINTED IN U.S.A.

# Well 60W (3)

RAIN/WAL WT 0940  
60W 8-25-79  
held  
redd  
d.t.w.  
10.00  
1.05  
8.35

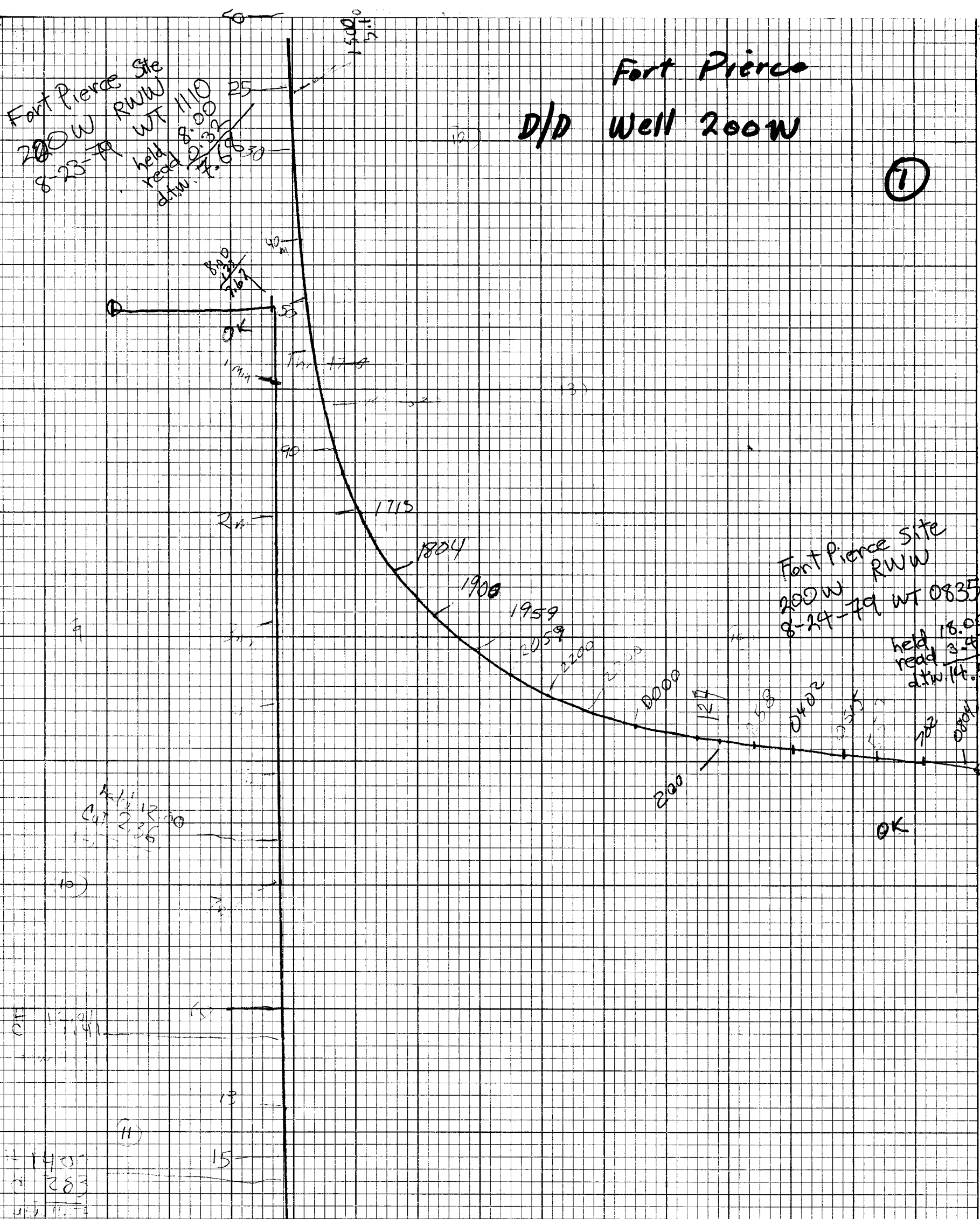


SSP 8 SF 10

WATER LEVEL RECORDER

Foot ...

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GRAPHIC CONTROLS CORPORATION  
BUFFALO, NEW YORK  
RECORDING CHARTS  
LD5-R (F-1)

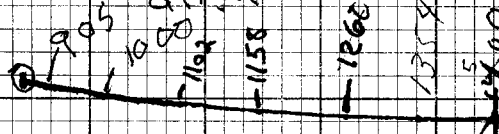


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RECORDING CHARTS GRAPHIC CONTROLS CORPORATION BUFFALO, NEW YORK  
LDS-X (P-1)

Fort Pierce Site  
200W RWW/JSW  
8-24-79 WT 0840

held 15.00  
read 0.46

14.54



19.41  
19.52  
00.82

RWW  
8-24-79  
WT 1512

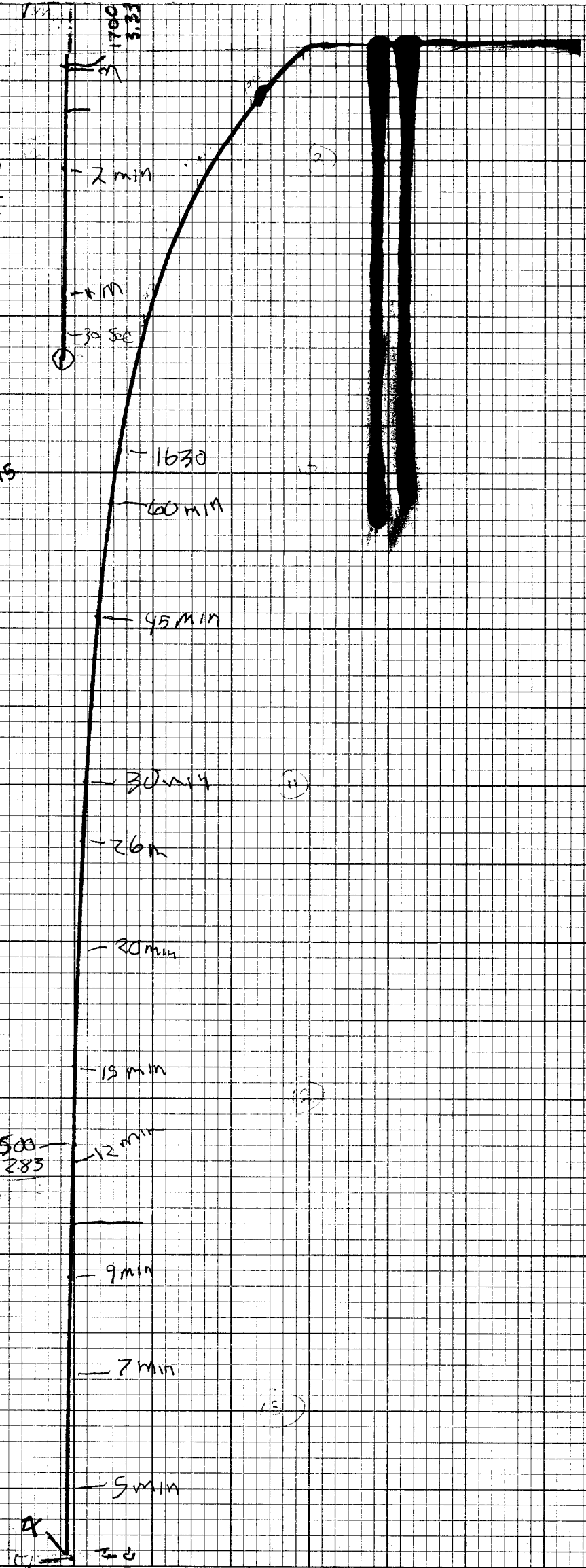
Fort Pierce Test  
D/D 200W

(2)

+0.07  
to all readings on chart  
RWW 8-24-79

Just this chart. Right?

PRINTED IN U.S.A.  
1463  
1465  
15  
500  
285  
LDS-R (F-1)



Fort Pierce  
R/D Well ~~200W~~

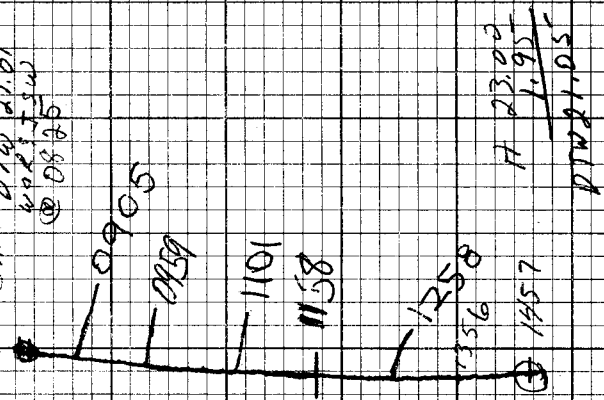
Fort Pierce Site  
pww/wal  
at 0930  
8-25-79  
held  
read  
a.k.w.  
71.94

Fort Pierce 71.94  
SSR 1 SR 70  
WATER LEVEL RECORDER



LDS-R (F-1) RECORDING CHARTS GRAPHIC CONTROLS CORPORATION BUFFALO, NEW YORK 8-29-79 PRINTED IN U.S.A.

