

GEOTECHNICAL ENGINEERING REPORT G-6A PUMP STATION WEST PALM BEACH, FLORIDA

UES PROJECT NO. 0630.2000012 UES REPORT NO. 17223

#### **Prepared For:**

South Florida Water Management District 3301 Gun Club Road West Palm Beach, FL 33406 Attn.: Ms. Holly Jarvinen

#### **Prepared By:**

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June 26, 2020

South Florida Water Management District 3301 Gun Club Road West Palm Beach, FL 33406

Attention: Ms. Holly Jarvinen

Reference: Draft Geotechnical Engineering Report G-6A Pump Station West Palm Beach, Palm Beach County, FL UES Project No. 0630.2000012; UES Report No. 17223

Dear Ms. Jarvinen:

Universal Engineering Sciences (UES) has completed geotechnical services for the abovereferenced project in general accordance with Work Order Revision No. 4600003736-WO03R2 dated June 8, 2020. These services were performed in accordance with generally accepted soil and foundation engineering practices, no other warranty, expressed or implied, is made.

This report contains the results of the subsurface exploration, an engineering interpretation of the results with respect to the project characteristics as described, and recommendations for foundation design.

We appreciate the opportunity to work with you on this project and look forward to a continued association. If you have any questions please contact the undersigned.

Respectfully submitted, UNIVERSAL ENGINEERING SCIENCES Certificate of Authorization No. 549

Allan G. Abubakar, PE Project Engineer Peter G. Read, PE Southeast Regional Vice President Florida Professional Engineer No. PE-35604

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### **1.0 INTRODUCTION**

#### 1.1 GENERAL

This report contains the results of a geotechnical exploration conducted for the proposed pump station in West Palm Beach, Palm Beach County, Florida. A Site Location Map is included as Page A-1 in Appendix A. This report includes the following sections:

- SCOPE OF SERVICES Defines what services were completed
- FINDINGS Describes what was encountered
- RECOMMENDATIONS Describes what we encourage you to do
- LIMITATIONS Describes the restrictions inherent in this report
- SUMMARY Reviews the material in this report
- APPENDICES Presents support materials referenced in this report.

#### **1.2 PROJECT DESCRIPTION**

Our understanding of the proposed construction is based on review of a site plan provided by South Florida Water Management District (SFWMD) that was referenced for our subsurface exploration and geotechnical engineering report.

The project consists of design and construction of 1,100 CFS pump station at about 800 feet west from the existing S-6 pump station, bridge, and stilling well. The new pump station will be located within the West Palm Beach Field Station Area. The project is located at the intersection of L-15 Canal and STA-2 Inflow Canal I, about 20 miles southeast of the Town of Belle Glade in Palm Beach County. A Site Location Map is included as Page A-1 in Appendix A.

The recommendations contained herein are based upon the above considerations. If any of this information is incorrect or if you anticipate any changes, UES should be notified immediately to review and possibly amend the recommendations contained in this report.

#### 2.0 SCOPE OF SERVICES

#### 2.1 PURPOSE

The purposes of this geotechnical exploration were:

- to explore and evaluate the subsurface conditions at the site by advancing SPT (Standard Penetration Test) soil borings with special attention to potential geotechnical considerations that may affect the proposed design, construction, and serviceability of the proposed improvements; and
- to provide geotechnical engineering recommendations for groundwater considerations, and foundation design.



This report presents an evaluation of site conditions on the basis of traditional geotechnical procedures for site characterization. The recovered samples were not examined, either visually or analytically, for chemical composition or environmental hazards. UES would be pleased to perform these services, if you desire.

#### 2.2 FIELD EXPLORATION

The subsurface conditions at the site were explored with a total of fifteen (15) Standard Penetration Test (SPT) borings designated B-1 through B-11, B-11A, and B-12 through B-14, drilled to depths of 30 to 100 feet. Borings B-1 and B-2 were drilled close to the center of canal. Borings B-3 through B-14 were drilled at the top of banks, and B-14 was drilled near the canal bank. The approximate locations of the soil borings are presented in Appendix B, Report of SPT Borings and Boring Location Plan.

The SPT borings were advanced to their respective depths using the rotary wash method; samples were collected while performing the SPT at regular intervals. We completed the SPT in general accordance with ASTM D-1586 guidelines, with continuous sampling to its full depth. The SPT test consists of driving a standard split-barrel sampler (split-spoon) into the subsurface using a 140-pound hammer free-falling 30 inches. The number of hammer blows required to drive the sampler 12 inches, after first seating it 6 inches, is designated the penetration resistance, or SPT-N value. This value is used as an index to soil strength and consistency.

Ten (10) 5-foot rock corings were performed at borings B-3 through B-6, B-9 through B-12, and B-11A. Rock cores were placed in a box and transported to our laboratory for inspection and testing. Soil samples collected during the SPT were placed in clean sample containers and transported to our laboratory where they were visually classified by a member of our geotechnical engineering staff in accordance with ASTM D-2488. These soil samples will be held in our laboratory for your inspection for 90 days, after which time they will be discarded unless we are otherwise notified.

#### 2.3 LABORATORY TESTING

The soil samples recovered from the split-barrel sampler were classified in general accordance with ASTM D 2488. Representative soil samples were then selected from the retained soils and tested in our laboratory for sample specific classification in general accordance with the guidelines of ASTM D 2487 Standard Classification of Soils for Engineering Purposes (Unified Soil Classification System). The samples will be retained for a period of six months from date of completion of field work. All laboratory data is summarized and report sheets included in Appendix B. The following is a summary of the laboratory tests performed for this study:

- Twenty-seven (27) Moisture Content Tests ASTM D 2216 (Standard Test Methods for Laboratory Determination of Water (Moisture) Content of Soil and Rock by Mass.
- Thirteen (13) Organic Content Tests ASTM D 2974 (Standard Test Methods for Moisture, Ash, and Organic Matter of Peat and other Organic Soils.



- Twenty (20) Grain Size Distribution ASTM C 136 (Standard Test Method for Sieve Analysis of Fine and Coarse Aggregates.
- Fourteen (14) Wash #200 Fines Content Determinations ASTM D 1140 (Standard Test Methods for Amount of Material in Soils Finer than No. 200 Sieve).
- Two (2) Corrosion Series Tests FM 5-550 Florida Method of Test for Determining pH of Soil and Water, FM 5-553 – Florida Method of Test for Determining Sulfate of Soil and Water, FM 5-552 – Florida Method of Test for Determining Chloride of Soil and Water, and FM 5-551 – Florida Method of Test for Determining Resistivity of Soil and Water
- Four (4) Unconfined Compressive Strength of Intact Rock Core Specimens ASTM D 2938 – 95
- ▶ Four (4) Split Tensile Strength of Intact Rock Core Specimens ASTM D 3967 08

#### 3.0 FINDINGS

#### 3.1 SURFACE CONDITIONS

The site lies on two dirt roads with an existing canal in between. Ground surface elevations of the soil borings ranged from +13.01 feet to 26.38 feet NAVD 88. Ground surface elevation of each boring is shown on the attached boring logs in Appendix B. Site photos are included in Appendix B. U.S.G.S topographic quadrangle maps and the USDA Soil Conservation Service Soil Survey of Palm Beach County were reviewed for relevant information about the site. Review of the Palm Beach County Soils Survey, indicates the site is mapped within Terra Ceia muck, drained, frequently ponded, 0 to 1 percent slopes and Water-Udorthents complex, 0 to 35 percent slopes.

Terra Ceia muck is a nearly level, very poorly drained, deep, organic soil. This soil is in broad, freshwater marsh areas. It formed in thick deposits of hydrophytic plant remains. It has the pedon described as representative of the series. Under natural conditions, this soil is covered by water, or the water table is within 10 inches of the surface for 6 to 12 months in most years, except during extended dry periods.

#### 3.2 SUBSURFACE CONDITIONS

The results of our field exploration and laboratory analysis, together with pertinent information obtained from the SPT borings, such as soil profiles, penetration resistance and groundwater levels are shown on the boring logs included in Appendix B. The Key to Boring Logs is also included in Appendix B. The stratification lines shown on the boring logs represent the approximate boundaries between soil types, and may not depict exact subsurface soil conditions. The actual soil boundaries may be more transitional than depicted. A generalized profile of the soils found at our boring locations is presented in Table 1. The soil profile was prepared from field logs after the recovered soil samples were visually classified by a member of our geotechnical staff.



	TABLE 1: GENERAL SOIL PROFILE					
Typical Depth (feet)	Soil Description					
0 – 12 Loose to very dense limerock (FILL), very loose muck/peat, loose to very dense limestone, silty limestone [SP, PT, GP]						
12 – 53	12 – 53 Very loose to very dense, limestone, silty sand with limestone, sand wit silt and limestone, silty sand [GP, SM, SP-SM, SM]					
53 – 100* Loose to very dense, sand with shell fragments [SP]						
* Deepest Boring Te	rmination depth					

Groundwater was measured at depths ranging from 4 to 12.5 feet below the existing land surface in the test borings. The difference in groundwater levels can most likely be attributed to the difference in ground surface elevations and groundwater levels at this site may also reflect the surface water level in the nearby L-15 and STA-2 Inflow Canals.

A notable feature found within the generalized subsurface soil profile is the presence of pockets of muck and peat layers found in the range of 2 to 20 feet below land surface (bls) in the test borings.

Thirteen (13) soil samples were tested for organic and moisture content. The test results indicate moisture content of 25 to 188 percent, and organic content of 20.6 to 84 percent. Note that soils with an organic content equal to or greater than 10 percent are typically considered unsuitable for foundation support. Organic soils encountered in structural areas should be removed and replaced with good quality fill according to the specifications and procedures outlined in the Site Preparation section of this report.

#### 3.3 SOIL CORROSION CHARACTERISTICS

UES performed pH, resistivity, sulfates and chloride tests for evaluation of corrosion potential of soils at borings B-11 and B-12 from 0 to feet of composite soil samples and boring B-1 from 0 to 14 feet of composite soil samples. According to the guidelines of the Florida Department of Transportation (FDOT) "Florida-Concrete Design, Environmental Classification and Construction Criteria" (based on the three tier scale of slightly, moderately, and extremely aggressive) the results of the pH, sulfate, chloride, and resistivity tests indicate that the sandy soils in the building area are "slight to moderate aggressive" to steel and concrete. Therefore, UES does not recommend special cement in concrete or special design or construction for below grade improvements. The results of these tests are listed on the Report of Corrosion Parameters sheet enclosed in Appendix B.



#### 4.0 RECOMMENDATIONS

#### 4.1 GENERAL

The following recommendations are made based on the attached test boring data, our stated understanding of the proposed construction, and our experience with similar projects and subsurface conditions. If subsurface conditions are encountered during construction which were not encountered in the borings, those conditions should be reported immediately to UES for evaluation and possible recommendations. In this section of the report, recommendations are presented for groundwater considerations, foundations and related services.

#### 4.2 GROUNDWATER CONSIDERATIONS

The groundwater table will fluctuate seasonally depending upon local rainfall. The rainy season in South Florida is normally between May and October. Based upon the test boring data, a reasonable estimate for the seasonal high groundwater table is approximately 2 to 10.5 feet below existing grade depending on location. The existing and estimated seasonal high groundwater table at each location appears on the boring logs in Appendix B.

Note that our estimate of seasonal high groundwater level is based on limited data and does not provide any assurance that groundwater levels will not exceed the estimated level during any given year in the future. If the rainfall intensity and duration or total rainfall quantities exceed those normally anticipated, then groundwater levels will likely exceed the seasonal high estimate.

The estimate of seasonal high groundwater level is made for the site at the present time. Future development of adjoining or nearby properties and development on a regional scale may affect the local seasonal high groundwater table. Universal makes no warranty on the estimate of the seasonal high groundwater table.

UES recommends that all foundation design incorporate assumption of the seasonal high groundwater condition. We recommend that positive drainage be established and maintained on the site during construction. UES further recommends that permanent measures be implemented to maintain positive drainage throughout the life of the project.

#### 4.3 BUILDING FOUNDATIONS

#### 4.3.1 SHALLOW FOUNDATIONS FOR PUMP STATION

After successful completion of the recommendations included in the Site Preparation section of this report, including removal of unsuitable organic soils and replacement with clean compacted granular fill, we anticipate that the proposed pump station can be supported on shallow foundations with a maximum allowable net soil bearing pressure of 4,000 pounds per square foot (psf).

Based on the soil borings, unsuitable organic soils will likely be present to depths of 20 feet or more below existing grade in the areas adjacent to the canal bank. These materials are not considered suitable for foundation support. Excavation of organic soils is feasible using track-mounted hydraulic backhoes. However, limestone layers will likely be present to depths of 10 feet or deeper; excavation through limestone layers will probably require at least the use of a rock toothed bucket, rock saw, or similar means. Excavations that extend below surface water and groundwater levels will require dewatering and sheet pile support (i.e. cofferdams).

Post-construction settlements of the structure will be influenced by several interrelated factors, including: (1) strength and compressibility characteristics of the subsurface; (2) footing size, bearing level, applied loads, and resulting bearing pressures beneath the foundations; and (3) site preparation and earthwork construction techniques used by the contractor. Our settlement estimates for the structure are based on the use of site preparation/earthwork construction techniques as recommended above and in Section 4.5 of this report. Any deviation from these recommendations could result in an increase in the estimated post-construction settlements of the structure.

Assuming all soils are properly prepared and using the recommended maximum bearing pressure, we estimate that total post construction settlements of the structure will be 1 inch or less.

Differential settlements result from differences in applied bearing pressures and variations in the compressibility characteristics of the subsurface soils. If the recommended site preparation and earthwork construction techniques outlined above and in Section 4.5 are followed, differential settlements of ½ inch or less should be anticipated.

#### 4.3.2 DEEP FOUNDATION FOR BRIDGE

Driven Pre-stressed Precast Concrete Piles (PPC) piles are considered as viable foundation for support of the proposed bridge structure. Pre-stressed concrete piles are readily available and generally have lower unit cost per ton of pile capacity than other pile types. Based on the test boring B-11A and our experience with similar projects, we expect that 18 and 24-inch square PPC piles will be sufficient for the proposed bridge. Pre-drilling may be required in the limestone layer.

#### 4.3.3 AXIAL LOAD ANALYSIS FOR BRIDGE

UES evaluated pile capacity versus tip elevation using the FBDeep computer program. Printouts of FBDeep Davisson Design Curves results are included in Appendix B. The estimated ultimate Davisson Capacity for 18 and 24-inch PPC piles are shown in Table 2.



PCP Pile Width (Inches)	Estimated Ultimate Davisson Capacity (Tons)	Anticipated Pile Tip Elevation (Ft, NAVD 88)
18	75	-6
18	103	-26
18	149	-46
18	260	-76
24	127	-6
24	188	-26
24	217	-46
24	377	-76

#### TABLE 2: ESTIMATED PILE CAPACITY & CORRESPONDING TIP ELEVATIONS

#### 4.3.4 DEEP FOUNDATION FOR STILLING WELL

Driven Pre-stressed Precast Concrete Piles (PPC) piles are considered as viable foundation for support of the proposed stilling well. Pre-stressed concrete piles are readily available and generally have lower unit cost per ton of pile capacity than other pile types. Based on the test boring B-13 and our experience with similar projects, we expect that 12-inch square PPC piles will be sufficient for the proposed stilling well.

#### 4.3.5 AXIAL LOAD ANALYSIS FOR STILLING WELL

UES evaluated pile capacity versus tip elevation using the FBDeep computer program. Printouts of FBDeep Davisson Design Curves results are included in Appendix B. The estimated ultimate capacity for 12-inch PPC piles are shown in Table 3.

PCP Pile Width (Inches)	Estimated Ultimate Davisson Capacity (Tons)	Anticipated Pile Tip Elevation (Ft, NAVD 88)
12	27	20.4
12	48	14.4
12	63	6.4

#### TABLE 3: ESTIMATED PILE CAPACITY & CORRESPONDING TIP ELEVATIONS



#### 4.3.6 GEOTECHNICAL PARAMETERS

Table No. 4 shows typical geotechnical design parameters for the materials found in the borings. Note that the specific parameters used for axial and lateral capacity analysis are dependent upon estimated soil density and effective stress conditions. Those estimates are based on Standard Penetration Test (SPT) 'N' values.

	TABL	E 4: RECOM	MENDED	SOIL DES	IGN PARAN	IETERS	
Layer Depth	Friction Angle	Bearing Capacity		ommended sure Coeff		Unit We	ight (pcf)
(Feet)	(degrees)	(psf)	Active	Passive	At Rest	Saturated	Submerged
			ka	<b>k</b> <sub>p</sub>	K₀		
0 – 12	28	2,500	0.36	2.77	0.53	110	47.6
12 – 53	32	4,000	0.31	3.26	0.47	125	62.6
53 – 100	33	2,500	0.30	3.39	0.46	120	57.6

#### 4.4 GENERAL PILE INSTALLATION ISSUES

#### 4.4.1 PILE GROUPS

No reduction of the individual pile capacities will be required if piles are spaced center-tocenter at three (3) times their width or greater. The pile caps for end bents usually contribute to the overall bearing capacity of the pile group provided they are supported on competent soil outside the outer perimeter of the group. However, we do not recommend including this additional capacity in design calculations due to the possible loss of soil cover at the pile cap.

#### 4.4.2 PILE SETTLEMENT

Settlement of pile supported bridge piers should be small and tolerable for a typical single row pile group. For the typical axial load considered, settlement of a typical 12-inch diameter concrete pile is estimated to be on the order of ½ inch. Pile group settlements are estimated to be on an order of magnitude similar to a single row pile group pattern, but will increase slightly for other pile group configurations.

#### 4.4.3 TEST PILES

We recommend a test pile program be conducted to verify driving conditions, determine pile driving criteria, evaluate the hammer system and pile capacities, and to refine production pile lengths. We recommend driving a minimum of 3 test piles at separate bent locations. The test piles should be located in permanent pile locations.



The test piles should be instrumented with the Pile Driving Analyzer (PDA) or equivalent in accordance with FDOT Specification 455. This monitoring will ensure allowable stress levels are not exceeded during driving and provide verification regarding pile capacity. CAPWAP analyses also be performed to confirm PDA results.

#### 4.5 SITE PREPARATION

We recommend normal, good practice site preparation procedures for areas of planned construction. These procedures include: stripping the site of any deleterious material, proof-rolling, proof-compacting or preparing the subgrade as described below, and filling to grade with engineered fill. A general outline of the anticipated earthwork is as follows:

- 1. If required, perform remedial dewatering prior to any earthwork operations. We recommend performing earthwork in-the-dry.
- 2. Prior to construction, any existing underground utility lines within the construction area should be located. Provisions should be made to relocate interfering utilities. Note that underground pipes not properly removed or plugged may serve as conduits for subsurface erosion which may lead to excessive settlement of overlying structures.
- 3. The proposed construction limits should be stripped of vegetation, construction debris, and other deleterious materials within and 5 feet beyond the perimeter of the proposed building.
- 4. The site should be graded to direct surface water runoff away from the construction areas. Positive drainage must be maintained throughout the design life of the project.
- 5. Prepare the pavement subgrade to a minimum of 5-feet beyond the perimeter of the proposed pavement area. The prepared subgrade soils should be observed by a qualified geotechnical engineer or his representative to locate deposits of organic soils, vegetation, excessive roots or debris. Organic soils, vegetation, or deleterious material should be undercut until clean natural soils are encountered.
- 6. Prior to construction of improvements or placement of fill, the subgrade should be compacted using a smooth drum vibratory roller *in the static mode*, having a minimum static, at-drum weight on the order of 10 tons and a drum diameter on the order of 3 to 4 feet making a minimum of eight overlapping passes with the second set of 4 passes perpendicular to the first set of 4 passes. Typically, the material should exhibit moisture content within +/- 2 percent of the Modified Proctor optimum moisture content (ASTM D-1557) during the compaction operations. Compaction should continue until densities of at least 95 percent of the Modified Proctor maximum dry density (ASTM D-1557) have been uniformly achieved within the upper 12 inches of the compacted natural soil surface.



- 7. Place fill material, as required. The fill should consist of sand with less than 10 percent soil fines. Place fill in uniform 10- to 12-inch loose lifts and compact each lift to a minimum density of at least 95 percent of the Modified Proctor maximum dry density (ASTM D1557). The last 6 inches of fill beneath pavement areas should be compacted to 98 percent of the Modified Proctor maximum dry density. Stabilize this zone with shell or limerock as required to meet the subgrade recommendations contained in the Pavements Section of this report.
- 8. Complete in-situ density tests on the subgrade and each lift of fill at a frequency of not less than one test per 2,500 square feet in the building area and one test per 10,000 square feet in paved areas.
- 9. In the lightly loaded structure areas, test compaction to a depth of 1 foot at the bottom of all column footings. We recommend conduct one test for every 50 lineal feet of wall footing.
- 10. If difficult compaction conditions are encountered during the site work operations, the compaction efforts should stop and the geotechnical engineer should be contacted. The geotechnical engineer or his representative should observe proof-rolling of the exposed subgrade to determine if additional compaction is warranted or if any material needs to be over-excavated and replaced.

If site preparation work is performed during the rainy season (May through October), special care should be taken to maintain positive drainage from the building pad and paved areas to drains or ditches around the site. Unexpected wet periods can also occur in Florida during the "dry" season. Such events can raise water tables to levels above seasonal highs without the associated high temperatures to evaporate ponded water. Therefore, the contractor should practice wet weather means and methods for earthwork during the "dry" season as well. Groundwater and surface water control, use of granular fill material and aeration are typical means to accomplish wet weather grading. All fill materials that are excavated from below the water table should be stockpiled for a sufficiently long period to allow drainage.

#### 4.6 CONSTRUCTION RELATED SERVICES

We recommend the owner retain UES to perform construction material testing and observations on this project. Field tests and observations could include items such as verification of foundation subgrade, monitoring of proof-rolling operations, and performing quality assurance tests on the placement of compacted structural fill.

The geotechnical engineering design does not end with the advertisement of the construction documents. The design is an on-going process throughout construction. Because of our familiarity with the site conditions and the intent of the engineering design, we are most qualified to address problems that might arise during construction in a timely and cost-effective manner.



### 5.0 LIMITATIONS

Our field exploration found unsuitable materials (i.e., peat) in the test borings. The test borings completed for this report were widely spaced and are not considered sufficient for reliably detecting the presence of isolated, anomalous surface or subsurface conditions, or reliably estimating unsuitable or suitable material quantities.

Accordingly, UES does not recommend relying on our boring information to negate the presence of anomalous materials or for estimation of material quantities. Therefore, UES will not be responsible for any extrapolation or use of our data by others beyond the purpose(s) for which it is applicable or intended.

During the early stages of this construction project, geotechnical issues not addressed in this report may arise. Because of the natural limitations inherent in working with the subsurface, it is not possible for a geotechnical engineer to predict and address all possible problems. An (ASFE) publication, "Important Information About Your Geotechnical Engineering Report" appears in Appendix C, and will help explain the nature of geotechnical issues.

Further, we present documents in Appendix C: Constraints and Restrictions, to bring to your attention the potential concerns and the basic limitations of a typical geotechnical report.

This report is for the exclusive use of our client and our client's design team for this specific project. Information contained in this report may not be used or relied on by others without the expressed written consent of UES.



#### 6.0 SUMMARY

In summary, we have completed a geotechnical exploration for the proposed pump station, bridge, and stilling well at the subject site. Field and laboratory tests have been performed to provide geotechnical engineering recommendations for foundation design.

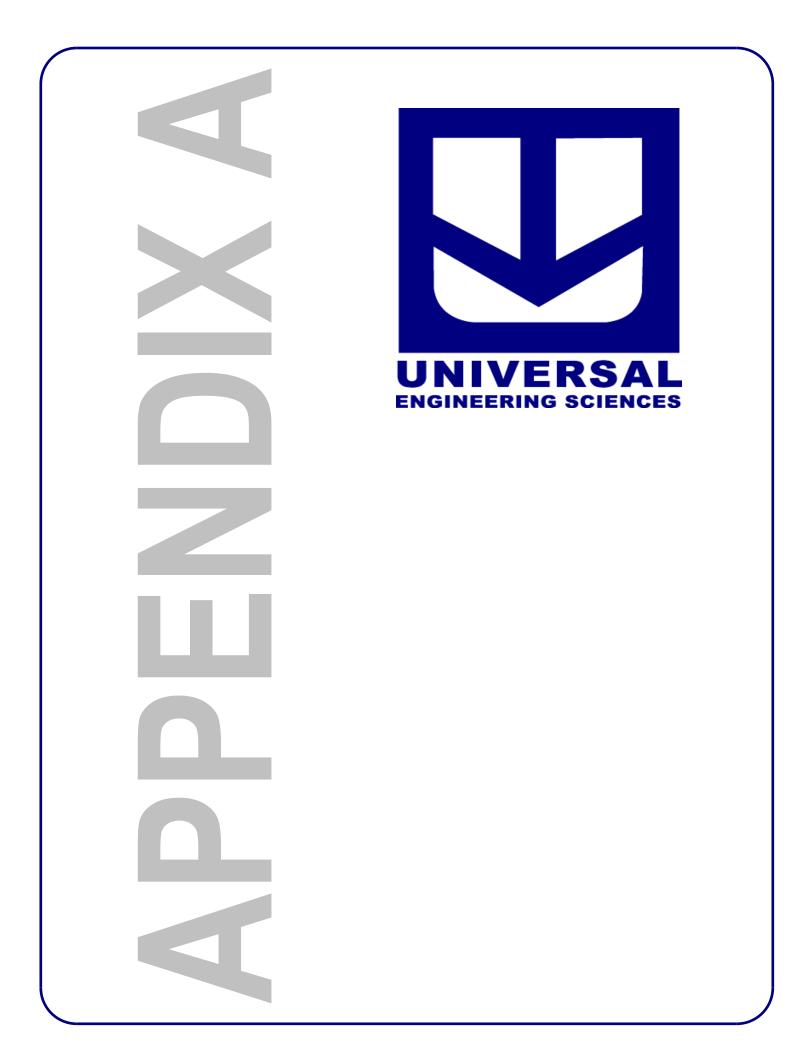
The soils encountered generally consist of loose to very dense limerock (FILL), very loose muck/peat, loose to very dense limestone, silty limestone [SP, PT, GP] from 0 to 12 feet below ground surface followed by very loose to very dense, limestone, silty sand with limestone, sand with silt and limestone, silty sand [GP, SM, SP-SM, SM] to a depth of 53 feet below ground surface underlain by loose to very dense, sand with shell fragments [SP] to the maximum explored depth of 100 feet (bls).

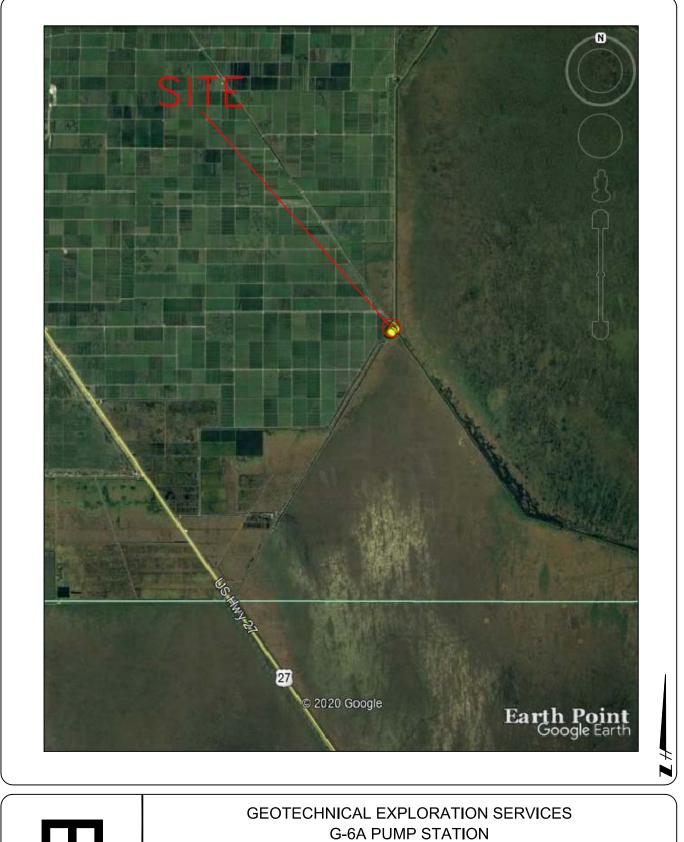
Groundwater was measured at 4 to 12.5 feet below the existing land surface in the test borings. A reasonable estimate for an average wet seasonal high groundwater table is 2 to 10.5 feet below land surface (bls).

Estimates of allowable soil bearing values and estimates of settlement for the proposed construction are covered in detail within the body of this report. If the subgrade soils are prepared as recommended, the proposed pump station can be supported on a conventional shallow foundation system. The bridge and stilling well can be supported on a deep foundation system.

UES recommends normal, good practice site preparation procedures to prepare the subgrade to support the structures.





