HYDROGEOLOGICAL REPORT

Blevin

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AQUIFER PERFORMANCE TESTING & GROUNDWATER FLOW MODELING

Prepared for:





DYER, RIDDLE, MILLS & PRECOURT, INC.

ENGINEERS • SURVEYORS • SCIENTISTS • PLANNERS ORLANDO • JACKSONVILLE • MELBOURNE • TAMPA

DYER, RIDDLE, MILLS & PRECOURT, INC.

ENGINEERS · SURVEYORS · SCIENTISTS · PLANNERS

January 14, 1991

DRMP #90-571.00

Mr. Jon Rackley Jon's Nursery, Inc. 24546 Nursery Way Eustis, FL 32726

SUBJECT: Jon's Nursery Aquifer Performance Test

Final Report

Dear Mr. Rackley:

On November 20, 1990, Dyer, Riddle, Mills and Precourt, Inc. (DRMP) was contracted to conduct an Aquifer Performance Test (APT) for your company, Jon's Nursery Inc. This test was performed in order to determine aquifer parameters such as transmissivity, storativity and leakance, in the immediate study area. These parameters were determined and then used in a groundwater flow model to simulate the influences on the surficial aquifer due to withdrawal from the Floridan aquifer. The test and modeling were performed to satisfy special conditions of the Consumptive Use Permit (CUP) and other concerns as requested by the St. Johns River Water Management District.

This report details data collection and analyses performed for the APT and describes the findings. It is presented in fulfillment of our November 20, 1990 agreement.

We appreciate the opportunity of providing these services to you. If we may be of any further assistance, or if you have any questions or comments concerning this report, please do not hesitate to give us a call.

Sincerely,

Dyer, Biddle, Mills & Precourt, Inc.

Patrick Barnes

Hydrogeology Group Manager

Joel Kimrey, P.G. Senior Hydrogeologist

Julyans 1

Douglas Dufresne

Project Hydrogeologist

DD/jkl/1-14jr

Please reply to: P.O. Box 538505

AQUIFER PERFORMANCE TESTING AND GROUNDWATER FLOW MODELING

Prepared for

Jon's Nursery, Inc.

Prepared by

Dyer, Riddle, Mills and Precourt, Inc.
Orlando Jacksonville Melbourne Tampa

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AQUIFER PERFORMANCE TESTING AND GROUNDWATER FLOW MODELING

1.0 GENERAL

Jon's Nursery, located one mile north of S.R. 44, off of S.R. 437 in Eustis, Florida, is the second largest nursery within the St. Johns River Water Management District's boundaries. In order to maintain the extremely large quantity of plants grown there, the nursery withdraws approximately 160 MGY from its 8 Floridan aquifer irrigation wells. Although a state of the art water reuse project is currently underway which will lead to an overall reduction in withdrawal of water, District concerns as to the overall growth of the nursery and the need to model the drawdown induced in the surficial aquifer by the pumping of the nursery's wells warrant hydrogeologic testing. The nursery is contained on approximately 200 acres of rolling hills in the Marion Upland Physiographic province. The area is in the middle stages of karstic development, with elevations ranging from approximately 75 ft to 105 ft above mean sea level. Generally, movement of surficial aquifer water is toward the southwest and northwest across the site. Site drainage is probably controlled, however, by site-specific conditions caused by groundwater mounding due to The water table below heavily irrigated areas is irrigation. approximately 20 feet higher than background water particularly with respect to areas adjacent to the planned nursery expansion area.

The property boundary and relative positions of wells on site pertinent to the study can be seen in Figure 1. Descriptions of these wells can be found in Table 1.

2.0 DATA COLLECTION

Background water levels were recorded every 15 minutes in wells 10, S-1 and S-2 for a week prior to the constant rate discharge test with the use of a Terra 8 data acquisition system and three pressure transducers. Recording of water level fluctuations in the surficial aquifer was accomplished by data collected on wells S-1 and S-2. The Floridan aquifer was monitored by recording potentiometric surface fluctuations in well 10.

On November 28 geophysical logging of well 10 was performed by Southern Resource Exploration. The geophysical log suite consisted of resistivity, spontaneous potential, natural gamma and caliper logs. Copies of these logs are included as Attachment A.

A constant rate discharge test was then performed in order to determine aquifer parameters and effects of withdrawal from the Floridan aquifer on both the surficial and Floridan aquifers.

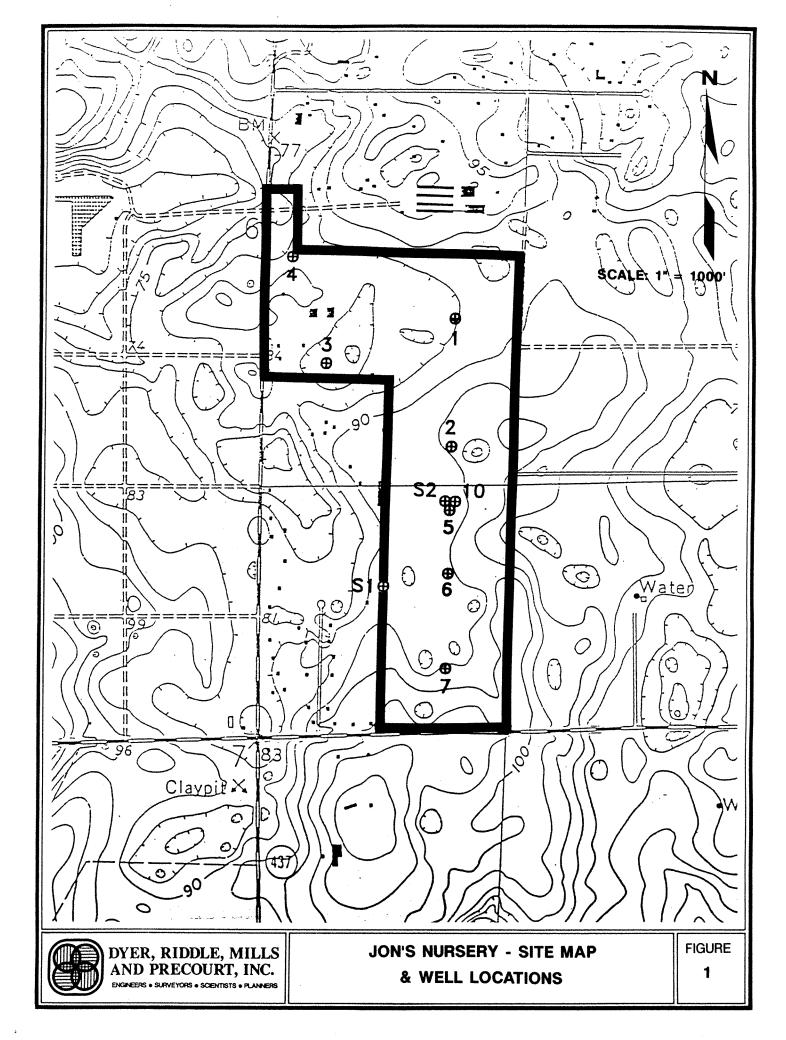


TABLE 1
WELL CONSTRUCTION AND WITHDRAWAL

WELL	WELL DIAMETER	CASING DEPTH	TOTAL DEPTH	AVERAGE WITHDRAWAL	SOURCE	
ID	(in)	(ft)	(ft)	(gpm)	AQUIFER	USE
1	10	65	475	600	Floridan	Nursery
2	10	65	150	600	Floridan	Nursery
3	10	70	150	100	Floridan	Nursery
4	10	65	200	600	Floridan	Nursery
5	10	65	200	600	Floridan	Nursery
6	10	65	200	1000	Floridan	Nursery
7*	10	65	200	1000	Floridan	Nursery
8**	4	65	150		Floridan	Abandon
9**	4	65	150	30	Floridan	Domestic
10	4	65	125	30	Floridan	Irrigation
S-1	2	50	60		Surficial	Observation
S-2	2	36	43	****	Surficial	Observation

Notes:

- * Well 7 is proposed
- ** Wells 8 and 9 were not included in the APT or the groundwater flow model and therefore were not included in Figure 1. Well 8 is going to be abandoned in the future and well 9 only withdraws 30 gpm for short durations and will not greatly influence drawdown in the area.

Well 5 was the pumping well in the test and was discharged at a constant rate of 600 gpm for 48 hours. Recovery was allowed for four hours after the test by no additional pumping in well 5. Well 10, which is approximately 42 feet north of well 5, was monitored with a pressure transducer for the duration of the pump test and the recovery period. Wells S-1 and S-2 are located approximately 1015 feet south-southwest and 44 feet north of well 5, respectively. Both of these wells were also monitored with pressure transducers during the pump test and recovery period.

Rainfall data was collected during the 48-hour test with a rainfall gauge setup near the pumping well station. No rainfall was recorded during this period.

Water samples were collected at the beginning of pumping, 24 hours into the pump test and at the end of the pump test. These samples were sent to Bionomics Laboratory, Inc. and analyzed for pH, bicarbonate, chlorides, conductivity, hardness, sulfates, total dissolved solids (TDS), calcium, iron, magnesium and sodium. Attachment B contains the results of the water quality testing.

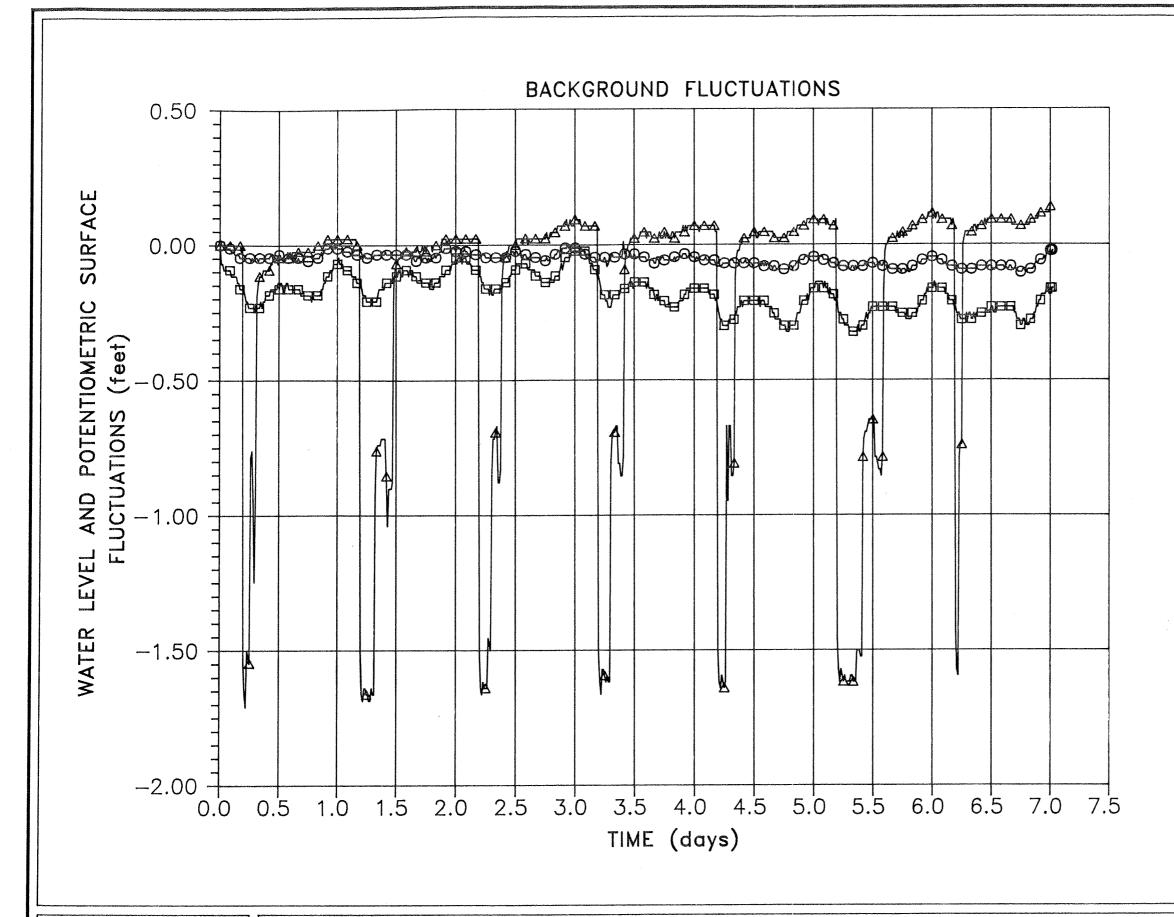
3.0 DATA ANALYSIS AND RESULTS

Background fluctuations in water levels and the potentiometric surface of the Floridan aquifer can be seen in Figure 2. The lines plotted on the graph reflect data collected every 15 minutes, but, in order to reduce clutter in this graph, symbols were only used to denote every hour of the sampling period.

Well 5 along with other wells at the nursery were being utilized for irrigation during this background collection period and effects from these periods of pumpage can be seen in all three of the observation wells. Naturally the greatest of these effects could be seen in the Floridan well #10 which had a fluctuation from the initial reading of 1.7 feet during a period of pumpage. Fluctuations in the surficial aquifer during pump periods are on the same order of magnitude as fluctuations seen during periods of non-pumpage or recovery periods. The fluctuations during non-pumping periods are a result of a combination of tidal forces, atmospheric pressure, natural leakance from the surficial aquifer to the Floridan aquifer and withdrawal from the surficial aquifer in off site wells. Overall there appears to be a slight increase in the elevation of the potentiometric surface of the Floridan aquifer and a slight decrease in the water table elevation; both are probably due to natural recharge to the Floridan.

The caliper log (Attachment A) indicates that the borehole of well 10 ranges from 4 to 18 inches in diameter. From the casing depth of 65 feet to 87 feet the log reflects a relatively tight hole. There are a few slightly larger openings in the borehole from 87 to 120 feet, with the largest opening extending to 6.8 inches. At the bottom of the hole the diameter increased to 18

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- O SHALLOW WELL S-1
- □ SHALLOW WELL S-2
- △ FLORIDAN WELL #10

inches. The gamma log appears to indicate that there is a source of higher radiation in the 40 foot range which may correspond to the presence of a 10 foot thick clay confining layer found also in the drill cuttings. Below the casing the gamma log along with the resistivity log indicate that the first fifteen feet of open hole may consist of marine clays interbedded with some limerock which may also add to the vertical hydraulic confinement. The high peak in the gamma log at a depth of 79 feet may indicate an unconformity between geologic units, possibly the contact between Miocene and Eocene formations.