# Fort Pierce Test (2) Well 30 South

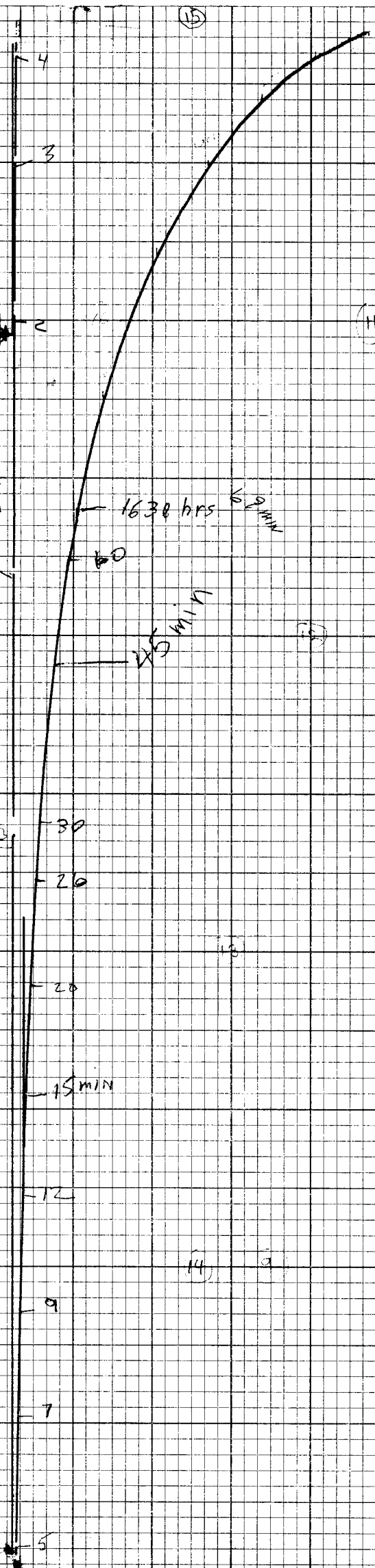




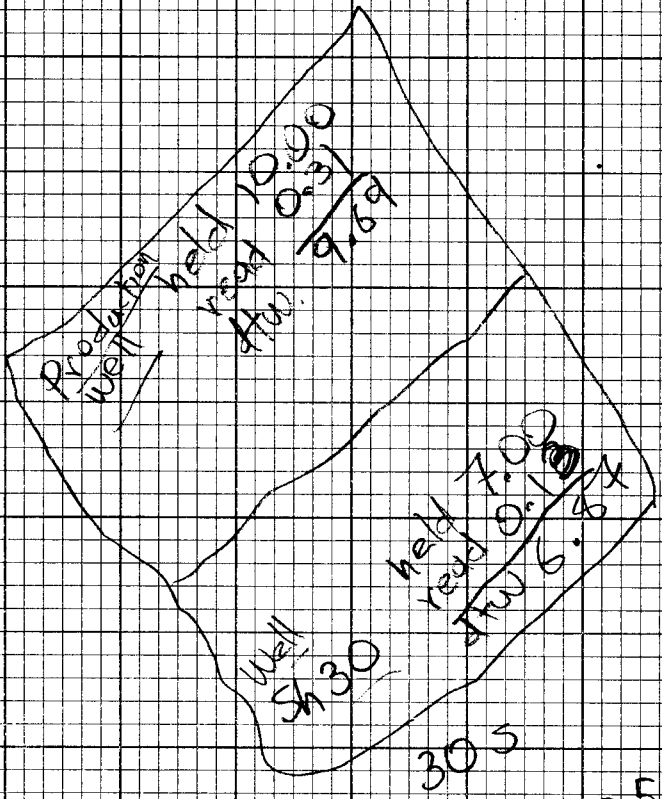
NEW YORK  
BUFFALO  
GRAPHIC CONTROLS CORPORATION  
RECORDING CHARTS  
LDS-R (F-1)

# Recovery 30 South

3



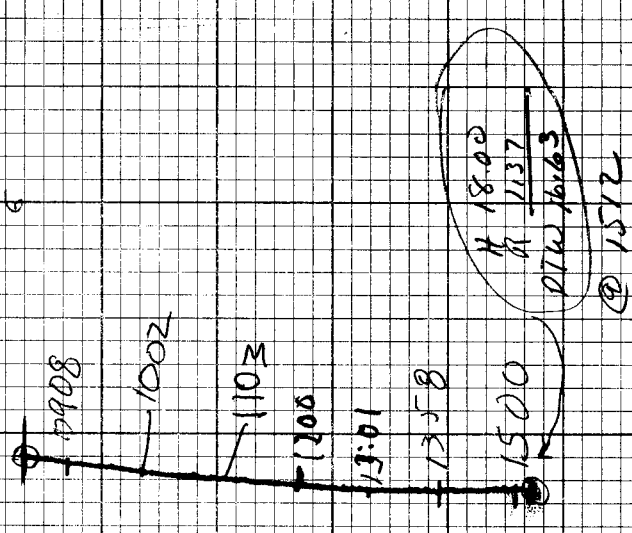
-0.02 correction applied for  
time from second tap  
RWL  
4.15 - 4.17



8-25-79  
wt 0950  
Max - RWL

held 10.00  
read 0.42  
flow 9.58





D/D

Fort Pierce Test Well 100 S

2

LUS-R (P-1)  
 RECORDING CHARTS  
 GRAPHIC CONTROLS CORPORATION  
 BUFFALO, NEW YORK  
 DTW 1663  
 1513 hrs.