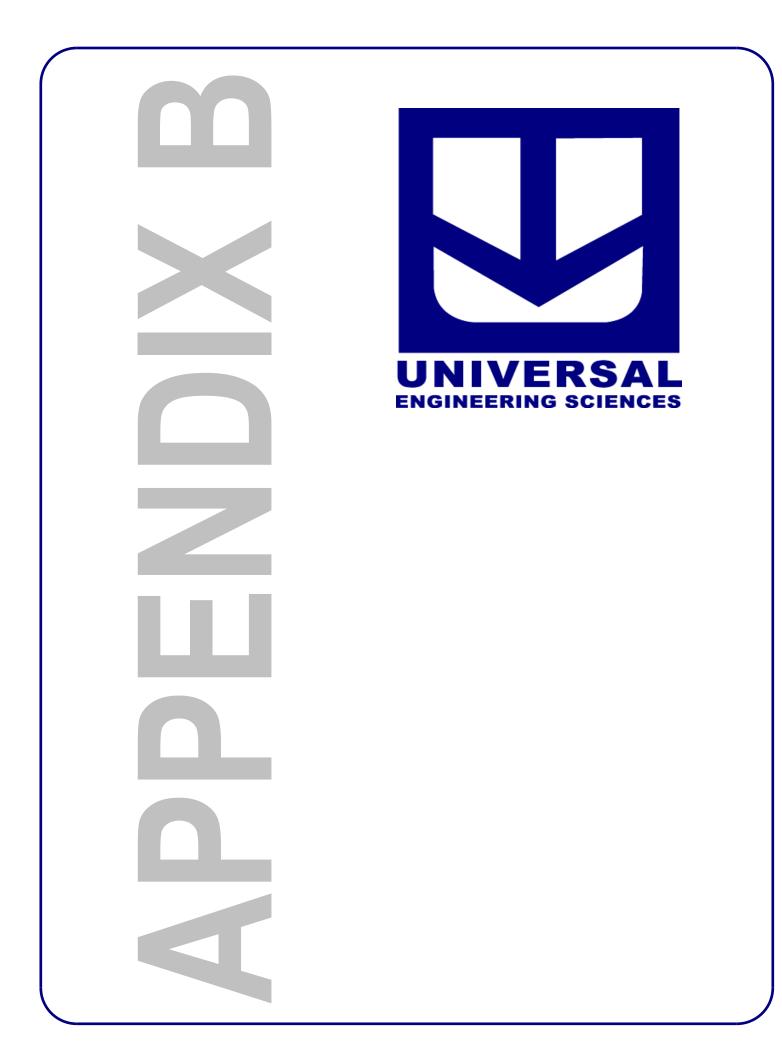


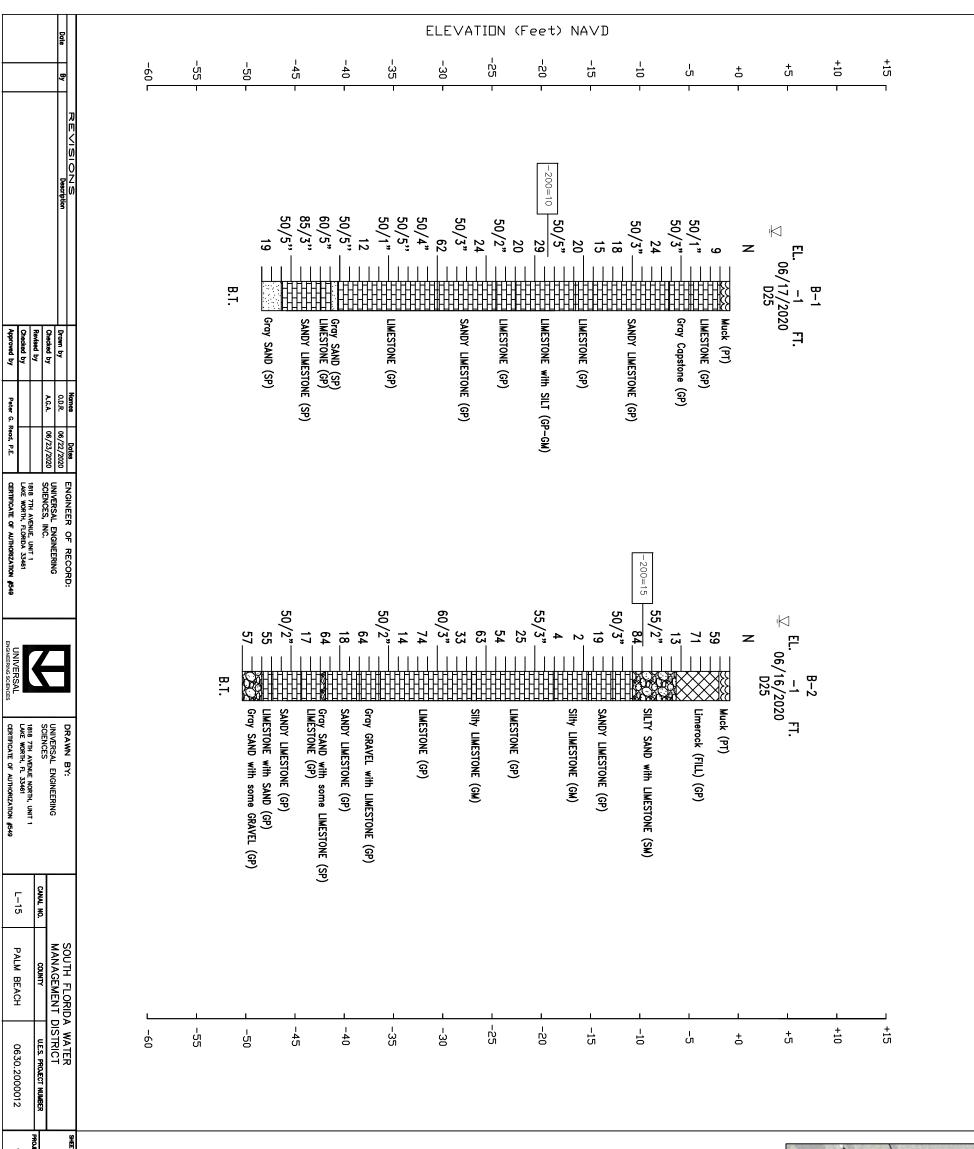
# WEST PALM BEACH, PALM BEACH COUNTY, FLORIDA

SITE LOCATION MAP

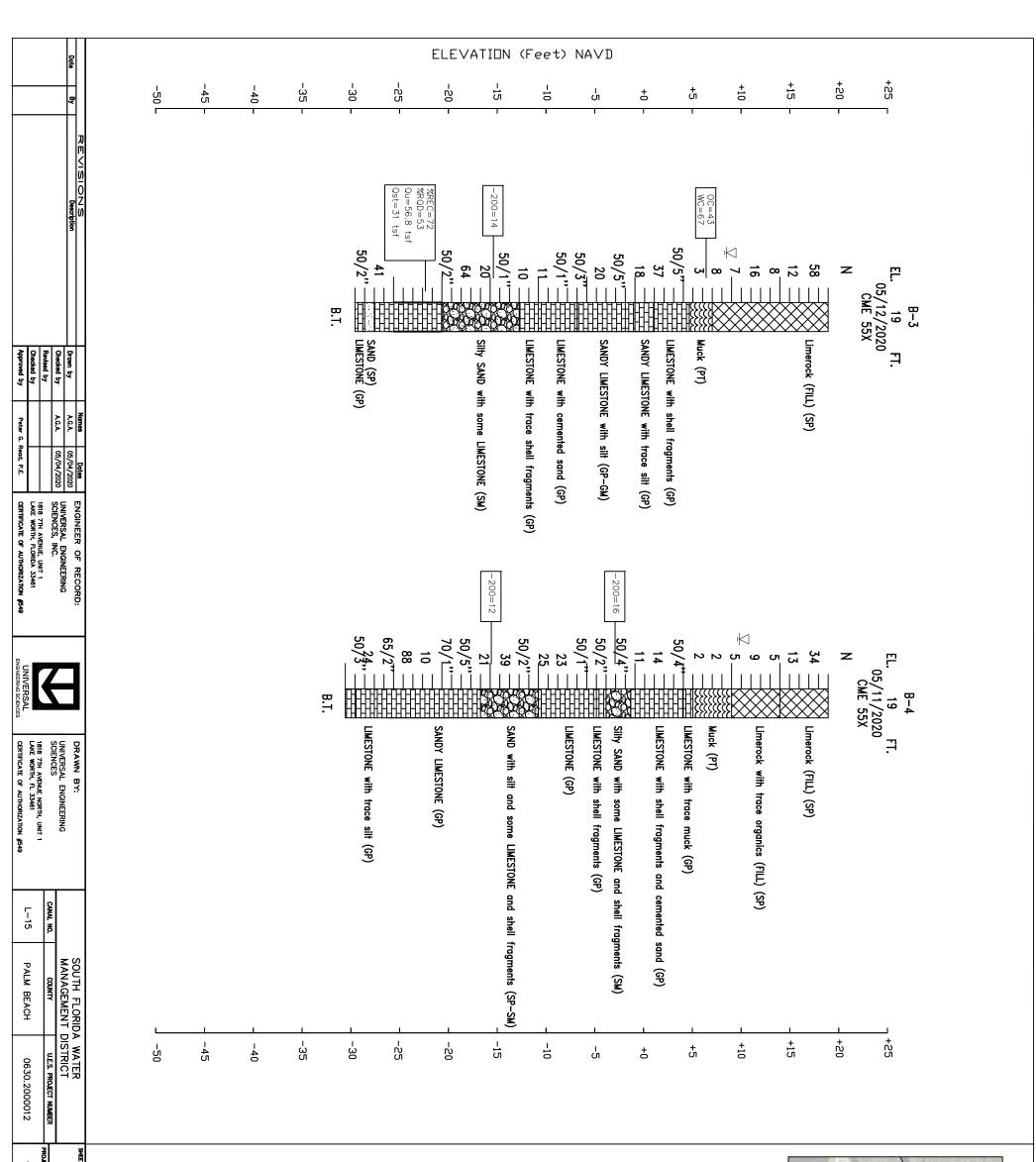
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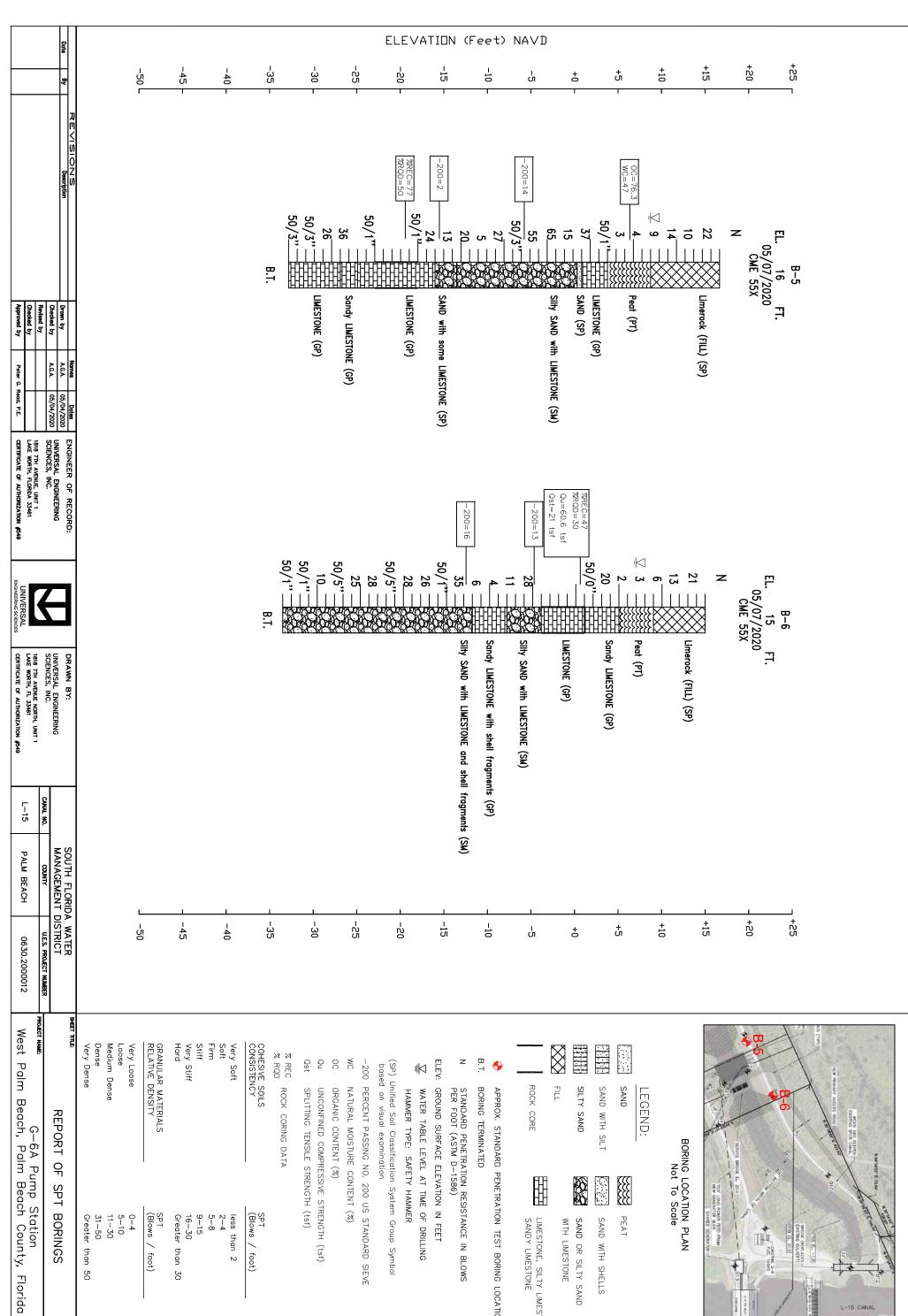


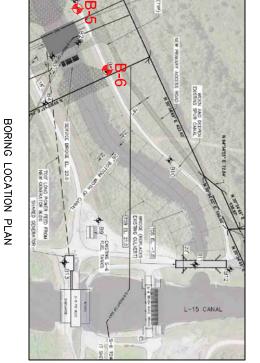


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	LEGEND:		č
	SAND		PEAT
	SAND WITH SILT	$C_{\tilde{G}}$	SAND WITH SHELLS
	SILTY SAND		SAND OR SILTY SAND
$\bigotimes$	FILL		WITH LIMESTONE
	ROCK CORE		LIMESTONE, SILTY LIMESTONE SANDY LIMESTONE
<del>•</del>	APPROX. STANDARD	PENETRAT	PENETRATION TEST BORING LOCATION
В.Т.	BORING TERMINATED		
z	STANDARD PENETRATION RESISTANCE IN BLOWS PER FOOT (ASTM D-1586)	TION RESIS -1586)	STANCE IN BLOWS
ELEV:	GROUND SURFACE ELEVATION IN FEET	LEVATION	IN FEET
Ø	WATER TABLE LEVEL AT TIME OF DRILLING	AT TIME	OF DRILLING

	BORING No	BORING LOCATION PLAN Not To Scale	Scale
	LEGEND:		
	SAND		PEAT
	SAND WITH SILT	Ċċ	SAND WITH SHELLS
	SILTY SAND		SAND OR SILTY SAND
$\bigotimes$	FILL		WITH LIMESTONE
	ROCK CORE		LIMESTONE, SILTY LIMESTONE SANDY LIMESTONE
<del>•</del>	APPROX. STANDARD I	PENETRATION TEST	ION TEST BORING LOCATION
B.T.	BORING TERMINATED		
z	STANDARD PENETRAT PER FOOT (ASTM D-	RATION RESIS D-1586)	PENETRATION RESISTANCE IN BLOWS (ASTM D-1586)
ELEV:	GROUND SURFACE EL	ELEVATION IN FEET	N FEET
	WATER TABLE LEVEL AT HAMMER TYPE: SAFETY	TIME	OF DRILLING MER
(SP) Ur based	(SP) Unified Soil Classification based on visual examination	on System m	n Group Symbol
-200	PERCENT PASSING NO.	). 200 US	STANDARD SIEVE
WC	NATURAL MOISTURE (	CONTENT (	(%)
oc	ORGANIC CONTENT (%)		
Qu	UNCONFINED COMPRESSIVE SPLITTING TENSILE STRENG	<u> </u>	STRENGTH (tsf) "H (tsf)
% REC % RQD	ROCK CORING DATA		
COHESIVE SOILS	SOILS	I	(Blows / foot)
Very Soft Soft Firm			less than 2 2-4 5-8
Stiff Very Stiff Hard			9–15 16–30 Greater than 30
GRANULAR RELATIVE D	R MATERIALS DENSITY	1	(Blows / foot)
ō	Ø		0-4 5-10
Dense			31-50

IIILE:

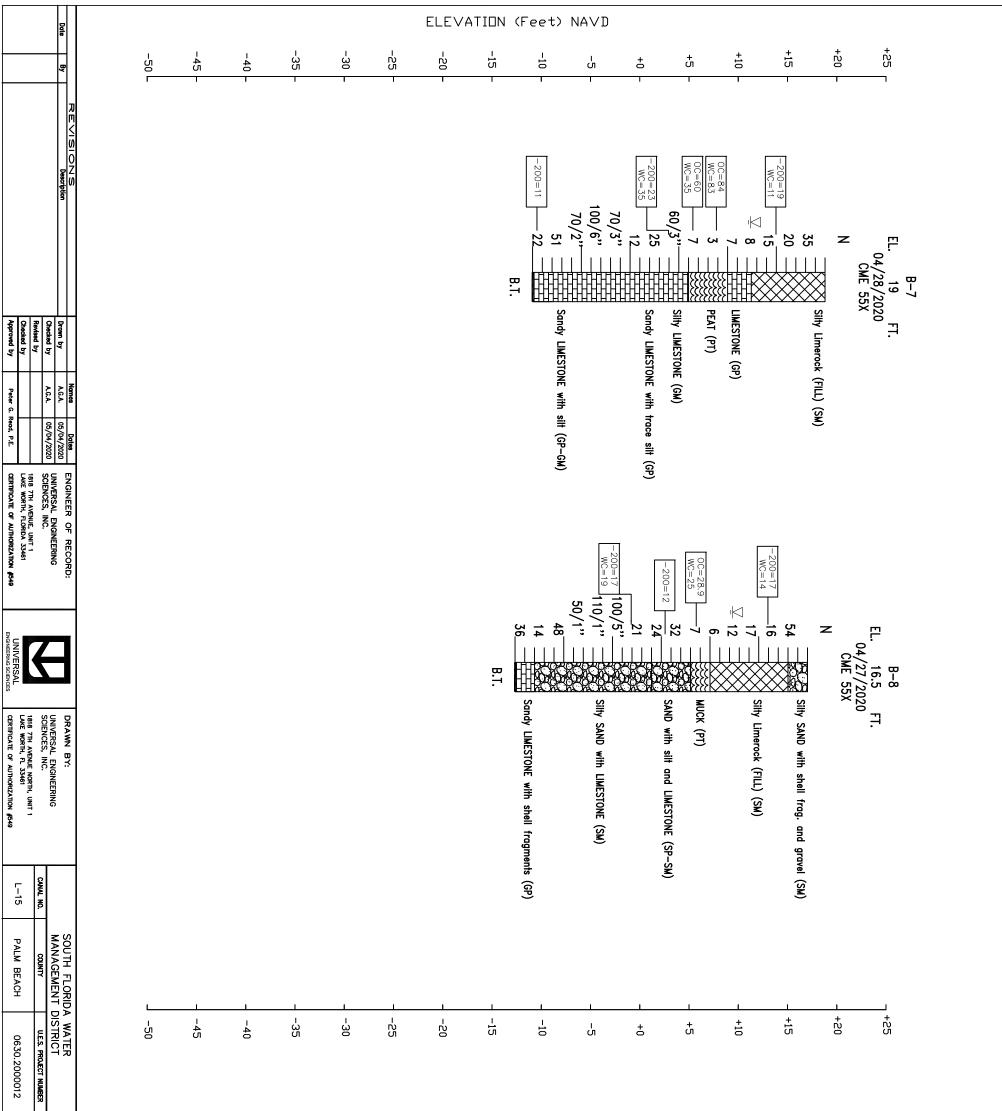
REPORT OF SPT BORINGS

B-3 DRAWING NO.

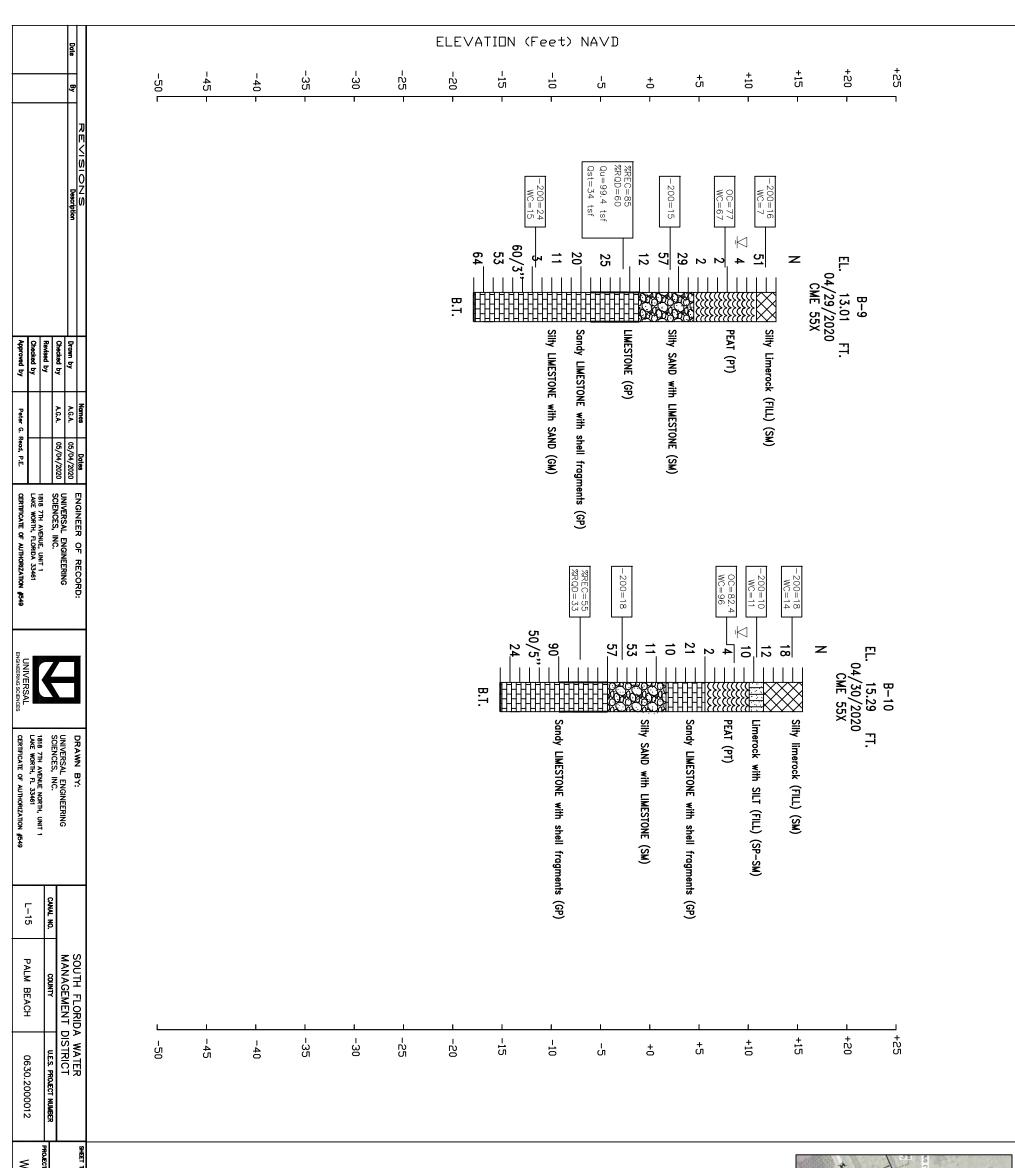
INDEX NO.

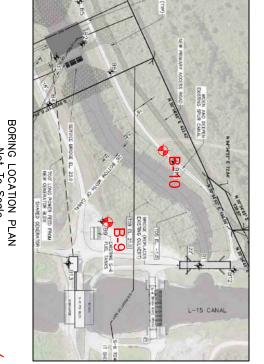
Very Dense

Greater than 50



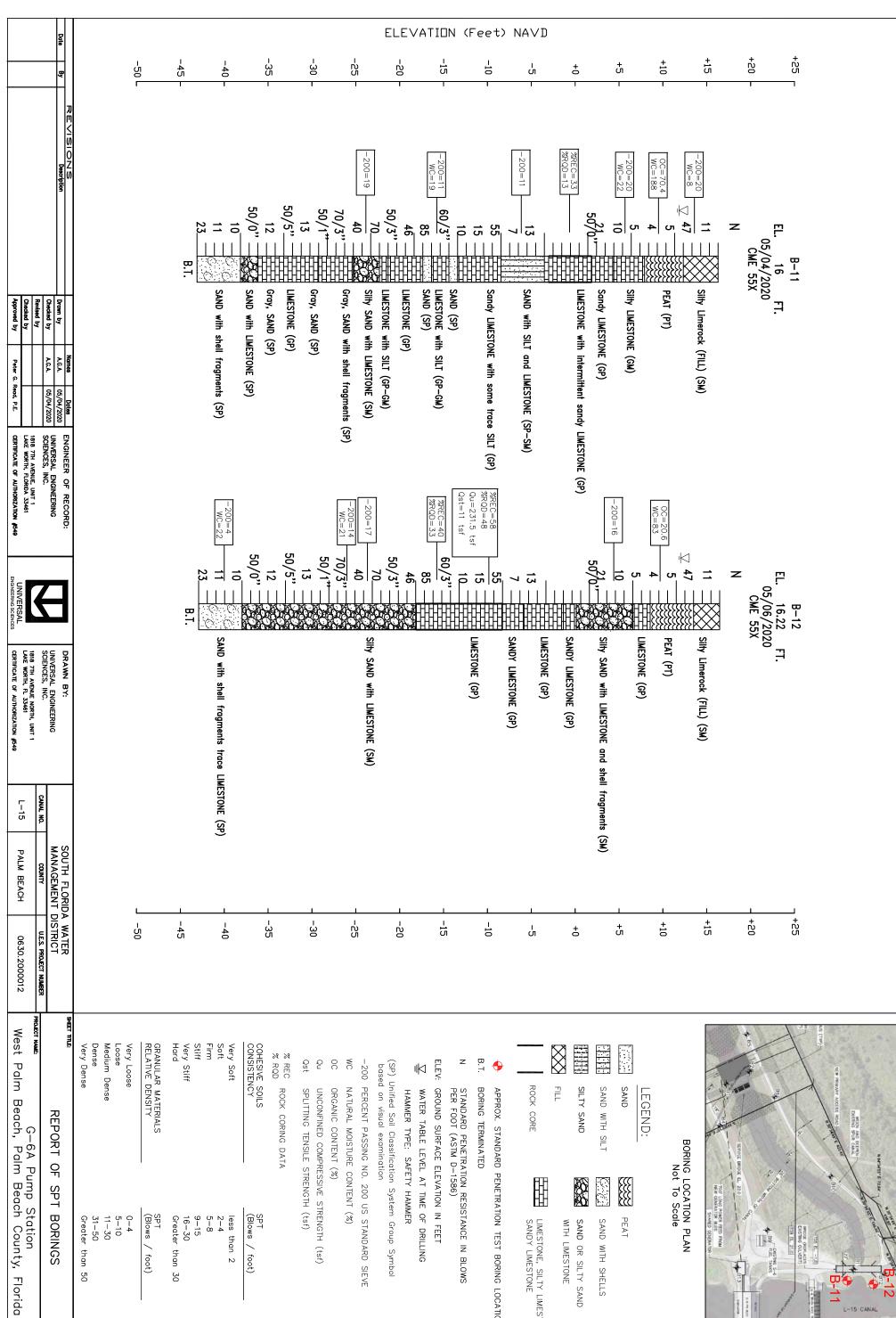
West Palm Beach, Palm Beach	REPORT	GRANULAR MATERIALS RELATIVE DENSITY Very Loose Loose Medium Dense Dense Very Dense	NG DATA	WATER TABLE LEVEL AT TI HAMMER TYPE: SAFETY HA Unified Soil Classification Sys d on visual examination PERCENT PASSING NO. 200 NATURAL MOISTURE CONTEN ORGANIC CONTENT (%) UNCONFINED COMPRESSIVE SPLITTING TENSILE STRENGT	LEGEND:       PEAT         SAND       With SILT       SAND         SAND       With SILT       SAND         SILTY       SAND       SAND         FILL       FILL       With         ROCK       CORE       LIMES         BORING       TERMINATED       LIMES         N       STANDARD       FER FOOT (ASTM D-1586)       LIMES         N       STANDARD       FER FOOT (ASTM D-1586)       LIMES	BORING LOCATION Not To Scale
ch County, Florida	ORINGS	SPT (Blows / foot) 0-4 5-10 11-30 31-50 Greater than 50	SPT (Blows / foot) less than 2 2-4 5-8 9-15 16-30 Greater than 30	ME OF DRILLING MMMER stem Group Symbol US STANDARD SIEVE UT (%) STRENGTH (tsf) H (tsf)	PEAT SAND WITH SHELLS SAND OR SILTY SAND WITH LIMESTONE LIMESTONE, SILTY LIMESTONE, LIMESTONE WITH SILT ETRATION TEST BORING LOCATION FRESISTANCE IN BLOWS )	HEAN HOLE SHE CHANGE

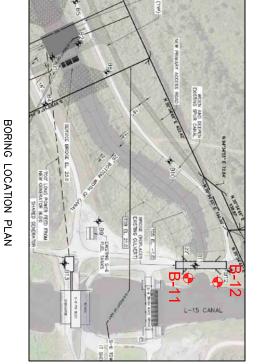




% REC % RQD	Qu	000	WC	-200	(SP) ( base	ļ	$\bowtie$	ELEV:	z	B.T.	<b>•</b>		$\bigotimes$					
ROCK CORING DATA	UNCONFINED COMPRESSIVE STRENGTH (tsf) SPLITTING TENSILE STRENGTH (tsf)	ORGANIC CONTENT (%)	NATURAL MOISTURE CONTENT (%)	PERCENT PASSING NO. 200	(SP) Unified Soil Classification System Group based on visual examination	HAMMER TYPE: SAFETY HAMMER	WATER TABLE LEVEL AT TIME OF	GROUND SURFACE ELEVATION IN FEET	STANDARD PENETRATION RESISTANCE IN BLOWS PER FOOT (ASTM D-1586)	BORING TERMINATED	APPROX. STANDARD PENE	ROCK CORE	FILL	SILTY SAND	SAND WITH SILT	SAND	LEGEND:	
	E STRENGTH (tsf) GTH (tsf)		ENT (%)	O US STANDARD SIEVE	ystem Group Symbol		TIME OF DRILLING	TION IN FEET	RESISTANCE IN BLOWS		PENETRATION TEST BORING LOCATION	LIMESTONE, SILTY LIMESTONE	WITH LIMESTONE	SAND OR SILTY SAND	法 SAND WITH SHELLS	PEAT		

INDEX NO.	Pump Station m Beach County Florida	œrwwe G−6A Pi
draming no. B—5	OF SPT BORINGS	REPORT
	Greater than 50	Very Dense
	31-50	Dense
	5-10 11-30	
		Very Loose
	SPT (Blows / foot)	GRANULAR MATERIALS RELATIVE DENSITY
	Greater than 30	
	9-10 16-30	Very Stiff
	0-17 0-17	Firm
	less than 2 2-4	Very Soft Soft
	SPT (Blows / foot)	COHESIVE SOILS CONSISTENCY
	-	% REC ROCK CORING DATA % RQD
	COMPRESSIVE STRENGTH (tst) NSILE STRENGTH (tsf)	Qu UNCONFINED COMP Qst SPLITTING TENSILE
		URGANIC CUR
	CONTENT (%)	NATURAL MOISTURE
	200 U	-200 PERCENT PASSING NO.
	tion System Group Symbol ion	(SP) Unified Soil Classification based on visual examination
	ETY HAMMER	HAMMER TYPE:
	L AT TIME OF DRILLING	WATER TABLE LEV
	FI EVATION IN FEFT	JRFACF
	RATION RESISTANCE IN BLOWS D-1586)	N STANDARD PENETRATION PER FOOT (ASTM D-1586
		BORING T
~	PENETRATION TEST BORING LOCATION	
ONE	LIMESTONE, SILTY LIMESTONE	ROCK CORE
	WITH LIMESTONE	FILL FILL
	SAND OR SILTY SAND	SILTY SAND
	SAND WITH SHELLS	SAND WITH SILT
Ż	PEAT	SAND
		LEGEND:
	4G LOCATION PLAN Not To Scale	BORING
Vie	- TOU LONG POWER FED FROM NEW GENERALIDE BLOE SINGED GEDIERNING	A DATE