After the pump test was completed, the water level data for the Floridan aquifer well (10) and the two surficial wells (S-1) and (S-2) were reduced and analyzed. The data were converted into feet of drawdown and feet of recovery with their corresponding times relative to the start of each data collection period (Attachment C).

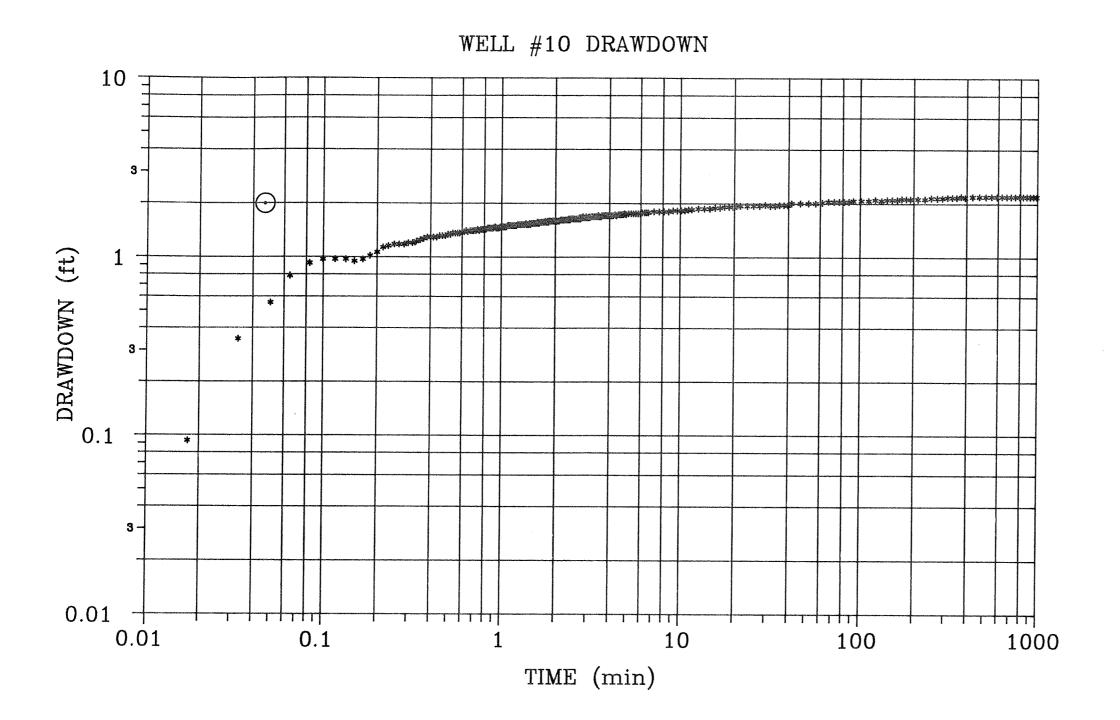
Figure 3 shows drawdown versus time (both plotted on log scale) for well 10 during the constant rate discharge test. Maximum drawdown after 2 days pumpage was 2.2 feet in this well. Using the Hantush-Jacob curve matching method it was possible to determine transmissivity, storativity and leakance from a match point. The match point and the calculations for the aquifer parameters are also shown in this figure. Variables used in the calculations are: T = transmissivity, gpd/ft; S = storativity; L = leakance, gpd/ft^3 ; Q = pumping rate, gpm; $W(u,r/B) = well function for leaky confined aquifers; <math>(h_0 - h) = drawdown$, feet; t = time after pumping began (or ended), minutes; u = coefficient of well function; r = radial distance between pumping well and observation well, feet; and r/B = coefficient of well function.

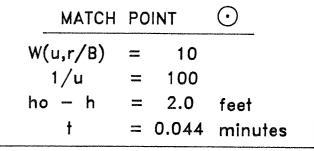
Transmissivity was calculated to be 343,800 gpd/ft; storativity and leakance were calculated from drawdown data to be 3.2×10^{-5} and 1.2×10^{-2} gpd/ft³, respectively.

Recovery in well 10 was plotted in Figure 4 similar to the drawdown plot. The total amount of recovery after 4 hours was 2.1 feet. Aquifer parameters were again calculated using the Hantush-Jacob method, and the calculations and match point are also shown in this figure. These data indicate slightly lower values for transmissivity and storativity of 298,957 gpd/ft and 2.6×10^{-5} , respectively, and a slightly higher value for leakance of 3.8×10^{-2} gpd/ft³.

Average transmissivity, storativity and leakance values for well 10 are 319,479 gpd/ft, 2.9 x 10^{-5} , and 2.5 x 10^{-2} gpd/ft³, respectively.

Drawdown and recovery plots were prepared for wells S-1 and S-2 in linear scale and are shown in Figure 5. At the beginning of the pump test the water level in well S-1 was not affected by the



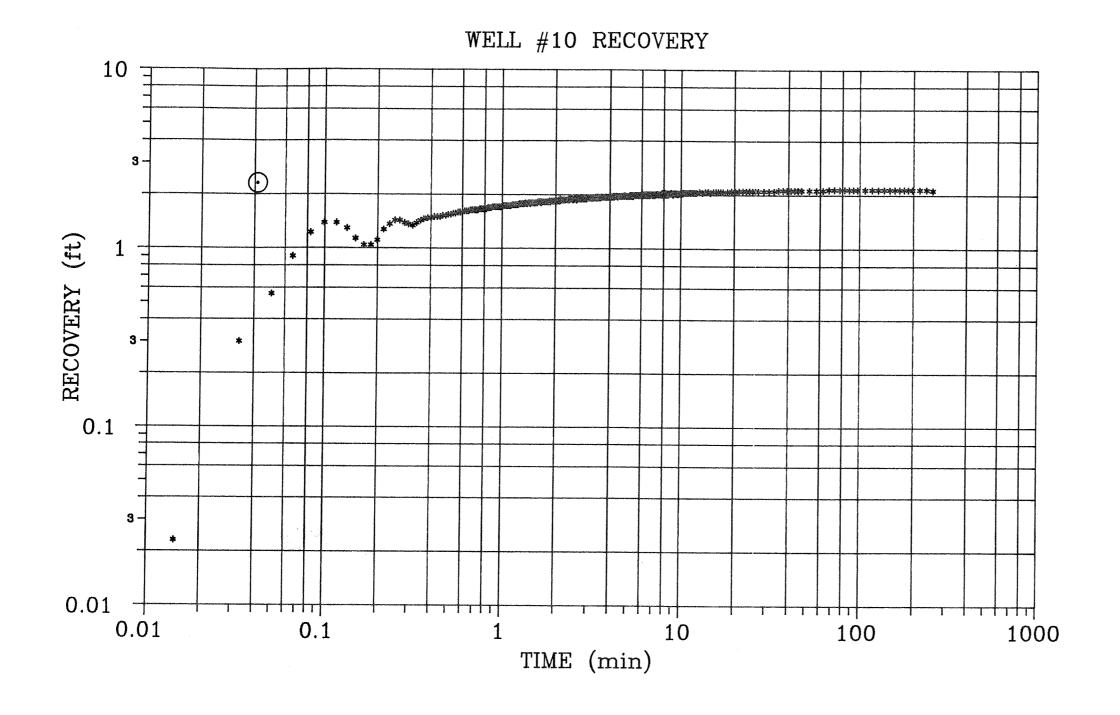


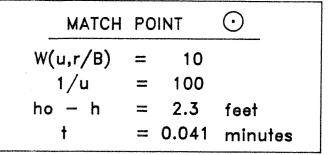
$$Q = 600 \text{ gpm}$$
 $r/B = 0.008$
 $r = 42 \text{ feet}$

$$T = \frac{114.6 \text{ Q}}{(\text{ho-h})} \text{ W(u,r/B)}$$

$$S = \frac{T \times t \times u}{2693 r^2}$$
$$= 3.2 \times 10^{-5}$$

$$L = \frac{T (r/B)^{2}}{r^{2}}$$
= 1.2 x 10⁻² gpd/ft³



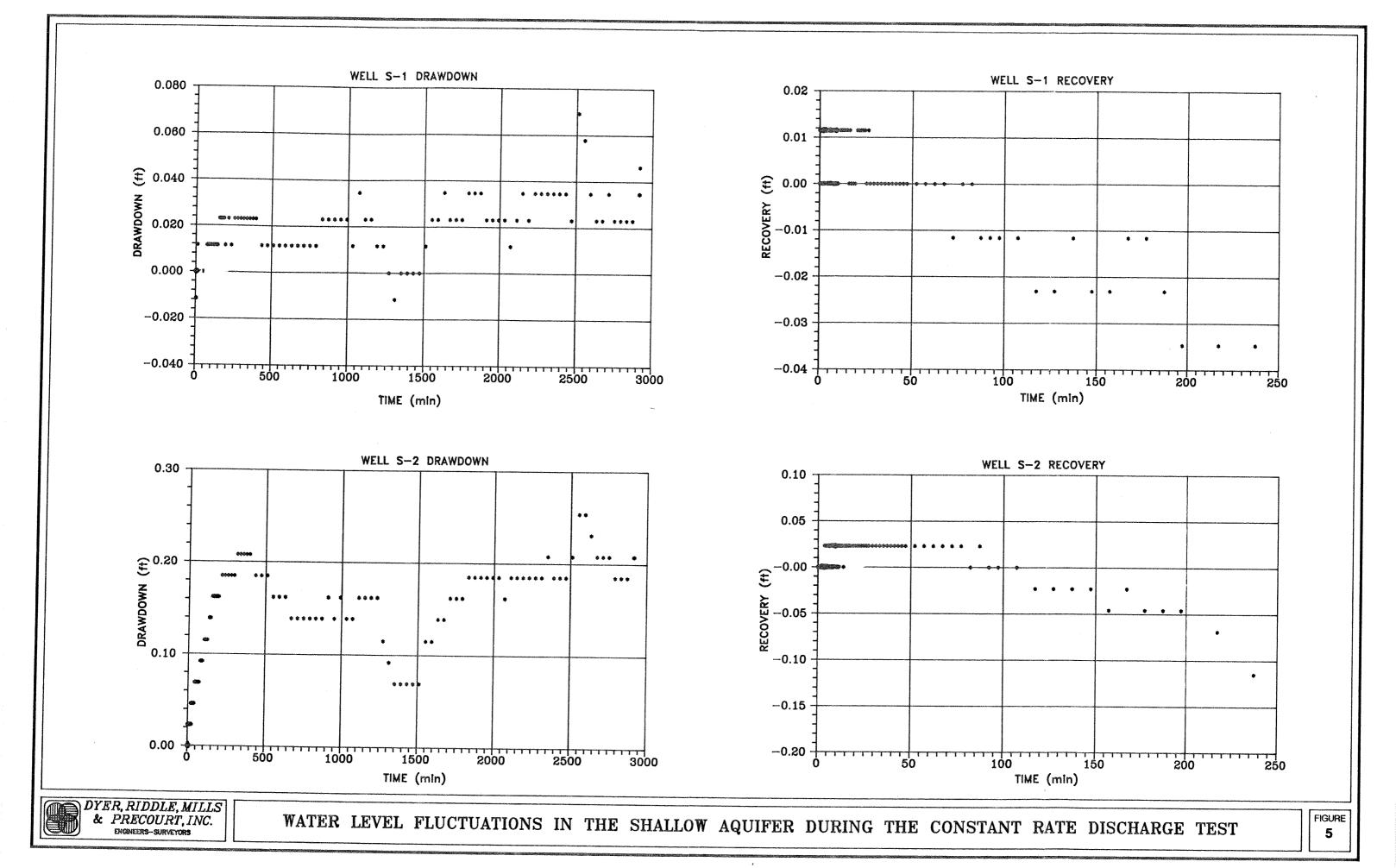


$$Q = 600 \text{ gpm}$$
 $r/B = 0.015$
 $r = 42 \text{ feet}$

$$T = \frac{114.6 \text{ Q}}{(\text{ho-h})}$$
 W(u,r/B)
= 298,957 gpd/ft

$$S = \frac{T \times t \times u}{2693 r^2}$$
$$= 2.6 \times 10^{-5}$$

$$L = \frac{T (r/B)^{2}}{r^{2}}$$
= 3.8 x 10⁻² gpd/ft³



cone of depression created in the Floridan and it actually rose 0.0115 feet before an effect was felt. Then, drawdown of 0.035 feet was measured from that point to a point 400 minutes into the test. After 400 minutes tidal and other influences overcame the drawdown which was probably induced by the test and again a rise in water level was recorded. Additional fluctuations were measured throughout the test which are probably linked to similar auxiliary sources and the test effects, but it is believed that drawdown induced by the test did not exceed 0.05 feet in well S-1.

Well S-2 shows a more rapid response to the pumping of well 5, but is affected by the cone of depression up to 400 minutes into the test before reflecting a rise in water level similar to well S-1. The fluctuations in well S-2 match relatively well with the fluctuations in well S-1, although they appear to be affected in a slightly different magnitude than in S-1. This difference is probably due to heterogeneity of the surficial aquifer in the immediate vicinities of these shallow wells. After thorough examination of the data, it is believed that drawdown induced by the pump test did not exceed 0.22 feet in well S-2.

The recovery plots show comparable responses between water levels fluctuations in wells S-1 and S-2 with outside influences outweighing the expected responses of continued recovery.