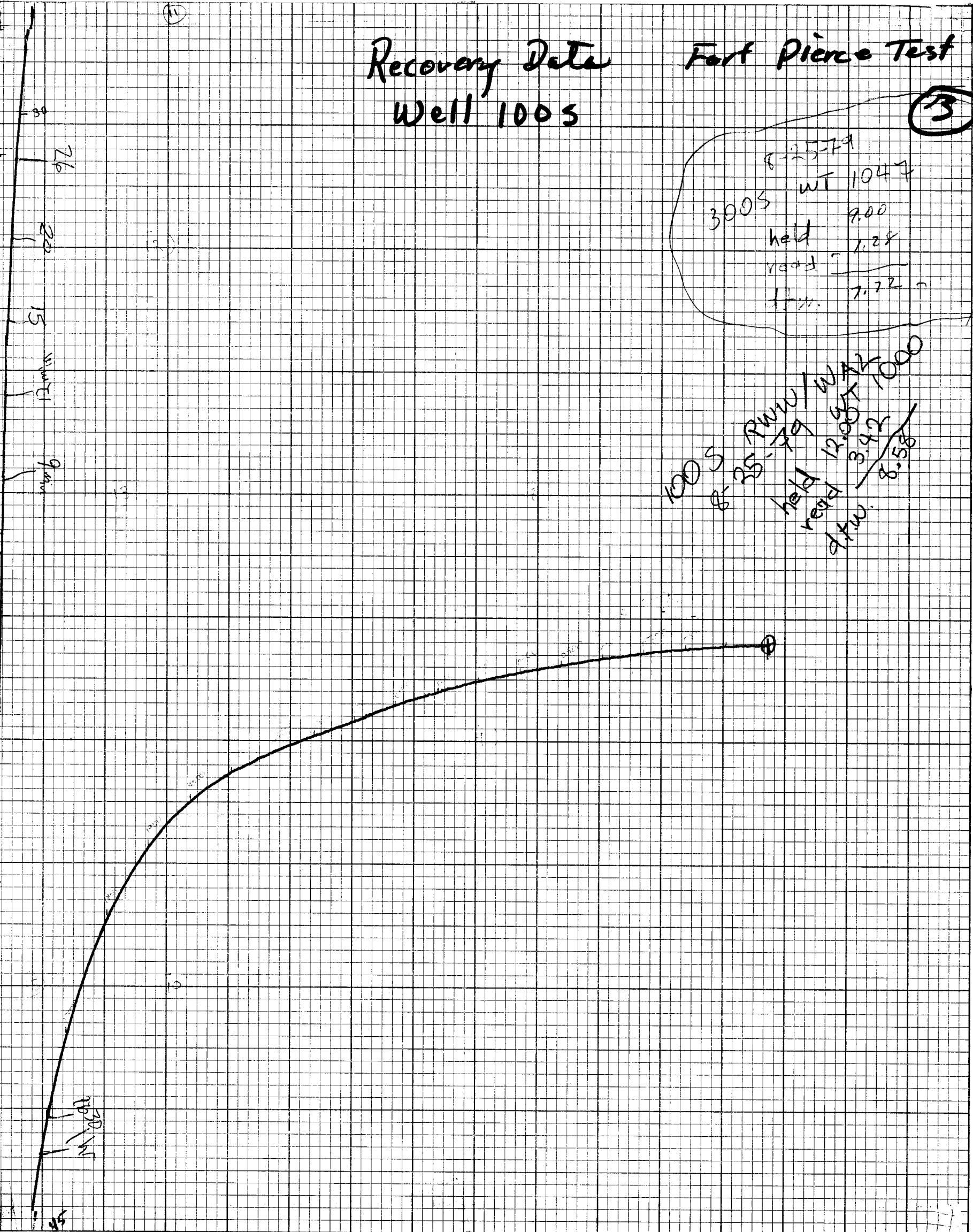
# Recovery Data Well 1005

# Fort Pierce Test

3

8-25-79  
 3005 WT 1047  
 held 9.00  
 read 1.28  
 H.W. 7.72

1005 PWU/WAZ  
 8-25-79  
 held 12.00  
 read 3.42  
 H.W. 8.58



SSP & SP70

WATER LEVEL RECORDER

Fort Pierce - Fla

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BUFFALO, NEW YORK

CHARLES CONCRETE CORPORATION

Ft. Pierce SITE

200 W

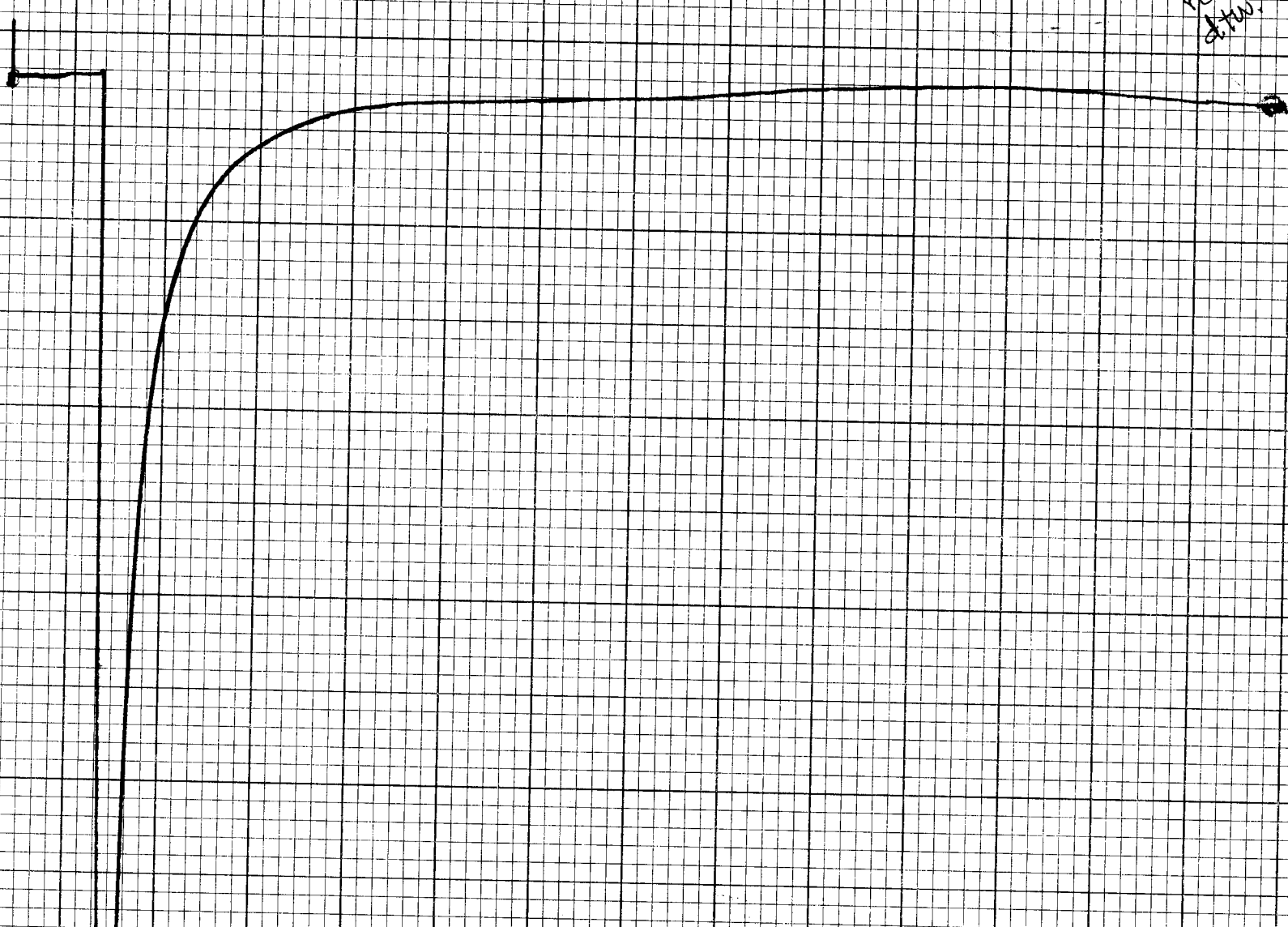
MAS 812/19  
WT 1425

H= 0.00  
R= 2.80

WT 7.62

Background  
water level  
200 W

200 W RW  
8-23-79  
height 5.00  
realt 0.33  
d.t.w. 7.57  
WT 1100



FT PIERCE SITE 1005  
 MAD 8/22/79  
 WFL 1505  
 H 10.00  
 R 1.7  
 DWL 8.29

scale?

Background  
 water level  
 well 1005

X.09

Fort Pierce Site  
 1005  
 8-23-79  
 WFL  
 H 9.00  
 R 0.57  
 DWL 8.43

X.09



9-194  
November 1949

UNITED STATES  
DEPARTMENT OF THE INTERIOR  
GEOLOGICAL SURVEY  
WATER RESOURCES DIVISION

Sh30

WATER LEVEL MEASUREMENTS (Field) Measured by Wilcox, Long, Wendorf  
Location of Project Fort Pierce Pumping test

DATE	HOUR	WELL NO.	TAPE READING AT—		DEPTH TO WATER	REMARKS
			Meas. point	Water level		
8-23-79	1445		8.00	3.69	4.31	
	1507		8.00	3.63	4.37	
	1514		9.00	4.62	4.37	
	1517	2 MIN	8.00	3.61	4.39	← total test
		3 MIN	8.00	3.61	4.39	1517
		14 MIN	8.00	3.59	4.41	
		30 MIN	6.00	1.56	4.44	
			7.00	2.52	4.48	
			7.50	3.01	4.49	
	1615	60 MIN	6.00	1.49	4.51	
	1630		5.00	.47	4.53	
	1646		5.00	.44	4.56	
	1703		6.00	1.44	4.56	
	1716		5.00	.41	4.59	
	1802		5.50	.84	4.66	
	1859		5.00	.66	4.74	
	2002		8.00	3.16	4.84	
	2103		14.00	9.06	4.94	* 2
	2204		6.00	.97	5.03	
	2302		10.00	0.90	5.10	
8-24-79	0004		6.00	.83	5.17	
	127		6.00	.73	5.27	
	204		6.00	.68	5.32	

Item 6

9-194  
November 1949

UNITED STATES  
DEPARTMENT OF THE INTERIOR  
GEOLOGICAL SURVEY  
WATER RESOURCES DIVISION

WATER LEVEL MEASUREMENTS (Field) Measured by \_\_\_\_\_  
Location of Project \_\_\_\_\_

DATE	HOUR	WELL NO.	TAPE READING AT—		DEPTH TO WATER	REMARKS
			Meas. point	Water level		
8/24/79	0302		6.00	.61	5.39	
	0400		6.00	.52	5.48	
	0510		6.00	0.16	5.54	
			6.00	.38	5.62	
	0707		6.00	0.32	5.68	
	0802		6.00	0.26	5.74	
	0906		6.00	0.18	5.82	
	1000		7.00	1.13	5.87	
	1101		7.00	1.08	5.92	
	1159		7.00	1.02	5.98	
	1259		7.00	0.97	6.03	
	1354		7.00	0.91	6.09	
	1500		7.00	0.85	6.15	
	1518		7.00	.84	6.16	
	1 MIN		7.00	.81	6.19	
	7'30"		7.00	.83	6.17	
	9'30"		7.00	.83	6.17	
	11 MIN		7.00	.83	6.17	
	2 DRAIN		7.00	.81	6.19	
	29 MIN		7.00	.79	6.21	
	45 MIN		9.00	2.79	6.21	
1627	65 MIN		7.00	.77	6.23	

UNITED STATES  
DEPARTMENT OF THE INTERIOR  
GEOLOGICAL SURVEY  
WATER RESOURCES DIVISION

300 S

Stat 1516 \*

WATER LEVEL MEASUREMENTS (Field)

Measured by

Location of Project

Fort Pierce (pumping test)

DATE	HOUR	WELL NO.	TAPE READING AT—		DEPTH TO WATER	REMARKS
			Meas. point	Water level		
8-23-79	1440		9.00	1.51	7.49	
	1518		9.00	1.28	7.72	
	1520		9.00	0.83	8.17	
	1522		12.00	3.43	8.57	
	1525		10.00	1.02	8.98	
	1535		10.00	0.29	9.71	
	1545		11.00	0.89	10.11	
	1600		11.00	0.49	10.51	
	1609		12.00	1.29	10.71	
	1636		12.00	0.91	11.09	
	1649		12.00	0.81	11.19	
	1725		12.00	0.55	11.45	
	1809		14.00	2.32	11.68	
	1908		13.00	1.14	11.86	
	1925		13.00	1.06	11.94	
	2008		13.00	1.05	11.95	
	2110		13.00	0.90	12.10	
	2222		13.00	0.84	12.16	
	2308		13.00	0.78	12.22	
8/24/79	0007		13.00	0.72	12.28	
	0141		13.00	0.67	12.33	
	0209		13.00	0.64	12.36	
	307		13.00	0.62	12.37	

Item 9

9-194  
November 1949

UNITED STATES  
DEPARTMENT OF THE INTERIOR  
GEOLOGICAL SURVEY  
WATER RESOURCES DIVISION

WATER LEVEL MEASUREMENTS (Field)