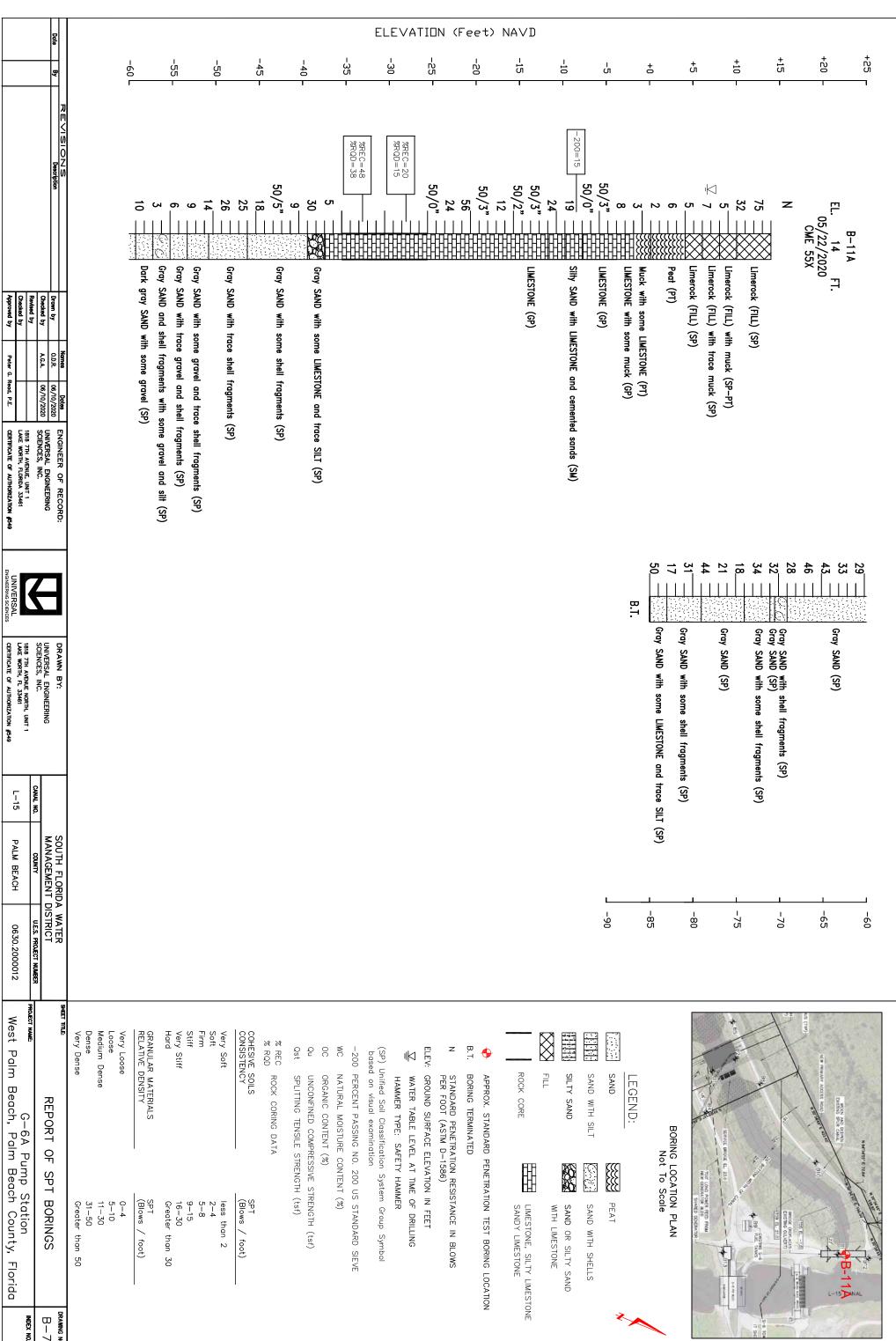
			77 6.	4
31–50 Greater than 50		s e	Dense Very Dense	
11-30		Dense	З	
0-4 5-10		se	Very Loose Loose	
SPT (Blows / foot)		GRANULAR MATERIALS RELATIVE DENSITY	GRANULA RELATIVE	
Greater than 30		-		
9–15 16–30		Ŧ	Stiff Verv Stiff	
5-8			Firm	
less than 2 2-4		ť	Very Soft Soft	
SPT (Blows / foot)		ENCY	COHESIVE SOIL	
	NG DATA	ROCK CORING	% REC % RQD	
(tsf)	NSILE STRENG	SPLITTING	Qst	
STRFNGTH (tsf)	COMPRESSIVE	ORGANIC CON	000000	
(%)	CONTENT		WC	
JS STANDARD SIEVE	PASSING NO. 200 US	PERCENT	-200	
em Group Symbol	Classification System examination	nified Soil on visual	(SP) Ur based	
AER 9		HAMMER T	Ik	
	WATER TABLE LEVEL AT TIME	WATER 1		
IN FEET	SURFACE ELEVATION IN FEET	GROUND	ELEV:	
RESISTANCE IN BLOWS 5)	PENETRATION RESI (ASTM D-1586)	STANDARD PER FOOT	z	
	TERMINATED	BORING TEF	B.T.	
TION TEST BORING LOCATION	STANDARD PENETRATION	APPROX. S	<b>+</b>	
LIMESTONE, SILTY LIMESTONE SANDY LIMESTONE		ROCK CORE		
WITH LIMESTONE		FILL	$\bigotimes$	
		SILTY SAND		
SAND WITH SHELLS	SILT	SAND WITH		
PEAT		SAND		
		LEGEND:		
Scale	BORING LOCATION PLAN Not To Scale			

TITLE:

REPORT OF SPT BORINGS

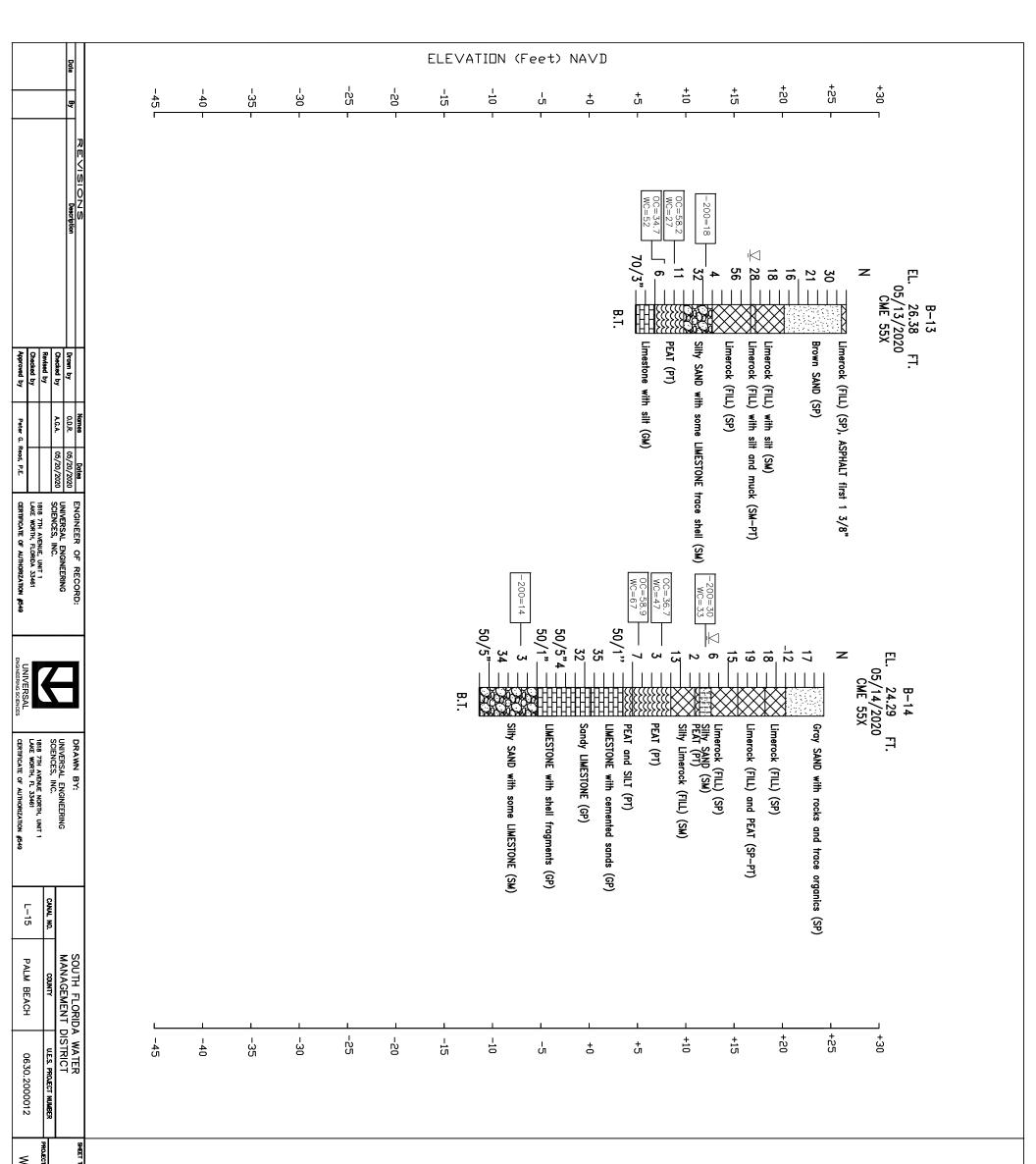
B-6 DRAWING NO.

INDEX NO.

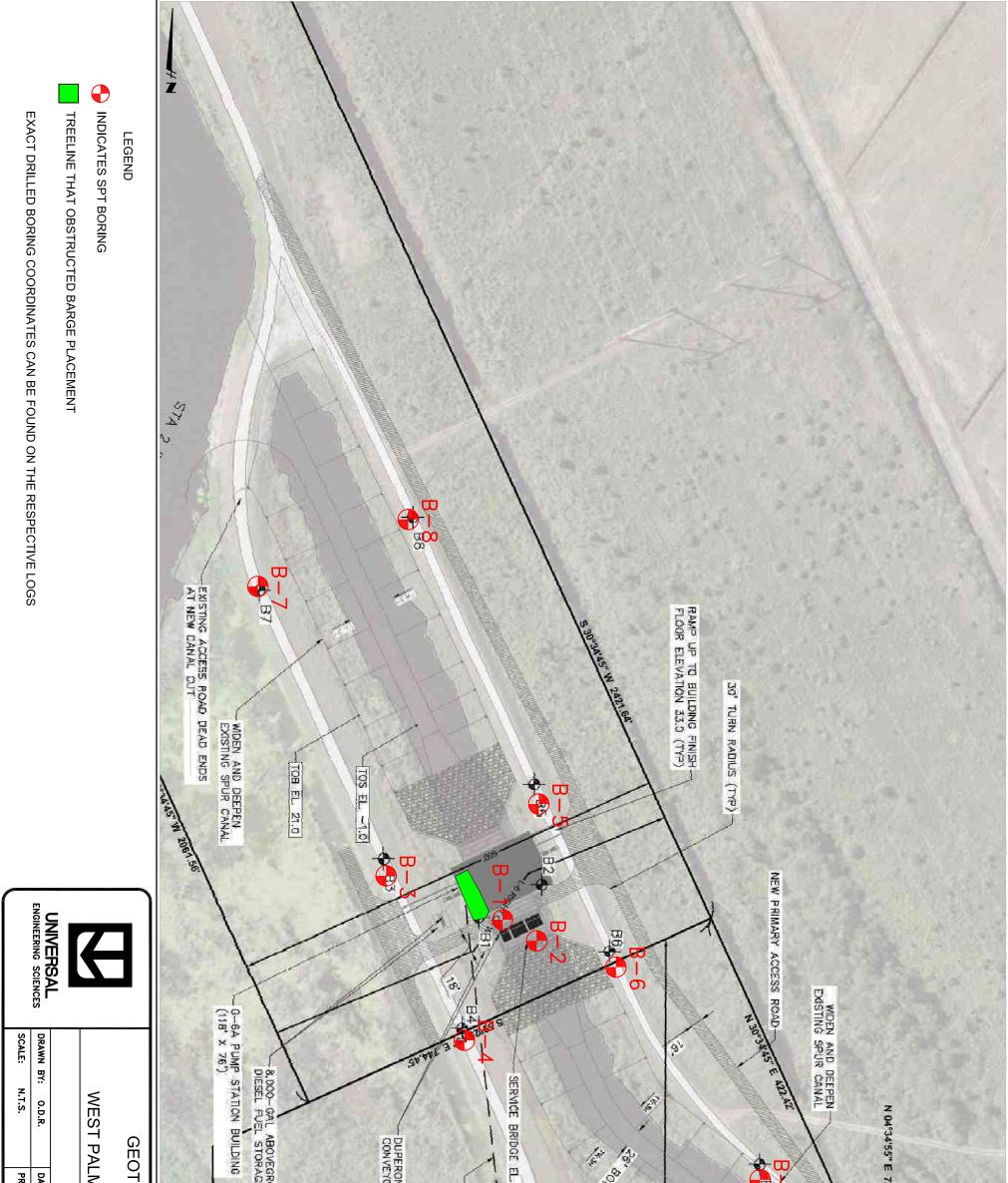


	N	Not To Scale	
	LEGEND:		
	SAND		PEAT
	SAND WITH SILT	Ċ.	SAND WITH SHELLS
	SILTY SAND		SAND OR SILTY SAND
$\bigotimes$	FILL		WITH LIMESTONE
	ROCK CORE		LIMESTONE, SILTY LIMESTONE SANDY LIMESTONE
<b>•</b>	APPROX. STANDARD	PENETRATIC	PENETRATION TEST BORING LOCATION
B.T.	BORING TERMINATED		
z	STANDARD PENETRATION RESISTANCE PER FOOT (ASTM D-1586)	10N RESIST 1586)	ANCE IN BLOWS
ELEV:	GROUND SURFACE ELEVATION IN FEET	EVATION IN	FEET
Ř	WATER TABLE LEVEL AT TIME OF HAMMER TYPE: SAFETY HAMMER	AT TIME O ETY HAMME	F DRILLING R
(SP) נ basec	(SP) Unified Soil Classification System Group Symbol based on visual examination	on System on	Group Symbol
-200	PERCENT PASSING NO. 200 US STANDARD SIEVE	0. 200 US	STANDARD SIEVE
WC	NATURAL MOISTURE CONTENT (%)	CONTENT (9	5)
00	ORGANIC CONTENT (%)	3	
Qu	UNCONFINED COMPRESSIVE		STRENGTH (tsf)
Qst	SPLITTING TENSILE STRENGTH (tsf)	TRENGTH (t	sf)
% REC % RQD	ROCK CORING DATA		
COHESIVE SOILS	SOILS	S	SPT

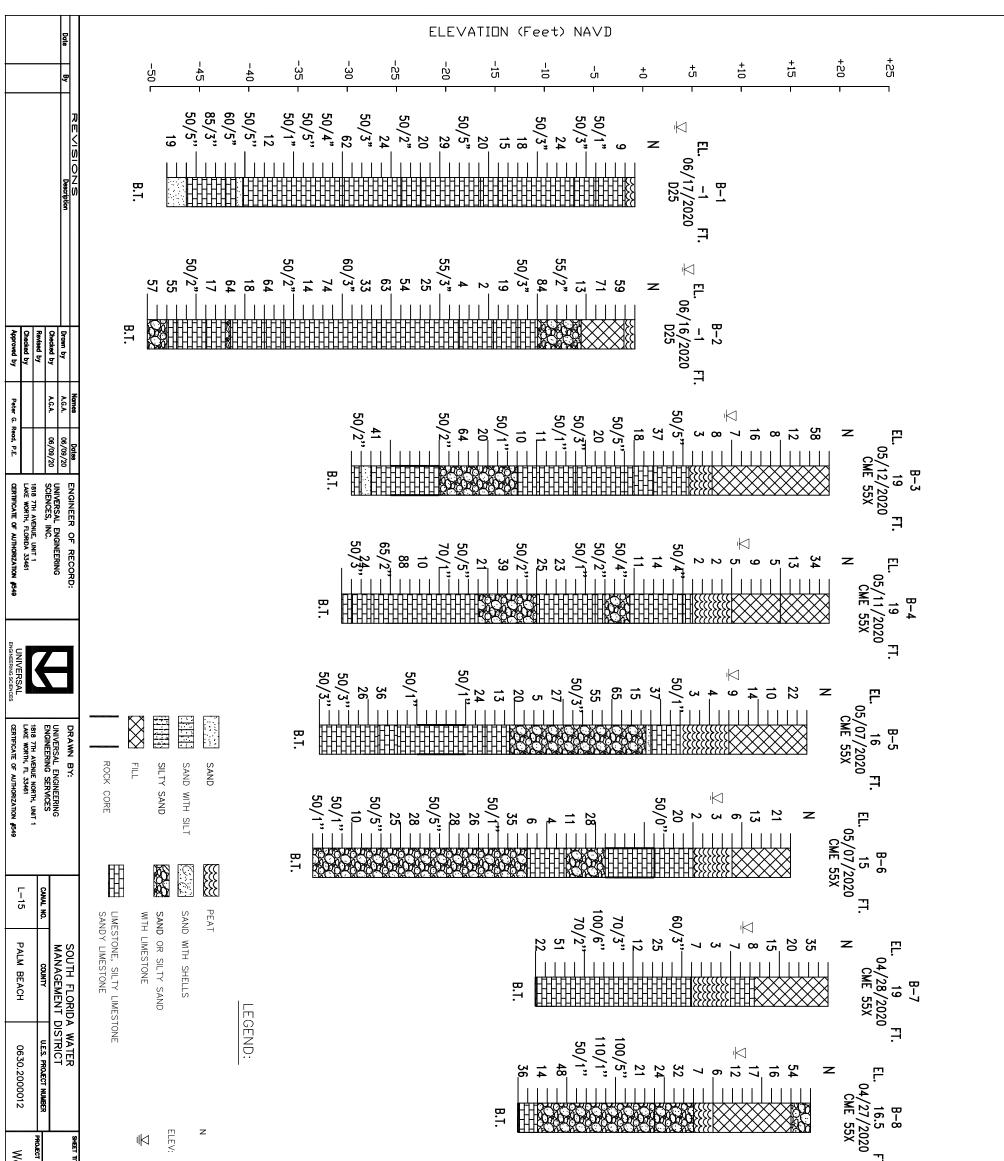
INDEX NO.	Pump Station m Beach County, Florida	rr אאונים G—6A Pi West Palm Beach, Palm	2 9
drawing no. B—7	F SPT BORINGS	THE REPORT OF	-
	Greater than 50	Very Dense	
	11-30	Medium Dense Dense	
	5-10	Loose	
	0-4	Very Loose	
	SPT (Blows / foot)	GRANULAR MATERIALS RELATIVE DENSITY	
	Greater than 30		
		Very Stiff	
	0-15 0-15	Firm Stiff	
	less than 2 2-4	Very Soft Soft	
	SPT (Blows / foot)	COHESIVE SOILS CONSISTENCY	
		% REC ROCK CORING DATA % RQD	
	STRENGTH (tsf)	Qst SPLITTING TENSILE S	
	ESSIVE STRENGTH (tsf)	Qu UNCONFINED COMPRESSIVE	
		ORGANIC CONTENT (	
	NTENT (%)	NATURAL MOISTURE	
	0. 200 US STANDARD SIEVE	PERCENT P	
	ion System Group Symbol on	(SP) Unified Soil Classification based on visual examination	
	ETY HAMMER	- HAMMER TYPE: SAFETY	
	AT TIME OF	WATER TABLE LEVI	
	ELEVATION IN FEET	ELEV: GROUND SURFACE EI	
	PENETRATION RESISTANCE IN BLOWS (ASTM D-1586)	N STANDARD PENETRA PER FOOT (ASTM D-	
		. BORING TE	
~	PENETRATION TEST BORING LOCATION	🔶 APPROX. STANDARD	
ONE	SANDY LIMESTONE, SILTY LIMESTONE	ROCK CORE	
	WITH LIMESTONE	FILL	
	SAND OR SILTY SAND	SILTY SAND	
	SAND WITH SHELLS	SAND WITH SILT	
×	PEAT	SAND	
		LEGEND:	
	BORING LOCATION PLAN Not To Scale	BORING	
	SHALL CLEAN OF -		100



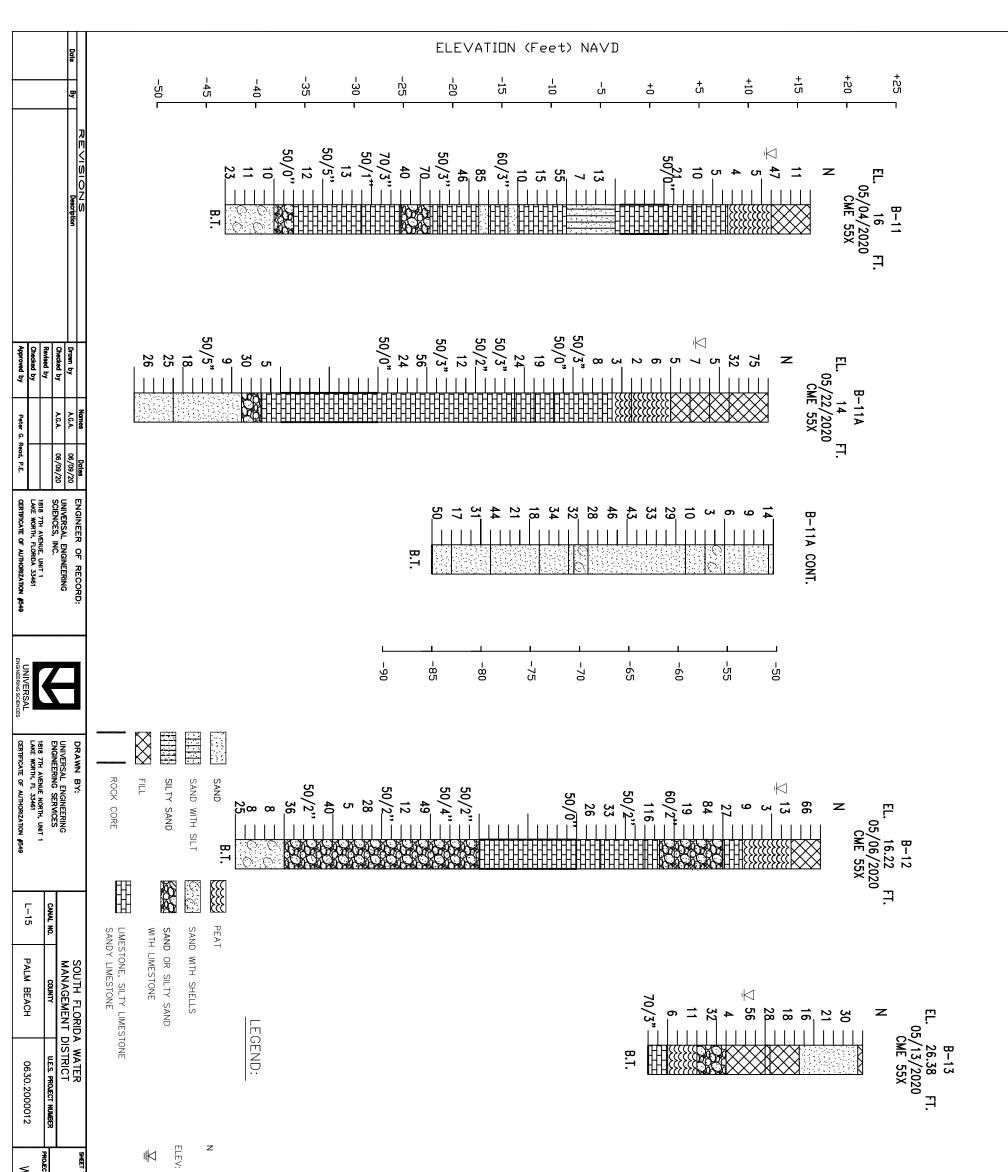
تت مسع G—6A Pump St West Palm Beach, Palm Beach	REPORT OF SP	ery ELA ery ery ery ery	<ul> <li>APPROX. STANDARD PENETRATION TE</li> <li>B.T. BORING TERMINATED</li> <li>N STANDARD PENETRATION RESISTANCE PER FOOT (ASTM D-1586)</li> <li>ELEV: GROUND SURFACE ELEVATION IN FEE:</li> <li>WATER TABLE LEVEL AT TIME OF DRI HAMMER TYPE: SAFETY HAMMER</li> <li>(SP) Unified Soil Classification System Group based on visual examination</li> <li>-200 PERCENT PASSING NO. 200 US STAN</li> <li>MC NATURAL MOISTURE CONTENT (%)</li> <li>OC ORGANIC CONTENT (%)</li> <li>UNCONFINED COMPRESSIVE STRENGTH (splitting TENSILE STRENGTH (tsf)</li> <li>REC ROCK CORING DATA</li> </ul>	LEGEND:     Reck core       Image: Sand     Sand       Image: Sand     Sand <t< th=""><th>Autored average weight wo define weight wo def</th></t<>	Autored average weight wo define weight wo def
Station ch County, Florida	T BORINGS B-8	SPT (Blows / foot) less than 2 2-4 5-8 9-15 16-30 Greater than 30 SPT (Blows / foot) 0-4 5-10 11-30 31-50 Greater than 50	PENETRATION TEST BORING LOCATION TION RESISTANCE IN BLOWS 1586 LEVATION IN FEET AT TIME OF DRILLING ETY HAMMER ETY HAMMER CONTENT Group Symbol on 0. 200 US STANDARD SIEVE CONTENT (%) %) SSIVE STRENGTH (tsf) TRENGTH (tsf)	Scole PEAT SAND WITH SHELLS WITH LIMESTONE LIMESTONE, SILTY LIMESTONE, LIMESTONE WITH SILT	AT BROCH LINE SALES IN A SALES IN



	06/23/20 R-9	DATE: 06/23/20 CHECKED BY: P.G.R. DATE:
		BORING LOCATION PLAN
	DA	M BEACH, PALM BEACH COUNTY, FLORIDA
J		
3	88	
3	87	
5	Be	N 54°45'54'' E 488.66' -
UT.	85	
E.	B4	GE TANKS
Ś	83	
S.	28	
g	IB.	
	# DNIHOR	B14
m		, m
		BUILDING (50° X 28')
		NEW GENERATOR BLDG
7		
32	DISCHARCE	
F	-2 ETHE Set 9-	
1	INTAGE	
Y		Line March
1	- The	BO FLIP TANKS
	A SHOW	
-		EXISTING CULVERT)
,Ph	T T T T	
p-		
	Ľ	×10 22 × B−1
	-15	
	CAN	B-11A
	IAL	72.84" V
		R
		on E 1 N 350 W WG VE TELES
S 35"14"0	T \$ 35	10 35.00 <sup>1</sup>



err سمعة: G-6A Pump Station West Palm Beach, Palm Beach County, F	SUBSUF	" GROUND SURFACE ELEVATION IN FEET	STANDARD PENETRATION RESISTANCE IN BLOWS PER FOOT (ASTM D-1586)					B.T.		3 - 50/5" - $50/5$ " -		$\begin{array}{cccccccccccccccccccccccccccccccccccc$		$ \begin{array}{c} 51 \\ \hline 2 \\ 4 \\ \hline \\ 4 \\ 4$	ĆME <sup>°</sup> 55X N N 18	EL. 13.01 FT. CME 55X 04/29/2020	FT. B-10	
Florida		ـــــــــــــــــــــــــــــــــــــ	- 45		- 35	- 30	25	20	-15	10		+0	 ភូ	+10	+15	- +20		
INDEX NO.	drawing no. B—10	50	U	40	UI	0	U	0	51	0	Ú	0	51	0	51	5	5	



هت G—6A Pump Station West Palm Beach, Palm Beach County,	™& SUBSURFACE PROFILES	WATER TABLE LEVEL AT TIME OF DRILLING	STANDARD PENETRATION RESISTANCE IN BLOWS PER FOOT (ASTM D-1586)					B.T.		50/5 <sup>°</sup> 4 $50/1$ <sup>°</sup> $$	35 32	50/1"					B-14 EL. 24.29 FT. 05/14/2020 CME 55X	
Florida		-4	- 4	-35	30	25	20	-15		I		ـــــــــــــــــــــــــــــــــــــ	- +10	+15	- +20	- +25	+30	
INDEX NO.	drawing no. B—11	4 5	40	ũ	0	U	0	U	0	U	0	U	0	U	0	0	0	

|--|

CLIENT:

LOCATION:

REMARKS:

## UNIVERSAL ENGINEERING SCIENCES **BORING LOG**

PROJECT NO .: 0630.2000012 REPORT NO .: 17223 PAGE: B-12

G-6A Pump Station PROJECT:

West Palm Beach
West Palm Beach, Florida
South Florida Water Management District

26.470577°, -80.447820°

SHEET: 1 of 1 B-1 BORING DESIGNATION: TOWNSHIP: SECTION: RANGE: G.S. ELEVATION (ft): -1 NAVD DATE STARTED: 6/17/20 WATER TABLE (ft): 6/19/20 0 DATE FINISHED: DATE OF READING: 6/17/2020 DRILLED BY: JW/CD/DZ EST. W.S.W.T. (ft): 0

TYPE OF SAMPLING: SPT

S DEPTH (FT)	BLOWS PER 6"	N (BLOWS/	W.T.	S Y M B	DESCRIPTION	-200	MC		RBERG 11TS	K (FT./	ORG. CONT
(FT.) P L E	INCREMENT	FT.)		Ö L		(%)	(%) (Term)	LL	PI	DAY)	(%)
0	/										
K	1-3-6-50/2"	9	•	70	Loose, muck [PT]						
_ 7	50/1"	50/1"		~	Very dense, limestone [GP]						
5	13-50/3"	50/3"			Very dense, gray capstone [GP]						
7	36-15-9-50/2'	24			Medium dense, sandy limestone [GP]						
10	50/3"	50/3"	•		Very dense						
	24-8-10-16	18			Medium dense						
7	21-10-5-4	15	•	-	Medium dense, limestone [GP]						
15 — X	5-8-12-8	20	•								
-12	5-50/5"	50/5"			Very dense, Limestone with silt [GP-GM]	10					
20	19-14-15-14	29			Medium dense						
-12	12-10-10-6	20									
-2	5/2"	50/2"		j.	Very dense, limestone [GP]						
25	6-19-5-32	24			Medium dense, sandy limestone [GP]						
	50/3"	50/3"			Very dense						
30	44-29-33-14	62									
	8-11-50/4"	50/4"			Very dense, limestone [GP]						
-2	50/5"	50/5"									
35	50/1"	50/1"									
->	12-7-5-8	12			Medium dense						
40	10-20-50/5"	50/5"			Very dense						
40-	21-60/5"	60/5"	•		Very dense, gray sand [SP]						
$\rightarrow$	6-5-6-85/3"	85/3"	•		Very dense, limestone [GP]						
45	50/5"	50/5"									
->	32-8-11-8	19			Medium dense, gray sand [SP]						
-		-			Soil boring terminated at 48 feet due to hole						
50 —			.		collapse						

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## UNIVERSAL ENGINEERING SCIENCES BORING LOG

 PROJECT NO.:
 0630.2000012

 REPORT NO.:
 17223

 PAGE:
 B-13

PROJECT: G-6A Pump Station West Palm Beach

West Palm Beach, Florida

 CLIENT:
 South Florida Water Management District

 LOCATION:
 26.470693°, -80.447879°

REMARKS:

BORING DESIGNATION: SECTION:	B-2 TOWNSHIF		ET: <b>1</b> GE:	of 1
G.S. ELEVATION (ft):	-1 NAVD	DATE STARTED:	6/16/	/20
WATER TABLE (ft):	0	DATE FINISHED:	6/17/	/20
DATE OF READING:	6/16/2020	DRILLED BY:	JW/0	CG/JD/CD/PG
EST. W.S.W.T. (ft):	0	TYPE OF SAMPLIN	G: SPT	

DEPTH M	BLOWS	N (BLOWS/	w.т.	S Y M B	DESCRIPTION	-200	MC (%)		RBERG IITS	K (FT./	ORG. CONT.
(FT.) F		FT.)		Ö L		(%)	(%) (Term)	LL	PI	DAY)	(%)
0			_▼_		_ Medium dense, muck [PT]						
	1-17-42-82/4										
5	14-24-47-10				Very dense, limerock [GP]						
	5-6-7-7	13		0	Very dense, silty sand with limestone [SM]						
1 7	6-43-55/2"	55/2"		0 0							
10-	5-27-57-44	84			Very dense, limestone [GP]	15					
1 7	50/3"	50/3"		•••							
$\downarrow$	5-8-11-20	19			Medium dense, sandy limestone [SP]						
	3-1-1-30	2			Very loose, silty limestone [GM]						
1 7	3-2-2-10	4		<b>Fer</b>	Loose						
20	55/3"	55/3"			Very dense, limestone [GP]						
1 7	42-15-10-22	25			Medium dense						
	3-24-30-50/3	" 54			Very dense						
25	30-55-8-10	63			- Dongo cilty limestono [CM]						
	6-7-26-52	33			Dense, silty limestone [GM]						
30	60/3"	60/3"			Very dense						
	40-54-20-20	74									
	9-8-6-28	14			Medium dense						
35-	38-50/2"	50/2"			Very dense						
	26-36-28-12	64			Very dense, gray stone with limestome [GP]						
40	12-9-9-15	18			Medium dense, sandy limestone [GP]						
	22-25-39-16	64			Very dense						
	6-8-9-10	17			Very dense, gray sand with some limestone [SP]						
45	9-38-50/2"	50/2"			Very dense, sandy limestone [GP]						
	14-24-31-23	55			_Very dense, limestone with sand [GP]						
50	18-29-28-30	57		0	Very dense, gray sand with some gravel [SP]						
					Soil boring terminated at 50 feet below the mudline.						