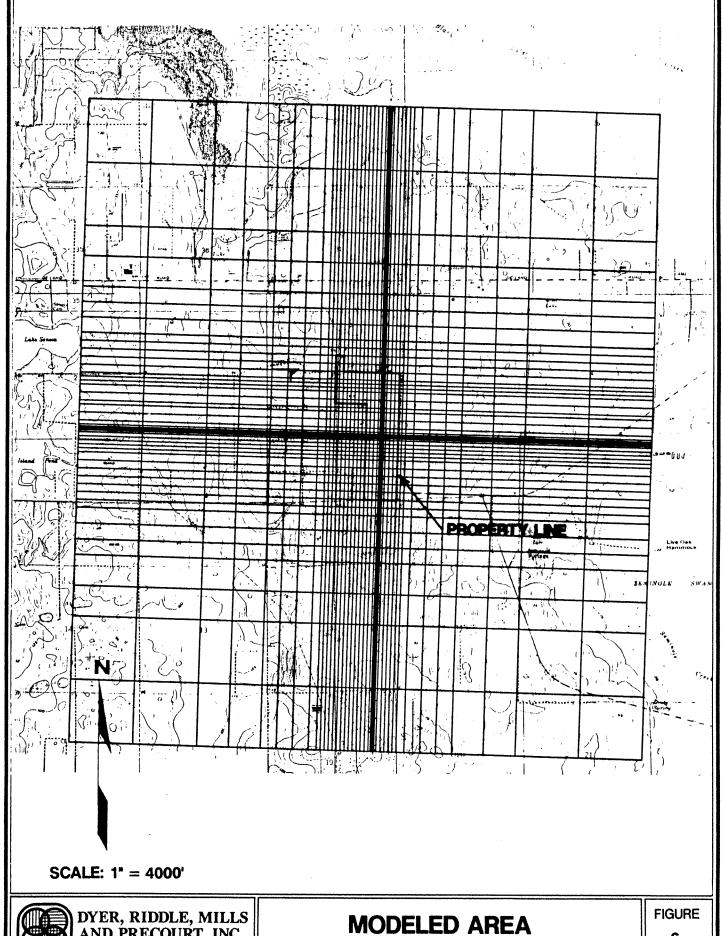
Results of the water quality analyses (Attachment B) indicated that the water chemistry remained stable throughout the entire test. Notable average concentrations are low chlorides of 11 mg/L, hardness of 248 mg/L and very low iron, < 0.030 mg/L.

4.0 GROUNDWATER FLOW MODEL ANALYSIS AND RESULTS

A three-dimensional groundwater flow model was constructed to predict the impacts that pumping the permitted withdrawal amount of water for the nursery would have on water levels in the surficial aquifer and the potentiometric surface of the Upper Floridan aquifer. A version of the Prickett-Lonnquist Aquifer Simulation Model (PLASM) was used to simulate flow and resulting drawdowns which would be induced from pumpage of 822,000 gpd from wells 1 through 7. A detailed description of PLASM is given in Bulletin 55, Illinois Water Survey, 1971.

The model was calibrated using drawdowns observed during the 48-hour constant rate discharge test. The calibration run was setup similar to the APT and the initial aquifer parameters used in the model were those determined by curve matching. After calibration was reached, the model was run at the permitted withdrawal amount for a thirty day period to predict possible impacts to neighboring properties.

The model consisted of a $43 \times 49 \times 2$ grid covering a 22 square mile area (Figure 6). The center of the grid was positioned over



AND PRECOURT, INC.

AND MODEL GRID

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the nursery with the densest portion of the grid around the wells involved in the APT. A large model area was chosen in order to minimize boundary effects.

Calibration involved globally changing values of transmissivity, storativity and leakance to attempt to match observed drawdowns. The calibration runs were performed with six uniform time steps of 1/3 day increments, totaling two (2) days, the duration of the constant rate discharge test. Withdrawal was from a single point (well 5) at a rate of 600 gpm (864,000 gpd).

The aquifer parameters that produced the best fit for each layer of the model and were still considered reasonable are as follows:

TABLE 2
MODEL CALIBRATION VALUES

	Transmissivity	Storativity	Leakance
STOCHUM KOONING THE PROMENSIONED AND OF HIS MENTING HE WAS A STOCK OF THE STOCK OF	(gpd/ft ³)	ARTINIPPIN UZBONAN OLEVIN PO URBONISTO NO OLEVIN SINGER PO PO SPOST SIGNINGO, PO ANTRE BLADONIN PRESENTANT MEDICAL PRESENTANT M	(gpd/ft ³)
Layer 1	2,250	0.070	
Layer 2	300,000	0.002	0.04

The observed and simulated drawdowns can be compared for the calibration run for the various observation wells in the following Table 3.

TABLE 3
DRAWDOWN CALIBRATION

WELL ID	OBSERVED	SIMULATED
#10	2.22'	2.26
S-1	0.05'	0.08'
S-2	0.22'	0.26'

In each observation well the simulated drawdown exceeded the observed drawdown. Any model simulation using the same aquifer parameters would produce additional drawdown and would therefore be a conservative approach to predicting impacts in the area.

Upon calibration, the total head error, which includes the sum of head changes between iterations for the two layers over the entire model area, was less than 0.17 feet. Water balance was within +1.46%.

After the model was calibrated, it was run at a withdrawal rate of 822,000 gpd distributed over 7 wells for a thirty (30) day period. Withdrawal amounts based upon proportions of average withdrawal rates to total withdrawal rate were used for the seven wells. The modeled withdrawal rates were as shown in Table 4. The thirty day model time period consisted of ten uniform time steps of three days. Model output can be found in Attachment D.

Head error at the end of the thirty day run was 0.21 feet and the water balance for the same run was -1.96%. Maximum drawdown simulated during this run in the surficial aquifer was 0.737 feet and in the Floridan aquifer was 1.161 feet. These maximum drawdowns were located at withdrawal points.

Figure 7 shows the simulated drawdown for the Floridan aquifer at $0.822~\mathrm{MGD}$ withdrawal for a thirty day period. The $-0.75~\mathrm{foot}$ drawdown contour does not extend beyond the property line as shown in this figure. Within $1200~\mathrm{feet}$ of the property line, drawdowns were between $0.50~\mathrm{and}~0.75~\mathrm{feet}$. The $-0.25~\mathrm{foot}$ contour extended a maximum of $3500~\mathrm{feet}$ of the property line for this simulation. Since impacts to the Floridan were simulated to be less than 2 feet at the property boundary, the well inventory was deemed unnecessary by the St. Johns River Water Management District.

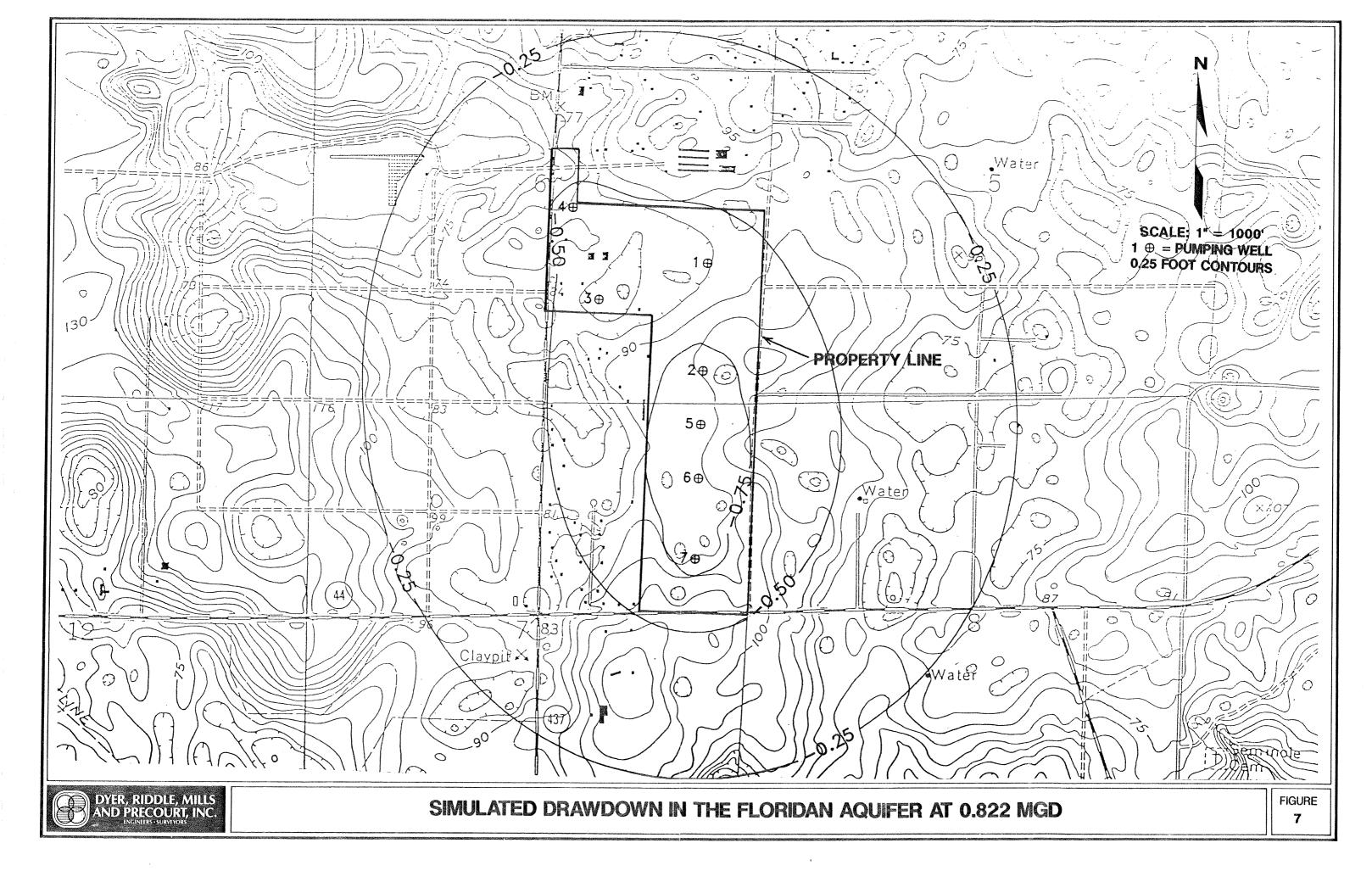
Simulated drawdown in the surficial aquifer for the same computer run is shown in Figure 8. The -0.50 foot drawdown contour extends approximately 500 feet west of the property line at its maximum extent. The extent of the -0.25 foot drawdown was approximately 2500 feet.

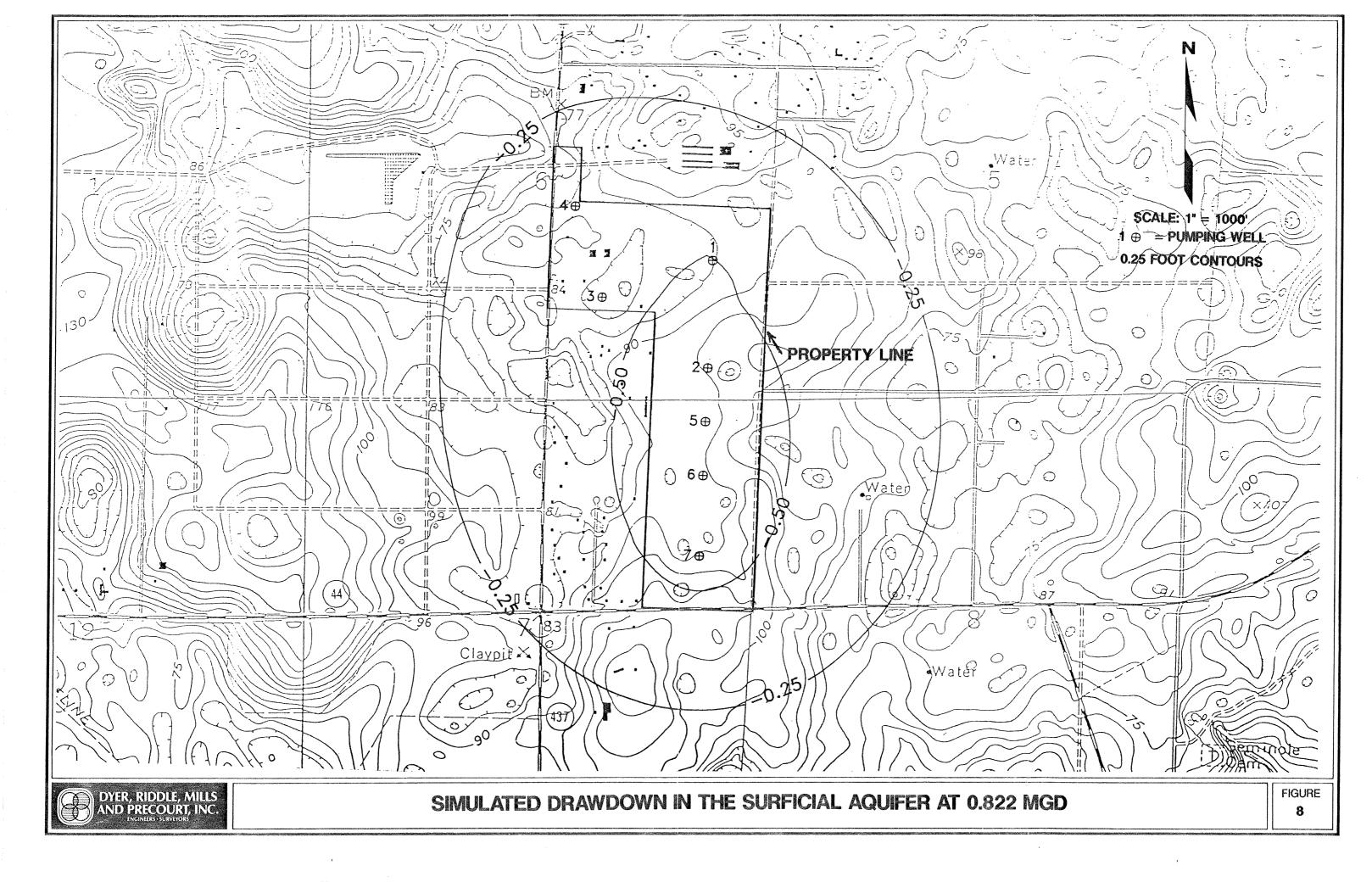
Based on the results of the groundwater flow model, it is believed that there will be only very minor impacts to both the Floridan and the surficial aquifers due to the nursery's withdrawal of their permitted amount. It is important to point out that the current average daily withdrawal from the nursery's wells is approximately 440,000 gpd, which is considerably less than the modeled withdrawal amount (822,000 gpd). Moreover, the model did not include any recharge to the surficial aquifer due to precipitation which would reduce the magnitude of impacts created by withdrawal from the Floridan aquifer.