Measured by

Location of Project

DATE	HOUR	WELL NO.	TAPE READING AT—		DEPTH TO WATER	REMARKS
			Meas. point	Water level		
8/24/79	356		13.00	0.61	12.39	
	0520		13.00	0.54	12.46	
	0602		13.00	0.57	12.43	
	0711		13.00	0.54	12.46	
	0715		13.00	0.57	12.43	
	0910		13.00	0.49	12.51	
	1004		13.00	0.47	12.53	
	1104		13.00	0.45	12.55	
	1204		13.00	0.43	12.57	
	1303		13.00	0.42	12.58	
	1404		13.00	0.42	12.58	
	1504		13.00	0.41	12.59	
	1516		13.00	0.41	12.59	
	1 min		13.00	0.58	12.42	Pump off
	3 min		13.00	1.27	11.73	
	5 min		12.00	0.22	11.78	← ?
	10 min		12.00	0.63	11.37	
	16 min		12.00	1.06	10.94	
	22		12.00	1.36	10.64	
	27		12.00	1.57	10.43	
	48 min		11.00	1.07	9.93	
	65 min		11.00	1.40	9.60	
8-25-79	1047		9.00	1.28	7.72	



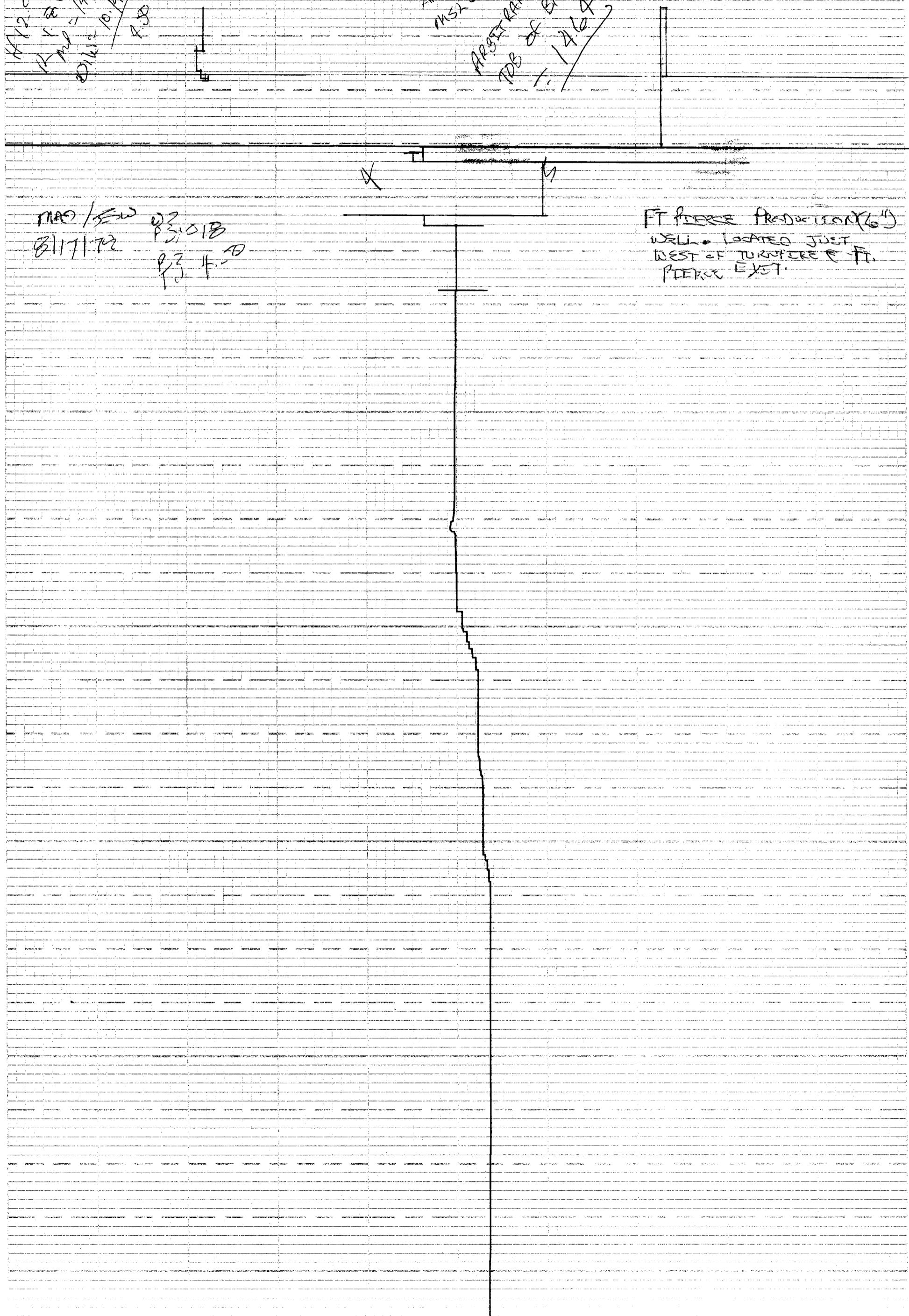
Background water levels

12.00  
1.86  
MP = 1464  
Dike 10.4  
7.30

4.10  
ARBITRARY  
MSL  
ARBITRARY MO  
TDS OF BASE  
1464

MAP / SW  
8/17/72  
P31018  
P34

FT PIERCE PRODUCTION (6")  
WELL LOCATED JUST  
WEST OF TURNPIKE & FT.  
PIERCE EXET.

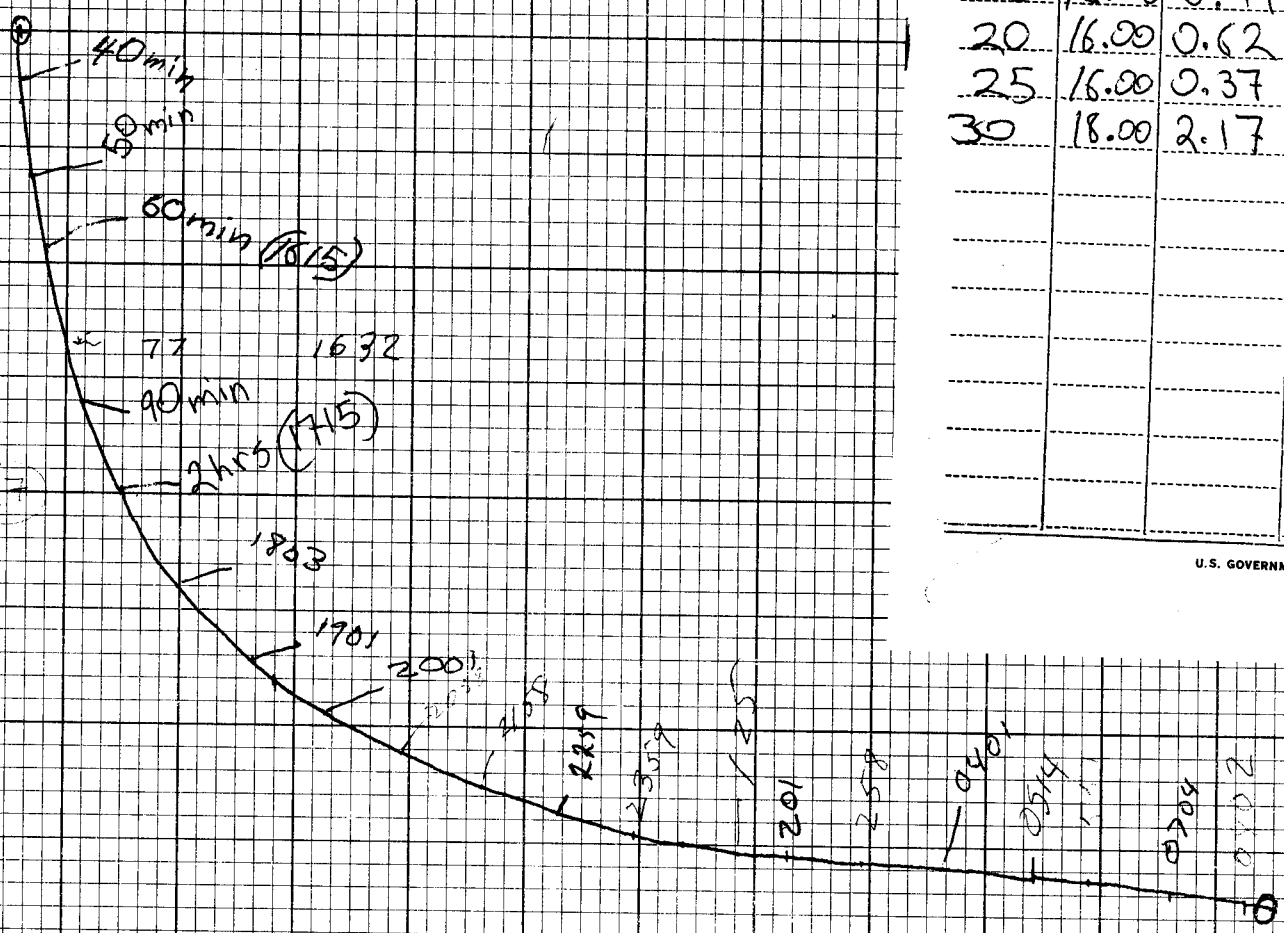


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 GRAPHIC CONTROLS CORPORATION  
 RECORDING CHARTS  
 LD5-R (F-1)

①

D/D  
 Well 60W

Fort Pierce  
 8-23-79 1553A



8-195  
 (July 1949)