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LOCATION:

REMARKS:

## UNIVERSAL ENGINEERING SCIENCES **BORING LOG**

PROJECT NO .: 0630.2000012 REPORT NO .: 17223 PAGE: B-14

PROJECT:	G-6A Pump Station
	West Palm Beach
	West Palm Beach, Florida
CLIENT:	South Florida Water Management District

26.470098°, -80.447706°

BORING DESIGNATION	I: <b>B-3</b>		SHEET: RANGE:	1 of 1
SECTION.	TOWNSHI	Ρ.	RANGE:	
G.S. ELEVATION (ft):	+19' NAVD	DATE STARTE	D:	5/12/20
WATER TABLE (ft):	10.5	DATE FINISHE	ED:	5/13/20
DATE OF READING:	5/14/2020	DRILLED BY:		CG/JD/PG/J

EST. W.S.W.T. (ft): 8.5 TYPE OF SAMPLING: SPT

CG/JD/PG/JW/CD

DEPTH M (FT.) L		N (BLOWS/ FT.)	W.T.	S Y B U L	DESCRIPTION	-200 (%)	MC (%) (Term)	ATTEF LIN	RBERG ITS PI	K (FT./ DAY)	ORG. CONT. (%)
0											
+	16-36-22-12	58			Dense, limerock fill [SP]						
1 7	5-6-6-10	12			medium dense						
5	6-4-4-5	8			loose						
	12-8-8-6	16			medium dense						
10	4-4-3-3	7			loose						
	5-6-2-2	8									
	2-1-2-3	3			Very loose, muck [PT]		67				43
	20-12-50/45"	50/5"			Very dense, limestone with shell fragments [GP]						
	8-24-135	37			dense						
20	6-8-10-20	18			Medium dense, sandy limestone with trace silt [GP]						
	10-50/5"	50/5"			√Very dense, sandy limestone with silt [GP-GM]						
	7-13-7-6	20			Medium dense, limestone [GP]						
25	12-40-50/3"	50/3"			very dense						
	12-50-50/1"	50/1"			Very dense, limestone with cemented sand [GP]						
30	7-5-6-12	11			medium dense						
	5-5-5-7	10			Medium dense, limestone with trace shell fragments [GP]						
	50-50/1"	50/1"		° 0	Very dense, silty sand with some limestone [SM]						
35	5-8-12-24	20		0	medium dense	14					
	42-40-24-50/3	64		o							
40	50/2"	50/2"		0							
40	2:11 min/ft 5:18 min/ft				Limestone [GP] REC = 43"/60" = 72%						
	3:37 min/ft 4:54 min/ft				RQD = 32"/60" = 53%						
45	4:42 min/ft										
$\frac{1}{1}$	10-18-23-15	41			dense Medium dense, gray sand [SP]						
1/	8-8-50/2"	50/2"			Very dense, limestone [GP]						
50 —					SPT Soil Boring Terminated at 49 Feet.						
DL3											

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## UNIVERSAL ENGINEERING SCIENCES **BORING LOG**

PROJECT NO .: 0630.2000012 REPORT NO .: 17223 PAGE: B-15

PROJECT:	G-6A Pump Station
	West Palm Beach
	West Palm Beach, F

	West Palm Beach, Florida
CLIENT:	South Florida Water Management District
LOCATION:	26.470683°, -80.447322°

REMARKS:

BORING DESIGNATION SECTION:	I: <b>B-4</b> TOWNSHII	•	Sheet: Range:	1 of 1
G.S. ELEVATION (ft):	+19' NAVD	DATE STARTE	ED:	5/11/20
WATER TABLE (ft):	9.2	DATE FINISHE	D:	5/11/20
DATE OF READING:	5/11/2020	DRILLED BY:		CG/JD/PG/JW/CD
EST. W.S.W.T. (ft):	7.2	TYPE OF SAM	PLING:	SPT

DEPTH (FT.)	S A P L E	BLOWS PER 6" NCREMENT	N (BLOWS/ FT.)	W.T.	S Y B O L	DESCRIPTION	-200 (%)	MC (%) (Term)	ATTEF LIM LL	K (FT./ DAY)	ORG. CONT. (%)
0	$\square$	1-11-23-12 10-10-3-3	34 13			Dense to medium dense, limerock (FILL) [SP]					
5		4-3-2-2 3-7-2-2 4-3-2-7	5 9 5	 		Loose, limerock (FILL) with trace organics [SP]				 	
10 — - - -		3-1-1-1 1-1-1-5	2			Very loose, muck [PT]				 	
15 — - - -		3-1-50/4" 8-4-10-7 4-4-7-27	50/4" 14 11			Very dense, limestone with trace muck [GP] Very dense to medium dense, limestone with shell fragments and cemented sand [GP]				 	
20	$\square$		50/4" 50/2"		0	Very dense, silty sand with some limestone and shell fragments [SM] Very dense, limestone with shell fragments [GP]	16			 	
25 — - -	$\square$	50/1" 11-7-16-11 6-11-14-8	50/1" 23 25			Very dense to medium dense, limestone [GP]				 	
30 — - - -		30-50/2" 23-7-32-13	50/2" 39		0 0	Very dense to medium dense, sand with silt and some limestone with shell fragments [SP-SM]	12			 	
35	$\nabla$	13-9-12-8 6-8-50/5" 70/1"	21 50/5" 70/1"			Very dense, limestone [GP]				 	
40	$\mathbf{N}$	70/1 3-4-6-60/1" -51-37-50/5	10							 	
45 — - -		65/2" 13-11-13-3	65/2" 24			Medium dense, sandy limestone [GP]				 	
50 —		8-50/3"	50/3"			Very dense, limestone with trace silt [GP] SPT Soil Boring Terminated at 50 Feet.				 	
BL3											

				= R S	AL ENGINEERING		2	PR	OJECT I	NO.:	0630.20000	12
NV		U		_1\0	BORING LOG		RE	REPORT NO.: 17223				
					BORING LOG			PA	PAGE: B-16			
PROJECT:	G-6A Pump S West Palm Be West Palm Be	each	а			BORING DESIGNA SECTION:		<b>B-5</b> WNSHIP:		SHE RAN		of 1
CLIENT:	South Florida	Water Man	ageme	nt Distrie	ct	G.S. ELEVATION (ft): +16' NAVD DATE STARTED: 5/7/20						
LOCATION:	26.470437°, -8	30.448300°				WATER TABLE (ft):	7.9	DA	TE FINIS	SHED:	5/7/20	
REMARKS:						DATE OF READING	G: 5/7/20	)20 DR	RILLED B	Y:	CG/JD	/PG
						EST. W.S.W.T. (ft):	5.9	TY	PE OF S	AMPLIN	G: SPT	
DEPTH M (FT.)	BLOWS PER 6"	N (BLOWS/	W.Т.	S Y M B	DESCRIPTION		-200 (%)	MC (%)		RBERG 11TS	K (FT./	ORG. CONT.
	INCREMENT	FT.)		O L			(70)	(70) (Term)	LL	PI	DAY)	(%)
0	ļ			XXX								
	12-12-10-10	22			Medium dense to loose, limerock	(FILL) [SP]						
	7-7-3-6	10		$\bigotimes$								
5	5-6-8-12	14		$\bigotimes$								
	13-5-4-3	9		$\bigotimes$								
10	2-2-2-2	4			Loose to very loose, peat [PT]			47				76.3
	1-1-2-3	3										
	7-20-50/1"	50/1"			Very dense to dense, limestone [0	GP1						
15 - 1	20-27-10-30	37										
	10-6-9-50/5"			0	Brown sand [SP]							
20	25-55-10-10			0	Medium dense to very dense, silty limestone [SM]	' sand with						
	25-25-30-50/C	" 55		0			14					
	50/3"	50/3"		0 0								
25 — X	8-21-6-5	27	1				• • • • • • • • • • • • •			1		

_	∕2/25-25-30-50/0	" 55	0		14			
_	50/3"	50/3"	0					
25 —	8-21-6-5	27	 0			 	 	
-	3-3-2-1	5	° 0					
 30 —	3-4-16-12	20	 0			 	 	
-	3-3-10-28	13	° 0	Medium dense, sand with some limestone [SP]	2			
	X 3-8-16-24 50-/1"	24 50/1"		Very dense, limestone [GP]		 		
	7:35 min/ft 5:18 min/ft 6:37 min/ft			REC = 20"/60" = 77%				
40 —	7:07 min/ft			RQD = 8"/60" = 50%				
40 -	16-50-50/1"	50/1"						
-	X 14-16-20-12	36		Dense, sandy limestone [GP]				
45—	12-16-10-50/5	" 26		Medium dense to very dense, limestone [GP]		 	 	
_	50/3"	50/3"						
 50 —	50/3"	50/3"				 		
50				SPT Soil Boring Terminated at 50 Feet.				

BL3

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## UNIVERSAL ENGINEERING SCIENCES BORING LOG

 PROJECT NO.:
 0630.2000012

 REPORT NO.:
 17223

 PAGE:
 B-17

PROJECT:	G-6A Pump Station
	West Palm Beach
	West Palm Beach, Florida
CLIENT:	South Florida Water Mana

 CLIENT:
 South Florida Water Management District

 LOCATION:
 26.471028°, -80.447900°

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REMARKS:

BORING DESIGNATION SECTION:	N: <b>B-</b> TOWNSH	•	SHEET: RANGE:	1 of 1
G.S. ELEVATION (ft):	+15' NAVD	DATE STARTE	ED:	5/6/20
WATER TABLE (ft):	7.5	DATE FINISHE	ED:	5/7/20
DATE OF READING:	5/7/2020	DRILLED BY:		CG/JD/PG
EST. W.S.W.T. (ft):	5.5	TYPE OF SAM	IPLING:	SPT

DEPTH	S A BLOW P PER 6	5"	N (BLOWS/	W.T.	S Y M B	DESCRIPTION	-200	MC (%)		RBERG IITS	K (FT./	ORG. CONT.
	L INCREM	ENT	FT.)		ŌL		(%)	(Term)	LL	PI	DAY)	(%)
0	17-11-1 5-7-6		21 13			Medium dense to loose, limerock (FILL) [SP]						
5	3-3-3	-3	6									
	2-2-1- 1-1-1-		3 2	<b>_</b>		Very loose, peat [PT]						
10	5-12-8	-12	20			Medium dense to very dense, sandy limestone [GP]						
15 — - - -	12-24-26 0:34 m 4:14 m 5:21 m 13:35 m 10:01 m	in/ft in/ft in/ft nin/ft				Limestone [GP] REC = 20"/60" = 47% RQD = 8"/60" = 30%	-					
20-	4-12-16		28		° 0	Medium.dense, silty sand with limestone.[SM]	13					
	× 8-5-6 1-2-2-		11 4		0	Loose, sandy limestone with shell fragments [GP]	-					
25	10-3-3		6									
+ - +	3-19-16		35		° 0	Dense to very dense, silty sand with limestone and shell fragments [SM]	16					
30 —	50/1	w	50/1"		0							
7	10-13-1		26		0							
35 -	×3-2-26-5 50/5		28 50/5"		0							
+	4-8-20		28		. o . O							
40	12-16-9		25		0							
-	50/5		50/5"		0 0							
45	3-4-6	-8	10		0							
	50/1 16-50/		50/1" 50/1"		° 0							
50 —		•				SPT Soil Boring Terminated at 49 Feet.						

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# UNIVERSAL ENGINEERING SCIENCES **BORING LOG**

PROJECT NO .: 0630.2000012 REPORT NO .: 17223 PAGE: B-18

PROJECT: G-6A Pump Station West Palm Beach West Palm Beach, Florida С

CLIENT:	South Florida Water Management District
LOCATION:	26.469061°, -80.448419°

REMARKS:

BORING DESIGNATION SECTION:	N: <b>B-</b> TOWNSHI	•	Sheet: Range:	
G.S. ELEVATION (ft):	+19' NAVD	DATE STARTE	ED:	4/28/20
WATER TABLE (ft):	8.8	DATE FINISHE	ED:	4/28/20
DATE OF READING:	4/28/2020	DRILLED BY:		CG/JD
EST. W.S.W.T. (ft):	6.8	TYPE OF SAM	IPLING:	SPT

DEPTH (FT.) E BLOWS PER 6" INCREMENT	N (BLOWS/ \ FT.)	W.T. B O L	DESCRIPTION	-200 (%)	MC (%) (Term)	ATTER LIM LL		K (FT./ DAY)	ORG. CONT. (%)
(F1.) L INCREMENT 0 22-20-15-13 10-10-10-10 5 8-8-7-7 5-5-3-5 10 1-1-2-2 1-1-7-60/2" 15 16-25-60/3" 24-14-11-14 7.5.7.0	FT.) 35 20 15 8 7 3 7 60/3"		Silty Limerock (FILL) [SM] dense medium dense Loose, gray limestone [GP] Very loose to loose, peat [PT] Very dense, silty limestone [GM] Medium dense, sandy limestone with trace silt [GM]	(%) 19 23	(%) (Term) 11 83 35 35 35		PI		
20 10-70/3" 100/6" 25 37-8-70/2" 6-17-34-38 30 17-12-10-36	70/3" 100/6" 70/2" 51		very dense Very dense, sandy limestone with silt [GP-GM] medium dense SPT Soil Boring Terminated at 30 Feet.						



LOCATION:

REMARKS:

# UNIVERSAL ENGINEERING SCIENCES **BORING LOG**

PROJECT NO .: 0630.2000012 REPORT NO .: 17223 PAGE: B-19

G PROJECT: W W

G-6A Pump Station
West Palm Beach
West Palm Beach, Florida
South Florida Water Management District

26.469387°, -80.449002°

SHEET: 1 of 1 **B-8** BORING DESIGNATION: SECTION: TOWNSHIP: RANGE: G.S. ELEVATION (ft): +16.5' NAVD DATE STARTED: 4/27/20 WATER TABLE (ft): 7.5 DATE FINISHED: 4/27/20 DATE OF READING: 4/27/2020 DRILLED BY:

EST. W.S.W.T. (ft): 5.5

CG/JD TYPE OF SAMPLING: SPT

	DEPTH (FT.)	S A M P	BLOWS PER 6"	N (BLOWS/	W.T.	S Y M B O	DESCRIPTION	-200 (%)	MC (%)	ATTEF	RBERG ITS	K (FT./	ORG. CONT.
	( )	L E	INCREMENT	FT.)		O L			(Ťerm)	LL	PI	DAY)	(%)
	0 —	X	21-24-30-18	54		о Л	Very dense, gray silty sand with shell fragmentsand gravel [SM]						
	_		7-9-7-11	16			Medium dense, silty limerock (FILL) [SM]	17	14				
	5	X	17-11-6-10	17									
	-	X	5-4-8-8	12	⊻								
	10 —	X	7-3-3-3	6									
		М	2-3-4-7	7			Loose, dark brown muck [PT]		25				28.9
	_	Д	2-8-24-17	32		° 0	Dense to medium dense, gray sand with silt and						
	15	X	4-14-10-25	24		0	limestone [SP-SM]	12					
	-	Д	8-10-11-10	21		° 0	Medium dense to very dense, gray silty sand with limestone [SM]	17	19				
	20 —	Д	100/5"	100/5"		0							
	_	Д	110/1"	110/1"		0 0							
	-	Д	55-83-50/1"	50/1"		0							
	25 —	X	7-25-23-12	48		0							
	_	Å	12-7-7-8	14		0	Dense, gray sandy limestone with shell						
		Д	11-20-16-18	36			fragments [GP]						
							SPT Soil Boring Terminated at 30 Feet.						
BL3													



LOCATION:

REMARKS:

# UNIVERSAL ENGINEERING SCIENCES **BORING LOG**

PROJECT NO .: 0630.2000012 REPORT NO .: 17223 PAGE: B-20

RANGE:

PROJECT: G-6A Pump Station

West Palm Beach
West Palm Beach, Florida
South Florida Water Management District

26.471692°, -80.446720°

SECTION: TOWNSHIP: G.S. ELEVATION (ft): +13.01' NAVDDATE STARTED: WATER TABLE (ft): 4.0 DATE OF READING:

BORING DESIGNATION:

DATE FINISHED: 4/29/2020 DRILLED BY:

**B-9** 

4/29/20 CG/JD/PG

4/29/20

SHEET: 1 of 1

EST. W.S.W.T. (ft): 2.0 Т

TYPE OF SAMPLING: SPT

DEPTH (FT.)	S A M P L E	BLOWS PER 6" INCREMENT	N (BLOWS/ FT.)	W.T.	SY MBOL	DESCRIPTION	-200 (%)	MC (%) (Term)	RBERG IITS PI	K (FT./ DAY)	ORG. CONT. (%)
(FT.) 0 - - 5 - - - - - - - - - - - - - -		7-24-27-23 4-2-2-3 2-1-1-2 1-1-1-2 5-12-17-44 5-17-40-45 5-5-7-100/5"	FT.) 51 4 2 2 29 57		ВО L	Very dense, silty limerock (FILL) [SM] Loose to very loose, peat [PT] Medium dense, very dense to medium dense, silty sand with limestone [SM]	(%) 16 15	(%) (Term) 7 67	 PI		
15	N A	9:22 min/ft 10:12 min/ft 9:57 min/ft 5:58 min/ft 5:04 min/ft 6-8-12-12 4-6-5-6 1-2-1-50/4" 60/3" 17-30-23-50 22-24-40-27	20 11 3 60/3" 53			Limestone [GP] REC = 51"/60" = 85% RQD = 36"/60" = 60% Medium dense, sandy limestone with shell fragments [GP] Medium dense to very dense, silty limestone with sand [GM]	24	15	 		
BL3											

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REMARKS:

# UNIVERSAL ENGINEERING SCIENCES **BORING LOG**

PROJECT NO .: 0630.2000012 REPORT NO .: 17223 PAGE: B-21

G-6A Pump Station PROJECT:

	West Palm Beach West Palm Beach, Florida
CLIENT:	South Florida Water Management District
LOCATION:	26.471916°, -80.447574°

## SECTION: G.S. ELEVATION (ft): +15.29' NAVDDATE STARTED: 6.7

BORING DESIGNATION:

TOWNSHIP:

**B-10** 

SHEET: 1 of 1 RANGE:

4/30/20

WATER TABLE (ft): DATE OF READING: EST. W.S.W.T. (ft):

DATE FINISHED: 5/1/2020 DRILLED BY:

5/1/20 CG/JD/PG

TYPE OF SAMPLING: SPT 4.7

		S A M P L E	BLOWS PER 6" INCREMENT	N (BLOWS/ FT.)	W.T.	S Y B O -	DESCRIPTION	-200 (%)	MC (%) (Term)	RBERG IITS PI	K (FT./ DAY)	ORG. CONT. (%)
_		-				L.						
	0		14-15-3-3 5-6-6-5	18 12			Medium dense, silty limerock (FILL) [SM]	18	14			
	5 —	XII	2-5-5-5	10			Loose, limerock (FILL) [SP-SM]	10	11	 		
	_		5-2-2-3	4	┸		Loose to very loose, peat [PT]	-	96			82.4
	_	$\overline{\mathbf{A}}$										02.4
	10 —	$\frac{1}{2}$	1-1-1-2	2			Medium dense, sandy limestone with shell			 		
	_	Ą٩	8-4-17-64/2"	21			fragments [GP]					
	_	Д	13-7-3-3	10				-				
	15 —	XII	3-4-7-6	11		0	Medium dense to very dense, silty sand with			 		
	-	X	4-27-26-44	53		0	limestone [SM]					
	_	$\overline{}$	5-7-50-50/1"			0		18				
	20 —		7:22 min/ft	57				1 10		 		
	-	Н	6:46 min/ft 4:14 min/ft				REC = 33"/60" = 55%					
			3:22 min/ft 1:44 min/ft				RQD = 20"/60" = 33%					
	25	$\backslash A$	27-44-46-50	90			RQD = 20'760" = 33% Very dense to medium dense, sandy limestone with shell fragments [GP]			 		
	_						with shell fragments [GP]					
	_	$\ominus$	50/5"	50/5"								
	30 —	<u> </u>	27-14-10-40	24			Call basis a terminate of at 24 fact			 		
							Soil boring terminated at 31 feet					
_												
BLS												

			630.2000012 7223	
	BORING LOG	PAGE: B-22		
PROJECT:	G-6A Pump Station West Palm Beach West Palm Beach, Florida	BORING DESIGNATION: B- SECTION: TOWNSH		
CLIENT:	South Florida Water Management District	G.S. ELEVATION (ft): +16' NAVD	DATE STARTED:	5/4/20
LOCATION:	26.472603°, -80.446750°	WATER TABLE (ft): 4.6	DATE FINISHED:	5/4/20
REMARKS:		DATE OF READING: 5/4/2020	DRILLED BY:	CG/JD/PG
		EST. W.S.W.T. (ft): 2.6	TYPE OF SAMPLING	: SPT
DEPTH M (FT.) L E	BLOWS N PER 6" (BLOWS/ W.T. B INCREMENT FT.) W.T. B O L	-200 M0 (%) (% (Tei	)	K ORG. (FT./ CONT. DAY) (%)

· ·.,	PER 6"	(BLOWS/ FT.)		B	DESCRIPTION	(%)	(%) (Term)	LL	PI	(FT./ DAY)	C
	E			L			()	LL	PI		
0											
-	X 1-4-7-17	11		$\bigotimes$	Medium dense to dense, silty limerock (FILL)						
1				$\bigotimes$	[SM]		•				
	24-27-20-10	47				20	8				
5 —	4-3-2-2	5			Loose, peat [PT]						
1	$\overline{\mathcal{A}}$										
	2-2-2-2	4					188				'
	2-2-3-6	5			Loose, silty limestone [GM]						
10	4-7-3-7	40				20	22				
	4-7-3-7	10				20	22				
	∑ 20-6-15-10	21			Medium dense, sandy limestone [GP]						
15 —	60-50/0"	50/0"			Limestone with intermittent sandy limestone [GP]						
-	<ul> <li>7:17 min/ft</li> <li>7:04 min/ft</li> </ul>				REC = 20"/60" = 33%						
_	12:54 min/ft										
_	- 44:54 min/ft			+++	RQD = 8"/60" = 13%						
20	4:50 min/ft			0							.
1	5-5-8-10	13		0	Medium dense to loose, sand with silt and						
-	4-5-2-1	7		0	limestone [SP-SM]	11					
~ +	$\overline{A}$			2							
25	2-5-50-55	55			Very dense to medium dense, sandy limestone						
-)	13-9-6-7	15			with some trace silt [GP]						
1	$\overline{\}$	-									
30	4-5-5-10	10			Loose, sandy limestone [GP]						
-	10-60/3"	60/3"			Gray sand [SP]	11	19				
1	$\overline{\ }$				Very dense, limestone with silt [GP-GM]						
+	<u>^</u> 27-55-30-50/3	" 85			_Gray sand [SP]						
35 —	X10-16-30-50/3	" 46			Very dense, limestone [GP]						
-	50/3"	50/3"									
+	$\overline{}$	30/3			Limestone with silt [GP-GM]						
40	5-40-30-26	70		0	Very dense to dense, silty sand with limestone						
-	X 24-20-20-12	40		0	[SM]	19					
Ť	$\overline{}$					10					
7	70/3"	70/3"		+ + + + + + + + + + + + + + + + + + +	Very dense, limestone [GP]						
45	50/1"	50/1"									
1	$\overline{\mathcal{A}}$				Madium dance from the second sec						
	7-6-7-10	13			Medium dense to very dense, sandy limestone with shell fragments [GP]						
50	10-50/5"	50/5"		[ ] ]							
JU	3-2-10-10	12		ГЦ							
+	$\overline{\mathcal{A}}$	12									
7	∐ 8-20-50/0"	50/0"		0	Very dense, sand with limestone [SP]						
55	42-6-4-6	10		Ω	Loose to medium dense, light gray sand with						
	$\overline{\mathcal{A}}$				shell fragments [SP]						
7	5-5-6-8	11			- · · ·						
	6-8-15-23	23									
60 -	1		• • • • • • • •		SPT Soil Boring Terminated at 60 Feet.						
					-						1



# UNIVERSAL ENGINEERING SCIENCES BORING LOG

 PROJECT NO.:
 0630.2000012

 REPORT NO.:
 17223

 PAGE:
 B-23

PROJECT: G-6A Pump Station West Palm Beach West Palm Beach

West Palm Beach
West Palm Beach, Florida
South Florida Water Management District

CLIENT: South Florida Water Mana LOCATION: 26.472678\*, -80.496936\*

REMARKS:

BORING DESIGNATION SECTION:	I: <b>B-'</b> TOWNSHI	11a P:	SHEET: RANGE:	1 of 2
G.S. ELEVATION (ft):	+14' NAVD	DATE STARTE	ED:	5/18/20
WATER TABLE (ft):	8.4	DATE FINISHE	ED:	5/22/20
DATE OF READING:	5/18/2020	DRILLED BY:		CG/JD/PG
EST. W.S.W.T. (ft):	6.4	TYPE OF SAM	IPLING:	SPT

	INCREMENT 9-35-40-42 22-19-13-6 2-2-3-3 2-3-4-4 2-2-3-3 4-3-3-2 2-1-1-1 1-2-1-1 1-1-7-50/3" 50/3"	FT.) 75 32 5 7 5 6 2 3 8 50/3"	 		Very dense to dense, limerock (FILL) [SP] Loose, limerock (FILL) with muck [SP-PT] Loose, limerock (FILL) with trace muck [SP] Loose, limerock (FILL) [SP] Loose to very loose, peat [PT]	(%)	(%) (Term)	 PI	DAY)	(%)
	22-19-13-6 2-2-3-3 2-3-4-4 2-2-3-3 4-3-3-2 2-1-1-1 1-2-1-1 1-1-7-50/3" 50/3"	32 5 7 5 6 2 3 8			Loose, limerock (FILL) with muck [SP-PT] Loose, limerock (FILL) with trace muck [SP] Loose, limerock (FILL) [SP]			 		
	22-19-13-6 2-2-3-3 2-3-4-4 2-2-3-3 4-3-3-2 2-1-1-1 1-2-1-1 1-1-7-50/3" 50/3"	32 5 7 5 6 2 3 8			Loose, limerock (FILL) with muck [SP-PT] Loose, limerock (FILL) with trace muck [SP] Loose, limerock (FILL) [SP]			 		
	2-2-3-3 2-3-4-4 2-2-3-3 4-3-3-2 2-1-1-1 1-2-1-1 1-1-7-50/3" 50/3"	5 7 5 6 2 3 8			Loose, limerock (FILL) with trace muck [SP] Loose, limerock (FILL) [SP]			 		
15 1	2-2-3-3 4-3-3-2 2-1-1-1 1-2-1-1 1-1-7-50/3" 50/3"	5 6 2 3 8			Loose, limerock (FILL) [SP]			 		
15 1	4-3-3-2 2-1-1-1 1-2-1-1 1-1-7-50/3" 50/3"	6 2 3 8	· · · · · · · · · · · · · · · · · · ·					 		
15 1	2-1-1-1 1-2-1-1 1-1-7-50/3" 50/3"	2 3 8			Loose to very loose, peat [PT]					
	1-2-1-1 1-1-7-50/3" 50/3"	3 8								
	1-1-7-50/3" 50/3"	8								
	50/3"				Very loose, muck with some limestone [PT]			 		
20		50/3"			Loose, limestone with some muck [GP]					
	50-50/0"	~~~~~			Very dense, limestone [GP]			 		
	1	50/0"								
	4-14-5-2	19			Medium dense, silty limestone with cemented sands [GM]	15				
25 - 25	9-16-8-8	24			→ Medium dense, silty limestone with cemented → → → sands [SM]			 		
	12-50/3"	50/3"			Very dense to medium dense, silty limestone					
30	50/2"	50/2"			[GM]			 		
	4-6-6-15	12								
-	50/3"	50/3"								
35 - 2	28-26-30-36	56						 		
	16-12-12-13	24								
	50-50/3"	50/0"								
	1:02 min/ft 3:55 min/ft				REC = 12"/60" = 20%			 		
2	2:36 min/ft				RQD = 9''/60'' = 15%					
15 <u> </u>	0:21 min/ft 1:24 min/ft				RQD - 9700 - 13%			 		
	2:53 min/ft 1:47 min/ft				REC = 29"/60" = 48%					
	2:08 min/ft 0:01 min/ft				RQD = 23"/60" = 38%					
	0:02 min/ft							 		
	2-2-3-5	5		0	Medium dense, gray sand with some limestone					
	20-20-10-7	30		0	_and trace silt [SP]					
55 - X	3-3-6-8	9			Loose to medium dense, gray sand with some shell fragments [SP]					
1	50/5"	50/5"								
60	8-12-6-6	18						 		
1\/1	8-10-15-18	25								



# UNIVERSAL ENGINEERING SCIENCES BORING LOG

 PROJECT NO.:
 0630.2000012

 REPORT NO.:
 17223

B-24

PAGE:

PROJECT:

G-6A Pump Station West Palm Beach West Palm Beach, Florida BORING DESIGNATION: B-11a SHEET: 2 of 2 SECTION: TOWNSHIP: RANGE:

S ATTERBERG A M P BLOWS Ν κ ORG. M B O DEPTH -200 MC LIMITS W.T. **PER 6**" (BLOWS/ DESCRIPTION (FT./ CONT. (%) (Term) (FT.) (%) INCREMENT FT.) DAY) (%) E LL ΡI 8-12-14-18 26 Medium dense, gray sand with trace shell fragments [SP] 65 6-6-8-10 14 Loose, gray sand with some gravel and trace shell fragments [SP] 4-5-4-4 9 Loose, gray sand with trace gravel and shell 3-2-4-6 fragments [SP] 6 70 Very loose, gray sand with shell fragments and trace silt [SP] 3 1-1-2-2 Loose, gray sand and shell fragments with some 3-5-5-5 10 gravel and silt [SP] 75 10-27-12-12 29 0 Medium dense, dark gray sand with some gravel [SP] 8-13-20-20 33 8-16-27-37 43 Dense to medium dense, gray sand [SP] 80 20-20-26-26 46 8-12-16-22 28 Dense, gray sand with shell fragments [SP] 85 8-17-15-17 32 Dense, gray sand [SP] 16-18-16-18 Dense to medium dense, gray sand with some 34 shell fragments [SP] 8-8-10-20 18 90 7-7-14-26 Medium dense to dense, gray sand [SP] 21 6-17-27-29 44 95 10-14-17-12 31 Dense to medium dense, gray sand with some shell fragments [SP] 5-7-10-16 17 Dense, gray sand with gravel and trace shell 0 12-20-30-20 50 fragments [SP] 100 SPT Soil Boring Terminated at 100 Feet.