In summation, given the relatively high transmissivity of the Floridan aquifer and the very conservative approach of this aquifer test, DRMP feels that it is unlikely that any considerable amount of drawdown in the surficial aquifer has been caused by the nursery's withdrawal. In fact, because a large portion of the water used for irrigation re-enters the surficial aquifer, it is entirely possible that the nursery's operation artificially recharges the surficial aquifer in the vicinity of the property.

TABLE 4 MODELED WITHDRAWAL RATES

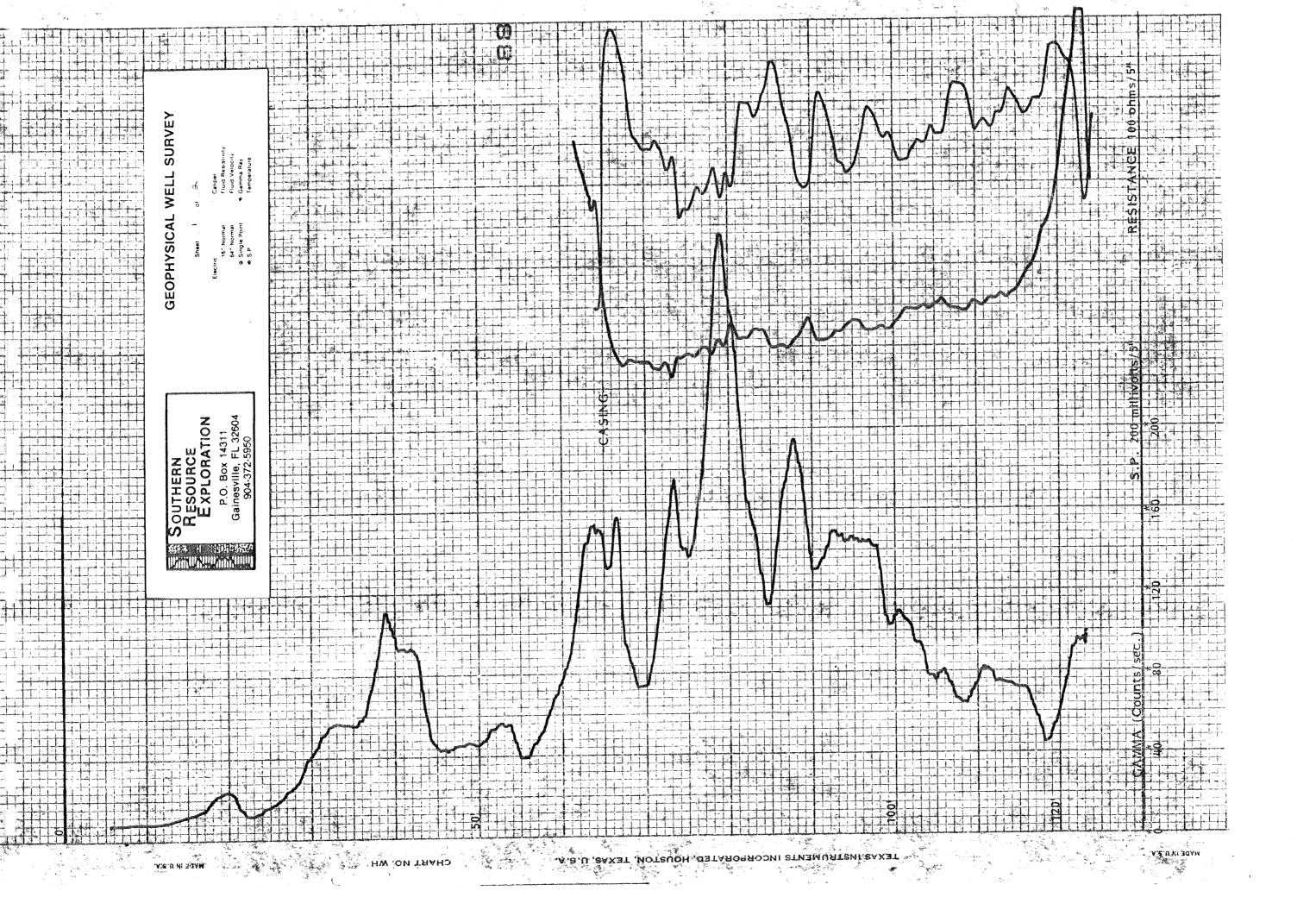
WELL ID	WITHDRAWAL (gpd)
1	109,600
2	109,600
3	18,250
4	109,600
5	109,600
6	182,650
7	182,700
TOTAL	822,000

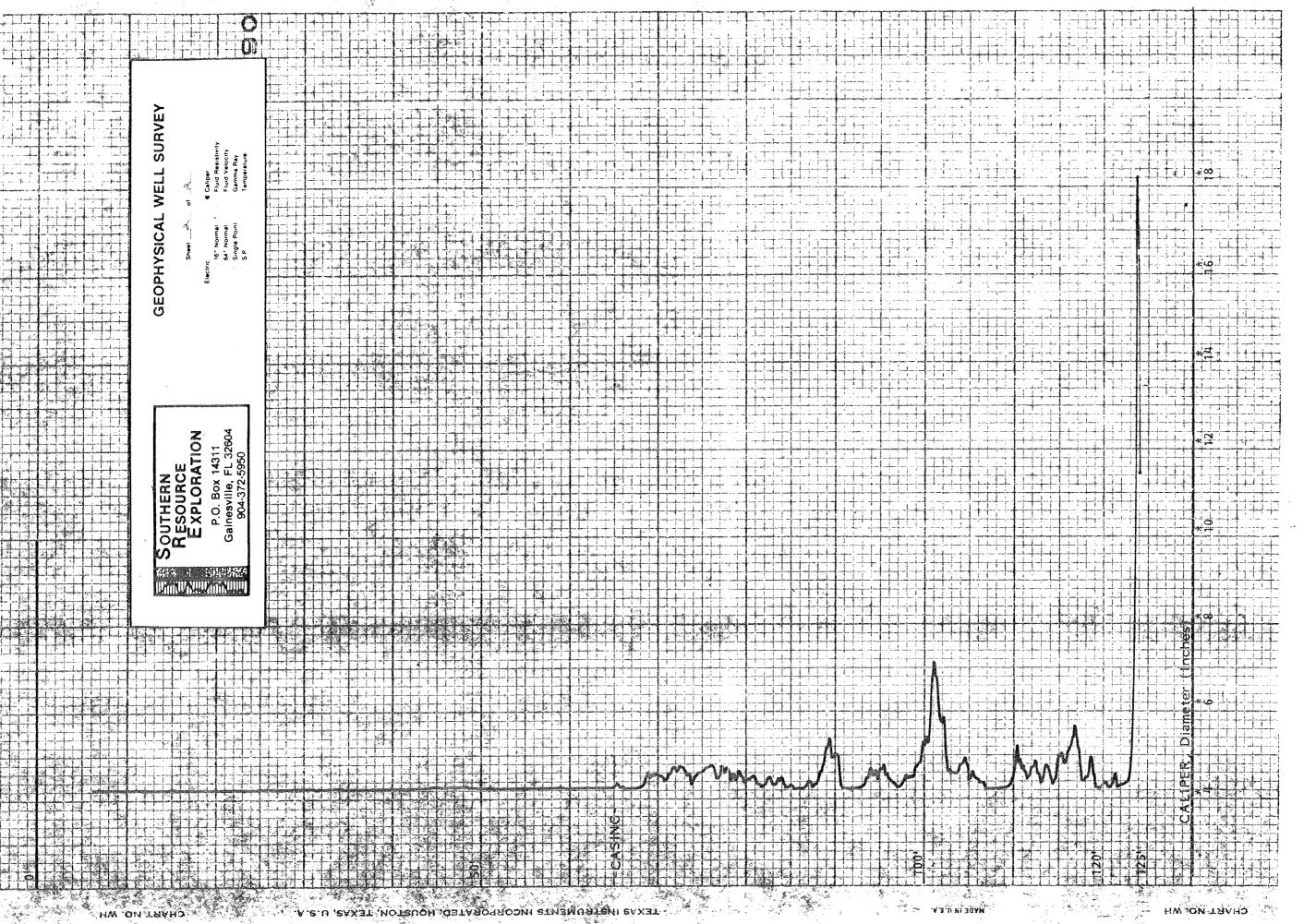




ATTACHMENT A

Geophysical Logs





ATTACHMENT B

Water Quality Information



Bionomics Laboratory, Inc.

4310 E. Anderson Road Orlando, Florida 32812 FDHRS Cert. No. 88008 (407) 851-2560 FAX (407) 856-0886

January 9, 1991

FOR: DYER, RIDDLE, MILLS & PRECOURT

1505 East Colonial Drive, Suite 200

Orlando, Florida 32803

RE: Sample(s) Received 12/10/90, Submitted By Client For Analysis.

JON'S APT. # 90-57100

LABORATORY REPORT

LAB I.D. NO. MARKS DATE SAMPLED TIME SAMPLED	9011608 PW 5 #1 12/3/90 3:35pm 24 HR	PW 5 #2 12/4/90 4:00pm	
pH, Lab	8.06	8.06	8.03
Bicarbonates as CaCo ₃ , mg/l	78	78	84
Chloride as Cl, mg/l	10	12	10
Conductivity, umhos/cm	470	480	500
Hardness as CaCO ₃ , mg/l	245	235	265
Sulfates as SO ₄ , mg/l	112	139	161 _{\$}
Total Dissolved Solids, mg/l	323	321	341
TOTAL METALS: mg/1			
Calcium as Ca	70.0	66.6	75.0
Iron as Fe	< 0.030	: 0.030	< 0.030
Magnesium as Mg	17.0	16.7	18.9
Sodium as Na	5.30	5.13	5.36

Signed

Mark Kromis, Chemist

ATTACHMENT C

Aquifer Performance Test Data
Drawdown and Recovery

Date Thursday December 6, 1990 8:15 AM PlotFile D:\SYM\JONSENO1.PRN
DataFile C:\GW\TERRA8\TERRACOM\JONSEND

JON'S NURSERY - APT DRMP #90-571.00

DRAWDOWN

		_	DIANDONI			
TIME (min)	Analog#01 5PSIGNEW	WELL S-1	Analog#02 10PSIGNEW	WELL #10	Analog#03 10PSIGOLD	WELL S-2
0	7.4613	0	22.592	0	15.731	0
0.017279	7.4613	0	22.499	0.093	15.731	0
0.033119	7.4613	0	22.245	0.347	15.731	0
0.050399	7.4613	0	22.037	0.555	15.708	0.023
0.064799	7.4613	Ō	21.806	0.786	15.731	0
0.083519	7.4613	0	21.668	0.924	15.731	0
0.099359	7.4613	0	21.622	0.97	15.731	0
0.116639	7.4613	0	21.622	0.97	15.731	0
0.133919	7.4613	0	21.622	0.97	15.731	0
0.149759	7.4613	0	21.645	0.947	15.731	0
0.167039	7.4613	0	21.622	0.97	15.708	0.023
0.182879 0.200159	7.4613 7.4613	0	21.575 21.529	1.017	15.708	0.023
0.215999	7.4613	0	21.529 21.46	1.063	15.731	0
0.231839	7.4613	0	21.437	1.132 1.155	15.731 15.731	0 0
0.250559	7.4613	0	21.437	1.178	15.731	0
0.266399	7.4613	0	21.414	1.178	15.731	0
0.283679	7.4613	0	21.414	1.178	15.731	0
0.299519	7.4613	Ŏ	21.391	1.201	15.708	0.023
0.316799	7.4613	Ō	21.391	1.201	15.731	0.023
0.332639	7.4613	Ŏ	21.367	1.225	15.731	ŏ
0.349919	7.4613	Ŏ	21.344	1.248	15.731	ő
0.367199	7.4613	Ō	21.321	1.271	15.731	Ö
0.383039	7.4613	0	21.298	1.294	15.708	0.023
0.400319	7.4613	0	21.298	1.294	15.731	. 0
0.414719	7.4613	0	21.298	1.294	15.731	0
0.433440	7.4613	0	21.298	1.294	15.731	. 0
0.449279	7.4613	0	21.275	1.317	15.731	0
0.466559	7.4613	0	21.275	1.317	15.731	0
0.483839	7.4613	0	21.275	1.317	15.731	0
0.499679	7.4613	0	21.252	1.34	15.731	0
0.516959	7.4613	0	21.252	1.34	15.731	0
0.532799	7.4613	0	21.229	1.363	15.708	0.023
0.550079	7.4613	0	21.229	1.363	15.731	0
0.567359	7.4613	0	21.229	1.363	15.731	0
0.581759	7.4613	0	21.229	1.363	15.731	0
0.600479	7.4613	0	21.206	1.386	15.731	0
0.616319	7.4613	0	21.206	1.386	15.731	0
0.633599	7.4613	0	21.183	1.409	15.708	0.023
0.649439	7.4613	0	21.206	1.386	15.731	0
0.666719	7.4613	0	21.183	1.409	15.731	0
0.683999	7.4613	0	21.183	1.409	15.731	0
0.699839 0.717119	7.4613 7.4613	0 0	21.183	1.409	15.731	0
0.732959	7.4613	0	21.183 21.16	1.409 1.432	15.731	0
.0.750239	7.4613	0	21.183	1.432	15.731	0
/	/.4013	U	41.103	1.409	15.731	0