UNITED STATES  
 DEPARTMENT OF THE INTERIOR  
 GEOLOGICAL SURVEY  
 WATER RESOURCES DIVISION

7-23-79

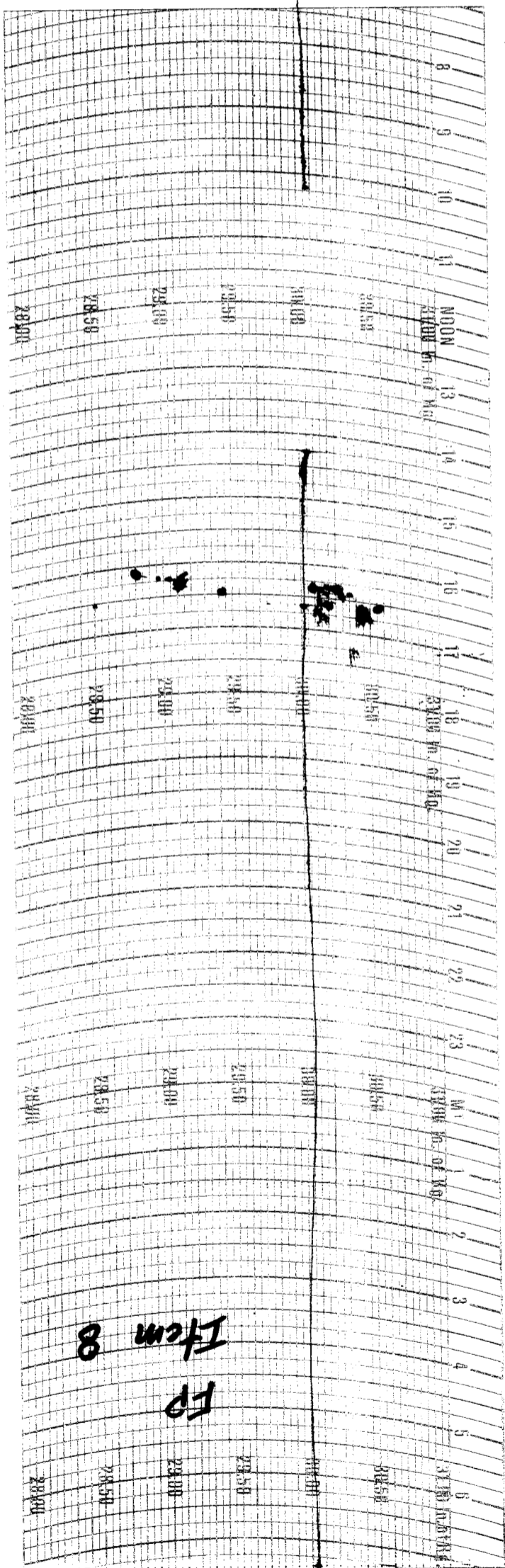
WATER LEVEL MEASUREMENTS (Office)  
 Well 60 S Field No. \_\_\_\_\_  
 Owner \_\_\_\_\_ Office No. \_\_\_\_\_  
 LOCATION Fort Pierce pumping test PROJECT \_\_\_\_\_  
 MEASURING POINT top of 2" coupling

ELEVATION OF MEASURING POINT \_\_\_\_\_

Time	Hour held	Depth read	Elevation d.t.w.	MEAS. BY	REMARKS (Nearby wells pumping, etc.)
3 min	18.00	5.60	12.40		malfunctioning.
4	15.00	1.69	13.31		Keck at beginning
5	14.00	0.40	13.60		of test, initial
7	15.00	0.95	14.05		d.t.w. prior to
10	15.00	0.60	14.40		start of test
13	16.00	1.17	14.83		8.08'
16	16.00	0.91	15.09		
20	16.00	0.62	15.38		
25	16.00	0.37	15.63		
30	18.00	2.17	15.83		

U.S. GOVERNMENT PRINTING OFFICE : 1963 O-688576  
 886-688

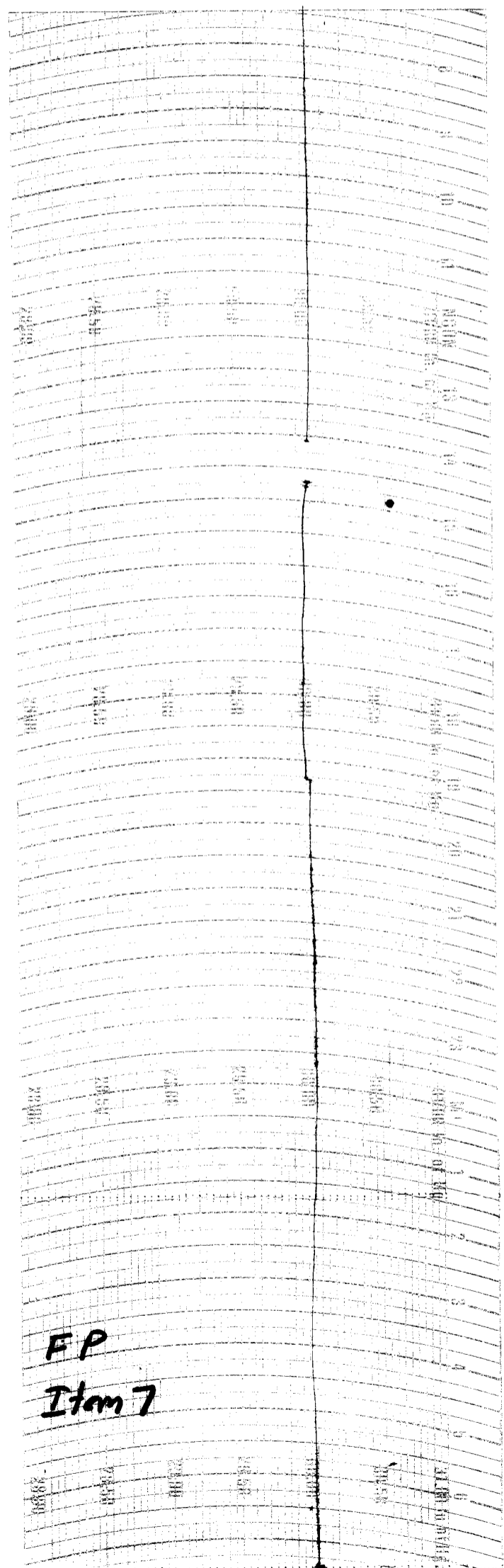
held 10  
 read 1.69  
 d.t.w. 13.31



WEATHER MEASURE CORPORATION P.O. BOX 41257 SACRAMENTO, CALIFORNIA 95841 TELEPHONE (916) 481-7585

BAROGRAPH C201-D-HG

STATION Fort Pierce DATE ON 8-24-79 DATE OFF 8-25-79  
 Remaining Test (1115) (1010)



WEATHER MEASURE CORPORATION P.O. BOX 41257 SACRAMENTO, CALIFORNIA 95841 TELEPHONE (916) 481-7585

BAROGRAPH C201-D-HG

STATION Fort Pierce DATE ON 8-23-79 DATE OFF 8-24-79  
 Remaining Test (1410) (1429)

Fort Pierce Test  
August 23-24, 1979

Comp. by GWH

Delayed Yield Solution PL 8, PP. 708

Well 200 W

Well 200  
r = 200 ft  
Q = 163

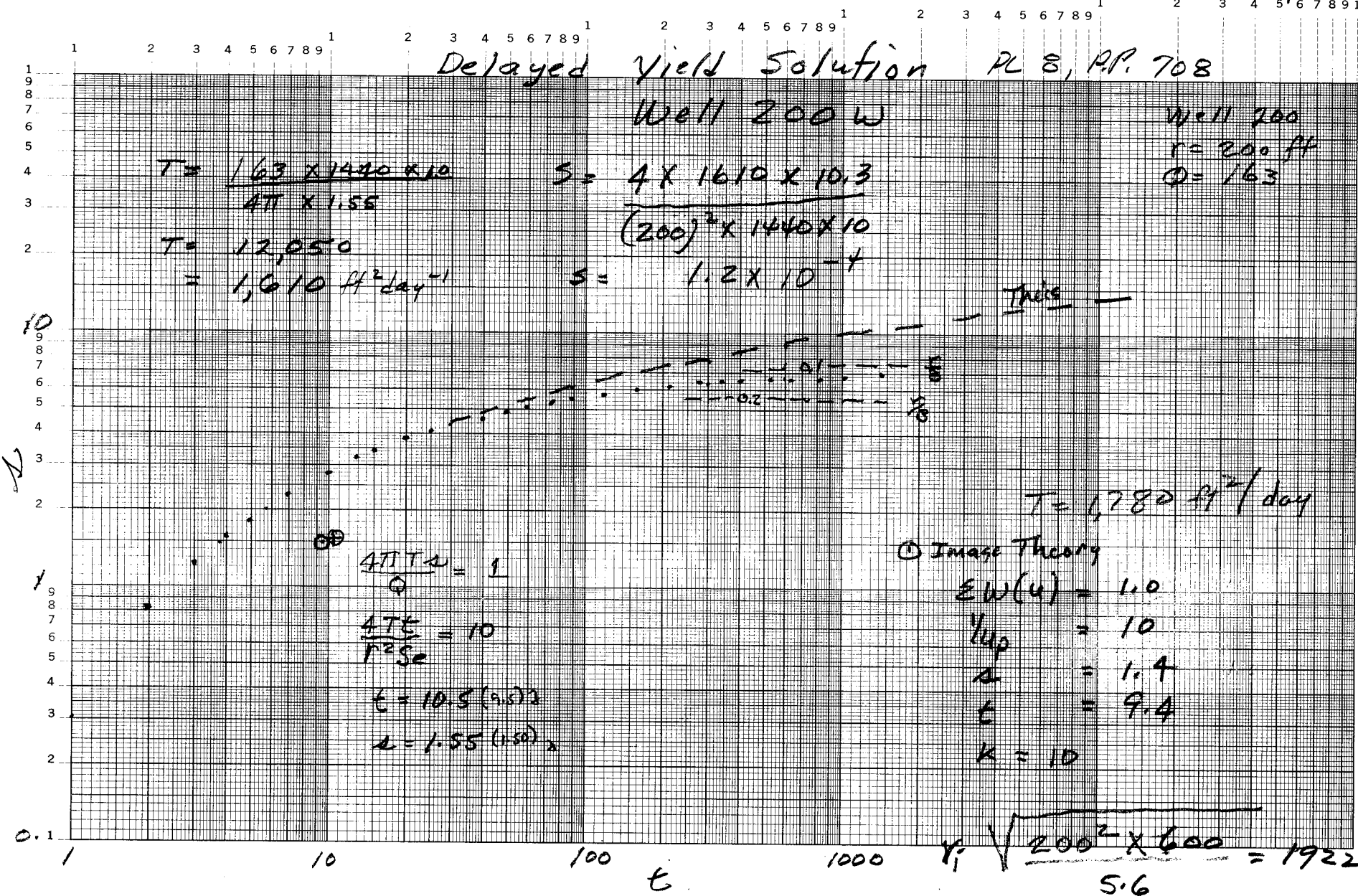
$$T = \frac{163 \times 1440 \times 10}{4\pi \times 1.55}$$