	UNIVERSAL ENGINEERING BORING LOG	PROJECT NO.:         0630.2000012           REPORT NO.:         17223					
			PAGE: B-2	25			
PROJECT:	G-6A Pump Station West Palm Beach West Palm Beach, Florida	BORING DESIGNATION: <b>B</b> - SECTION: TOWNSH					
CLIENT:	South Florida Water Management District	G.S. ELEVATION (ft): +16.22' NAV	DDATE STARTED:	5/5/20			
LOCATION:	26.472832°, -80.446883°	WATER TABLE (ft): 4.4	DATE FINISHED:	5/6/20			
REMARKS:		DATE OF READING: 5/6/2020	DRILLED BY:	CG/JD/PG			
		EST. W.S.W.T. (ft): 2.4	TYPE OF SAMPLING:	SPT			
DEPTH M (FT.) L	BLOWS N Y PER 6" (BLOWS/ W.T. B DESCRIPTION	-200 MG (%) (%		K ORG. (FT./ CONT. DAY) (%)			

EPTH M (FT.) P	PER 6" INCREMENT	(BLOWS/ FT.)	W.T.	B O	DESCRIPTION	-200 (%)	MC (%)		S (FT./	CON <sup>-</sup> (%)
Ē				Ľ			(Ťerm)	LL	PI	(70)
0				XXX	\Topsoil /					
14	12-22-44-20	66		$\bigotimes$	Very dense, limerock (FILL) [SP]					
-12	12-7-6-3	13	▁		Loose, peat [PT]	1				
5 - X	1-2-1-2	3								
- >	1-2-7-7	9					83			20.
10	5-7-20-50/2"	27			Medium dense, limestone [GP]					
	12-44-40-25	84		° 0	Very dense, gray silty sand with limestone and	16				
- >	5-7-12-36	19		0	shell fragments [SM]					
15 - X	60/2"	60/2"		0						
-1	50-60-56-35				Very dense, sandy limestone [GP]	-				
	1					1				
20	50/2"	50/2"			Very dense to dense, limestone [GP]					
$\mathcal{H}$	7-27-6-5	33								
	5-16-10-16	26 50/0"			Medium dense to very dense, sandy limestone [GP]					
25	6:14 min/ft 4:14 min/ft				REC = 35"/60" = 58%	-				
	0:41 min/ft									
30	8:17 min/ft 1:59 min/ft				RQD = 29"/60" = 48%					
	7:15 min/ft 2:13 min/ft				REC = 24"/60" = 40%					
_	0:42 min/ft 1:23 min/ft				RQD = 22"/60" = 33%					
35 -	5:28 min/ft					4				
-12	6-50/2"	50/2"		° 0	Very dense to medium dense, silty sand with limestone [SM]					
-12	7-12-50/4"	50/4"		0						
40-X	14-35-14-10	49		0		17				
-	2-2-10-14	12		0		14	21			
-1	15-50/12"	50/12"		0						
45	1			0 0						
£	16-15-13-13			0						
50 - X	5-3-2-5	5								
	31-30-10-9	40		0						
14	6-6-50/2"	50/2"		. 0						
55	4-11-25-13	36		0		<b>.</b>				
	8-5-3-2	8			Loose to medium dense, gray sand with shell fragments and trace limestone [SP]					
- >	2-3-5-6	8			- • •	4	22			
60 - X	5-12-13-13	25								
F					SPT Soil Boring Terminated at 61 Feet.	1				

|--|

LOCATION:

REMARKS:

# UNIVERSAL ENGINEERING SCIENCES **BORING LOG**

PROJECT NO .: 0630.2000012 REPORT NO .: 17223 PAGE: B-26

PROJECT: G-6A Pump Station West Palm Beach West Palm Beach, Florida

South Florida Water Management District

26.471598°, -80.446142°

BORING DESIGNATION:
SECTION:

B-13 TOWNSHIP:

SHEET: 1 of 1 RANGE:

5/13/20

5/13/20

G.S. ELEVATION (ft): WATER TABLE (ft): DATE OF READING:

+26.38' NAVDDATE STARTED: 12.0 DATE FINISHED: 5/14/2020

DRILLED BY:

EST. W.S.W.T. (ft): 10.0

TYPE OF SAMPLING: SPT

CG/JD/PG/JW/CD

DEPTH M (FT.)	BLOWS PER 6" INCREMENT	N (BLOWS/ FT.)	W.T.	S Y B O	DESCRIPTION	-200 (%)	MC (%)		ITS	K (FT./ DAY)	ORG. CONT. (%)
L E		,		L			(Ťerm)	LL	PI	DAT	(70)
0	9-16-14-12 9-9-12-12	30 21			Asphalt 1 3/8" thick Dense, limerock (FILL) [SP] Medium dense, brown sand [SP]						
5	9-10-6-5	16									
	4-6-12-8	18			Medium dense, limerock (FILL) with trace silt [SP]						
10	17-17-11-15	28		XXX	$\mathcal{T}_{muck [GP]}^{Medium dense, limerock fill with trace silt and }$						
	12-22-34-30 17-17-30-30	56 4			Very dense, limerock (FILL) [SP] dense						
15 - X	14-18-14-17	32		° 0	Dense, silty sand with some limestone and trace shell fragments [SM]	18					
	11-7-4-4	11			Medium dense, peat [PT]		27				58.2
20	3-3-3-12	6			loose		52				34.7
	3-4-70/3"	70/3"			Very dense, limestone with some silt [GP] SPT Soil Boring Terminated at 21 Feet.						
21											



LOCATION:

REMARKS:

# UNIVERSAL ENGINEERING SCIENCES **BORING LOG**

PROJECT NO .: 0630.2000012 REPORT NO .: 17223 PAGE: B-27

PROJECT: G-6A Pump Station V

West Palm Beach
West Palm Beach, Florida
South Florida Water Management District

26.471105°, -80.445946°

12.5

G.S. ELEVATION (ft): WATER TABLE (ft): DATE OF READING: EST. W.S.W.T. (ft):

+24.29' NAVDDATE STARTED: DATE FINISHED: 5/14/2020 DRILLED BY:

5/14/20 CG/JD/PG

5/14/20

TYPE OF SAMPLING: SPT 10.5

	DEPTH (FT.)	S A M P L E	BLOWS PER 6" INCREMENT	N (BLOWS/ FT.)	W.T.	S Y M B O L	DESCRIPTION	-200 (%)	MC (%) (Term)	ATTEF LIM	RBERG ITS PI	K (FT./ DAY)	ORG. CONT. (%)
	0	X	2-10-7-4 5-6-6-7	17 12		0 0	Medium dense, gray sand with gravel and trace organics [SP]						
	5		6-8-10-7 10-9-10-8	18 19			Medium dense, limerock (FILL) [SP] Medium dense, limerock (FILL) with trace peat						
	- - 10	Ø	7-8-7-10	15	· <u>· ·</u> · ·		[SP] Medium dense to loose, limerock (FILL) [SP]						
	-		6-4-2-2 /OH-WOH-2-	6 32	<b>_</b>		_Silty sand [SM]	30	33				
	15 — - -		7-7-6-3 WOH-1-2-2	13 3			Medium dense, silty limerock (FILL) [SM] Very loose to loose, peat [PT]		47				36.7
	- - 20 —		4-4-3-7	7			Muck and silt [PT]		67				58.9
	-	X	WOH-1-50/1 3-15-20-6	50/1" 35			Very dense to dense, limestone with cemented sand [GP]						
	25—		7-20-12-50/1' 50/5"	32 50/5"			Dense, sandy limestone [GP] Very dense, limestone with shell fragments [GP]						
	- - 30 —		24-50/1"	50/5 50/1"									
	-	Å	2-1-2-2 2-12-22-6	3 34		0 0	Very loose to very dense, silty sand with some limestone [SM]	14					
	35 —	X	4-6-50/5"	50/5"		0	SPT Soil Boring Terminated at 36 Feet.						
BL3													



DESCRIPTION

**SYMBOL** 

# **KEY TO BORING LOGS**

## SYMBOLS AND ABBREVIATIONS

<u></u>	
N-Value	No. of Blows of a 140-lb. Weight Falling 30 Inches Required to Drive a Standard Spoon 1 Foot
WOR	Weight of Drill Rods
WOH	Weight of Drill Rods and Hammer
Þ	Sample from Auger Cuttings
$\square$	Standard Penetration Test Sample
	Thin-wall Shelby Tube Sample (Undisturbed Sampler Used)
RQD	Rock Quality Designation
	Stabilized Groundwater Level
$\overline{\nabla}$	Seasonal High Groundwater Level (also referred to as the W.S.W.T.)
NE	Not Encountered
GNE	Groundwater Not Encountered
BT	Boring Terminated
-200 (%)	Fines Content or % Passing No. 200 Sieve
MC (%)	Moisture Content
LL	Liquid Limit (Atterberg Limits Test)
PI	Plasticity Index (Atterberg Limits Test)
NP	Non-Plastic (Atterberg Limits Test)
К	Coefficient of Permeability
Org. Cont.	Organic Content
G.S. Elevation	Ground Surface Elevation

### **RELATIVE DENSITY**

(Sands and Gravels) Very loose – Less than 4 Blow/Foot Loose – 4 to 10 Blows/Foot Medium Dense – 11 to 30 Blows/Foot Dense – 31 to 50 Blows/Foot Very Dense – More than 50 Blows/Foot

### CONSISTENCY

(Silts and Clays) Very Soft – Less than 2 Blows/Foot Soft – 2 to 4 Blows/Foot Firm – 5 to 8 Blows/Foot Stiff – 9 to 15 Blows/Foot Very Stiff – 16 to 30 Blows/Foot Hard – More than 30 Blows/Foot

### **RELATIVE HARDNESS**

(Limestone) Soft – 100 Blows for more than 2 Inches Hard – 100 Blows for less than 2 Inches

			GROUP	
	MAJOR DIVIS	SIONS	SYMBOLS	TYPICAL NAMES
eve*	GRAVELS	CLEAN	GW	Well-graded gravels and gravel- sand mixtures, little or no fines
COARSE GRAINED SOILS More than 50% retained on the No. 200 sieve*	50% or more of coarse	GRAVELS	GP	Poorly graded gravels and gravel-sand mixtures, little or no fines
o SOIL ne No.	fraction retained on	GRAVELS	GM	Silty gravels and gravel-sand- silt mixtures
COARSE GRAINED SOILS 150% retained on the No. 2	No. 4 sieve	WITH FINES	GC	Clayey gravels and gravel- sand-clay mixtures
sE GR/ etaine	SANDS	CLEAN SANDS 5% or less	SW**	Well-graded sands and gravelly sands, little or no fines
OARS 50% r	More than 50% of coarse	passing No. 200 sieve	SP**	Poorly graded sands and gravelly sands, little or no fines
C than	fraction passes No.	SANDS with 12% or more	SM**	Silty sands, sand-silt mixtures
More	4 sieve	passing No. 200 sieve	SC**	Clayey sands, sand-clay mixtures
ł			ML	Inorganic silts, very fine sands, rock flour, silty or clayey fine sands
s 00 sieve*	Liqu	ND CLAYS id limit or less	CL	Inorganic clays of low to medium plasticity, gravelly clays, sandy clays, lean clays
SOILS No. 2(			OL	Organic silts and organic silty clays of low plasticity
FINE-GRAINED SOILS 50% or more passes the No. 200 sieve*				Inorganic silts, micaceous or diamicaceous fine sands or silts, elastic silts
FINE-G more pa	Liqu	ND CLAYS id limit	СН	Inorganic clays or clays of high plasticity, fat clays
50% or	greater	than 50%	ОН	Organic clays of medium to high plasticity
			PT	Peat, muck and other highly organic soils
*Based		ial passing the		m) sieve

\*\* Use dual symbol (such as SP-SM and SP-SC) for soils with more than 5% but less than 12% passing the No. 200 sieve

### **MODIFIERS**

These modifiers Provide Our Estimate of the Amount of Minor Constituents (Silt or Clay Size Particles) in the Soil Sample Trace – 5% or less With Silt or With Clay – 6% to 11% Silty or Clayey – 12% to 30% Very Silty or Very Clayey – 31% to 50%

These Modifiers Provide Our Estimate of the Amount of Organic Components in the Soil Sample Trace – Less than 3% Few – 3% to 4% Some – 5% to 8%

Many – Greater than 8%

### These Modifiers Provide Our Estimate of the Amount of Other Components (Shell, Gravel, Etc.) in the Soil Sample

Trace -5% or less Few -6% to 12% Some -13% to 30% Many -31% to 50%

Organic Moisture Content % Content %						Sieve A	Analysis Resu	Sieve Analysis Results % Passing						nscs
							Sieve Sizes	es						
1½ inch 3/4 inch		3/4 incl	c	3/8 inch	No.4	No.8	No.10	No.16	No.30	No.40	No.50	No.100	No.200	
100 76	100	76		61	48	44	36	31	26	24	21	17	10	GP-GM
100 93	100	93		83	72	60	58	50	42	38	35	20	15	SM
43 67	:	1		1	-	1	-	-	1	1	1	1	1	РТ
100 93	100	93		79	65	53	51	44	36	33	31	23	14	SM
100 95	100	95		82	70	58	56	47	39	35	31	21	16	SM
100 84	100	84		69	58	48	46	40	34	31	29	21	12	SP-SM
76.3 47	1	1		1	1	1	-	1	-	1	1	1	1	РТ
- 88 88	88	 88		84	73	62	60	51	40	35	33	20	14	SM
100 93	100	93		73	57	46	44	37	31	28	26	15	2	SP
100 87	100	87		78	69	63	58	56	48	43	36	20	13	SM
100 98	100	98		87	75	64	62	54	46	43	40	27	16	SM
	-	1		1	1	1	-	-	1	:	:	:	19	SM
84 83	:	1		1	-	1	-	-	1	1	:	1	1	РТ
60 35	:	1		:	1	:	1	:	1	:	:	:	:	РТ
35	-	-		-	-	1	-	-	1	:	:	:	23	GM
- 100 86	0	86		;	52	40	38	32	26	24	22	16	<u>,</u>	GP-GM



USCS			SM	РТ	SM	SP-SM	SM	РТ	SM	GM	SM	SP-SM	РТ	SM
						SI				-		Ś		
		No.200	17	:	17	12	16	1	15	24	18	10	1	18
		No.100	:	:	:	16	-	-	19	-	-	:	1	23
		No.50	:	:	ł	24	ł	ł	27	ł	ł	ł	ł	33
		No.40	;	;	ł	26	-	-	30	-	-	ł	-	36
		No.30	ł	1	-	29	-	-	33	-	-	-	-	40
ts % Passing	Si	No.16	;	;	1	35	1	1	41	1	1	1	1	49
Sieve Analysis Results % Passing	Sieve Sizes	No.10	1	ł	1	42	1	1	48	1	1	1	1	58
Sieve A		No.8	ł	ł	1	45	1	1	50	ł	1	1	ł	61
		No.4	:	:	:	58	1	1	62	-	-	:	-	74
		3/8 inch	;	;	1	1	1	1	74	1	1	1	1	88
		3/4 inch	;	;	ł	95	ł	1	93	1	1	ł	1	98
			ł	ł	1	100	ł	ł	100	1	1	ł	1	100
Moisture Content %			14	25	19	:	7	67	1	15	14	11	96	1
Organic Content %			:	28.9	:	-	1	77	1	-	-	:	82.4	:
Sample Depth 0	(feet)		2 – 4	10 – 12	18	12 – 16	0 – 2	6 – 8	8 – 12	23 – 25	2 – 4	4 – 6	6 – 8	16 – 20
Location			B-8	B-8	B-8	B-8	B-9	B-9	B-9	B-9	B-10	B-10	B-10	B-10

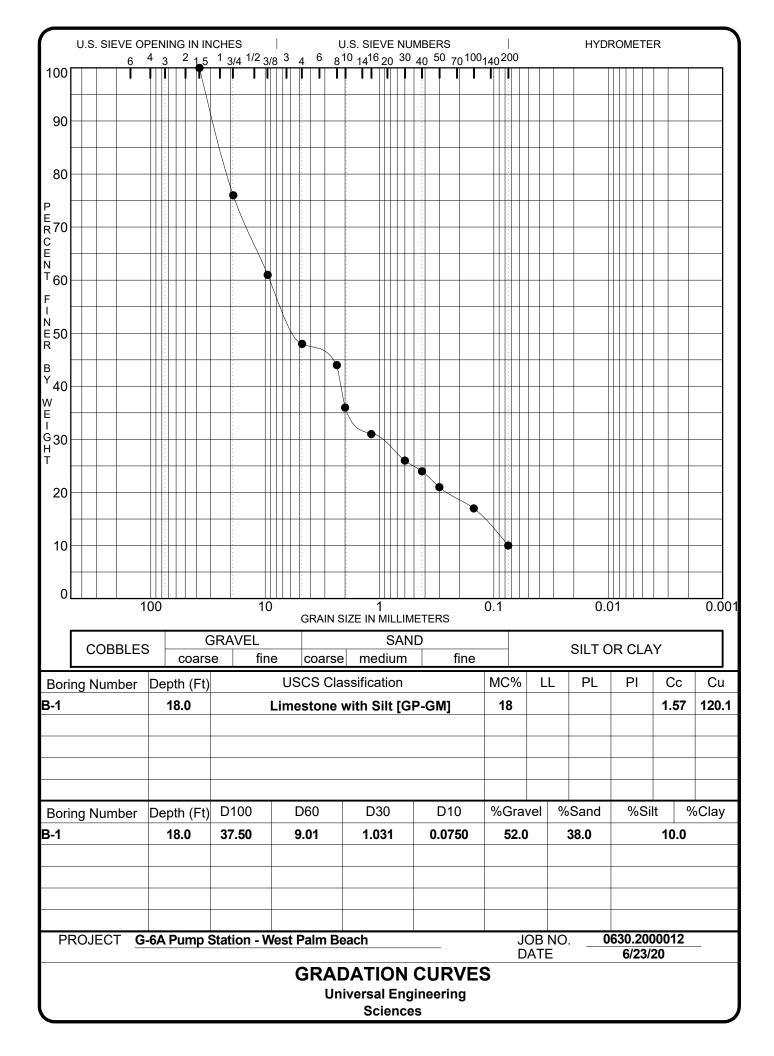


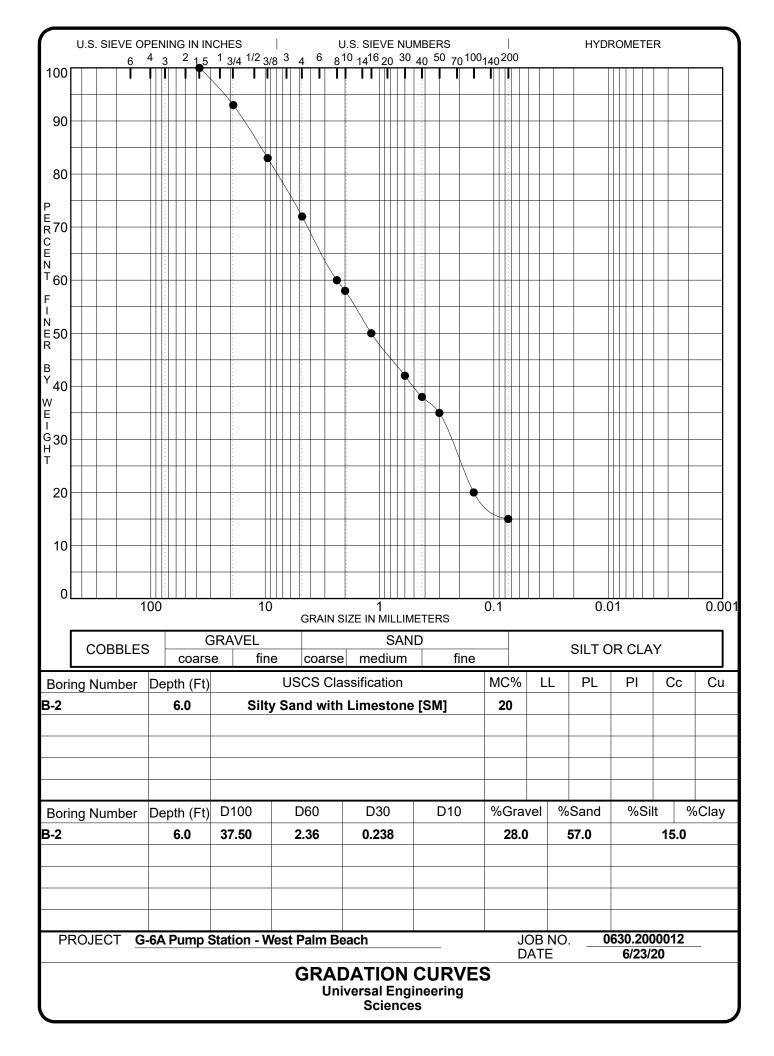
uscs			SM	РТ	GM	SP-SM	GP-GM	SM	SM	РТ	SM	SM	SM	SP	SM	РТ	РТ
		No.200	20		20	11	11	19	15		16	17	14	4	18		
		No.100 N		:		17		31	21		23	26			24		
		No.50	:	:	-	23	-	43	29	-	39	34	-	1	35	-	ł
		No.40	1	1	1	26	1	46	32	1	42	36	1	1	38	1	
		No.30	1	-	-	29	-	48	36	-	45	39	-	1	41	1	1
6 Passing		No.16	1			36		55	43		53	45		1	48	1	1
Sieve Analysis Results % Passing	Sieve Sizes	No.10				44		61	50		61	51			55		
Sieve Anal		No.8		1		46		63	52		64	54		1	57	1	1
		No.4	-			59		73	63	-	77	64		1	68	-	
		3/8 inch	1	1		76		86	76		06	78		1	81	1	
		3/4 inch 3/				92		66	89		100	93			95		1
		1½ inch 3/4				100		100	100		100	100			100		
ture ent %		11/2															
<ul><li>Moisture</li><li>Content %</li></ul>			8	188	22	1	19	-		83	1	-	21	22	-	27	52
Organic Content %			1	70.4	1	1	:	1	1	20.6	:	1	1	1	1	58	34.7
	(feet)		2 - 4	6 – 8	10 – 12	20 – 24	30 – 32	40 – 42	22 – 28	6 – 8	10 – 12	37 – 41	41 – 43	57 – 59	14 – 17	16 – 18	18 – 20
Location			B-11	B-11	B-11	B-11	B-11	B-11	B-11A	B-12	B-12	B-12	B-12	B-12	B-13	B-13	B-13

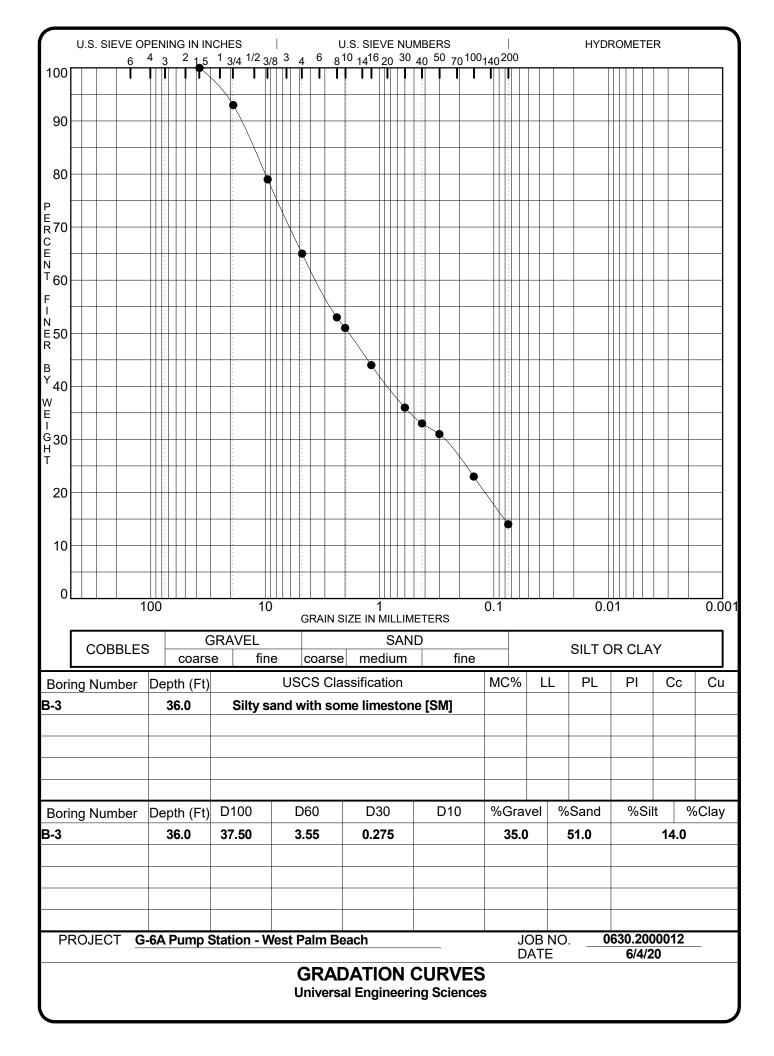


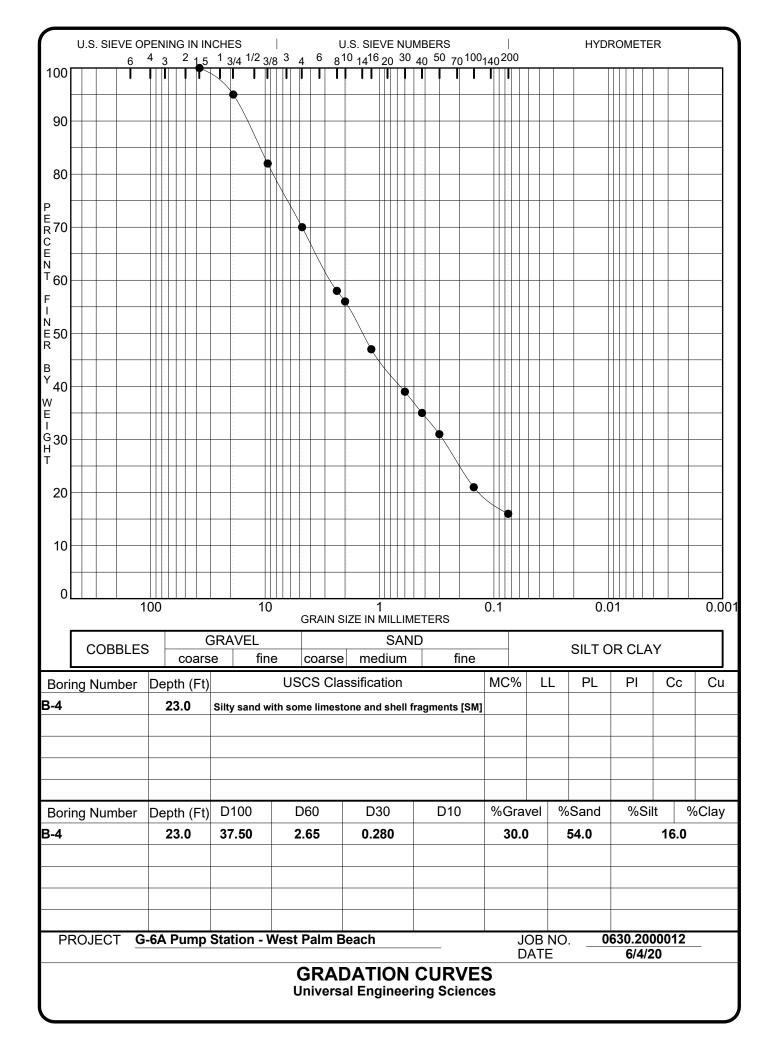
USCS		No.40 No.50 No.100 No.200	SM	FT	LA	36 33 20 14 SM
		No.30	1	-	-	40
ts % Passing	Sé	No.16	1	1	1	48
Sieve Analysis Results % Passing	Sieve Sizes	No.10	-	ı		56
Sieve A		No.8	1	1	1	58
		No.4	-	-	-	20
		3/8 inch	1	:	:	83
		3/4 inch	-			26
		1½ inch				100
Sample Organic Moisture Depth Content % Content %			88	747	29	
Organic Content %			:	36.7	58.9	
Sample Depth	(feet)		12 – 14	16 – 18	18 – 20	28 – 34
Location			B-14	B-14	B-14	B-14