0,764639 7	4613	0	71 15	1 400	15 700	0.000
	.4013 .4613	0 0	21.16	1.432	15.708	0.023
	.4613 .4613	0	21.16 21.16	1.432 1.432	15.731 15.731	0
	.4613 .4613	Ö	21.16	1.432	15.731	0
	.4613	0	21.136	1.456	15.731	0
	.4613	0	21.136	1.456	15.731	0
	.4613	Ö	21.136	1.456	15.731	0.023
	.4613	Ö	21.136	1.456	15.731	0.023
	.4613	ŏ	21.136	1.456	15.731	0
	.4613	ő	21.113	1.479	15.731	0
	.4613	ŏ	21.136	1.456	15.731	0
	.4613	ō	21.136	1.456	15.731	0
	.4613	ő	21.136	1.456	15.731	0
	.4613	ŏ	21.113	1.479	15.731	0
	.4613	Ö	21.113	1.479	15.731	Ö
	.4613	ō	21.113	1.479	15.731	Ö
	.4613	Ö	21.113	1.479	15.731	0
	.4613	Ö	21.113	1.479	15.708	0.023
	.4613	Ō	21.113	1.479	15.708	0.023
	.4613	Ö	21.09	1.502	15.731	0.023
	.4613	Ö	21.09	1.502	15.731	Õ
	.4613	ŏ	21.09	1.502	15.731	o
	.4613	ō	21.09	1.502	15.731	Ö
	.4613	ŏ	21.09	1.502	15.731	o
	.4613	ŏ	21.09	1.502	15.731	0
	.4613	ŏ	21.09	1.502	15.731	0
	.4613	Ö	21.09	1.502	15.708	0.023
	.4613	ŏ	21.09	1.502	15.731	0.023
	.4613	ŏ	21.067	1.525	15.731	ő
	.4613	Ŏ	21.067	1.525	15.731	0
	.4613	Ö	21.067	1.525	15.731	Ö
	.4613	Ō	21.067	1.525	15.708	0.023
	.4613	Ō	21.067	1.525	15.731	0
1.316159 7	.4613	0	21.067	1.525	15.731	Ō
1.333439 7	.4613	0	21.067	1.525	15.731	Ö
1.349279 7	.4613	0	21.067	1.525	15.731	0
1.366559 7	.4613	Q	21.044	1.548	15.731	0
1.383839 7	. 4613	0	21.067	1.525	15.731	0
1.399679 7	. 4613	0	21.067	1.525	15.708	0.023
	.4613	0	21.067	1.525	15.731	0
	. 4613	0	21.044	1.548	15.731	0
	. 4613	0	21.067	1.525	15.731	. 0
1.464479 7.	. 4613	0	21.044	1.548	15.708	0.023
1.483199 7	. 4613	0	21.044	1.548	15.731	0
1.500479 7.	. 4613	0	21.044	1.548	15.731	0
1.516319 7.	. 4613	0	21.044	1.548	15.731	0
1.533599 7.	. 4613	0	21.044	1.548	15.731	0
1.549439 7.	. 4613	0	21.044	1.548	15.731	0
1.566719 7.	.4728 -0.01	15	21.044	1.548	15.731	0
1.583999 7.	. 4613	0	21.021	1.571	15.731	0
	. 4613	0	21.044	1.548	15.731	Ó
	4613	0	21.021	1.571	15.731	Ö
	. 4613	0	21.044	1.548	15.731	0
	. 4613	0	21.021	1.571	15.731	0
	. 4613	0	21.021	1.571	15.731	0
·1.683359 7.	4613	Ō.	21.021	1.571	15.708	0.023

1.700639	7.4613	0	21.021	1.571	15.731	0
1.716479	7.4613	ő	21.021	1.571	15.731	
						0
1.733760	7.4613	0	21.021	1.571	15.731	0
1.749599	7.4613	0	21.021	1.571	15.731	0
1.766879	7.4613	0	20.998	1.594	15.731	0
1.782719	7.4613	0	21.021	1.571	15.731	0
1.799999	7.4613	0	21.021	1.571	15.731	0
1.814399	7.4613	Ō	20.998	1.594	15.731	ő
1.833119	7.4613	ő	21.021	1.571	15.731	
						0
1.850399	7.4613	Ō	20.998	1.594	15.731	0
1.866239	7.4613	0	20.998	1.594	15.731	0
1.883519	7.4613	0	20.998	1.594	15.731	0
1.899359	7.4613	0	20.998	1.594	15.731	0
1.916639	7.4613	0	20.998	1.594	15.731	Ō
1.933919	7.4613	Ö	20.998	1.594	15.731	ŏ
1.94976	7.4613	0	20.998			
				1.594	15.731	0
1.967039	7.4613	0	20.998	1.594	15.731	0
1.981440	7.4613	О	20.9 9 8	1.594	15.731	.0
2.000159	7.4613	0	20.998	1.594	15.731	0
2.015999	7.4613	0	20.998	1.594	15.731	0
2.033279	7.4613	0	20.998	1.594	15.708	0.023
2.050559	7.4613	Ō	20.998	1.594	15.731	0
2.066399	7.4613	ő	20.998	1.594	15.708	0.023
2.083679						
	7.4613	0	20.998	1.594	15.731	0
2.099519	7.4613	0	20.998	1.594	15.731	0
2.116799	7.4613	0	20.975	1.617	15.731	0
2.132639	7.4613	0	20.975	1.617	15.731	0
2.149919	7.4613	0	20.975	1.617	15.731	0
2.164319	7.4613	0	20.975	1.617	15.731	0
2.183039	7.4613	0	20.975	1.617	15.731	0
2.200319	7.4613	Ö	20.975	1.617	15.731	Õ
2.216159	7.4613	0	20.975	1.617	15.731	0
2.233439						
	7.4613	0	20.975	1.617	15.731	0
2.249279	7.4613	0	20.975	1.617	15.731	0
2.266559	7.4613	0	20.975	1.617	15.708	0.023
2.283839	7.4613	0	20.975	1.617	15.731	0
2.299679	7.4613	0	20.975	1.617	15.731	0
2.316959	7.4613	0	20.975	1.617	15.731	0
2.331359	7.4613	Ō	20.975	1.617	15.731	Ö
2.350079	7.4613	ŏ	20.975	1.617		Ö
					15.731	
2.367359	7.4613	0	20.952	1.64	15.731	0
2.3832	7.4613	0	20.975	1.617	15.731	0
2.400479	7.4613	0	20.975	1.617	15.731	0
2.416319	7.4613	0	20.952	1.64	15.731	0
2.433599	7.4613	0	20.952	1.64	15.731	0
2.449439	7.4613	O	20.952	1.64	15.731	0
2.466719	7.4613	Ö	20.952	1.64	15.731	Ō
2.483999	7.4613	ő	20.952	1.64		Ö
2.499839					15.731	
	7.4613	0	20.952	1.64	15.731	0
2.515679	7.4613	0	20.952	1.64	15.731	0
2.532959	7.4613	0	20.952	1.64	15.708	0.023
2.550239	7.4613	0	20.952	1.64	15.731	0
2.566079	7.4613	0	20.952	1.64	15.731	0
2.583359	7.4613	0	20.952	1.64	15.731	0
2.600640	7.4613	Ö	20.952	1.64	15.731	Ō
.2.616479	7.4613	ő	20.952	1.64	15.731	ő
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2.649599 7.4613 0 20.952 1.64 15.708 0.023 2.668679 7.4613 0 20.952 1.64 15.731 0 2.668679 7.4613 0 20.952 1.64 15.731 0 2.699999 7.4613 0 20.952 1.64 15.731 0 2.717279 7.4613 0 20.929 1.663 15.708 0.023 2.733119 7.4613 0 20.929 1.663 15.708 0.023 2.753299 7.4613 0 20.929 1.663 15.708 0.023 2.783519 7.4613 0 20.929 1.663 15.731 0 2.849759 7.4613 0 20.929 1.663 15.731 0 2.849759 7.4613 0 20.929 1.663 15.731 0 2.882879 7.4613 0 20.929 1.663 15.731 0 2.932279 7.4613 0 </th <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th>							
2.649599 7.4613 0 20.952 1.64 15.708 0.029 2.666879 7.4613 0 20.952 1.64 15.731 0 2.699999 7.4613 0 20.952 1.64 15.731 0 2.717279 7.4613 0 20.952 1.663 15.708 0.023 2.750399 7.4613 0 20.952 1.64 15.708 0.023 2.766239 7.4613 0 20.952 1.663 15.708 0.023 2.783519 7.4613 0 20.992 1.663 15.731 0 2.799359 7.4613 0 20.929 1.663 15.731 0 2.818640 7.4613 0 20.929 1.663 15.731 0 2.845759 7.4613 0 20.929 1.663 15.731 0 2.882879 7.4613 0 20.929 1.663 15.731 0 2.901559 7.4613 0 </td <td>2.633759</td> <td>7.4613</td> <td>0</td> <td>20.952</td> <td>1.64</td> <td>15.731</td> <td>Ω</td>	2.633759	7.4613	0	20.952	1.64	15.731	Ω
2.666879 7.4613 0 20.952 1.64 15.731 0 2.691279 7.4613 0 20.952 1.64 15.731 0 2.6919999 7.4613 0 20.952 1.663 15.708 0.023 2.733119 7.4613 0 20.929 1.663 15.708 0.023 2.750399 7.4613 0 20.929 1.663 15.708 0.023 2.766239 7.4613 0 20.929 1.663 15.731 0 2.783519 7.4613 0 20.929 1.663 15.731 0 2.849759 7.4613 0 20.929 1.663 15.731 0 2.849759 7.4613 0 20.929 1.663 15.731 0 2.862879 7.4613 0 20.929 1.663 15.731 0 2.901597 7.4613 0 20.929 1.663 15.731 0 2.93279 7.4613 0 20.929 1.663 15.731 0 2.93279 7.4613	2.649599		0				-
2.681279 7.4613 0 20.952 1.64 15.731 0 2.699999 7.4613 0 20.929 1.663 15.708 0.023 2.733119 7.4613 0 20.929 1.663 15.708 0.023 2.750399 7.4613 0 20.929 1.663 15.708 0.023 2.766239 7.4613 0 20.929 1.663 15.731 0 2.783519 7.4613 0 20.929 1.663 15.731 0 2.799359 7.4613 0 20.929 1.663 15.731 0 2.84359 7.4613 0 20.929 1.663 15.731 0 2.845959 7.4613 0 20.929 1.663 15.731 0 2.855599 7.4613 0 20.929 1.663 15.731 0 2.900159 7.4613 0 20.929 1.663 15.731 0 2.915999 7.4613 0 <td>2.666879</td> <td>7.4613</td> <td></td> <td></td> <td></td> <td></td> <td></td>	2.666879	7.4613					
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3.565439	7.4613	0	20.905	1.687	15.708	0.023
3.582719	7.4613	0	20.905	1.687	15.731	0
3.599999	7.4613	0	20.905	1.687	15.731	Ō
3.617279	7.4613	0	20.882	1.71	15.708	0.023
3.633119	7.4613	0	20.882	1.71	15.731	0
3.650399	7.4613	0	20.882	1.71	15.731	0
3.666239	7.4613	0	20.882	1.71	15.731	0
3.683520	7.4613	0	20.882	1.71	15,731	Ō
3.699359	7.4613	0	20.882	1.71	15.731	Ō
3.716639	7.4613	0	20.882	1.71	15.731	0
3.731039	7.4613	0	20.882	1.71	15.708	0.023
3.749759	7.4613	0	20.882	1.71	15.708	0.023
3.767039	7.4613	0	20.882	1.71	15.731	0
3.782879	7.4613	Ō	20.882	1.71	15.708	0.023
3.800159	7.4613	0	20.882	1.71	15,708	0.023
3.815999	7.4613	0	20.882	1.71	15.731	0
3.833279	7.4613	0	20.882	1.71	15.731	0
3.850559	7.4613	0	20.882	1.71	15.731	0
3.866399	7.4613	0	20.882	1.71	15.731	0
3.883679	7.4613	0	20.882	1.71	15.731	0
3.89952	7.4613	0	20.882	1.71	15.731	0
3.915359	7.4613	0	20.882	1.71	15.731	0
3.932639	7.4613	0	20.882	1.71	15.731	.0
3.949919	7.4613	0	20.882	1.71	15.731	0
3.967199	7.4613	0	20.882	1.71	15.731	0
3.983039	7.4613	0	20.882	1.71	15.708	0.023
4.000319	7.4613	0	20.882	1.71	15.731	0
4.016159	7.4613	0	20.882	1.71	15.731	0
4.033439	7.4613	0	20.882	1.71	15.731	0
4.049279	7.4613	0	20.882	1.71	15.708	0.023
4.066559	7.4613	0	20.882	1.71	15.731	0
4.080959	7.4613	0	20.882	1.71	15.731	0
4.099679	7.4613	0	20.882	1.71	15.731	0
4.116960	7.4613	0	20.882	1.71	15.708	0.023
4.132799	7.4613	O	20.882	1.71	15.731	0
4.216319	7.4613	0	20.882	1.71	15.708	0.023
4.299839	7.4613	. 0	20.859	1.733	15.731	0
4.383359	7.4613	0	20.882	1.71	15.731	0
4.466879	7.4728	-0.0115	20.859	1.733	15.708	0.023
4.550400	7.4613	0	20.859	1.733	15.708	0.023
4.633919	7.4613	0	20.859	1.733	15.731	0
4.715999	7.4613	0	20.859	1.733	15.731	0
4.799519	7.4613	0	20.859	1.733	15.731	0
4.883039	7.4613	0	20.836	1.756	15.731	0
4.966559	7.4613	0	20.859	1.733	15.731	0
5.133599	7.4728	-0.0115	20.836	1.756	15.731	0
5.300639	7.4728	-0.0115	20.836	1.756	15.731	0
5.466239	7.4613	0	20.836	1.756	15.708	0.023
5.633280	7.4728	-0.0115	20.836	1.756	15.731	0
5.800319	7.4613	0	20.836	1.756	15.731	0
5.965919	7.4613	0	20.836	1.756	15.731	0
6.132959 6.299999	7.4613 7.4728	0 -0.0115	20.813 20.813	1.779 1.779	15.731 15.708	0 0.023
6.467039	7.4613	-0.0115	20.813	1.779	15.700	0.023
6.632639	7.4728	-0.0115	20.813	1.779	15.731	0
.7.133759	7.4613	0.0113	20.79	1.802	15.731	Ö
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76.63391 7.4497 0.0116 20.536 2.056 15.639 0.092 81.63359 7.4497 0.0116 20.536 2.056 15.639 0.092 86.63327 7.4497 0.0116 20.536 2.056 15.639 0.092 91.63295 7.4497 0.0116 20.513 2.079 15.639 0.092 101.6337 7.4497 0.0116 20.513 2.079 15.616 0.115
81.63359 7.4497 0.0116 20.536 2.056 15.639 0.092 86.63327 7.4497 0.0116 20.536 2.056 15.639 0.092 91.63295 7.4497 0.0116 20.513 2.079 15.639 0.092 101.6337 7.4497 0.0116 20.513 2.079 15.616 0.115
86.63327 7.4497 0.0116 20.536 2.056 15.639 0.092 91.63295 7.4497 0.0116 20.513 2.079 15.639 0.092 101.6337 7.4497 0.0116 20.513 2.079 15.616 0.115
91.63295 7.4497 0.0116 20.513 2.079 15.639 0.092 101.6337 7.4497 0.0116 20.513 2.079 15.616 0.115
101.6337 7.4497 0.0116 20.513 2.079 15.616 0.115
121.6339 7.4497 0.0116 20.49 2.102 15.616 0.115
131.6332 7.4497 0.0116 20.513 2.079 15.592 0.139
141.6326 7.4497 0.0116 20.49 2.102 15.592 0.139
151.6334 7.4382 0.0231 20.49 2.102 15.569 0.162
161.6328 7.4382 0.0231 20.49 2.102 15.569 0.162
171.6336 7.4382 0.0231 20.467 2.125 15.569 0.162
181.6329 7.4382 0.0231 20.467 2.125 15.569 0.162
191.6337 7.4497 0.0116 20.467 2.125 15.569 0.162 211.6339 7.4382 0.0231 20.467 2.125 15.546 0.185
231.6326 7.4497 0.0116 20.467 2.125 15.546 0.185 251.6328 7.4382 0.0231 20.443 2.149 15.546 0.185
271.6329 7.4382 0.0231 20.443 2.149 15.546 0.185
291.6331 7.4382 0.0231 20.443 2.149 15.546 0.185
311.6332 7.4382 0.0231 20.42 2.172 15.523 0.208
-331.6334 7.4382 0.0231 20.42 2.172 15.523 0.208