$$S = \frac{4 \times 1610 \times 10.3}{(200)^2 \times 1440 \times 10}$$

$$T = 12,050$$

$$S = 1.2 \times 10^{-4}$$

$$= 1,010 \text{ ft}^2 \text{ day}^{-1}$$



$$\frac{4\pi T Q}{Q} = 9$$

$$\frac{4\pi T Q}{r^2 S e} = 10$$

$$t = 10.5 (2.5)^2$$

$$\alpha = 1.55 (1.50)^2$$

Image Theory

$$EW(u) = 1.0$$

$$y/yp = 10$$

$$A = 1.4$$

$$C = 9.4$$

$$K = 10$$

$$y_1 = \sqrt{200^2 \times 600} = 1922$$

5.6



Fort Pierce Test  
August 23-24, 1979

Comp. by GWH

Delayed Yield Solution

$$T = \frac{163 \times 1440 \times 10}{477 \times 1.55}$$

$$= 12,050$$

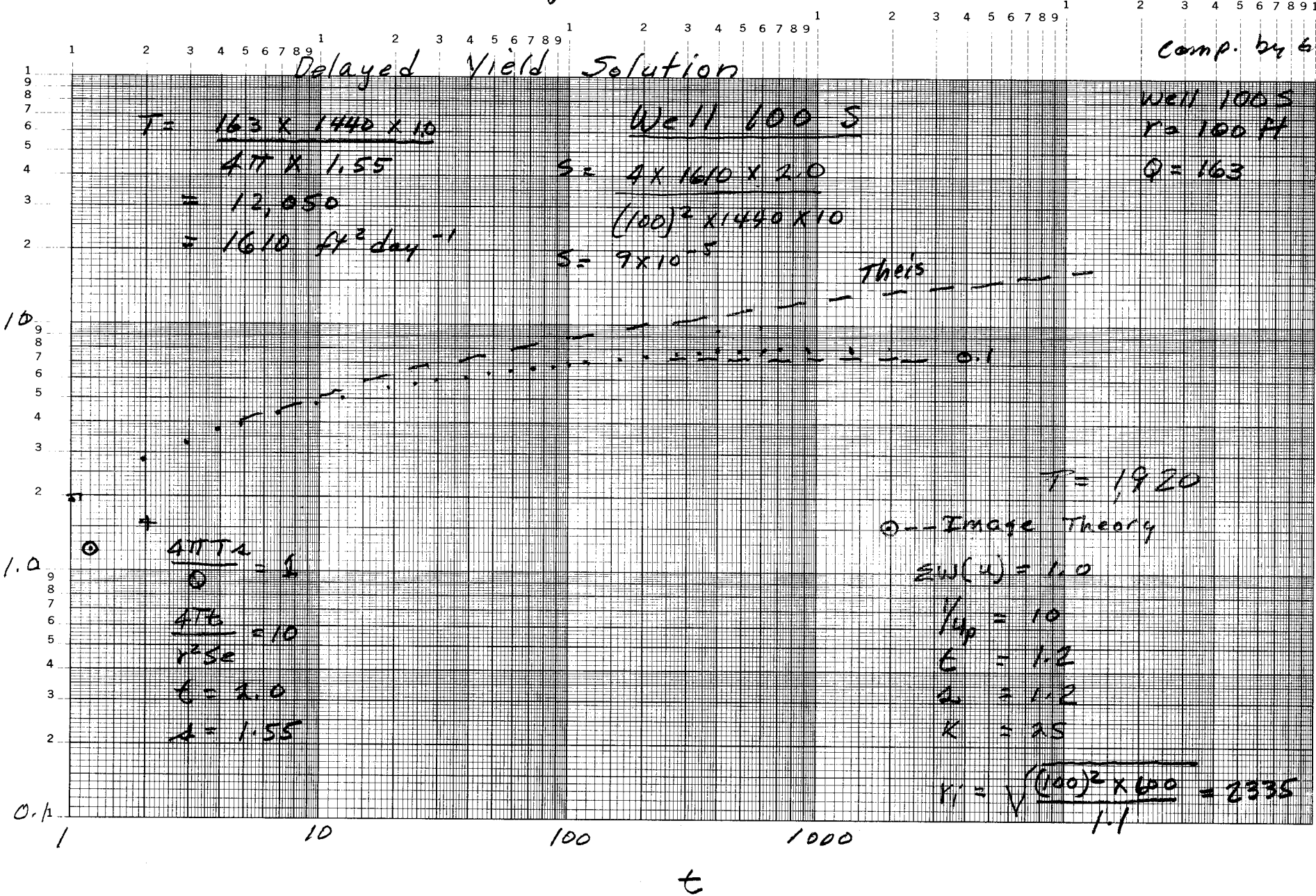
$$= 1610 \text{ ft}^2 \text{ day}^{-1}$$

Well 100 S

$$S = \frac{4 \times 1610 \times 2.0}{(100)^2 \times 1490 \times 10}$$

$$S = 9 \times 10^{-5}$$

Well 100 S  
r = 100 ft  
Q = 163



$$\frac{477T}{Q} = 1$$

$$\frac{477T}{r^2 S} = 10$$

$$t = 2.0$$

$$s = 1.55$$

T = 1920

Image Theory

$$EW(u) = 1.0$$

$$v_{up} = 10$$

$$E = 1.2$$

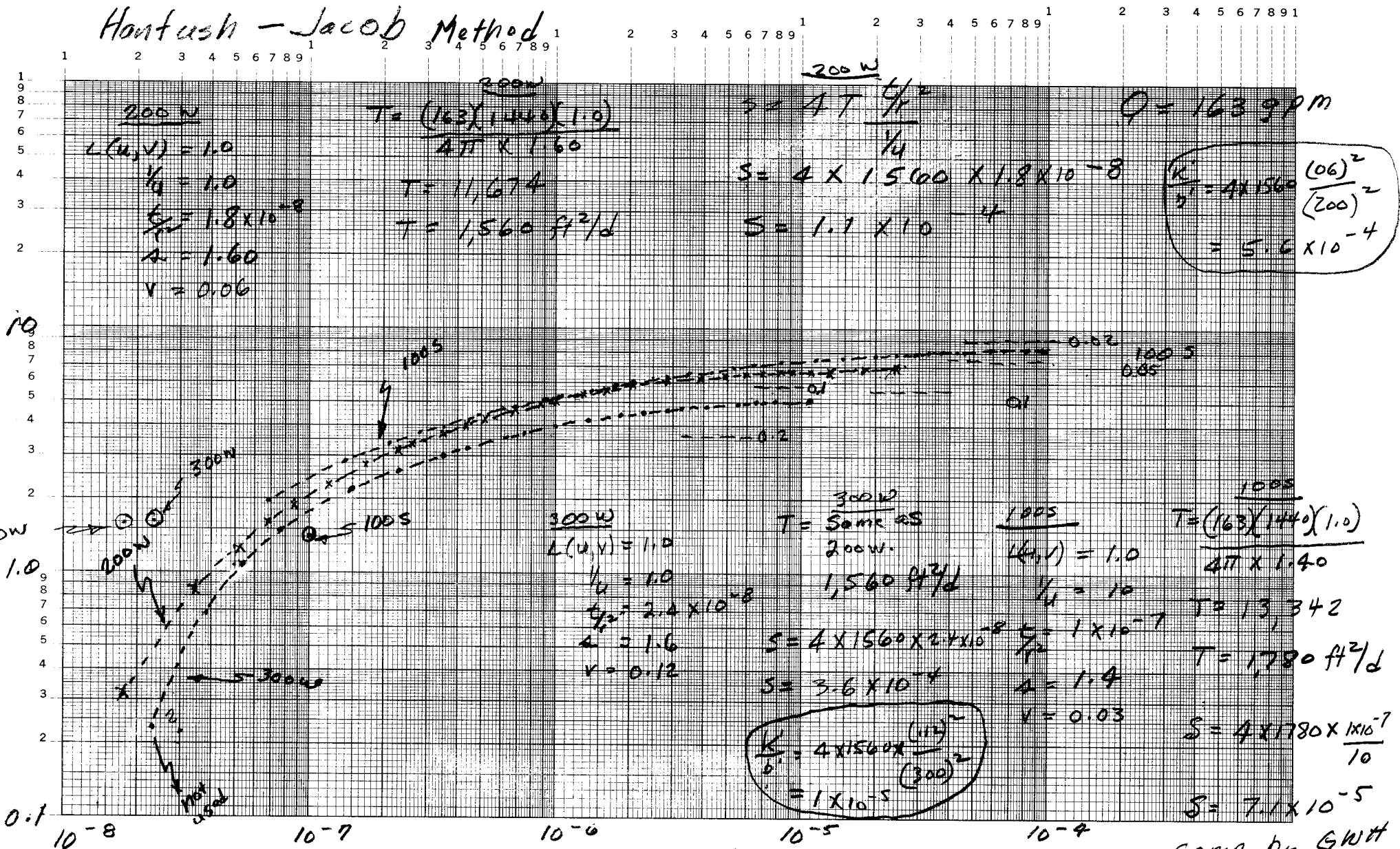
$$G = 1.2$$

$$K = 25$$

$$r_i = \sqrt{\frac{(100)^2 \times 100}{1.1}} = 2335$$

# Fort Pierce Test

## Hantush - Jacob Method



200 W  
 $L(u,v) = 1.0$   
 $\frac{t}{y^2} = 1.60$   
 $\frac{t}{y^2} = 1.8 \times 10^{-8}$   
 $A = 1.60$   
 $v = 0.06$