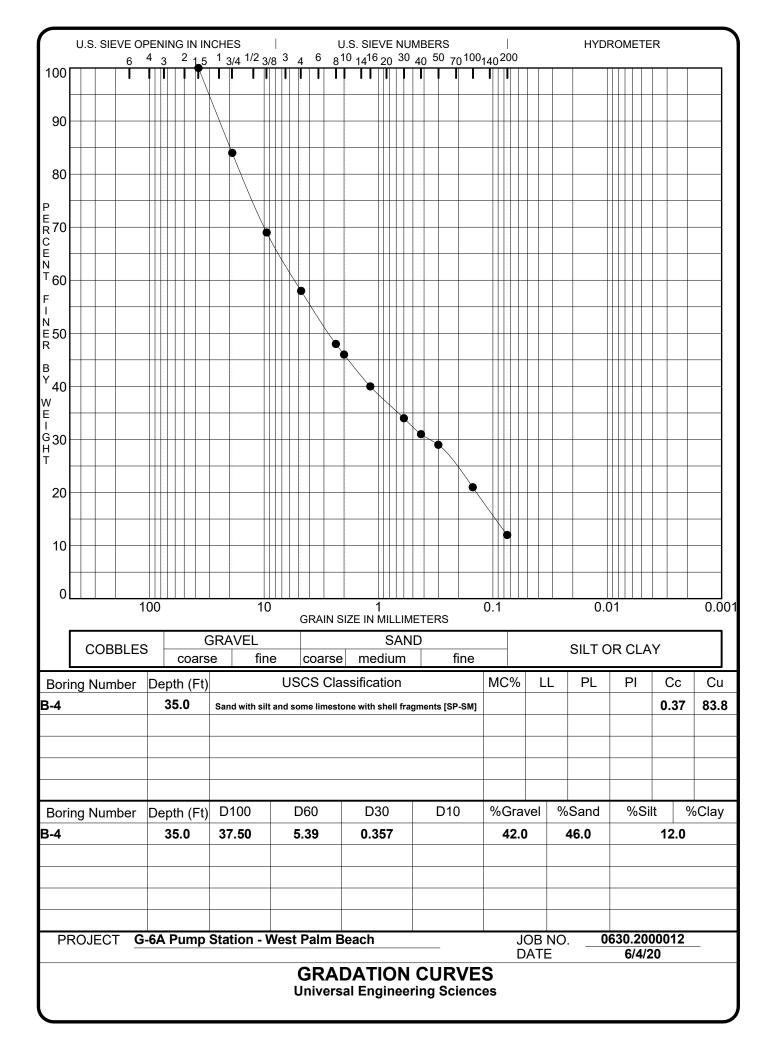


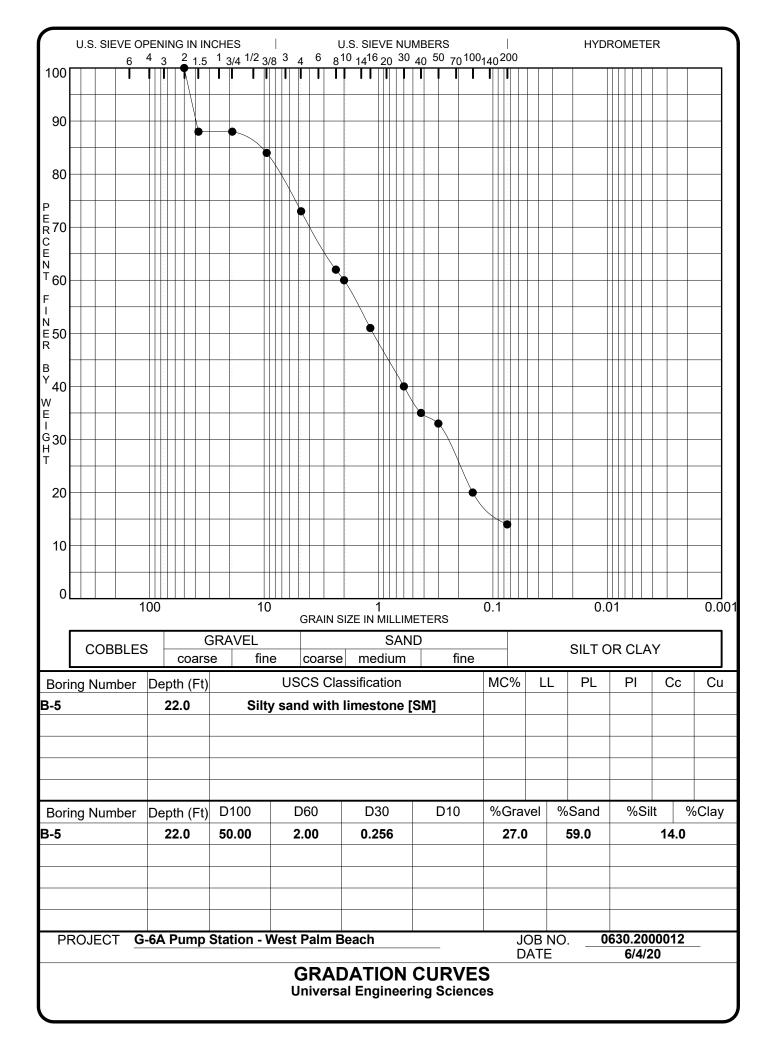


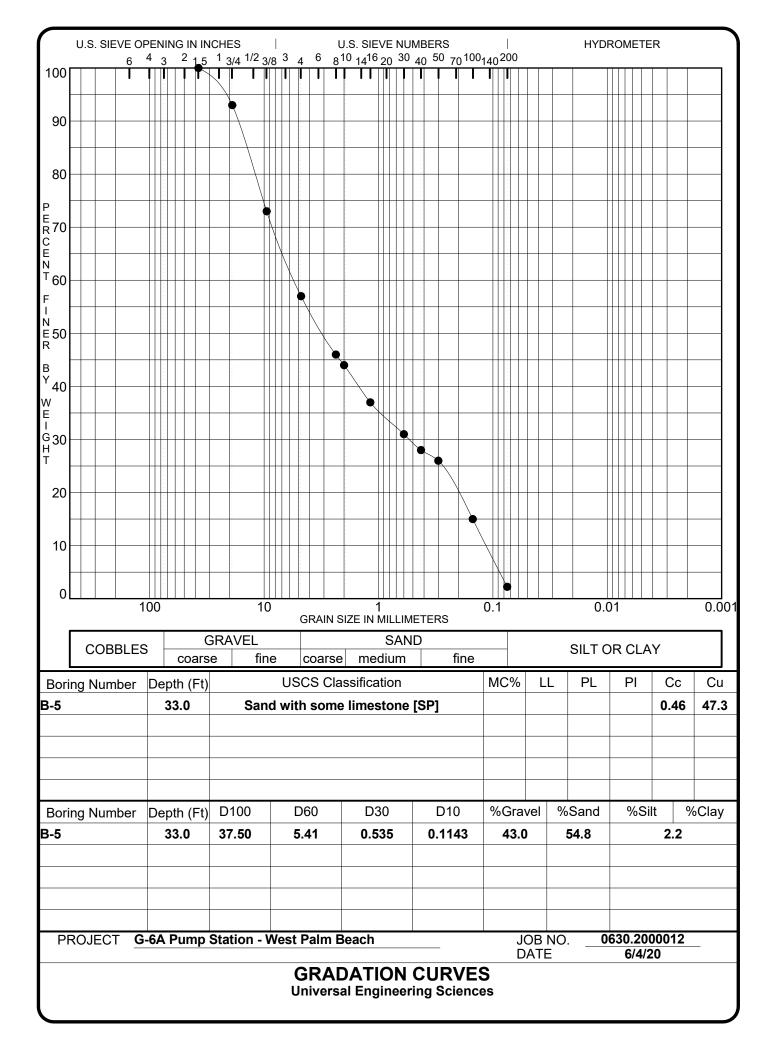


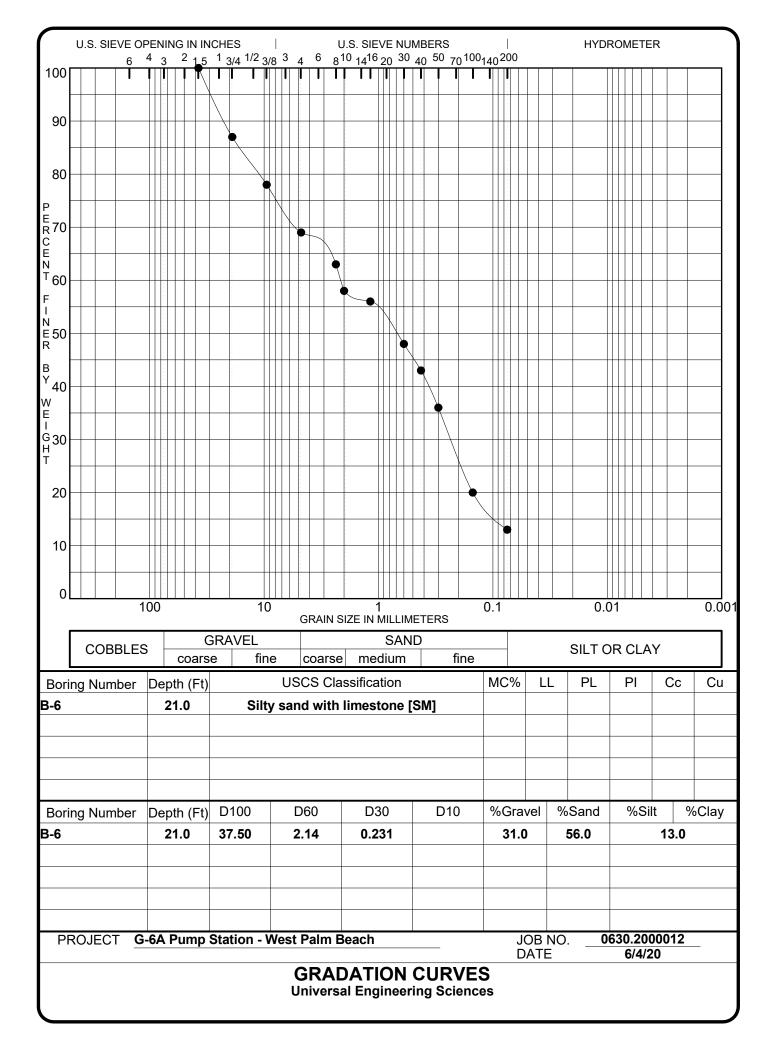


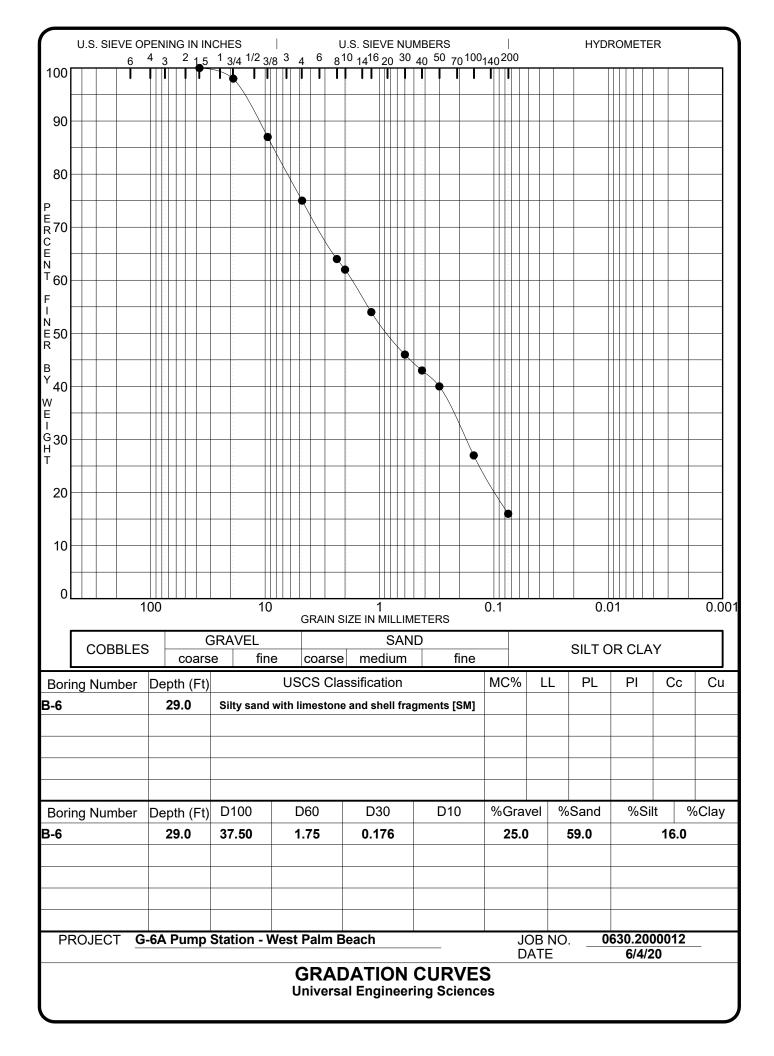


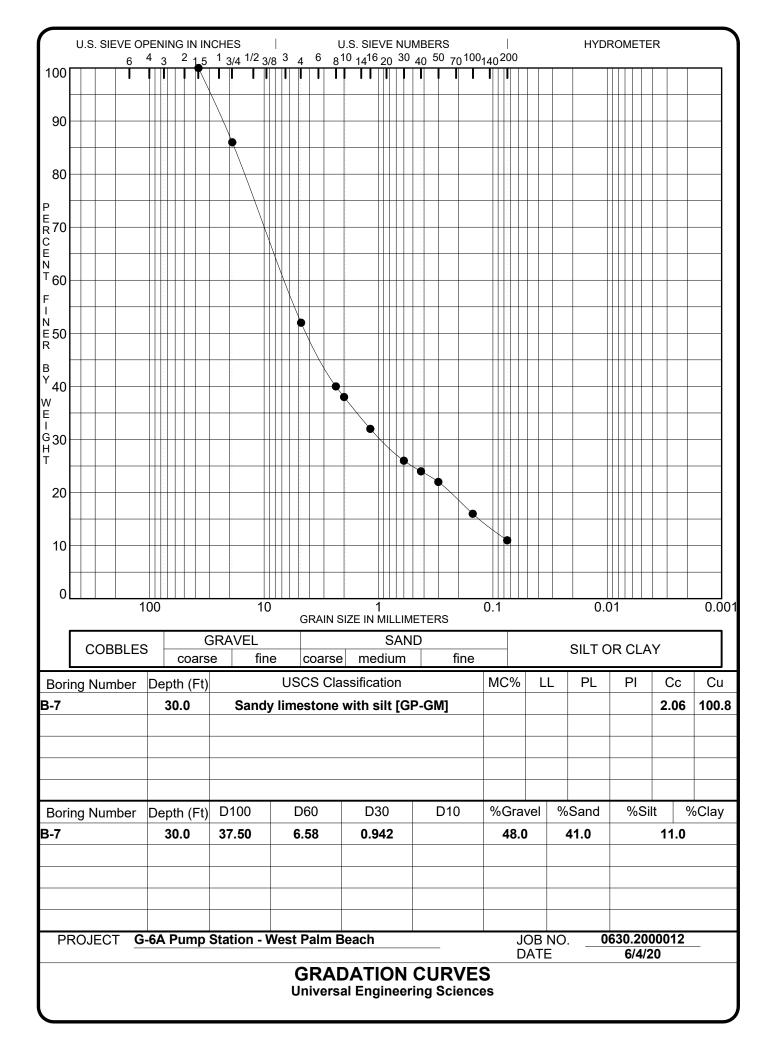


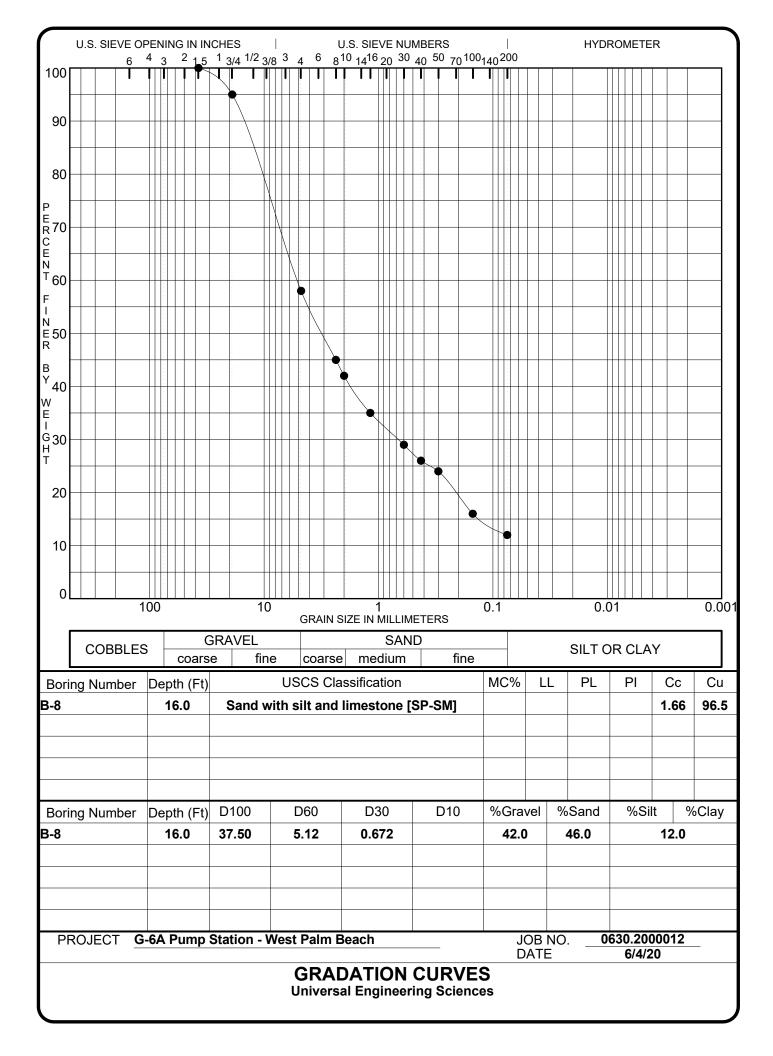


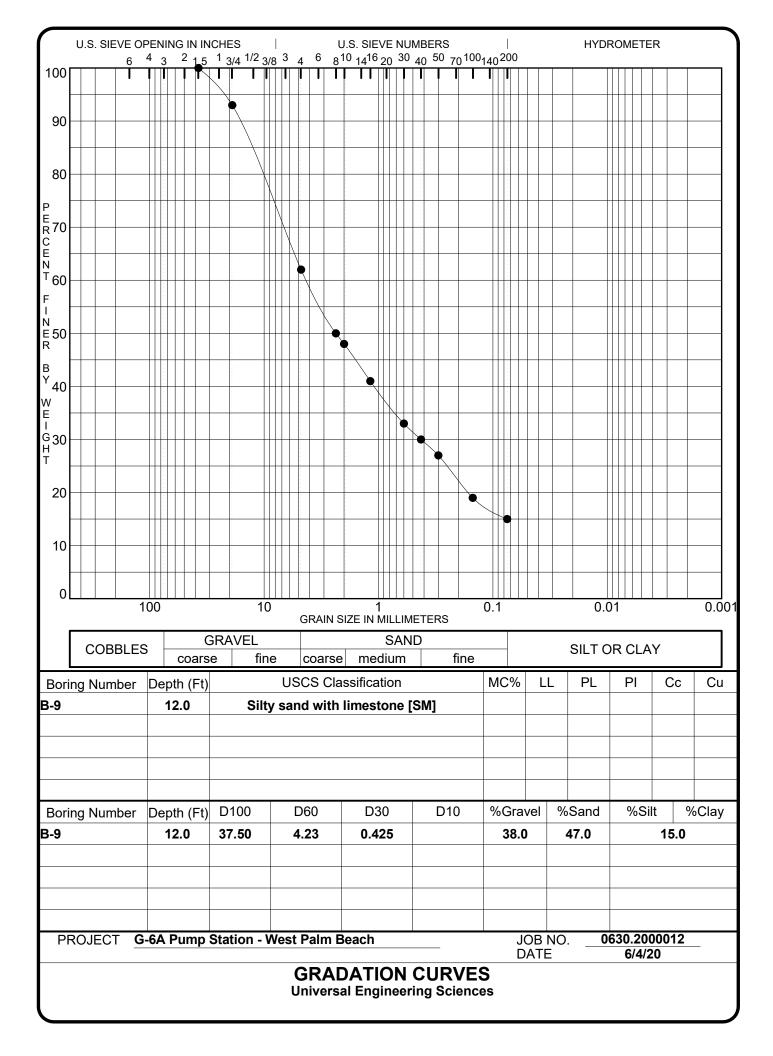


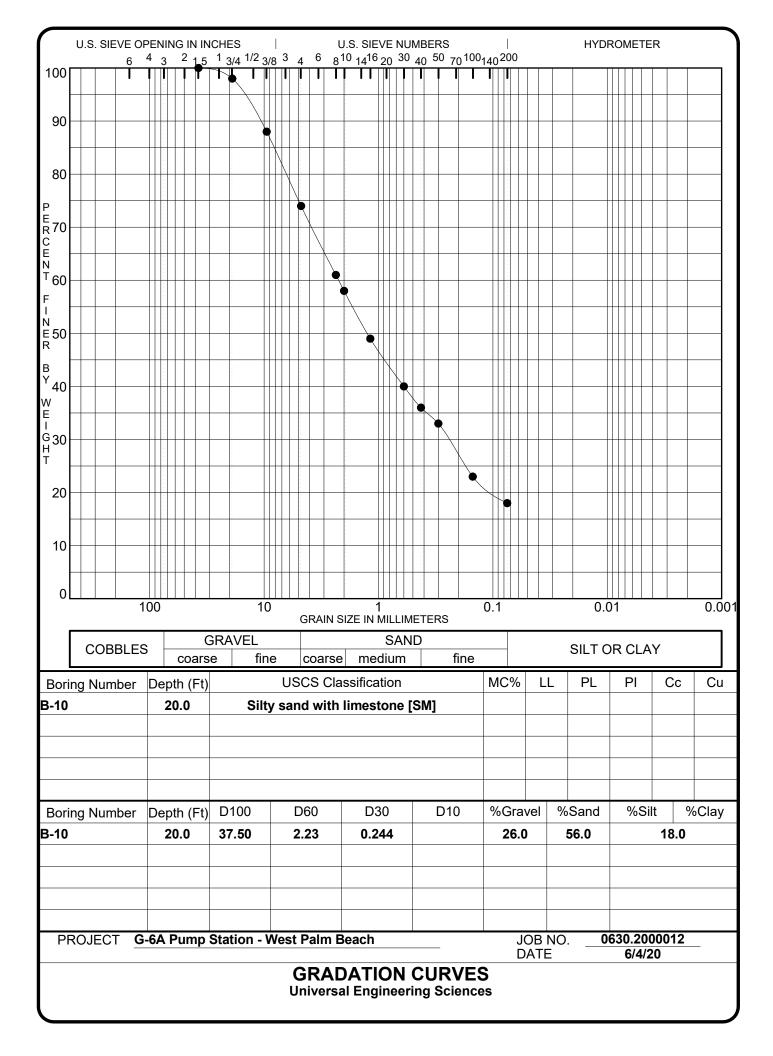


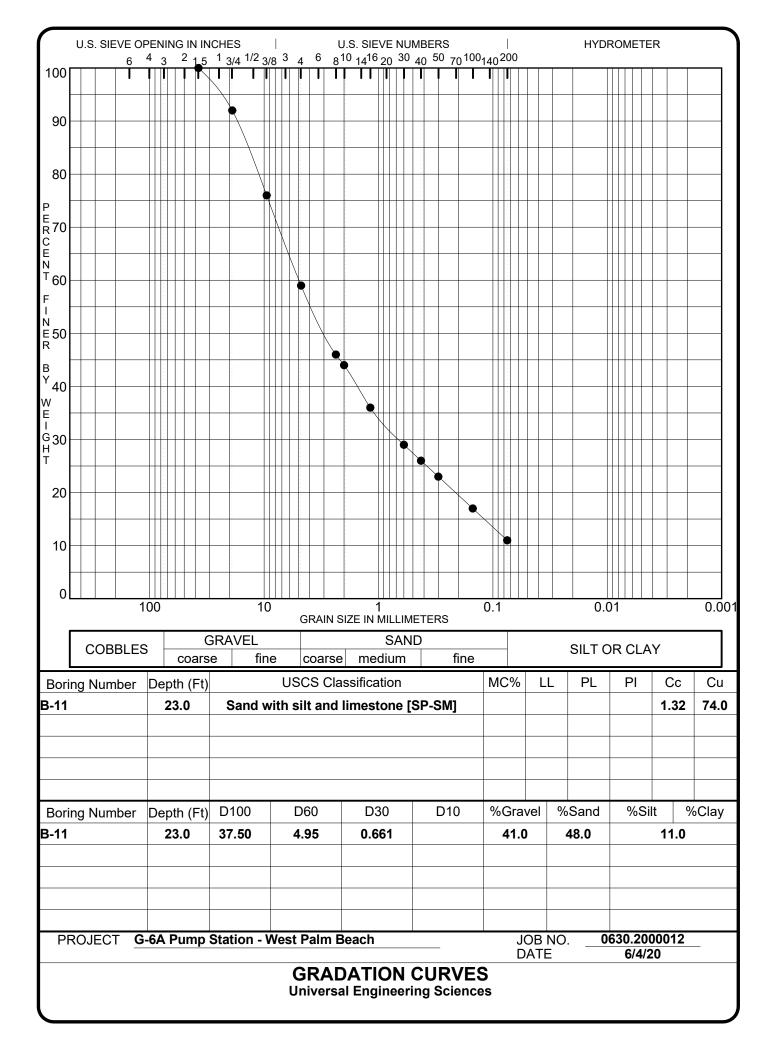


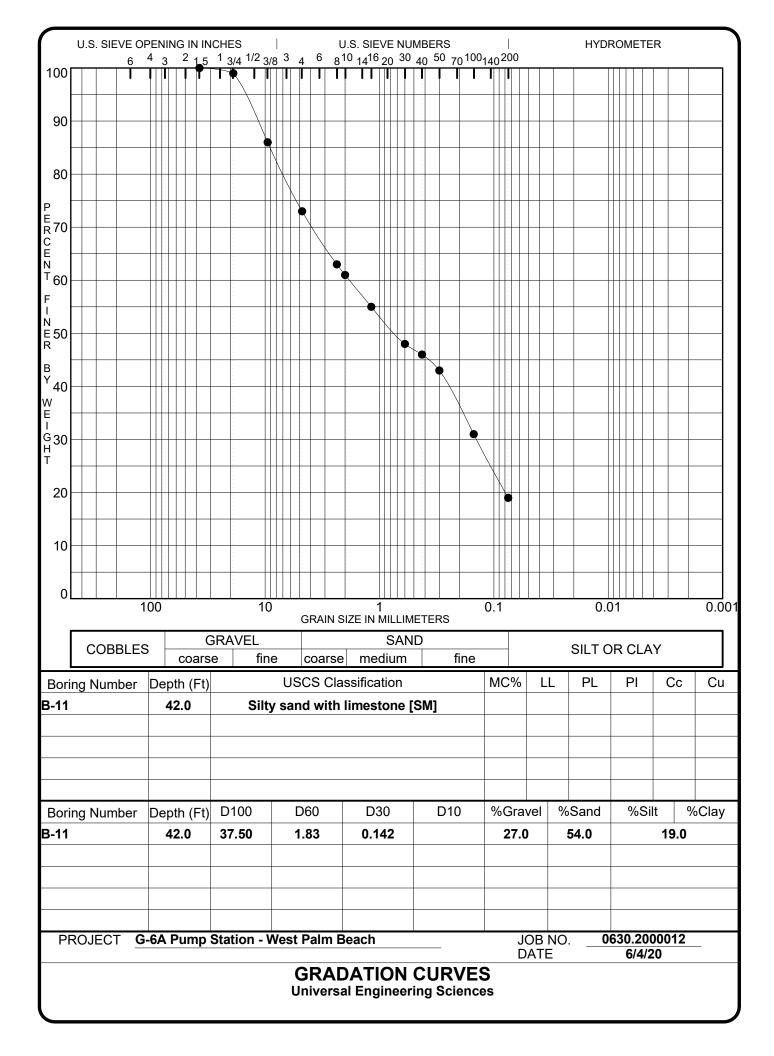


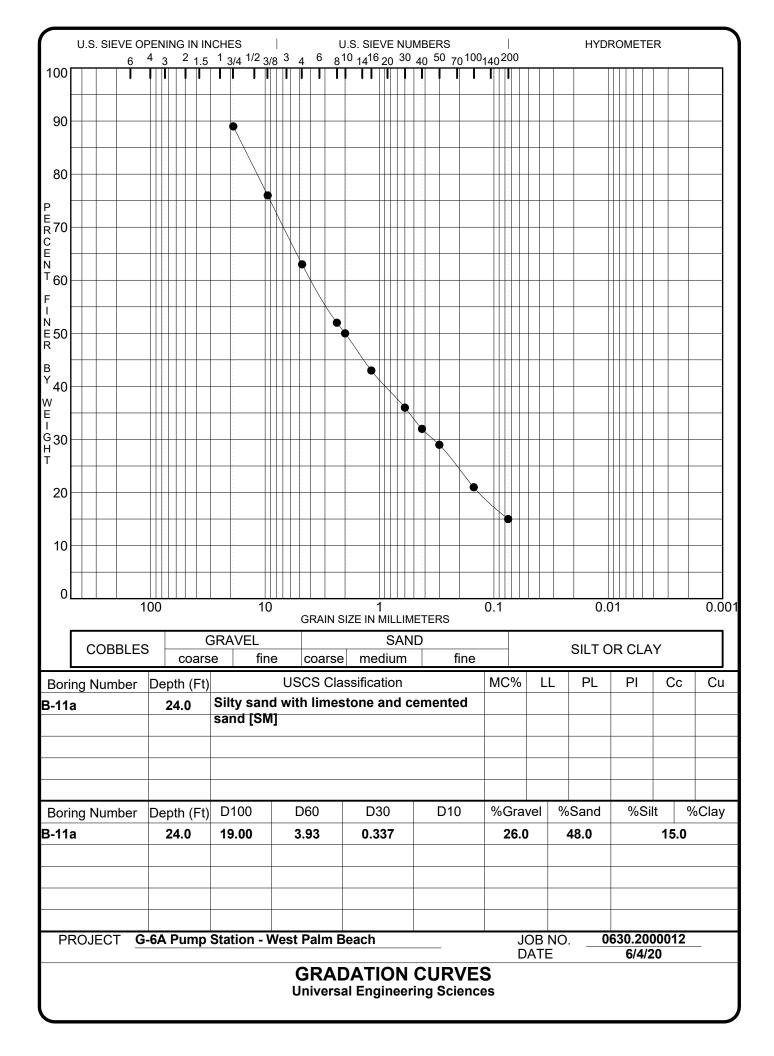


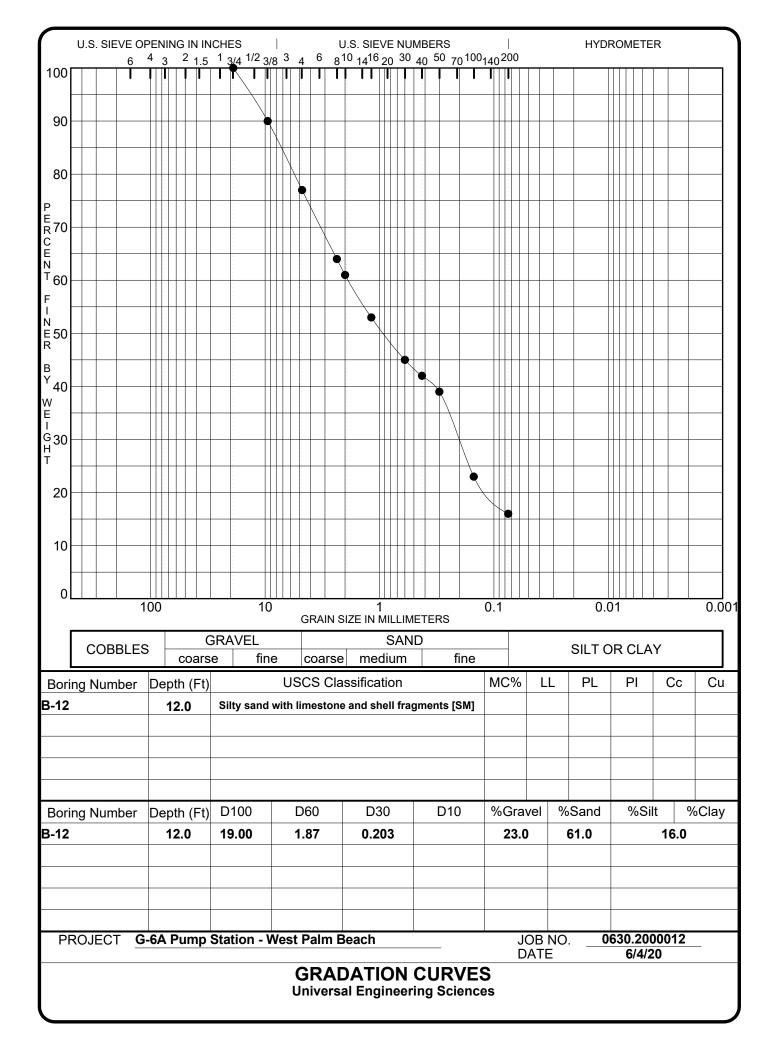


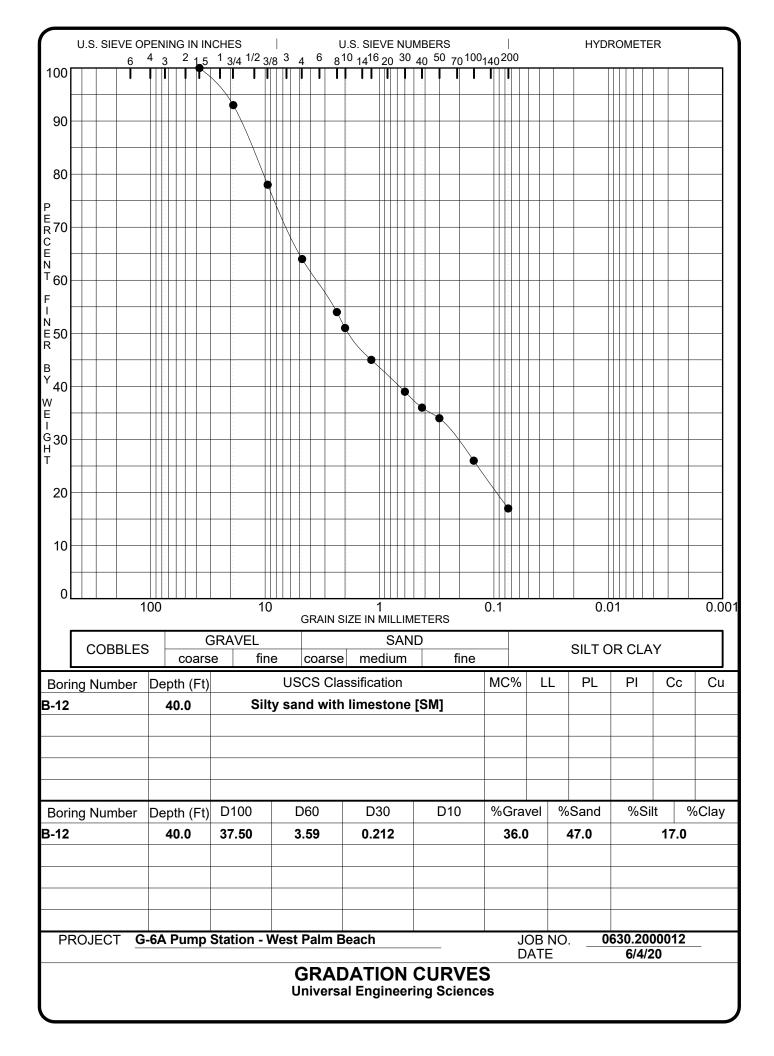


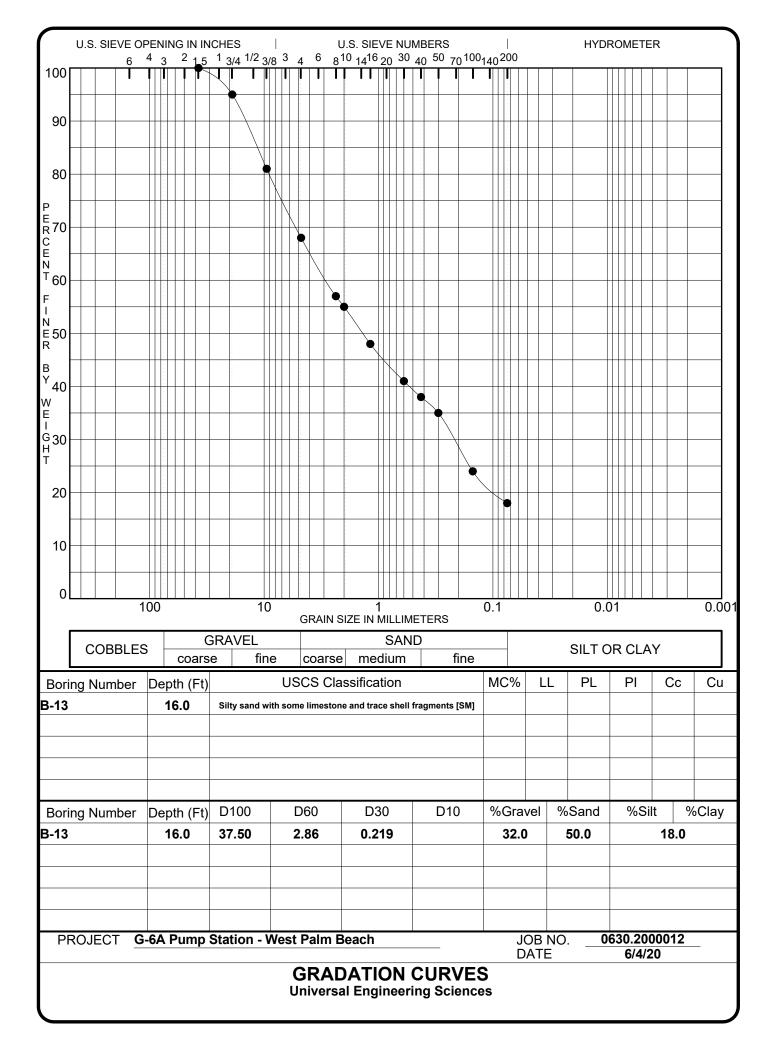


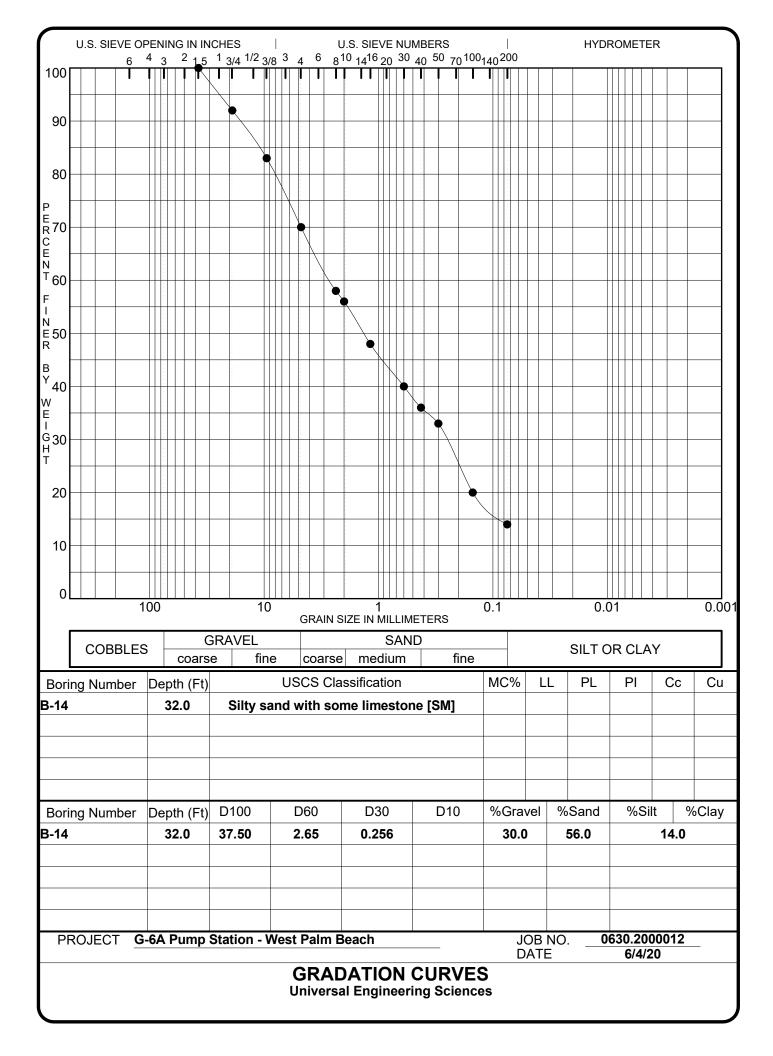












### G-6A Pump Station West Palm Beach, Palm Beach County, Florida UES Project No. 0630.2000012 UES Report No. 17223

### **REPORT OF CORROSION PARAMETERS**

Date Tested: May 15, 2020

Location: Bridge area. Borings B-11; 8-14 ft bls, B-12; 8-14 ft bls

Location	Sample Description	рН	Sulfate (ppm)	Chloride (ppm)	Resistivity (Ohm-cm)	Environmental Classification
Bridge Area	Silty limestone, sandy limestone [GP]	8.67	177	30	2,520	Slight to Moderate