351.6336	7.4382	0.0231	20.42	2.172	15.523	0.208
371.6337	7.4382	0.0231	20.397	2.195	15.523	0.208
391.6339	7.4382	0.0231	20.42	2.172	15.523	0.208
431.6328	7.4497	0.0116	20.397	2.195	15.546	0.185
471.6331	7.4497	0.0116	20.397	2.195	15.546	0.185
511.6334	7.4497	0.0116	20.397	2.195	15.546	
551.6337	7.4497	0.0116	20.397	2.195		0.185
591.6326	7.4497	0.0116			15.569	0.162
631.6329	7.4497	0.0116	20.397	2.195	15.569	0.162
			20.397	2.195	15.569	0.162
671.6332	7.4497	0.0116	20.397	2.195	15.592	0.139
711.6336	7.4497	0.0116	20.397	2.195	15.592	0.139
751.6339	7.4497	0.0116	20.397	2.195	15.592	0.139
791.6328	7.4497	0.0116	20.397	2.195	15.592	0.139
831.6331	7.4382	0.0231	20.397	2.195	15.592	0.139
871.6334	7.4382	0.0231	20.397	2.195	15.592	0.139
911.6337	7.4382	0.0231	20.397	2.195	15.569	0.162
951.6326	7.4382	0.0231	20.397	2.195	15.592	0.139
991.6329	7.4382	0.0231	20.397	2.195	15.569	0.162
1031.633	7.4497	0.0116	20.397	2.195	15.592	0.139
1071.633	7.4266	0.0347	20.397	2.195	15.592	0.139
1111.633	7.4382	0.0231	20.42	2.172	15.569	0.162
. 1151.632	7.4382	0.0231	20.42	2.172	15.569	0.162
1191.633	7.4497	0.0116	20.42	2.172	15.569	0.162
1231.633	7.4497	0.0116	20.42	2.172	15.569	0.162
1271.633	7.4613	0	20.42	2.172	15.616	0.115
1311.632	7.4728	-0.0115	20.443	2.149	15.639	0.092
1351.632	7.4613	0	20.42	2.172	15.662	0.069
1391.633	7.4613	0	20.443	2.149	15.662	0.069
1431.633	7.4613	0	20.443	2.149	15.662	0.069
1471.633	7,4613	0	20.443	2.149	15.662	0.069
1511.632	7.4497	0.0116	20.42	2.172	15.662	0.069
1551.633	7.4382	0.0231	20.42	2.172	15.616	0.115
1591.633	7.4382	0.0231	20.397	2.195	15.616	0.115
1631.633	7,4266	0.0347	20.397	2.195	15.592	0.139
1671.632	7.4382	0.0231	20.397	2.195	15.592	0.139
1711.632	7.4382	0.0231	20.397	2.195	15.569	0.162
1751.633	7.4382	0.0231	20.374	2.218	15.569	0.162
1791.633	7.4266	0.0347	20.374	2.218	15.569	0.162
1831.633	7.4266	0.0347	20.374	2.218	15.546	0.185
1871.632	7.4266	0.0347	20.374	2.218	15.546	0.185
1911.633	7.4382	0.0231	20.374	2.218	15.546	0.185
1951.633	7.4382	0.0231	20.374	2.218	15.546	0.185
1991.633	7.4382	0.0231	20.374	2.218	15.546	0.185
2031.632	7.4382	0.0231	20.374	2.218	15.546	0.185
2071.632	7.4497	0.0116	20.374	2.241	15.569	0.163
2111.633	7.4382	0.0231	20.351	2.241		
2151.633	7.4266	0.0231	20.331	2.241	15.546 15.546	0.185
2191.633	7.4282	0.0231				0.185
2231.632	7.4362	0.0231	20.374	2.218	15.546	0.185
			20.374	2.218	15.546	0.185
2271.633	7.4266	0.0347	20.374	2.218	15.546	0.185
2311.633	7.4266	0.0347	20.374	2.218	15.546	0.185
2351.633	7.4266	0.0347	20.374	2.218	15.523	0.208
2391.632	7.4266	0.0347	20.374	2.218	15.546	0.185
2431.632	7.4266	0.0347	20.374	2.218	15.546	0.185
2471.633	7.4382	0.0231	20.328	2.264	15.546	0.185
.2511.633	7.392	0.0693	20.374	2.218	15.523	0.208

2551.633	7.4035	0.0578	20.397	2.195	15.477	0.254
2591.632	7.4266	0.0347	20.397	2.195	15.477	0.254
2631.633	7.4382	0.0231	20.42	2.172	15.5	0.231
2671.633	7.4382	0.0231	20.42	2.172	15.523	0.231
2711.633	7.4266	0.0347	20.397	2.195	15.523	
2751.632	7.4382	0.0347	20.397			0.208
2791.632	7.4382			2.195	15.523	0.208
2831.633		0.0231	20.42	2.172	15.546	0.185
	7.4382	0.0231	20.397	2.195	15.546	0.185
2871.633	7.4382	0.0231	20.374	2.218	15.546	0.185
2911.633	7.4266	0.0347	20.374	2.218	15.523	0.208
2917.404	7.4266	0.0347	20.397	2.195	15.523	0.208
2917.415	7.4266	0.0347	20.397	2.195	15.523	0.208
2917.432	7.4266	0.0347	20.397	2.195	15.523	0.208
2917.450	7.4151	0.0462	20.397	2.195	15.523	0.208
2917.467	7.4266	0.0347	20.374	2.218	15.523	0.208
2917.483	7.4266	0.0347	20.374	2.218	15.523	0.208
2917.500	7.4266	0.0347	20.374	2.218	15.523	0.208
2917.516	7.4266	0.0347	20.374	2.218	15.523	0.208
2917.532	7.4266	0.0347	20.374	2.218	15.523	0.208
2917.549	7.4266	0.0347	20.374	2.218	15.523	0.208
2917.566	7.4266	0.0347	20.374	2.218	15.523	0.208
2917.584	7.4266	0.0347	20.374	2.218	15.523	0.208
2917.599	7.4266	0.0347	20.374	2.218	15.523	0.208
2917.617	7.4266	0.0347	20.374	2.218	15.523	0.208
2917.632	7.4266	0.0347	20.374	2.218	15.523	0.208
2917.650	7.4266	0.0347	20.374	2.218	15.523	0.208
2917.666	7.4266	0.0347	20.374	2.218	15.523	0.208
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RECOVERY

	TIME (min)	Analog#01 5PSIGNEW	WELL S-1	Analog#02 10PSIGNEW	WELL #10	Analog#03 10PSIGOLD	WELL S-2	
	0	7.4151	0	20.374	0	15.523	0	
	0.014400	7.4266	0.0115	20.397	0.023	15.523	ō	
	0.033120	7.4266	0.0115	20.674	0.3	15.523	Ö	
	0.050399	7.4266	0.0115	20.929	0.555	15.523	ō	
	0.066240	7.4151	0	21.275	0.901	15.523	Ö	
	0.083519	7.4266	0.0115	21.598	1.224	15.523	0	
	0.099360	7.4151	0	21.76	1.386	15.523	0	
	0.116639	7.4266	0.0115	21.76	1.386	15.523	0	
	0.133920	7.4266	0.0115	21.668	1.294	15.523	0	
	0.149759	7.4266	0.0115	21.506	1.132	15.523	0	
	0.167040	7.4266	0.0115	21.414	1.04	15.523	0	
	0.182879	7.4151	0	21.414	1.04	15.523	0	
	0.198720	7.4266	0.0115	21.483	1.109	15.523	0 ·	
	0.215999	7.4266	0.0115	21.645	1.271	15.523	0	
	0.233279	7.4266	0.0115	21.737	1.363	15.523	0	
	0.250560	7.4151	0	21.806	1.432	15.523	0	
	0.266399	7.4266	0.0115	21.806	1.432	15.523	0	
	0.283680	7.4266	0.0115	21.76	1.386	15.523	0	
	0.299519	7.4151	0	21.737	1.363	15.523	0	
	0.316800	7.4151	0	21.714	1.34	15.523	0	
	0.332639	7.4266	0.0115	21.76	1.386	15.523	0	
	0.349920	7.4266	0.0115	21.806	1.432	15.523	0	
٠	0.364319	7.4266	0.0115	21.829	1.455	15.523	0	