300 W  
 $T = \frac{(163)(144)(1.0)}{4\pi \times 1.60}$   
 $T = 11,674$   
 $T = 1,560 \text{ ft}^2/d$

200 W  
 $S = 4T \frac{t}{y^2}$   
 $S = 4 \times 1560 \times 1.8 \times 10^{-8}$   
 $S = 1.1 \times 10^{-4}$

$Q = 163 \text{ gpm}$   
 $\frac{K}{b^2} = 4 \times 1560 \frac{(06)^2}{(200)^2}$   
 $= 5.6 \times 10^{-4}$

300 W  
 $L(u,v) = 1.0$   
 $\frac{t}{y^2} = 1.0$   
 $\frac{t}{y^2} = 2.4 \times 10^{-8}$   
 $A = 1.6$   
 $v = 0.12$

300 W  
 $T = \text{Same as } 200 \text{ W.}$   
 $1,560 \text{ ft}^2/d$   
 $S = 4 \times 1560 \times 2.4 \times 10^{-8}$   
 $S = 3.6 \times 10^{-4}$

100 S  
 $L(u,v) = 1.0$   
 $\frac{t}{y^2} = 1.0$   
 $\frac{t}{y^2} = 1 \times 10^{-7}$   
 $A = 1.4$   
 $v = 0.03$

100 S  
 $T = \frac{(163)(144)(1.0)}{4\pi \times 1.40}$   
 $T = 13,342$   
 $T = 1,780 \text{ ft}^2/d$   
 $S = 4 \times 1780 \times \frac{1 \times 10^{-7}}{10}$   
 $S = 7.1 \times 10^{-5}$

$\frac{K}{b^2} = 4 \times 1560 \times \frac{(112)^2}{(300)^2}$   
 $= 1 \times 10^{-5}$

Comp. by GWHT

$\frac{t}{y^2}$

$\frac{K}{b^2} = 4 \times 1780 \times \frac{(03)^2}{(100)^2}$   
 $= 6.4 \times 10^{-4}$

Fort Pierce Test  
August 23-24, 1979

Superceded

Bounded Aquifer (Plate 9)

Obs. Wells 100 S & 200 W

Well 100 S

Well 200 W

$$\Delta \Sigma W(u) = 1.0 \quad T = \frac{163 \times 1.0}{4\pi \times 1.40}$$

$$\frac{1}{u} = 10 \quad t = 8.2 \quad S = 1.40$$

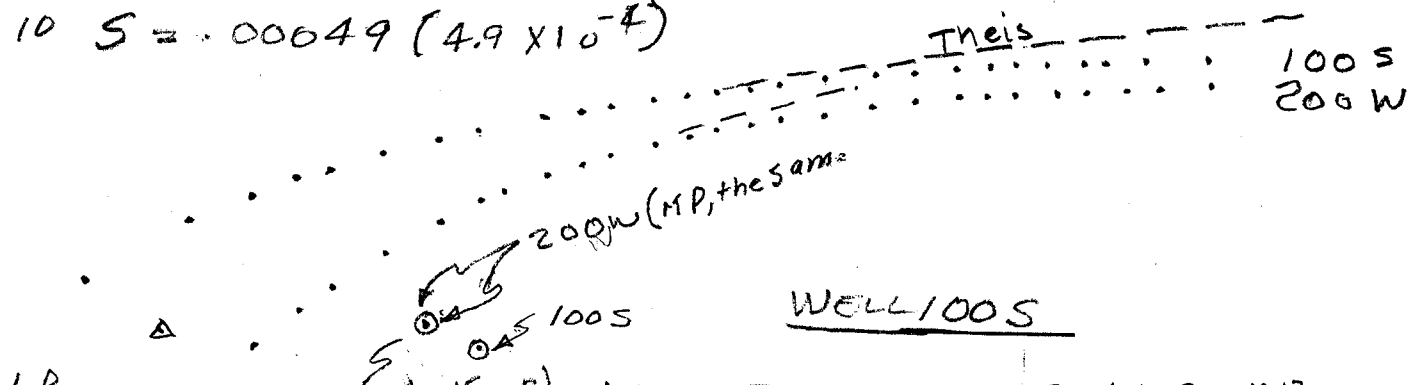
$$k = 20 \quad S = \frac{4 \times 2,153 \times 8.2}{100^2 \times 1440 \times 10}$$

$$\Delta \Sigma W(u) = 1.0 \quad T = \frac{163 \times 1.0}{4\pi \times 1.46}$$

$$\frac{1}{u} = 10 \quad t = 9.0 \quad S = 1.46$$

$$k = 10 \quad S = \frac{4 \times 1710 \times 9.0}{200^2 \times 1440 \times 10} \quad Q = 163$$

$$10 \quad S = .00049 (4.9 \times 10^{-4})$$



K 35  
K=10  
WELL 200 W

$$T = \frac{163 \times 1.0}{4\pi \times 1.46} = 12,790 = 1,710$$

$$S = \frac{4 \times 1710 \times 9.0}{40000 \times 1440 \times 10} = .000011 (1.1 \times 10^{-4})$$

1.0

$$H(u, \beta) = 1.0 \quad \frac{1}{u} = 10^2 \quad t = 13.0 \quad S = 1.27$$

$$t = 9.0 \quad S = 1.46$$

WELL 100 S

$$T = \frac{163 \times 1.0}{4\pi \times 1.27} = 14,710 = 1,970$$

$$S = \frac{4 \times 1970 \times 13.0}{10000 \times 1440 \times 10} = .00071 (7.1 \times 10^{-4})$$