Date Tested: June 26, 2020

Location: Pump Station. Borings B-1; 2-14 ft bls

Location	Sample Description	рН	Sulfate (ppm)	Chloride (ppm)	Resistivity (Ohm-cm)	Environmental Classification
Building Area	Limestone, sandy limestone [GP]	8.73	135	15	2,260	Slight to Moderate



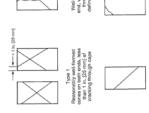
Client: SFWMD Project Name: G-6A Pump Station UES Project No. 0630.2000012.0000

Unconfined Compressive Strength of Intact Rock Core Specimens

# **ASTM D-2938**

gth				
Unconfined Compressive Strengtl of Rock (tsf)	56.8	60.6	99.4	231.5
Unconfined Compressive Strength of Rock (Ib)	6,503	6,984	11,451	26,671
Failure Type	Э	З	З	3
ĽD	2.22	1.82	2.08	2.06
Length of Length of Specimen Specimen after (inch) Capping (in)	7.19	5.91	6.76	6.71
Length of Specimen (inch)	6.72	5.21	6.50	6.50
Average Diameter (inch)	3.24	3.25	3.25	3.25
Diameter 2 (inch)	3.24	3.25	3.25	3.25
Diameter 1 (inch)	3.24	3.25	3.25	3.25
Sample Core Depth Diameter Number (Feet) (inch)	S-1 43.2 - 44	S-1 17.9 - 18.5	S-1 15 - 15.8	S-1 25 - 25.8
Sample Number	S-1	S-1	\$-1	S-1
Boring Number	B-3	B-6	B-9	B-12

Failure Type Legend









Type 6 Similar to Type 5 but end of cylinder is pointed

Type 5 Side fractures at top or bottom (occur commonly with unbonded cape)

Type 4 Diagonal fracture with no cracking through ends; tap with hammer to distinguish from Type 1



Client: SFWMD Project Name: G-6A Pump Station UES Project No. 0630.2000012.0000

# Splitting Tensile Strength of Intact Rock Core Specimens

# **ASTM D-3967-05**

Boring Number	Sample Number	Sample Core Depth Length 1 Number (Feet) (inch)	Length 1 (inch)	Length 2 (inch)	Length 2 Length 3 (inch)	Average Length (inch)	Diameter (inch)	ГЛ	Split Tensile Strength of Rock (lb)	Split Tensile Strength of Rock (Ib) of Rock (tsf)
B-3	S-2	S-2 44.4 - 45	5.95	5.94	5.95	5.95	3.24	1.84	13,122	31
B-6	S-2	S-2 17 - 17.5	5.00	5.00	5.00	5.00	3.24	1.54	7,377	21
B-9	S-2	S-2 17.2 - 17.8	6.94	6.94	6.93	6.94	3.24	2.14	16,661	34
B-12	S-2	S-2 29.4 - 30	4.98	5.00	4.99	4.99	3.23	1.54	3,879	11

Fracture Sketch

B-3, S-2

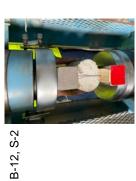


B-6, S-2



Fracture Sketch





Project No.: 0630.2000012 Report No.: 17223

# G-6A Pump Station West Palm Beach, Palm Beach County, Florida UES Project No. 0630.2000012 UES Report No. 17223

# Laboratory Testing Procedures

# **Natural Moisture Content**

The water content of the sample tested was determined in general accordance with the latest revision of ASTM D 2216. The water content is defined as the ratio of "pore" of "free" water in a given mass of material to the mass of solid material particles.

# Organic Content Determination (ASTM D2974)

The organic content is obtained by selecting a representative soil sample and measuring its dry weight. The sample is then ignited in a muffle furnace to burn off all the organic material in the sample. After an allotted time period the after-ignition weight is obtained. The percentage of organic material within the sample is then calculated.

# Percent Fines Content

The percent fines or material passing the No. 200 mesh sieve of the sample tested was determined in general accordance with the latest revision of ASTM D 1140. The percent fines are the soil particles in the silt and clay size range.

# Soil Gradation Analysis (ASTM C 136)

The soil gradation test is performed by passing a representative soil sample over a standard set of nested sieves. The percentage of the soil grains (by dry weight basis) retained on each sieve is measured and a grain size distribution curve is plotted.

# Resistivity Testing (FM 5-551)

The resistivity test is performed by preparing a sample with soil passing the No. 8 sieve, adding distilled water, and mixing. The sample is then placed in a soil box with electrodes, where it is connected to a resistivity meter. The resistivity is measured passing through the soil. The sample is removed from the box and further diluted with distilled water, and the procedure is repeated until a minimum resistivity is obtained.

# <u>pH (FM 5-550)</u>

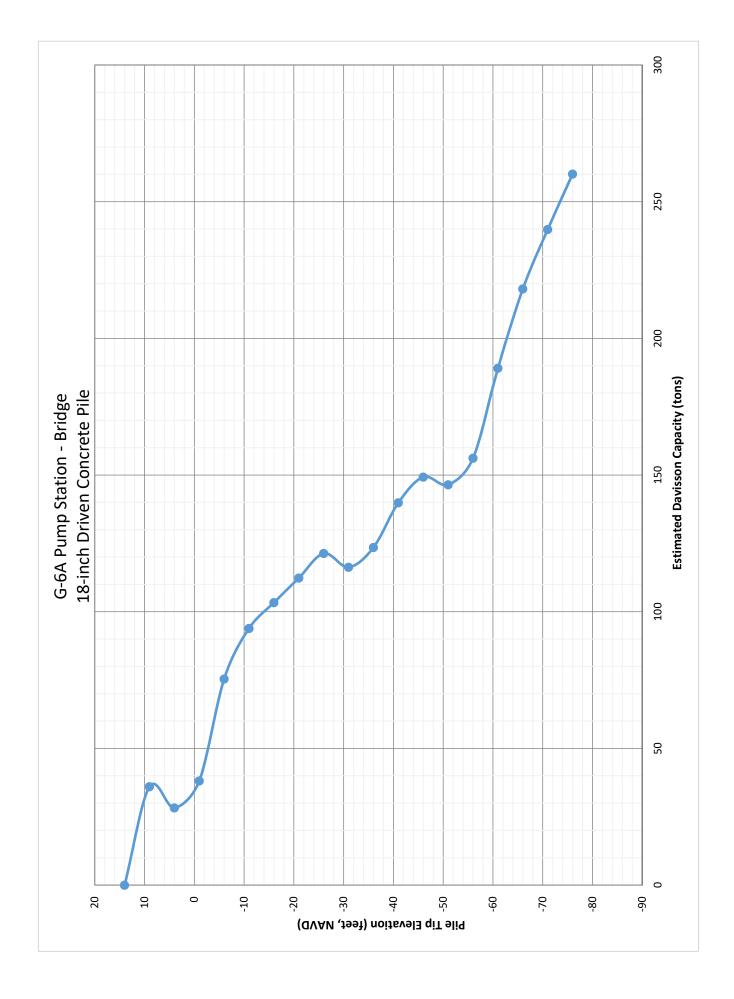
The pH is measured by mixing distilled water with a soil sample until the soil particles are dispersed. Then the sample is checked for pH, using a pH meter.

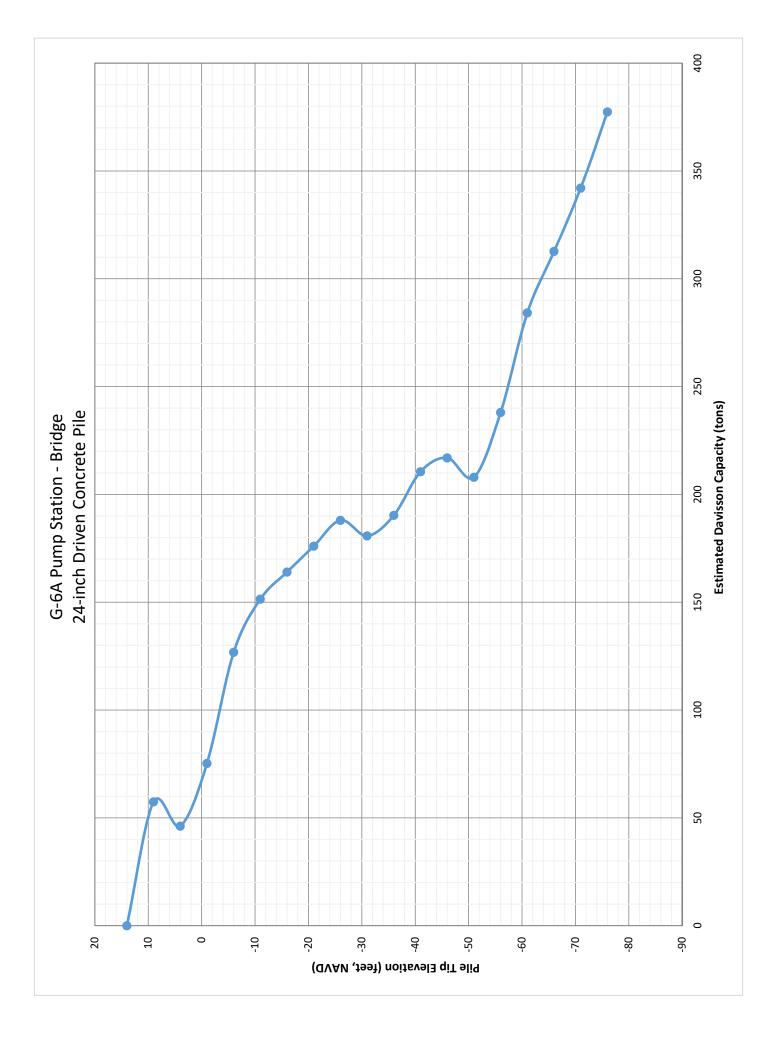
# Sulfate (FM 5-553)

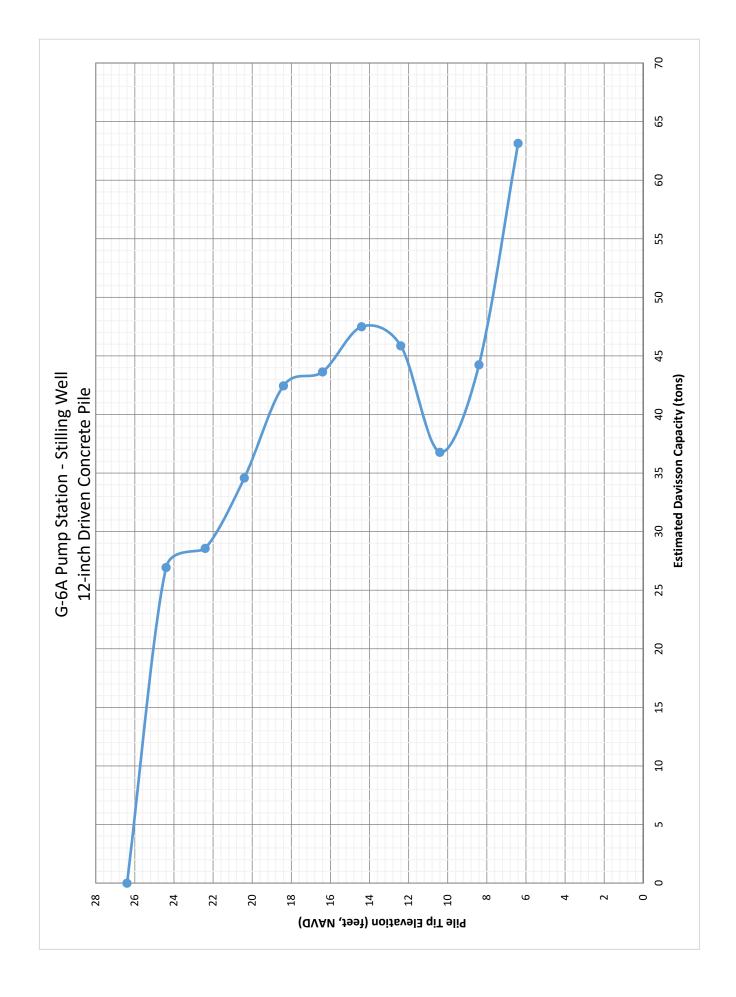
A representative sample is saturated with distilled water, agitated thoroughly and aspirated over a qualitative filter. A reagent is added to the retrieved liquid. The liquid is then placed in a nephelometer to measure concentration of sulfate.

# Chloride (FM 5-552)

A representative sample is saturated with distilled water, agitated thoroughly and aspirated over a qualitative filter. The retrieved liquid is mixed with an indicator liquid. Change in color of the sample is monitored and converted to concentration of chlorides.







Florida Bridge Software Institute Shaft and Pile Analysis (FB-Deep v.2.06) Date: June 08, 2020 Time: 12:37:18

General Information: \_\_\_\_\_ Input file: .....ojects\2020\200012 G-6A Pump Station West Palm\G-6A\_Bridge.in Project number: 0630.2000012.0000 Job name: G-6A Pump Station Engineer: ASW Units: English Analysis Information: \_\_\_\_\_ Analysis Type: SPT Soil Information: \_\_\_\_\_ Boring date: 5/22/20, Boring Number: B-11A Station number: Offset: Ground Elevation: 14.000(ft) Hammer type: Safety Hammer ID Depth No. of Blows Soil Type (Blows/ft) (ft) \_\_\_\_\_ \_\_\_\_\_ 0.00 25.00 3- Clean sand 1 25.00 3- Clean sand 2 2.00 5.00 3- Clean sand 3 4.00 7.00 3- Clean sand 4 6.00 5.00 3- Clean sand 5 8.00 6.00 1- Plastic Clay 6 10.00 2.00 1- Plastic Clay 7 12.00 8 14.00 3.00 1- Plastic Clay 9 8.00 1- Plastic Clay 16.00 10 30.00 4- Lime Stone/Very shelly sand 18.00 30.00 4- Lime Stone/Very shelly sand 11 20.00 12 22.00 19.00 4- Lime Stone/Very shelly sand 13 24.00 24.00 4- Lime Stone/Very shelly sand 14 30.00 4- Lime Stone/Very shelly sand 26.00 15 30.00 4- Lime Stone/Very shelly sand 28.00 30.00 4- Lime Stone/Very shelly sand 16 30.00 17 30.00 4- Lime Stone/Very shelly sand 32.00 18 34.00 30.00 4- Lime Stone/Very shelly sand 19 30.00 4- Lime Stone/Very shelly sand 36.00 20 30.00 4- Lime Stone/Very shelly sand 38.00 21 30.00 4- Lime Stone/Very shelly sand 40.00 22 30.00 4- Lime Stone/Very shelly sand 42.00 23 44.00 30.00 4- Lime Stone/Very shelly sand 24 46.00 30.00 4- Lime Stone/Very shelly sand 25 48.00 30.00 4- Lime Stone/Very shelly sand 26 5.00 4- Lime Stone/Very shelly sand 50.00 30.00 3- Clean sand 27 52.00 28 54.00 9.00 3- Clean sand 29 56.00 30.00 3- Clean sand 18.00 3- Clean sand 58.00 30

31	60.00	25.00	3- Clean sand
32	62.00	26.00	3- Clean sand
33	64.00	14.00	3- Clean sand
34	66.00	9.00	3- Clean sand
35	68.00	6.00	3- Clean sand
36	70.00	3.00	3- Clean sand
37	72.00	10.00	3- Clean sand
38	74.00	29.00	3- Clean sand
39	76.00	33.00	3- Clean sand
40	78.00	43.00	3- Clean sand
41	80.00	46.00	3- Clean sand
42	82.00	28.00	3- Clean sand
43	84.00	32.00	3- Clean sand
44	86.00	34.00	3- Clean sand
45	88.00	18.00	3- Clean sand
46	90.00	21.00	3- Clean sand
47	92.00	44.00	3- Clean sand
48	94.00	31.00	3- Clean sand
49	96.00	17.00	3- Clean sand
50	98.00	50.00	3- Clean sand
51	100.00	0.00	5- Cavity layer

# Blowcount Average Per Soil Layer

-----

Layer Num.	Starting Elevation (ft)	Bottom Elevation (ft)	Thickness (ft)	Average Blowcount (Blows/ft)	Soil Type
1	14.00	4.00	10.00	13.40	3-Clean Sand
2	4.00	-4.00	8.00	4.75	1-Plastic Clay
3	-4.00	-38.00	34.00	27.53	4-Limestone, Very Shelly Sand
4	-38.00	-86.00	48.00	25.25	3-Clean Sand
5	-86.00	-86.00	0.00	0.00	5-

# Driven Pile Data:

\_\_\_\_\_

Pile unit weight = 150.00(pcf), Section Type: Square

# Pile Geometry:

Width (in)	Length (ft)	Tip Elev. (ft)
18.00	5.00	9.00
18.00	10.00	4.00
18.00	15.00	-1.00
18.00	20.00	-6.00
18.00	25.00	-11.00
18.00	30.00	-16.00
18.00	35.00	-21.00
18.00	40.00	-26.00
18.00	45.00	-31.00
18.00	50.00	-36.00
18.00	55.00	-41.00
18.00	60.00	-46.00
18.00	65.00	-51.00
18.00	70.00	-56.00

18.00	75.00	-61.00
18.00	80.00	-66.00
18.00	85.00	-71.00
18.00	90.00	-76.00
24.00	5.00	9.00
24.00	10.00	4.00
24.00	15.00	-1.00
24.00	20.00	-6.00
24.00	25.00	-11.00
24.00	30.00	-16.00
24.00	35.00	-21.00
24.00	40.00	-26.00
24.00	45.00	-31.00
24.00	50.00	-36.00
24.00	55.00	-41.00
24.00	60.00	-46.00
24.00	65.00	-51.00
24.00	70.00	-56.00
24.00	75.00	-61.00
24.00	80.00	-66.00
24.00	85.00	-71.00
24.00	90.00	-76.00

# Driven Pile Capacity:

-----

Section Type:	Square	
Pile Width:	18.00	(in)

Test	Pile	Ultimate	Mobilized	Estimated	Allowable	Ultimate
Pile	Width	Side	End	Davisson	Pile	Pile
Length		Friction	Bearing	Capacity	Capacity	Capacity
(ft)	(in)	(tons)	(tons)	(tons)	(tons)	(tons)
5.00	18.0	9.75	26.26	36.01	18.00	88.53
10.00	18.0	14.29	13.97	28.27	14.13	56.21
15.00	18.0	18.46	19.67	38.12	19.06	77.45
20.00	18.0	28.37	47.04	75.42	37.71	169.51
25.00	18.0	35.42	58.48	93.91	46.95	210.87
30.00	18.0	44.33	59.02	103.35	51.67	221.38
35.00	18.0	53.33	59.02	112.35	56.17	230.38
40.00	18.0	62.33	59.02	121.35	60.67	239.38
45.00	18.0	71.33	44.97	116.30	58.15	206.25
50.00	18.0	78.83	44.70	123.54	61.77	212.94
55.00	18.0	88.57	51.32	139.89	69.95	242.54
60.00	18.0	101.82	47.46	149.28	74.64	244.21
65.00	18.0	113.65	32.83	146.47	73.24	212.12
70.00	18.0	117.55	38.63	156.18	78.09	233.44
75.00	18.0	126.90	62.19	189.09	94.55	313.48
80.00	18.0	149.36	68.75	218.11	109.05	355.61
85.00	18.0	168.34	71.51	239.85	119.93	382.88
90.00	18.0	182.53	77.61	260.14	130.07	415.35

Section Type: Square

Pile Width:	24.00	(in)
-------------	-------	------

Test Pile Length (ft)	Pile Width (in)	Ultimate Side Friction (tons)	Mobilized End Bearing (tons)	Estimated Davisson Capacity (tons)	Allowable Pile Capacity (tons)	Ultimate Pile Capacity (tons)
5.00	24.0	13.00	44.44	57.44	28.72	146.32
10.00	24.0	19.06	27.14	46.20	23.10	100.48
15.00	24.0	23.66	51.62	75.28	37.64	178.52
20.00	24.0	37.83	88.95	126.79	63.39	304.70
25.00	24.0	47.23	104.20	151.44	75.72	359.84
30.00	24.0	59.11	104.92	164.03	82.01	373.86
35.00	24.0	71.11	104.92	176.03	88.01	385.86
40.00	24.0	83.11	104.92	188.03	94.01	397.86
45.00	24.0	95.11	85.66	180.77	90.39	352.10
50.00	24.0	105.11	85.20	190.31	95.16	360.72
55.00	24.0	117.88	92.65	210.54	105.27	395.84
60.00	24.0	135.76	81.18	216.95	108.47	379.31
65.00	24.0	151.53	56.46	207.99	104.00	320.92
70.00	24.0	156.74	81.30	238.03	119.02	400.62
75.00	24.0	169.20	115.02	284.22	142.11	514.27
80.00	24.0	199.14	113.56	312.71	156.35	539.83
85.00	24.0	224.45	117.65	342.11	171.05	577.41
90.00	24.0	243.38	134.06	377.43	188.72	645.55

NOTES

- 2. DAVISSON PILE CAPACITY IS AN ESTIMATE BASED ON FAILURE CRITERIA, AND EQUALS ULTIMATE SIDE FRICTION PLUS MOBILIZED END BEARING.
- 3. ALLOWABLE PILE CAPACITY IS 1/2 THE DAVISSON PILE CAPACITY.
- 4. ULTIMATE PILE CAPACITY IS ULTIMATE SIDE FRICTION PLUS 3 x THE MOBILIZED END BEARING. EXCEPTION: FOR H-PILES TIPPED IN SAND OR LIMESTONE, THE ULTIMATE PILE CAPACITY IS ULTIMATE SIDE FRICTION PLUS 2 x THE MOBILIZED END BEARING.

<sup>1.</sup> MOBILIZED END BEARING IS 1/3 OF THE ORIGINAL RB-121 VALUES.

Florida Bridge Software Institute Shaft and Pile Analysis (FB-Deep v.2.06)

General Information:

Date: June 08, 2020 Time: 12:47:40

\_\_\_\_\_ Input file: .....\2020\2000012 G-6A Pump Station West Palm\G-6A\_StillingWell.in Project number: 0630.2000012.0000 Job name: G-6A Pump Station Engineer: ASW Units: English Analysis Information: ------Analysis Type: SPT Soil Information: \_\_\_\_\_ Boring date: 5/13/20, Boring Number: B-13 Station number: Offset: Ground Elevation: 26.400(ft) Hammer type: Safety Hammer No. of Blows Depth Soil Type ID (ft) (Blows/ft) \_\_\_\_\_ \_\_\_\_ 1 0.00 30.00 3- Clean sand 21.00 3- Clean sand 2 2.00 16.00 3- Clean sand 18.00 3- Clean sand 28.00 3- Clean sand 56.00 3- Clean sand 4.00 3- Clean sand 32.00 3- Clean sand 11.00 1- Plastic Clay 6.00 1- Plastic Clay 30.00 4- Lime Stone/Very shelly sand 0.00 5- Cavity layer 16.00 3- Clean sand 3 4.00 4 6.00 6.00 8.00 10.00 12.00 14.00 16.00 18.00 20.00 22.00 24.00 26.00 30.00 5 6 7 8 9 10 11 12 13 14 0.00 5- Cavity layer 15 30.00 Blowcount Average Per Soil Layer -----Layer Bottom Thickness Average Soil Type Starting Num. Elevation Elevation Blowcount (ft) (ft) (ft) (Blows/ft) \_\_\_\_\_ \_\_\_\_\_ 
 26.40
 10.40
 16.00
 25.63

 10.40
 6.40
 4.00
 8.50

 6.40
 -3.60
 10.00
 30.00

 -3.60
 -3.60
 0.00
 0.00
 1 3-Clean Sand 1-Plastic Clay 2 4-Limestone, Very Shelly Sand 3 4 5Driven Pile Data:

Pile unit weight = 150.00(pcf), Section Type: Square

# Pile Geometry:

	-	
Width	Length	Tip Elev.
(in)	(ft)	(ft)
12.00 12.00 12.00 12.00 12.00 12.00 12.00 12.00	2.00 4.00 6.00 8.00 10.00 12.00 14.00	24.40 22.40 20.40 18.40 16.40 14.40 12.40
12.00	16.00	10.40
12.00	18.00	8.40
12.00	20.00	6.40

# Driven Pile Capacity:

Section Type:	Square	
Pile Width:	12.00	(in)

Test Pile Length (ft)	Pile Width (in)	Ultimate Side Friction (tons)	Mobilized End Bearing (tons)	Estimated Davisson Capacity (tons)	Allowable Pile Capacity (tons)	Ultimate Pile Capacity (tons)
2.00	12.0	3.88	23.07	26.94	13.47	73.08
4.00	12.0	6.69	21.89	28.57	14.29	72.35
6.00	12.0	8.72	25.86	34.59	17.29	86.32
8.00	12.0	11.00	31.45	42.45	21.22	105.34
10.00	12.0	17.78	25.86	43.64	21.82	95.36
12.00	12.0	22.30	25.20	47.50	23.75	97.89
14.00	12.0	25.10	20.77	45.87	22.93	87.40
16.00	12.0	31.05	5.72	36.78	18.39	48.23
18.00	12.0	33.69	10.56	44.25	22.13	65.37
20.00	12.0	36.92	26.23	63.15	31.57	115.61

NOTES

\_\_\_\_\_

- 1. MOBILIZED END BEARING IS 1/3 OF THE ORIGINAL RB-121 VALUES.
- 2. DAVISSON PILE CAPACITY IS AN ESTIMATE BASED ON FAILURE CRITERIA, AND EQUALS ULTIMATE SIDE FRICTION PLUS MOBILIZED END BEARING.
- 3. ALLOWABLE PILE CAPACITY IS 1/2 THE DAVISSON PILE CAPACITY.
- 4. ULTIMATE PILE CAPACITY IS ULTIMATE SIDE FRICTION PLUS 3 x THE MOBILIZED END BEARING. EXCEPTION: FOR H-PILES TIPPED IN SAND OR LIMESTONE, THE

ULTIMATE PILE CAPACITY IS ULTIMATE SIDE FRICTION PLUS 2  $\times$  THE MOBILIZED END BEARING.