0.383040	7.4266	0.0115	21.853	1.479	15.523	0
0.400319	7.4266	0.0115	21.853	1.479	15.523	0
0.416160	7.4266	0.0115	21.876	1.502	15.523	
						0
0.433440	7.4266	0.0115	21.876	1.502	15.523	0
0.449279	7.4266	0.0115	21.876	1.502	15.523	0
0.466560	7.4151	0	21.899	1.525	15.523	0
0.483839	7.4266	0.0115	21.899	1.525	15.523	Ō
0.499680	7.4266	0.0115	21.922	1.548	15.523	ŏ
0.516959	7.4266	0.0115	21.922	1.548	15.523	0
0.532800	7.4266	0.0115	21.945	1.571	15.523	0
0.548639	7.4266	0.0115	21.945	1.571	15.523	0
0.565920	7.4151	0	21.968	1.594	15.523	0
0.583199	7,4266	0.0115	21.968	1.594	15.523	ŏ
0.600480	7.4266	0.0115	21.968	1.594	15.523	0
0.616319	7.4266	0.0115	21.991	1.617	15.523	О
0.633599	7.4266	0.0115	21.991	1.617	15.523	0
0.649439	7.4266	0.0115	21.991	1.617	15.523	0
0.666719	7.4266	0.0115	22.014	1.64	15.523	0
0.682560	7.4266	0.0115	22.014	1.64	15.523	ő
0.699839	7.4266	0.0115	22.014	1.64	15.523	0
0.714240	7.4266	0.0115	22.014	1.64	15.523	0
0.732959	7.4266	0.0115	22.014	1.64	15.523	0
0.750240	7.4266	0.0115	22.037	1.663	15.523	0
0.766079	7.4266	0.0115	22.037	1.663	15.523	Ō
0.783360	7.4266	0.0115	22.037	1.663	15.523	ő
0.800639	7.4266	0.0115	22.037	1.663	15.523	0
0.816480	7.4266	0.0115	22.037	1.663	15.523	0
0.833759	7.4266	0.0115	22.06	1.686	15.523	0
0.849600	7.4266	0.0115	22.06	1.686	15.523	0
0.866880	7.4151	0	22.06	1.686	15.523	Ō
0.882719	7.4151	ő	22.084	1.71	15.523	ō
0.902880	7.4266	0.0115	22.084	1.71	15.523	0
0.917279	7.4266	0.0115	22.084	1.71	15.523	0
0.933120	7.4266	0.0115	22.084	1.71	15.523	0
0.950399	7.4266	0.0115	22.084	1.71	15.523	0
0.966240	7.4266	0.0115	22.084	1.71	15.523	0
0.983519	7.4266	0.0115	22.084	1.71	15.523	0
0.999360	7.4266	0.0115	22.084	1.71	15.523	Ö
						1.
1.016639	7.4266	0.0115	22.107	1.733	15.523	0
1.033920	7.426 6	0.0115	22.107	1.733	15.523	0
1.049759	7.4151	0	22.107	1.733	15.523	0
1.065600	7.4266	0.0115	22.107	1.733	15.523	О
1.082879	7.4151	0	22.107	1.733	15.523	0
1.100159	7.4151	ŏ	22.107	1.733	15.523	Ō
1.116000	7.4266	0.0115	22.107	1.733	15.523	0
1.133279	7.4266	0.0115	22.13	1.756	15.523	0
1.150560	7.4266	0.0115	22.13	1.756	15.523	0
1.166399	7.4266	0.0115	22.13	1.756	15.523	0
1.183680	7.4266	0.0115	22.13	1.756	15.523	0
1.199519	7.4266	0.0115	22.13	1.756	15.523	Ö
1.216800	7.4266	0.0115	22.13	1.756	15.523	0
1.232639	7.4266	0.0115	22.13	1.756	15.523	0
1.248480	7.4151	0	22.153	1.779	15.523	0
1.267199	7.4266	0.0115	22.153	1.779	15.523	0
1.283040	7.4151	0	22.153	1.779	15.523	0
.1.300320	7.4266	0.0115	22.153	1.779	15.523	Ō
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1.316159	7.4266	0.0115	22,153	1.779	15.523	ſ)
1.333440	7.4151	0	22.153	1.779			
					15.523		Э
1.349279	7.4151	0	22.176	1.802	15.523)
1.366560	7.4266	0.0115	22.153	1.779	15.523	C)
1.383839	7.4266	0.0115	22.153	1.779			
					15.523	C	
1.399680	7.4266	0.0115	22.176	1.802	15.523	C)
1.419839	7.4151	0	22.176	1.802	15.523	C)
1.432800	7.4266	0.0115	22.153	1.779	15.523		
						C	
1.450079	7.4266	0.0115	22.176	1.802	15.523	C)
1.465920	7.4266	0.0115	22.176	1.802	15.523	C)
1.483199	7.4266	0.0115	22.176	1.802	15.523	Ö	
1.500479	7.4266	0.0115	22.176	1.802	15.523	C)
1.516319	7.4266	0.0115	22.176	1.802	15.523	O)
1.533599	7.4266	0.0115	22.176	1.802	15.523	C	
1.549440	7.4266						
		0.0115	22.176	1.802	15.523	C	
1.566719	7.4266	0.0115	22.176	1.802	15.523	C)
1.582560	7.4266	0.0115	22.199	1.825	15.523	O)
1.598399	7.4266	0.0115	22.199	1.825			
					15.523	C	
1.617120	7.4266	0.0115	22.199	1.825	15.523	0)
1.632959	7.4266	0.0115	22.199	1.825	15.523	0)
1.650240	7.4151	0	22.176	1.802	15.523	Ö	
1.666079	7.4266	0.0115	22.199	1.825	15.523	0)
1.683360	7.4266	0.0115	22.199	1.825	15.523	0)
1.700639	7.4266	0.0115	22.199	1.825	15.523	0	
1.716480	7.4151	_					
		0	22.199	1.825	15.523	0	
1.733760	7.4266	0.0115	22.199	1.825	15.523	0)
1.749599	7.4151	0	22.199	1.825	15.523	0)
1.765440	7.4151	0	22.199	1.825	15.523	Ō	
		-					
1.782719	7.4266	0.0115	22.199	1.825	15.523	0)
1.800000	7.4151	0	22.199	1.825	15.523	0)
1.817279	7.4266	0.0115	22.199	1.825	15.523	0)
1.833120							
	7.4266	0.0115	22.222	1.848	15.523	0	
1.850399	7.4151	0	22.222	1.848	15.523	0)
1.866240	7.4151	0	22.199	1.825	15.523	0)
1.883519	7.4151	0	22.222	1.848	15.523	Ő	
1.899360	7.4151	0	22.222	1.848	15.523	0	į
1.916639	7.4266	0.0115	22.222	1.848	15.523	0)
1.933919	7.4266	0.0115	22.222	1.848	15.523	0	}
1.948319	7.4266						
		0.0115	22.222	1.848	15.523	0	
1.967039	7.4266	0.0115	22.222	1.848	15.523	0)
1.982880	7.4266	0.0115	22.222	1.848	15.523	0	1
2.000159	7.4266	0.0115	22.222	1.848	15.523	ŏ	
2.016000	7.4151	0	22.222	1.848	15.523	0	1
2.033279	7.4266	0.0115	22.222	1.848	15.523	0	ł
2.050560	7.4266	0.0115	22.222	1.848	15.523	Ō	
2.066399	7.4151	0	22.245	1.871	15.523	0	
2.083680	7.4151	0	22.222	1.848	15.523	0	1
2.099519	7.4151	0	22.245	1.871	15.523	0	,
2.115360	7.4266	0.0115	22.222	1.848	15.523	0	
2.132639	7.4266	0.0115	22.245	1.871	15.523	0	
2.149920	7.4266	0.0115	22.245	1.871	15.523	0	
2.167200	7.4266	0.0115	22.245	1.871	15.523	ō	
2.183039	7.4151	0	22.245	1.871	15.523	0	
2.200320	7.4151	0	22.245	1.871	15.523	O	
2.216159	7.4151	0	22.245	1.871	15.523	0	
.2.233440	7.4266	0.0115	22.245	1.871	15.523	Ö	
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2.249279	7.4151	0	22.245	1.871	15.523	0
2.266560	7.4266	0.0115	22.245	1.871	15.523	Ŏ
2.283839	7.4266	0.0115	22.245	1.871	15.523	ő
2.298240	7.4151	0	22.245	1.871	15.523	Ŏ
2.316959	7.4266	0.0115	22.245	1.871	15.523	0
2.332800	7.4266	0.0115	22.245	1.871	15.523	Ö
2.350079	7.4266	0.0115	22.245	1.871	15.523	0
2.365920	7.4151	0.0119	22.268	1.894	15.523	0
2.3832	7.4266	0.0115	22.245	1.871	15.523	Ö
2.400479	7.4151	0.0113	22.268	1.894	15.523	Ő
2.416320	7.4151	ŏ	22.268	1.894	15.523	0
2.433599	7.4266	0.0115	22.268	1.894	15.523	Ö
2.449440	7.4266	0.0115	22.268	1.894	15.523	0
2.465279	7.4266	0.0115	22.268	1.894	15.523	0
2.484000	7.4266	0.0115	22.245	1.871	15.523	0
2.499839	7.4151	0.0113	22.245	1.871	15.523	0
2.517120	7.4151	0	22.268	1.894	15.523	0
2.532959	7.4266	0.0115	22.268	1.894	15.523	0
2.550240	7.4151	0.0113	22.268	1.894	15.523	0
2.566079	7.4266	0.0115	22.268	1.894	15.523	0
2.583359	7.4266	0.0115	22.268	1.894	15.523	0
2.600640		0.0115	22.245			
2.616479	7.4151			1.871	15.523	0
	7.4266	0.0115	22.245	1.871	15.523	0
2.633760	7.4266	0.0115	22.268	1.894	15.523	0
2.648159	7.4266	0.0115	22.268	1.894	15.523	0
2.666880	7.4266	0.0115	22.268	1.894	15.523	0
2.682719	7.4266	0.0115	22.268	1.894	15.523	0
2.700000	7.4266	0.0115	22.268	1.894	15.523	0
2.717279	7.4266	0.0115	22.268	1.894	15.523	0
2.733120 2.750399	7.4151 7.4266	0 0.0 115	22.268	1.894	15.523	0 0
2.750399	7.4200	0.0115	22.268 22.268	1.894 1.894	15.523 15.523	0
2.783519	7.4151	0	22.268	1.894	15.523	0
2.799360	7.4151	0	22.268	1.894	15.523	0
2.815199	7.4151	0	22.268	1.894	15.523	0
2.833919	7.4266	0.0115	22.291	1.917	15.523	0
2.849760	7.4266	0.0115	22.268	1.894	15.523	Ö
2.867039	7.4266	0.0115	22.268	1.894	15.523	Õ
2.882880	7.4266	0.0115	22.268	1.894	15.523	ů
2.900159	7.4266	0.0115	22.291	1.917	15.523	Ö
2.916000	7.4266	0.0115	22.268	1.894	15.523	ő
2.933279	7.4266	0.0115	22.291	1.917	15.523	Ö
2.950560	7.4151	0	22.268	1.894	15.523	ō
2.966399	7.4266	0.0115	22.291	1.917	15.523	ő
2.983680	7.4266	0.0115	22.291	1.917	15.523	ō
2.998079	7.4266	0.0115	22.291	1.917	15.523	ō
3.016799	7.4266	0.0115	22.291	1.917	15.523	0
3.032639	7.4266	0.0115	22.291	1.917	15.523	Ö
3.049919	7.4266	0.0115	22.291	1.917	15.523	ō
3.067200	7.4266	0.0115	22.291	1.917	15.523	ő
3.083039	7.4266	0.0115	22.291	1.917	15.523	Ö
3.100320	7.4266	0.0115	22.291	1.917	15.523	Ö
3.116159	7.4266	0.0115	22.291	1.917	15.523	0
3.133440	7.4266	0.0115	22.291	1.917	15.523	Ö
3.149279	7.4266	0.0115	22.291	1.917	15.523	Ö
·3.169440	7.4266	0.0115	22.291	1.917	15.523	Ö
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3.183839	7.4266	0.0115	22.291	1.917	15.523	O
3.199680	7.4151	0	22.291	1.917	15.523	0
3.216959	7.4266	0.0115	22.291	1.917	15.523	0
3.232800	7.4266	0.0115	22.291	1.917	15.523	0
3.250080		0.0115	22.291	1.917	15.523	0
3.265919	7.4266	0.0115	22.291	1.917	15.523	0
3.283200	7.4266	0.0115	22.291	1.917	15.523	0
3.300479	7.4151	O	22.291	1.917	15.523	0
3.316320	7.4151	0	22.291	1.917	15.523	0
3.333599	7.4266	0.0115	22.315	1.941	15.523	0
3.348000	7.4266	0.0115	22.315	1.941	15.523	0
3.366719	7.4266	0.0115	22.291	1.917	15.523	0
3.382560	7.4266	0.0115	22.315	1.941	15.523	0
3.399839	7.4266	0.0115	22.315	1.941	15.523	0
3.417120	7.4266	0.0115	22.291	1.917	15.523	0
3.432959	7.4266	0.0115	22.315	1.941	15.523	0
3.450239	7.4266	0.0115	22.315	1.941	15.523	0
3.466079	7.4266	0.0115	22.315	1.941	15.523	0
3.483359	7.4266	0.0115	22.291	1.917	15.523	0
3.500640	7.4266	0.0115	22.291	1.917	15.523	0
3.515039	7.4266	0.0115	22.315	1.941	15.546	0.023
3.533760	7.4151	0	22.291	1.917	15.523	0
3.549599	7.4151	0	22.315	1.941	15.523	0
3.566880	7.4151	0	22.315	1.941	15.523	0
3.582719	7.4266	0.0115	22.315	1.941	15.523	0
3.600000 3.617279	7.4266	0.0115	22.315	1.941	15.523	0
3.633120	7.4266 7.4151	0.0 115 0	22.315	1.941	15.523	0
3.650399	7.4266	0.0115	22.315 22.315	1.941 1.941	15.523	0
3.666240	7.4151	0.0113	22.315	1.941	15.523	0
3.683520	7.4266	0.0115	22.315	1.941	15.523 15.523	0
3.697919	7.4266	0.0115	22.315	1.941	15.523	0
3.716640	7.4151	0.0113	22.315	1.941	15.523	0
3.733919	7.4266	0.0115	22.315	1.941	15.523	0
3.749760	7.4266	0.0115	22.315	1.941	15.523	0
3.767039	7.4266	0.0115	22.315	1.941	15.523	Ö
3.782880	7.4151	0	22.315	1.941	15.546	0.023
3.800159	7.4266	0.0115	22.315	1.941	15.523	0.029
3.816000	7.4266	0.0115	22.315	1.941	15.523	. 0
3.833279	7.4151	0	22.315	1.941	15.523	Ö
3.850560	7.4266	0.0115	22.315	1.941	15.523	ŏ
3.864959	7.4266	0.0115	22.315	1.941	15.523	. 0
3.883679	7.4266	0.0115	22.315	1.941	15.523	ő
3.89952	7.4266	0.0115	22.315	1.941	15.523	Ö
3.916799	7.4151	0	22.315	1.941	15.546	0.023
3.932640	7.4266	0.0115	22.315	1.941	15.523	0
3.949919	7.4151	0	22.315	1.941	15.523	Ō
3.967200	7.4266	0.0115	22.315	1.941	15.523	Ō
3.983039	7.4266	0.0115	22.315	1.941	15.523	ō
4.000320	7.4266	0.0115	22.315	1.941	15.523	Ō
4.016159	7.4266	0.0115	22.315	1.941	15.523	Ō
4.033440	7.4266	0.0115	22.315	1.941	15.523	Ó
4.053599	7.4266	0.0115	22.315	1.941	15.523	0
4.066560	7.4151	0	22.315	1.941	15.523	0
4.083839	7.4266	0.0115	22.315	1.941	15.523	0
4.099680	7.4266	0.0115	22.315	1.941	15.546	0.023