0.1  $\odot$  Hantush modified

100                      1000  
t

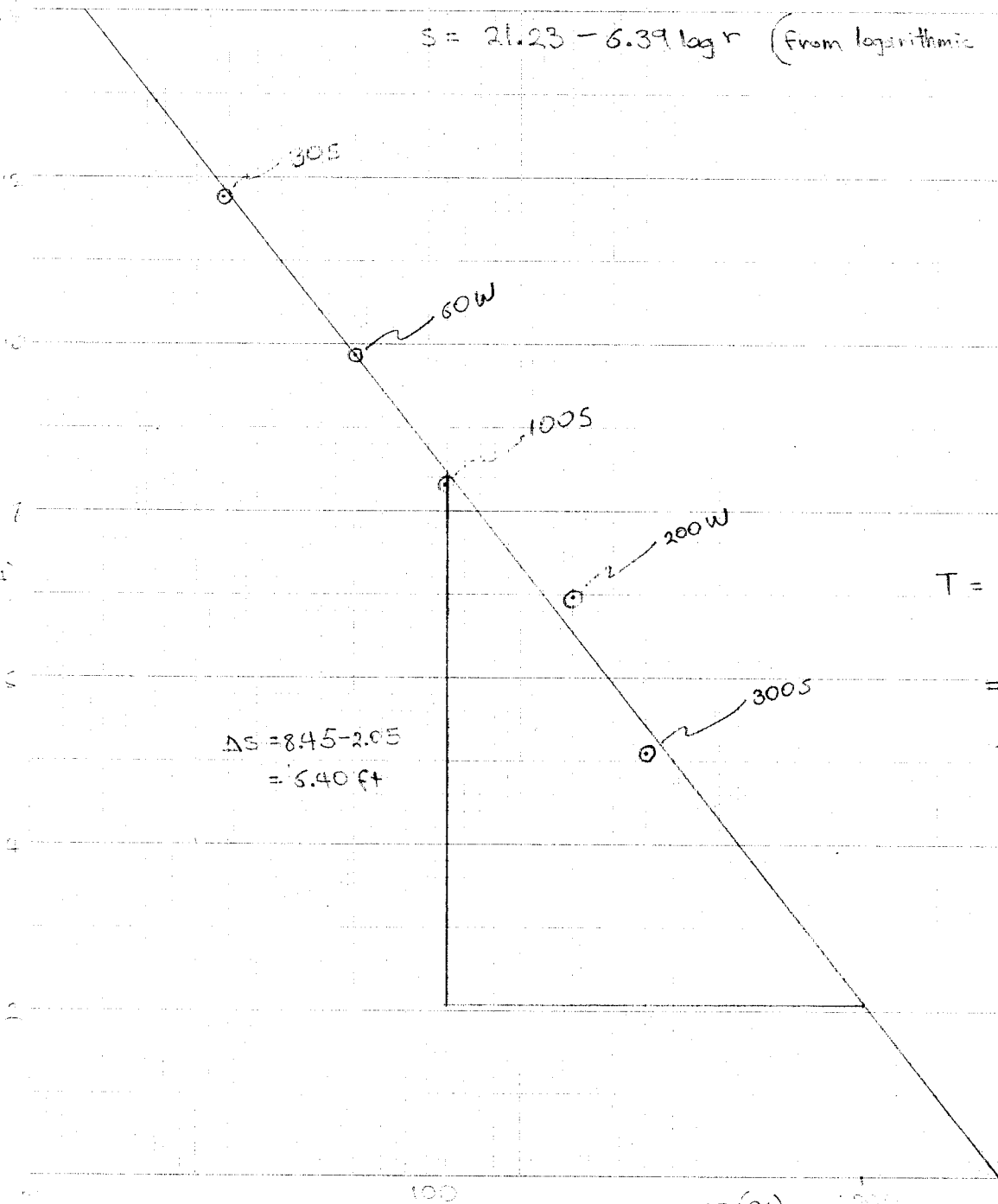
Comp by GWH



Forl Pierce Pumping test  
8-23-74-79

# THEIM METHOD

$$s = 21.23 - 6.39 \log r \quad (\text{from logarithmic regression of points, NP-77})$$



$$\Delta s = 8.45 - 2.05 = 6.40 \text{ ft}$$

$$T = \frac{2.30 Q}{2\pi \Delta s} = \frac{2.30 (163) \text{ gal/min} (1440) \text{ min/d}}{2\pi (6.40 \text{ ft})}$$

$$= 13,400 \text{ gal d}^{-1} \text{ ft}^{-1}$$

$$= 1,790 \text{ ft}^2 \text{ d}^{-1}$$

RWW  
7-21-77

30.00	***
11.77	***
60.00	***
9.88	***
99.00	***
8.32	***
200.00	***
6.97	***
300.00	***
5.10	***

coefficients

$r^2 =$	0.99	***
$a =$	21.23	***
$b =$	-2.78	***

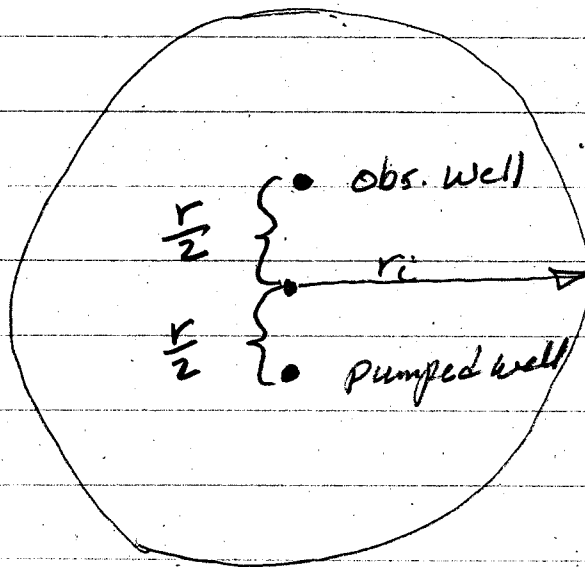
# Fort Pierce Aquifer Test

August 23-24, 1979

by: GWHill 1/6/80

## Estimation of Image well radius, PL 9

$r = 60$	$K = 25$	$r_i = 1500$	$r/2 = 30$	$\frac{r_i}{2} = 750$
$r = 100$	$K = 20$	$r_i = 2,000$	$r/2 = 50$	$\frac{r_i}{2} = 1000$
$r = 200$	$K = 10$	$r_i = 2000$	$r/2 = 100$	$\frac{r_i}{2} = 1000$
$r = 300$	$K = 7$	$r_i = 2100$	$r/2 = 150$	$\frac{r_i}{2} = 1,100$



This checks results of the Log-log Method shown in the test report on page 4.

Fort Pierce Test August 23-24, 1979  
 Computed by George Hill

Delayed Yield Solution PL 8; PP. 708

<u>Well No.</u>	<u>Transmissivity</u>	<u>S</u>
100 S	1,610 ft <sup>2</sup> /d	
200 W	1,610 ft <sup>2</sup> /d	1.2 x 10 <sup>-4</sup>
300 S	1,890 ft <sup>2</sup> /d	5.1 x 10 <sup>-4</sup> 9.0 x 10 <sup>-5</sup>

Hantush - Jacob PL 3; P.P. 708

USE

<u>Well No</u>	<u>Transmissivity</u>	<u>S</u>
100 S	1,780 ft <sup>2</sup> /d	7.1 x 10 <sup>-5</sup>
200 W	1,560 ft <sup>2</sup> /d	1.1 x 10 <sup>-4</sup>
300 S	1,560 ft <sup>2</sup> /d	3.6 x 10 <sup>-4</sup>

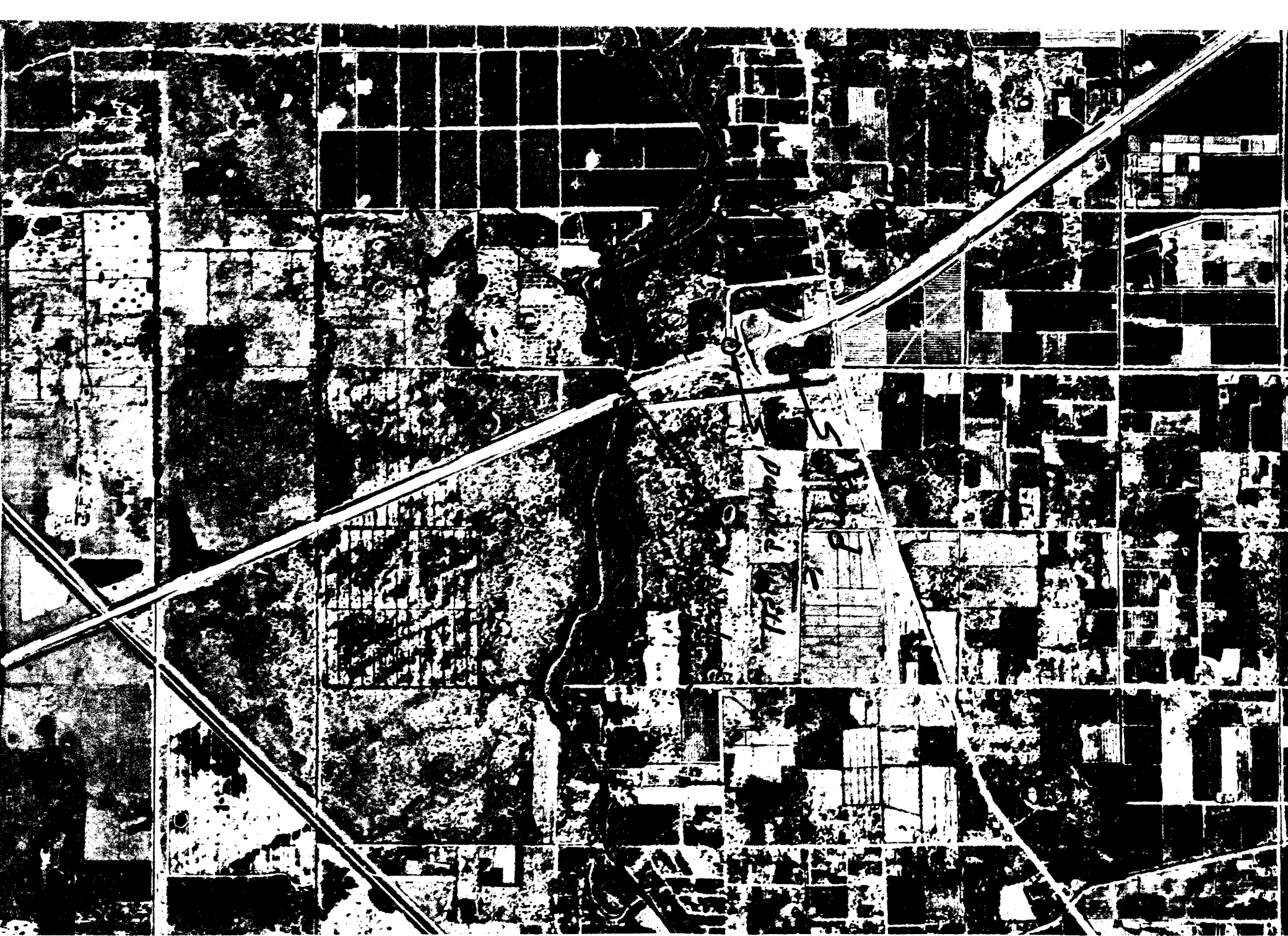
Thiem

$$T = 1,790 \text{ ft}^2/\text{d}$$

All in same well pack

Image Well Theory

<u>Well No.</u>	<u>Transmissivity</u>	<u>S</u>
60 W	1,650 ft <sup>2</sup> /d	4.2 x 10 <sup>-4</sup>
100 S	2,153 ft <sup>2</sup> /d	4.9 x 10 <sup>-4</sup>
200 W	1,710 ft <sup>2</sup> /d	1.1 x 10 <sup>-4</sup>
300 S	1,920 ft <sup>2</sup> /d	1.3 x 10 <sup>-4</sup>



Fort Pierce Interchange Aquifer Test