Photo No. 1: B-6 Facing southwest



Photo No. 2: B-8 Facing southwest

	G-6A Pump Station West Palm Beach Palm Beach County, Florida			
	SITE PHOTOGRAPHS			
UNIVERSAL	Project No. 0630.2000012	Date: June 10, 2020		
ENGINEERING SCIENCES	Report No. 17223	Page B-68		



Photo No. 3: B-9 Facing north



Photo No. 4: B-11 Facing southeast

	G-6A Pump Station West Palm Beach Palm Beach County, Florida			
	SITE PHOTOGRAPHS			
UNIVERSAL	Project No. 0630.2000012	Date: June 10, 2020		
ENGINEERING SCIENCES	Report No. 17223	Page B-69		

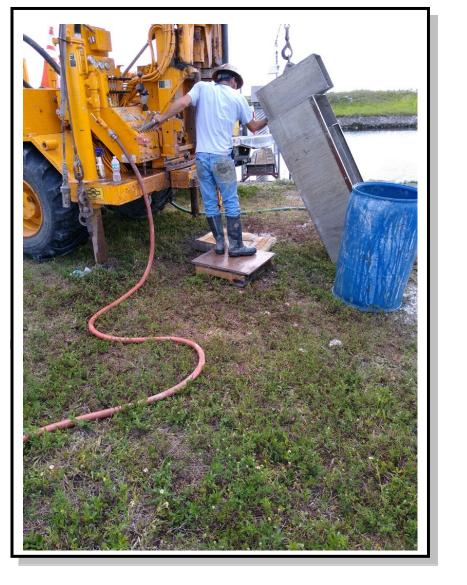
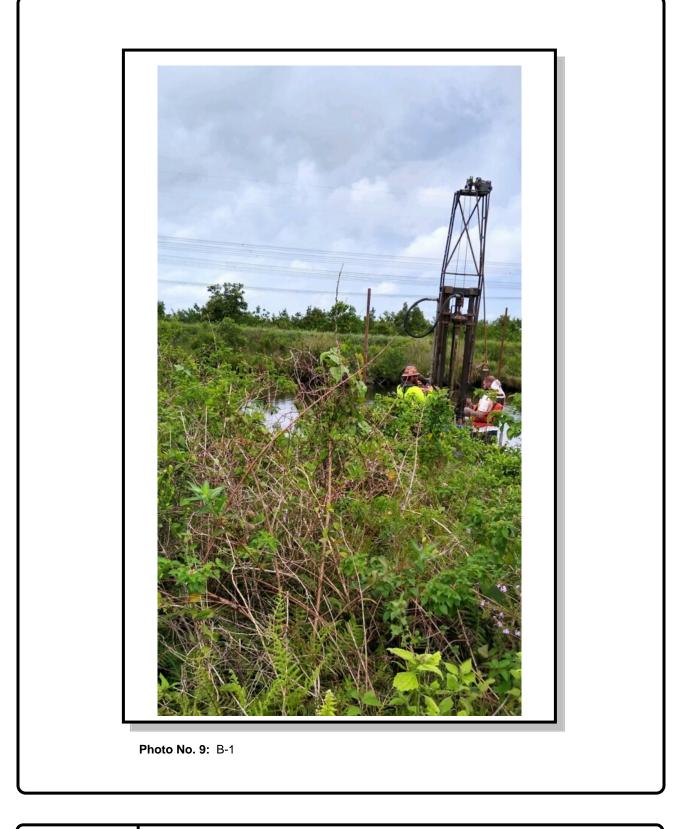
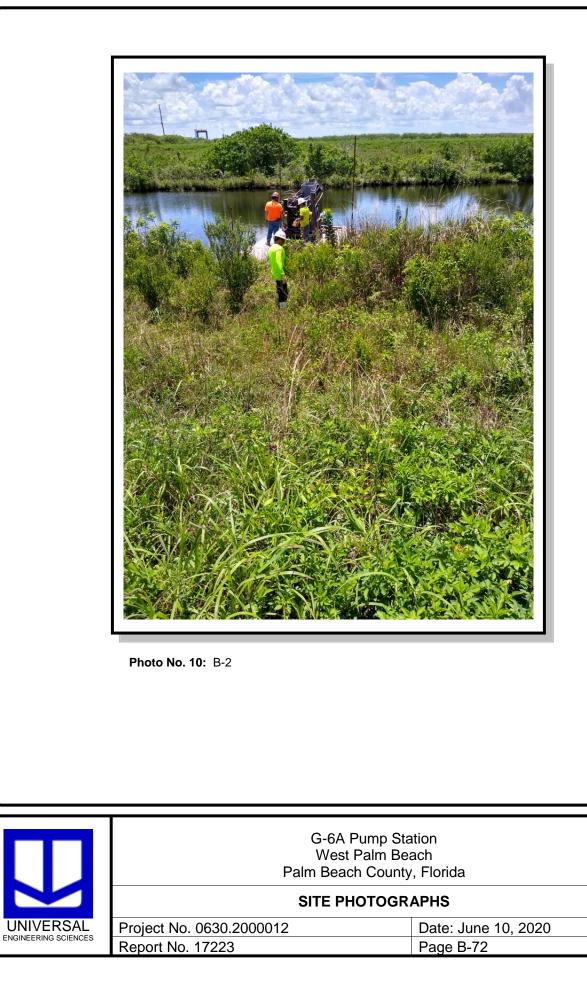


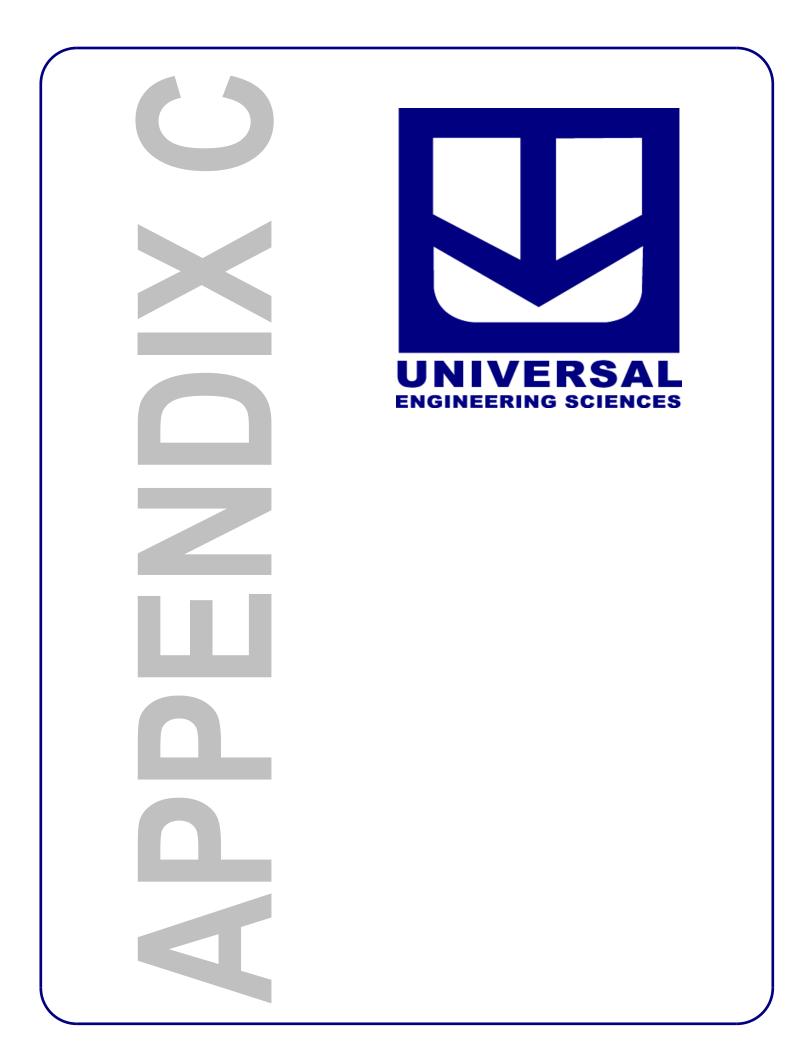
Photo No. 5: B-12 Facing northeast

	G-6A Pump Station West Palm Beach Palm Beach County, Florida			
	SITE PHOTOGRAPHS			
UNIVERSAL	Project No. 0630.2000012	Date: June 10, 2020		
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	G-6A Pump Station West Palm Beach Palm Beach County, Florida		
	SITE PHOTOGRAPHS		
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# Important Information about This Geotechnical-Engineering Report

Subsurface problems are a principal cause of construction delays, cost overruns, claims, and disputes.

While you cannot eliminate all such risks, you can manage them. The following information is provided to help.

# Geotechnical Services Are Performed for Specific Purposes, Persons, and Projects

Geotechnical engineers structure their services to meet the specific needs of their clients. A geotechnical-engineering study conducted for a civil engineer may not fulfill the needs of a constructor — a construction contractor — or even another civil engineer. Because each geotechnical- engineering study is unique, each geotechnical-engineering report is unique, prepared *solely* for the client. No one except you should rely on this geotechnical-engineering report without first conferring with the geotechnical engineer who prepared it. *And no one* — *not even you* — should apply this report for any purpose or project except the one originally contemplated.

# **Read the Full Report**

Serious problems have occurred because those relying on a geotechnical-engineering report did not read it all. Do not rely on an executive summary. Do not read selected elements only.

# Geotechnical Engineers Base Each Report on a Unique Set of Project-Specific Factors

Geotechnical engineers consider many unique, project-specific factors when establishing the scope of a study. Typical factors include: the client's goals, objectives, and risk-management preferences; the general nature of the structure involved, its size, and configuration; the location of the structure on the site; and other planned or existing site improvements, such as access roads, parking lots, and underground utilities. Unless the geotechnical engineer who conducted the study specifically indicates otherwise, do not rely on a geotechnical-engineering report that was:

- not prepared for you;
- not prepared for your project;
- not prepared for the specific site explored; or
- completed before important project changes were made.

Typical changes that can erode the reliability of an existing geotechnical-engineering report include those that affect:

- the function of the proposed structure, as when it's changed from a parking garage to an office building, or from a lightindustrial plant to a refrigerated warehouse;
- the elevation, configuration, location, orientation, or weight of the proposed structure;
- the composition of the design team; or
- project ownership.

As a general rule, *always* inform your geotechnical engineer of project changes—even minor ones—and request an

assessment of their impact. Geotechnical engineers cannot accept responsibility or liability for problems that occur because their reports do not consider developments of which they were not informed.

# Subsurface Conditions Can Change

A geotechnical-engineering report is based on conditions that existed at the time the geotechnical engineer performed the study. *Do not rely on a geotechnical-engineering report whose adequacy may have been affected by*: the passage of time; man-made events, such as construction on or adjacent to the site; or natural events, such as floods, droughts, earthquakes, or groundwater fluctuations. *Contact the geotechnical engineer before applying this report to determine if it is still reliable.* A minor amount of additional testing or analysis could prevent major problems.

# Most Geotechnical Findings Are Professional Opinions

Site exploration identifies subsurface conditions only at those points where subsurface tests are conducted or samples are taken. Geotechnical engineers review field and laboratory data and then apply their professional judgment to render an opinion about subsurface conditions throughout the site. Actual subsurface conditions may differ — sometimes significantly — from those indicated in your report. Retaining the geotechnical engineer who developed your report to provide geotechnical-construction observation is the most effective method of managing the risks associated with unanticipated conditions.

# A Report's Recommendations Are Not Final

Do not overrely on the confirmation-dependent recommendations included in your report. *Confirmationdependent recommendations are not final*, because geotechnical engineers develop them principally from judgment and opinion. Geotechnical engineers can finalize their recommendations *only* by observing actual subsurface conditions revealed during construction. *The geotechnical engineer who developed your report cannot assume responsibility or liability for the report's confirmation-dependent recommendations if that engineer does not perform the geotechnical-construction observation required to confirm the recommendations' applicability.* 

# A Geotechnical-Engineering Report Is Subject to Misinterpretation

Other design-team members' misinterpretation of geotechnical-engineering reports has resulted in costly

problems. Confront that risk by having your geotechnical engineer confer with appropriate members of the design team after submitting the report. Also retain your geotechnical engineer to review pertinent elements of the design team's plans and specifications. Constructors can also misinterpret a geotechnical-engineering report. Confront that risk by having your geotechnical engineer participate in prebid and preconstruction conferences, and by providing geotechnical construction observation.

# Do Not Redraw the Engineer's Logs

Geotechnical engineers prepare final boring and testing logs based upon their interpretation of field logs and laboratory data. To prevent errors or omissions, the logs included in a geotechnical-engineering report should *never* be redrawn for inclusion in architectural or other design drawings. Only photographic or electronic reproduction is acceptable, *but recognize that separating logs from the report can elevate risk.* 

# Give Constructors a Complete Report and Guidance

Some owners and design professionals mistakenly believe they can make constructors liable for unanticipated subsurface conditions by limiting what they provide for bid preparation. To help prevent costly problems, give constructors the complete geotechnical-engineering report, but preface it with a clearly written letter of transmittal. In that letter, advise constructors that the report was not prepared for purposes of bid development and that the report's accuracy is limited; encourage them to confer with the geotechnical engineer who prepared the report (a modest fee may be required) and/ or to conduct additional study to obtain the specific types of information they need or prefer. A prebid conference can also be valuable. *Be sure constructors have sufficient time* to perform additional study. Only then might you be in a position to give constructors the best information available to you, while requiring them to at least share some of the financial responsibilities stemming from unanticipated conditions.

# **Read Responsibility Provisions Closely**

Some clients, design professionals, and constructors fail to recognize that geotechnical engineering is far less exact than other engineering disciplines. This lack of understanding has created unrealistic expectations that have led to disappointments, claims, and disputes. To help reduce the risk of such outcomes, geotechnical engineers commonly include a variety of explanatory provisions in their reports. Sometimes labeled "limitations," many of these provisions indicate where geotechnical engineers' responsibilities begin and end, to help others recognize their own responsibilities and risks. *Read these provisions closely*. Ask questions. Your geotechnical engineer should respond fully and frankly.

# **Environmental Concerns Are Not Covered**

The equipment, techniques, and personnel used to perform an *environmental* study differ significantly from those used to perform a *geotechnical* study. For that reason, a geotechnicalengineering report does not usually relate any environmental findings, conclusions, or recommendations; e.g., about the likelihood of encountering underground storage tanks or regulated contaminants. *Unanticipated environmental problems have led to numerous project failures*. If you have not yet obtained your own environmental information, ask your geotechnical consultant for risk-management guidance. *Do not rely on an environmental report prepared for someone else.* 

# Obtain Professional Assistance To Deal with Mold

Diverse strategies can be applied during building design, construction, operation, and maintenance to prevent significant amounts of mold from growing on indoor surfaces. To be effective, all such strategies should be devised for the express purpose of mold prevention, integrated into a comprehensive plan, and executed with diligent oversight by a professional mold-prevention consultant. Because just a small amount of water or moisture can lead to the development of severe mold infestations, many mold- prevention strategies focus on keeping building surfaces dry. While groundwater, water infiltration, and similar issues may have been addressed as part of the geotechnical- engineering study whose findings are conveyed in this report, the geotechnical engineer in charge of this project is not a mold prevention consultant; none of the services performed in connection with the geotechnical engineer's study were designed or conducted for the purpose of mold prevention. Proper implementation of the recommendations conveyed in this report will not of itself be sufficient to prevent mold from growing in or on the structure involved.

# Rely, on Your GBC-Member Geotechnical Engineer for Additional Assistance

Membership in the Geotechnical Business Council of the Geoprofessional Business Association exposes geotechnical engineers to a wide array of risk-confrontation techniques that can be of genuine benefit for everyone involved with a construction project. Confer with you GBC-Member geotechnical engineer for more information.



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# **CONSTRAINTS & RESTRICTIONS**

The intent of this document is to bring to your attention the potential concerns and the basic limitations of a typical geotechnical report.

# WARRANTY

Universal Engineering Sciences has prepared this report for our client for his exclusive use, in accordance with generally accepted soil and foundation engineering practices, and makes no other warranty either expressed or implied as to the professional advice provided in the report.

# UNANTICIPATED SOIL CONDITIONS

The analysis and recommendations submitted in this report are based upon the data obtained from soil borings performed at the locations indicated on the Boring Location Plan. This report does not reflect any variations which may occur between these borings.

The nature and extent of variations between borings may not become known until excavation begins. If variations appear, we may have to re-evaluate our recommendations after performing on-site observations and noting the characteristics of any variations.

# **CHANGED CONDITIONS**

We recommend that the specifications for the project require that the contractor immediately notify Universal Engineering Sciences, as well as the owner, when subsurface conditions are encountered that are different from those present in this report.

No claim by the contractor for any conditions differing from those anticipated in the plans, specifications, and those found in this report, should be allowed unless the contractor notifies the owner and Universal Engineering Sciences of such changed conditions. Further, we recommend that all foundation work and site improvements be observed by a representative of Universal Engineering Sciences to monitor field conditions and changes, to verify design assumptions and to evaluate and recommend any appropriate modifications to this report.

# MISINTERPRETATION OF SOIL ENGINEERING REPORT

Universal Engineering Sciences is responsible for the conclusions and opinions contained within this report based upon the data relating only to the specific project and location discussed herein. If the conclusions or recommendations based upon the data presented are made by others, those conclusions or recommendations are not the responsibility of Universal Engineering Sciences.

# CHANGED STRUCTURE OR LOCATION

This report was prepared in order to aid in the evaluation of this project and to assist the architect or engineer in the design of this project. If any changes in the design or location of the structure as outlined in this report are planned, or if any structures are included or added that are not discussed in the report, the conclusions and recommendations contained in this report shall not be considered valid unless the changes are reviewed and the conclusions modified or approved by Universal Engineering Sciences.

# USE OF REPORT BY BIDDERS

Bidders who are examining the report prior to submission of a bid are cautioned that this report was prepared as an aid to the designers of the project and it may affect actual construction operations. Bidders are urged to make their own soil borings, test pits, test caissons or other investigations to determine those conditions that may affect construction operations. Universal Engineering Sciences cannot be responsible for any interpretations made from this report or the attached boring logs with regard to their adequacy in reflecting subsurface conditions which will affect construction operations.

# STRATA CHANGES

Strata changes are indicated by a definite line on the boring logs which accompany this report. However, the actual change in the ground may be more gradual. Where changes occur between soil samples, the location of the change must necessarily be estimated using all available information and may not be shown at the exact depth.

# **OBSERVATIONS DURING DRILLING**

Attempts are made to detect and/or identify occurrences during drilling and sampling, such as: water level, boulders, zones of lost circulation, relative ease or resistance to drilling progress, unusual sample recovery, variation of driving resistance, obstructions, etc.; however, lack of mention does not preclude their presence.

# WATER LEVELS

Water level readings have been made in the drill holes during drilling and they indicate normally occurring conditions. Water levels may not have been stabilized at the last reading. This data has been reviewed and interpretations made in this report. However, it must be noted that fluctuations in the level of the groundwater may occur due to variations in rainfall, temperature, tides, and other factors not evident at the time measurements were made and reported. Since the probability of such variations is anticipated, design drawings and specifications should accommodate such possibilities and construction planning should be based upon such assumptions of variations.

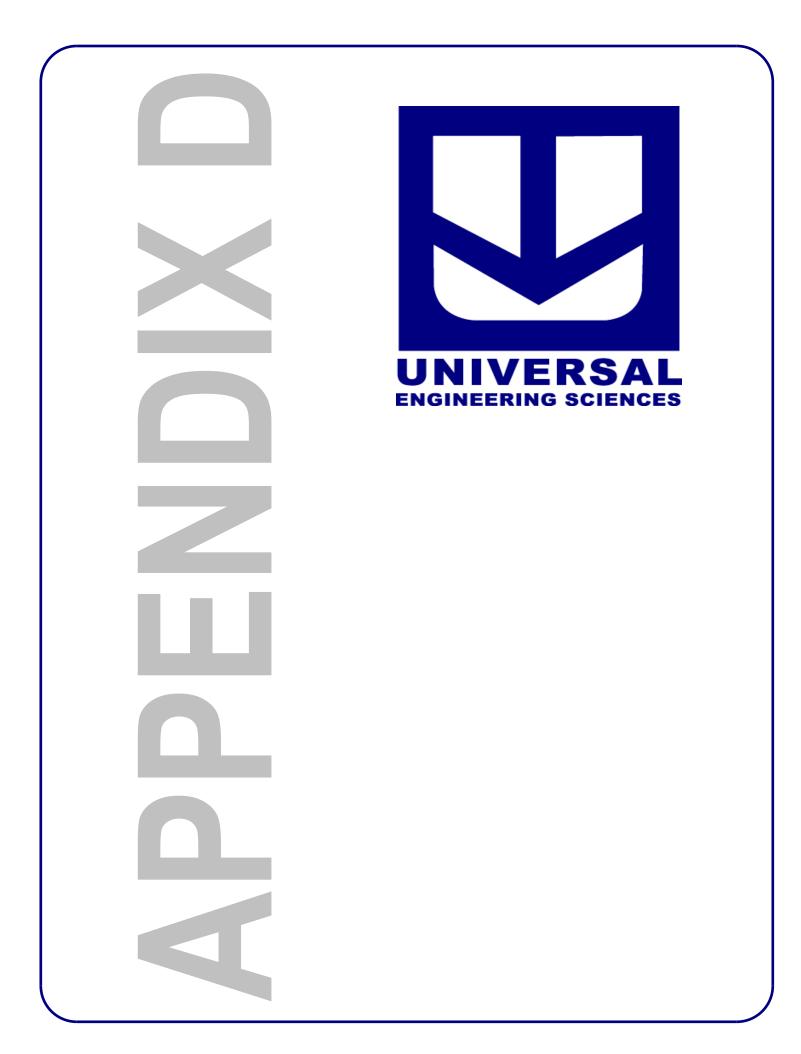
# LOCATION OF BURIED OBJECTS

All users of this report are cautioned that there was no requirement for Universal Engineering Sciences to attempt to locate any man-made buried objects during the course of this exploration and that no attempt was made by Universal Engineering Sciences to locate any such buried objects. Universal Engineering Sciences cannot be responsible for any buried man-made objects which are subsequently encountered during construction that are not discussed within the text of this report.

# TIME

This report reflects the soil conditions at the time of exploration. If the report is not used in a reasonable amount of time, significant changes to the site may occur and additional reviews may be required.





# Universal Engineering Sciences, Inc. GENERAL CONDITIONS

# SECTION 1: RESPONSIBILITIES

- 1.1 Universal Engineering Sciences, LLC, Universal Engineering Inspections, LLC, and GFA International Inc. ("UES"), have the responsibility for providing the services described under the Scope of Services section. The work is to be performed according to accepted standards of care and is to be completed in a timely manner. The term "UES" as used herein includes all of Universal Engineering Sciences, LLC, Universal Engineering Inspections, LLC, GFA International, Inc., its' agents, employees, professional staff, and subcontractors.
- 1.2 The Client or a duly authorized representative is responsible for providing UES with a clear understanding of the project nature and scope. The Client shall supply UES with sufficient and adequate information, including, but not limited to, maps, site plans, reports, surveys and designs, to allow UES to properly complete the specified services. The Client shall also communicate changes in the nature and scope of the project as soon as possible during performance of the work so that the changes can be incorporated into the work product.
- 1.3 The Client acknowledges that UES's responsibilities in providing the services described under the Scope of Services section is limited to those services described therein, and the Client hereby assumes any collateral or affiliated duties necessitated by or for those services. Such duties may include, but are not limited to, reporting requirements imposed by any third party such as federal, state, or local entities, the provision of any required notices to any third party, or the securing of necessary permits or permissions from any third parties required for UES's provision of the services so described, unless otherwise agreed upon by both parties.
- 1.4 Universal will not be responsible for scheduling our services and will not be responsible for tests or inspections that are not performed due to a failure to schedule our services on the project or any resulting damages.

# 1.5 PURSUANT TO FLORIDA STATUTES §558.0035, ANY INDIVIDUAL EMPLOYEE OR AGENT OF UES MAY NOT BE HELD INDIVIDUALLY LIABLE FOR NEGLIGENCE.

# SECTION 2: STANDARD OF CARE

- 2.1 Services performed by UES under this Agreement will be conducted in a manner consistent with the level of care and skill ordinarily exercised by members of UES's profession practicing contemporaneously under similar conditions in the locality of the project. No other warranty, express or implied, is made.
- 2.2 The Client recognizes that subsurface conditions may vary from those observed at locations where borings, surveys, or other explorations are made, and that site conditions may change with time. Data, interpretations, and recommendations by UES will be based solely on information available to UES at the time of service. UES is responsible for those data, interpretations, and recommendations, but will not be responsible for other parties' interpretations or use of the information developed.
- 2.3 Execution of this document by UES is not a representation that UES has visited the site, become generally familiar with local conditions under which the services are to be performed, or correlated personal observations with the requirements of the Scope of Services. It is the Client's responsibility to provide UES with all information necessary for UES to provide the services described under the Scope of Services, and the Client assumes all liability for information not provided to UES that may affect the quality or sufficiency of the services so described.
- 2.4 Should UES be retained to provide threshold inspection services under Florida Statutes §553.79, Client acknowledges that UES's services thereunder do not constitute a guarantee that the construction in question has been properly designed or constructed, and UES's services do not replace any of the obligations or liabilities associated with any architect, contractor, or structural engineer. Therefore it is explicitly agreed that the Client will not hold UES responsible for the proper performance of service by any architect, contractor, structural engineer or any other entity associated with the project.

# SECTION 3: SITE ACCESS AND SITE CONDITIONS

- 3.1 Client will grant or obtain free access to the site for all equipment and personnel necessary for UES to perform the work set forth in this Agreement. The Client will notify any and all possessors of the project site that Client has granted UES free access to the site. UES will take reasonable precautions to minimize damage to the site, but it is understood by Client that, in the normal course of work, some damage may occur, and the correction of such damage is not part of this Agreement unless so specified in the Proposal.
- 3.2 The Client is responsible for the accuracy of locations for all subterranean structures and utilities. UES will take reasonable precautions to avoid known subterranean structures, and the Client waives any claim against UES, and agrees to defend, indemnify, and hold UES harmless from any claim or liability for injury or loss, including costs of defense, arising from damage done to subterranean structures and utilities not identified or accurately located. In addition, Client agrees to compensate UES for any time spent or expenses incurred by UES in defense of any such claim with compensation to be based upon UES's prevailing fee schedule and expense reimbursement policy.

# SECTION 4: SAMPLE OWNERSHIP AND DISPOSAL

- 4.1 Soil or water samples obtained from the project during performance of the work shall remain the property of the Client.
- 4.2 UES will dispose of or return to Client all remaining soils and rock samples 60 days after submission of report covering those samples. Further storage or transfer of samples can be made at Client's expense upon Client's prior written request.
- 4.3 Samples which are contaminated by petroleum products or other chemical waste will be returned to Client for treatment or disposal, consistent with all appropriate federal, state, or local regulations.

# SECTION 5: BILLING AND PAYMENT

- 5.1 UES will submit invoices to Client monthly or upon completion of services. Invoices will show charges for different personnel and expense classifications.
- 5.2 Payment is due 30 days after presentation of invoice and is past due 31 days from invoice date. Client agrees to pay a finance charge of one and one-half percent (1 ½ %) per month, or the maximum rate allowed by law, on past due accounts.
- 5.3 If UES incurs any expenses to collect overdue billings on invoices, the sums paid by UES for reasonable attorneys' fees, court costs, UES's time, UES's expenses, and interest will be due and owing by the Client.

# SECTION 6: OWNERSHIP AND USE OF DOCUMENTS

- 6.1 All reports, boring logs, field data, field notes, laboratory test data, calculations, estimates, and other documents prepared by UES, as instruments of service, shall remain the property of UES.
- 6.2 Client agrees that all reports and other work furnished to the Client or his agents, which are not paid for, will be returned upon demand and will not be used by the Client for any purpose.
- 6.3 UES will retain all pertinent records relating to the services performed for a period of five years following submission of the report, during which period the records will be made available to the Client at all reasonable times.
- 6.4 All reports, boring logs, field data, field notes, laboratory test data, calculations, estimates, and other documents prepared by UES, are prepared for the sole and exclusive use of Client, and may not be given to any other party or used or relied upon by any such party without the express written consent of UES.

# SECTION 7: DISCOVERY OF UNANTICIPATED HAZARDOUS MATERIALS

- Client warrants that a reasonable effort has been made to inform UES of known or suspected hazardous materials on or near the project site.
   Under this agreement, the term hazardous materials include hazardous materials (40 CFR 172.01), hazardous wastes (40 CFR 261.2),
- hazardous substances (40 CFR 300.6), petroleum products, polychlorinated biphenyls, and asbestos.
- 7.3 Hazardous materials may exist at a site where there is no reason to believe they could or should be present. UES and Client agree that the discovery of unanticipated hazardous materials constitutes a changed condition mandating a renegotiation of the scope of work. UES and Client also agree that the discovery of unanticipated hazardous materials may make it necessary for UES to take immediate measures to protect health and safety. Client agrees to compensate UES for any equipment decontamination or other costs incident to the discovery of unanticipated hazardous waste.
- 7.4 UES agrees to notify Client when unanticipated hazardous materials or suspected hazardous materials are encountered. Client agrees to make any disclosures required by law to the appropriate governing agencies. Client also agrees to hold UES harmless for any and all consequences of disclosures made by UES which are required by governing law. In the event the project site is not owned by Client, Client recognizes that it is the Client's responsibility to inform the property owner of the discovery of unanticipated hazardous materials or suspected hazardous materials.
- 7.5 Notwithstanding any other provision of the Agreement, Client waives any claim against UES, and to the maximum extent permitted by law, agrees to defend, indemnify, and save UES harmless from any claim, liability, and/or defense costs for injury or loss arising from UES's discovery of unanticipated hazardous materials or suspected hazardous materials including any costs created by delay of the project and any cost associated with possible reduction of the property's value. Client will be responsible for ultimate disposal of any samples secured by UES which are found to be contaminated.

# SECTION 8: RISK ALLOCATION

8.1 Client agrees that UES's liability for any damage on account of any breach of contract, error, omission or other professional negligence will be limited to a sum not to exceed \$50,000 or UES's fee, whichever is greater. If Client prefers to have higher limits on contractual or professional liability, UES agrees to increase the limits up to a maximum of \$1,000,000.00 upon Client's written request at the time of accepting our proposal provided that Client agrees to pay an additional consideration of four percent of the total fee, or \$400.00, whichever is greater. The additional charge for the higher liability limits is because of the greater risk assumed and is not strictly a charge for additional professional liability insurance.

### SECTION 9: INSURANCE

9.1 UES represents and warrants that it and its agents, staff and consultants employed by it, is and are protected by worker's compensation insurance and that UES has such coverage under public liability and property damage insurance policies which UES deems to be adequate. Certificates for all such policies of insurance shall be provided to Client upon request in writing. Within the limits and conditions of such insurance, UES agrees to indemnify and save Client harmless from and against loss, damage, or liability arising from negligent acts by UES, its agents, staff, and consultants employed by it. UES shall not be responsible for any loss, damage or liability beyond the amounts, limits, and conditions of such insurance or the limits described in Section 8, whichever is less. The Client agrees to defend, indemnify and save UES harmless for loss, damage or liability arising from acts by Client, Client's agent, staff, and other UESs employed by Client.

# SECTION 10: DISPUTE RESOLUTION

- 10.1 All claims, disputes, and other matters in controversy between UES and Client arising out of or in any way related to this Agreement will be submitted to alternative dispute resolution (ADR) such as mediation or arbitration, before and as a condition precedent to other remedies provided by law, including the commencement of litigation.
- 10.2 If a dispute arises related to the services provided under this Agreement and that dispute requires litigation instead of ADR as provided above, then:
  - (a) the claim will be brought and tried in judicial jurisdiction of the court of the county where UES's principal place of business is located and Client waives the right to remove the action to any other county or judicial jurisdiction, and
  - (b) The prevailing party will be entitled to recovery of all reasonable costs incurred, including staff time, court costs, attorneys' fees, and other claim related expenses.

### SECTION 11: TERMINATION

- 11.1 This agreement may be terminated by either party upon seven (7) days written notice in the event of substantial failure by the other party to perform in accordance with the terms hereof. Such termination shall not be effective if that substantial failure has been remedied before expiration of the period specified in the written notice. In the event of termination, UES shall be paid for services performed to the termination notice date plus reasonable termination expenses.
- 11.2 In the event of termination, or suspension for more than three (3) months, prior to completion of all reports contemplated by the Agreement, UES may complete such analyses and records as are necessary to complete its files and may also complete a report on the services performed to the date of notice of termination or suspension. The expense of termination or suspension shall include all direct costs of UES in completing such analyses, records and reports.

# SECTION 12: ASSIGNS

12.1 Neither the Client nor UES may delegate, assign, sublet or transfer their duties or interest in this Agreement without the written consent of the other party.

# SECTION 13. GOVERNING LAW AND SURVIVAL

- 13.1 The laws of the State of Florida will govern the validity of these Terms, their interpretation and performance.
- 13.2 If any of the provisions contained in this Agreement are held illegal, invalid, or unenforceable, the enforceability of the remaining provisions will not be impaired. Limitations of liability and indemnities will survive termination of this Agreement for any cause.

### SECTION 14. INTEGRATION CLAUSE

- 14.1 This Agreement represents and contains the entire and only agreement and understanding among the parties with respect to the subject matter of this Agreement, and supersedes any and all prior and contemporaneous oral and written agreements, understandings, representations, inducements, promises, warranties, and conditions among the parties. No agreement, understanding, representation, inducement, promise, warranty, or condition of any kind with respect to the subject matter of this Agreement shall be relied upon by the parties unless expressly incorporated herein.
- 14.2 This Agreement may not be amended or modified except by an agreement in writing signed by the party against whom the enforcement of any modification or amendment is sought.

Rev. 3/26/2020 (Docs No. 1758555)