4.116960 7.4151 0 22.315 1.941 15.523 0 4.130799 7.4266 0.0115 22.315 1.941 15.523 0 4.150800 7.4266 0.0115 22.315 1.941 15.523 0 4.183200 7.4266 0.0115 22.315 1.941 15.523 0 4.200479 7.4151 0 22.315 1.941 15.523 0 4.233599 7.4266 0.0115 22.338 1.964 15.523 0 4.286719 7.4151 0 22.338 1.964 15.523 0 4.286719 7.4151 0 22.338 1.964 15.523 0 4.299939 7.4266 0.0115 22.338 1.964 15.523 0 4.330239 7.4266 0.0115 22.338 1.964 15.523 0 4.3360239 7.4266 0.0115 22.338 1.964 15.523 0 4.33760 7.42							
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4.150080 7.4266 0.0115 22.315 1.941 15.523 0.023 4.165919 7.4266 0.0115 22.315 1.941 15.523 0 4.200479 7.4151 0 22.315 1.941 15.523 0 4.214880 7.4266 0.0115 22.315 1.941 15.523 0 4.233599 7.4266 0.0115 22.338 1.964 15.523 0 4.284000 7.4151 0 22.338 1.964 15.523 0 4.289000 7.4266 0.0115 22.338 1.964 15.523 0 4.337119 7.4266 0.0115 22.338 1.964 15.523 0 4.337296 7.4151 0 22.338 1.964 15.523 0 4.337297 7.4266 0.0115 22.338 1.964 15.523 0 4.3873296 7.4266 0.0115 22.338 1.964 15.523 0 4.387360 7.4266 0.0115 22.338 1.964 15.523 0 <							
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5.798880 7.4266 0.0115 22.361 1.987 15.523 0 5.816159 7.4266 0.0115 22.361 1.987 15.546 0.023 5.833439 7.4266 0.0115 22.361 1.987 15.546 0.023 5.84928 7.4266 0.0115 22.361 1.987 15.546 0.023 5.866559 7.4266 0.0115 22.361 1.987 15.523 0 5.893840 7.4266 0.0115 22.361 1.987 15.523 0 5.916960 7.4266 0.0115 22.361 1.987 15.523 0 5.932799 7.4266 0.0115 22.361 1.987 15.546 0.023 5.950080 7.4151 0 22.361 1.987 15.546 0.023							0.023
5.816159 7.4266 0.0115 22.361 1.987 15.546 0.023 5.833439 7.4266 0.0115 22.361 1.987 15.546 0.023 5.84928 7.4266 0.0115 22.361 1.987 15.546 0.023 5.866559 7.4266 0.0115 22.361 1.987 15.546 0.023 5.883840 7.4266 0.0115 22.361 1.987 15.523 0 5.899679 7.4266 0.0115 22.361 1.987 15.523 0 5.916960 7.4266 0.0115 22.361 1.987 15.523 0 5.932799 7.4266 0.0115 22.361 1.987 15.546 0.023 5.950080 7.4151 0 22.361 1.987 15.546 0.023							
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5.84928 7.4266 0.0115 22.361 1.987 15.546 0.023 5.866559 7.4266 0.0115 22.361 1.987 15.546 0.023 5.883840 7.4266 0.0115 22.361 1.987 15.523 0 5.899679 7.4266 0.0115 22.361 1.987 15.523 0 5.916960 7.4266 0.0115 22.361 1.987 15.523 0 5.932799 7.4266 0.0115 22.361 1.987 15.546 0.023 5.950080 7.4151 0 22.361 1.987 15.546 0.023							
5.866559 7.4266 0.0115 22.361 1.987 15.546 0.023 5.883840 7.4266 0.0115 22.361 1.987 15.523 0 5.899679 7.4266 0.0115 22.361 1.987 15.523 0 5.916960 7.4266 0.0115 22.361 1.987 15.523 0 5.932799 7.4266 0.0115 22.361 1.987 15.546 0.023 5.950080 7.4151 0 22.361 1.987 15.546 0.023							
5.883840 7.4266 0.0115 22.361 1.987 15.523 0 5.899679 7.4266 0.0115 22.361 1.987 15.523 0 5.916960 7.4266 0.0115 22.361 1.987 15.523 0 5.932799 7.4266 0.0115 22.361 1.987 15.546 0.023 5.950080 7.4151 0 22.361 1.987 15.546 0.023							
5.899679 7.4266 0.0115 22.361 1.987 15.523 0 5.916960 7.4266 0.0115 22.361 1.987 15.523 0 5.932799 7.4266 0.0115 22.361 1.987 15.546 0.023 5.950080 7.4151 0 22.361 1.987 15.546 0.023							
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5.932799 7.4266 0.0115 22.361 1.987 15.546 0.023 5.950080 7.4151 0 22.361 1.987 15.546 0.023							
5.950080 7.4151 0 22.361 1.987 15.546 0.023							0.023
	5.950080						0.023
	•5.964479	7.4266	0.0115		1.987	15.523	O

5.983200	7.4266	0.0115	22.361	1.987	15.546	0.023
6.000479	7.4266	0.0115	22.361	1.987	15.546	0.023
6.016320	7.4266	0.0115	22.361	1.987	15.523	0
6.033599	7.4266	0.0115	22.361	1.987	15.546	0.023
6.049440	7.4151	0.0113	22.361	1.987	15.523	0.023
6.066720	7.4266	0.0115	22.361	1.987	15.523	0
6.082559	7.4151	0.0113	22.361	1.987	15.523	0
6.099840	7.4266	0.0115	22.361			
				1.987	15.546	0.023
6.117119	7.4266	0.0115	22.361	1.987	15.546	0.023
6.132960	7.4266	0.0115	22.361	1.987	15.523	0
6.148799	7.4266	0.0115	22.384	2.01	15.523	0
6.166080	7.4266	0.0115	22.384	2.01	15.523	0
6.183359	7.4266	0.0115	22.361	1.987	15.523	0
6.200640	7.4151	0	22.361	1.987	15.523	0
6.216479	7.4266	0.0115	22.384	2.01	15.523	0
6.233760	7.4266	0.0115	22.361	1.987	15.523	0
6.249599	7.4266	0.0115	22.384	2.01	15.546	0.023
6.266879	7.4266	0.0115	22.384	2.01	15.546	0.023
6.28272	7.4266	0.0115	22.384	2.01	15.546	0.023
6.299999	7.4266	0.0115	22.361	1.987	15.523	0
6.314400	7.4266	0.0115	22.384	2.01	15.523	0
6.333119	7.4151	0	22.384	2.01	15.523	0
6.350400	7.4266	0.0115	22.361	1.987	15.546	0.023
6.366239	7.4266	0.0115	22.384	2.01	15.546	0.023
6.383520	7.4266	0.0115	22.361	1.987	15.546	0.023
6.399359	7.4266	0.0115	22.384	2.01	15.546	0.023
6.416640	7.4151	0.0113	22.384	2.01	15.523	0.023
6.433919	7.4151	0	22.384	2.01	15.523	0
		-				_
6.449760	7.4266	0.0115	22.384	2.01	15.546	0.023
6.467039	7.4266	0.0115	22.361	1.987	15.546	0.023
6.482880	7.4266	0.0115	22.384	2.01	15.546	0.023
6.498719	7.4266	0.0115	22.384	2.01	15.546	0.023
6.515999	7.4266	0.0115	22.384	2.01	15.523	0
6.533280	7.4266	0.0115	22.361	1.987	15.523	0
6.550559	7.4266	0.0115	22.361	1.987	15.523	0
6.566400	7.4266	0.0115	22.384	2.01	15.546	0.023
6.583679	7.4151	. 0	22.361	1.987	15.523	0
6.599520	7.4266	0.0115	22.361	1.987	15.546	0.023
6.616799	7.4266	0.0115	22.384	2.01	15.546	0.023
6.632640	7.4266	0.0115	22.384	2.01	15.523	0
6.649919	7.4151	0	22.384	2.01	15.523	0
6.664320	7.4266	0.0115	22.384	2.01	15.546	0.023
6.683039	7.4151	0	22.384	2.01	15.546	
6.700319	7.4266	0.0115	22.384	2.01	15.523	0
6.716160	7.4151	0	22.361	1.987	15.546	
6.733439	7.4151	Ö	22.384	2.01	15.546	0.023
6.749280	7.4266		22.384	2.01	15.546	0.023
6.766559	7.4266	0.0115	22.384	2.01	15.523	0.023
6.783840						
6.799679	7.4151	0 0115	22.384	2.01	15.546	
	7.4266	0.0115	22.384	2.01	15.523	0
6.816960	7.4266	0.0115	22.384	2.01	15.523	0
6.832799	7.4151	0	22.384	2.01	15.546	0.023
6.848640	7.4151	0	22.384	2.01	15.546	0.023
6.865919	7.4151	0	22.384	2.01	15.523	0
6.883200			22.384	2.01	15.546	0.023
•6.900479	7.4266	0.0115	22.384	2.01	15.523	0

6.916319	7.4266	0.0115	22.361	1.987	15.523	O
6.933600	7.4151	0	22.384	2.01	15.523	0
6.949439	7.4151	Ö	22.384	2.01	15.523	Ö
6.966720	7.4266	0.0115	22.384	2.01	15.546	0.023
6.983999	7.4266	0.0115	22.384	2.01	15.523	0.025
6.999840	7.4266	0.0115	22.384	2.01	15.523	o
7.014239	7.4266	0.0115	22.384	2.01	15.523	0
7.032960	7.4266	0.0115	22.384	2.01	15.546	0.023
7.050239	7.4266	0.0115	22.384	2.01	15.546	0.023
7.066080	7.4151	0	22.384	2.01	15.546	0.023
7.083359	7.4151	Ō	22.384	2.01	15.546	0.023
7.100640	7.4266	0.0115	22.361	1.987	15.523	0.023
7.116479	7.4266	0.0115	22.384	2.01	15.546	0.023
7.133759	7.4266	0.0115	22.384	2.01	15.546	0.023
7.149600	7.4266	0.0115	22.384	2.01	15.546	0.023
7.166879	7.4266	0.0115	22.384	2.01	15.523	0.029
7.182720	7.4266	0.0115	22.384	2.01	15.523	ő
7.198559	7.4151	0	22.384	2.01	15.546	0.023
7.217280	7.4151	Ō	22.384	2.01	15.546	0.023
7.233119	7.4266	0.0115	22.384	2.01	15.546	0.023
7.250400	7.4266	0.0115	22.384	2.01	15.523	0.023
7.266239	7.4266	0.0115	22.384	2.01	15.546	0.023
7.283520	7.4266	0.0115	22.384	2.01	15.523	0.029
7.299359	7.4266	0.0115	22.384	2.01	15.546	0.023
7.316640	7.4151	0	22.384	2.01	15.523	0
7.333919	7.4266	0.0115	22.384	2.01	15.523	Ö
7.349759	7.4266	0.0115	22.384	2.01	15.546	0.023
7.365599	7.4266	0.0115	22.384	2.01	15.523	0
7.382879	7.4151	0	22.384	2.01	15.546	0.023
7.400160	7.4151	0	22.384	2.01	15.523	O
7.415999	7.4151	0	22.384	2.01	15.523	O
7.433280	7.4151	0	22.384	2.01	15.546	0.023
7.450559	7.4266	0.0115	22.384	2.01	15.523	0
7.466400	7.4266	0.0115	22.384	2.01	15.523	O
7.483679	7.4151	0	22.384	2.01	15.546	0.023
7.499520	7.4266	0.0115	22.384	2.01	15.523	0
7.516799	7.4266	0.0115	22.384	2.01	15.523	0
7.532640	7.4266	0.0115	22.384	2.01	15.523	0
7.548479	7.4266	0.0115	22.384	2.01	15.523	0
7.567199	7.4151	0	22.384	2.01	15.546	0.023
7.583040	7.4151	0	22.384	2.01	15.546	0.023
7.600319	7.4151	0	22.384	2.01	15.546	0.023
7.616160 7.633439	7.4266	0.0115	22.384	2.01	15.523	0
7.649280	7.4266	0.0115	22.384	2.01	15.546	0.023
	7.4266	0.0115	22.384	2.01	15.546	0.023
7.666559 7.683840	7.4266 7.4151	0.0115	22.384 22.384	2.01	15.546	0.023
7.699679	7.4151	0 0.0115	22.384	2.01 2.033	15.546 15.523	0.023
7.715520	7.4266	0.0115	22.407	2.033	15.546	0 0.023
7.73320	7.4266	0.0115	22.384	2.033	15.546	0.023
7.750080	7.4266	0.0115	22.384	2.01	15.523	0.023
7.765919	7.4266	0.0115	22.407	2.033	15.523	0
7.783199	7.4266	0.0115	22.384	2.01	15.523	ő
7.800480	7.4266	0.0115	22.407	2.033	15.546	0.023
7.816319	7.4266	0.0115	22.384	2.01	15.546	0.023
•7.833600	7.4266	0.0115	22.384	2.01	15.546	0.023
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7.849439	7.4266	0.0115	22.407	2.033	15.546	0.023
7.866720	7.4266	0.0115	22.384	2.01	15.546	0.023
7.883999	7.4151	0	22.384	2.01	15.546	0.023
7.898400	7.4266	0.0115	22.407	2.033	15.546	
						0.023
7.917119	7.4266	0.0115	22.407	2.033	15.546	0.023
7.932960	7.4266	0.0115	22.407	2.033	15.546	0.023
7.950239	7.4266	0.0115	22.384	2.01	15.546	0.023
7.966080	7.4266	0.0115	22.407	2.033	15.523	0
7.983359	7.4266	0.0115	22.407	2.033	15.523	Ō
8.000639	7.4266	0.0115	22.407	2.033	15.523	ő
8.016480	7.4266	0.0115	22.407	2.033	15.523	0
8.033759	7.4266	0.0115	22.384	2.01	15.523	0
8.049600	7.4266	0.0115	22.407	2.033	15.523	0
8:005439	7,4151	0	22.384	2.01	15.546	0.023
8.082720	7.4266	0.0115	22.384	2.01	15.546	0.023
8.099999	7.4266	0.0115	22.407	2.033	15.546	0.023
8.117280	7.4266	0.0115	22.407	2.033	15.546	0.023
8.133119	7.4151	0.0113	22.384	2.01		
					15.546	0.023
8.150400	7.4151	0	22.384	2.01	15.546	0.023
8.166239	7.4266	0.0115	22.407	2.033	15.546	0.023
8.183520	7.4266	0.0115	22.384	2.01	15.523	0
8.199359	7.4151	0	22.407	2.033	15.546	0.023
8.216639	7.4266	0.0115	22.407	2.033	15.523	0
8.233920	7.4266	0.0115	22.407	2.033	15.546	0.023
8.248319	7.4266	0.0115	22.407	2.033	15.523	0.023
8.267040		0.0115				-
	7.4266		22.384	2.01	15.546	0.023
8.282879	7.4266	0.0115	22.407	2.033	15.546	0.023
8.300160	7.4151	0	22.407	2.033	15.546	0.023
8.315999	7.4151	0	22.384	2.01	15.546	0.023
8.333280	7.4266	0.0115	22.384	2.01	15.546	0.023
8.350559	7.4151	. 0	22.407	2.033	15.546	0.023
8.366400	7.4266	0.0115	22.407	2.033	15.546	0.023
8.383679	7.4151	0.0110	22.407	2.033	15.546	
		-				0.023
8.399520	7.4266	0.0115	22.384	2.01	15.523	0
8.415359	7.4266	0.0115	22.407	2.033	15.523	0
8.432640	7.4266	0.0115	22.384	2.01	15.546	0.023
8.449920	7.4266	0.0115	22.384	2.01	15.546	0.023
8.467199	7.4266	0.0115	22.407	2.033	15.546	0.023
8.483040	7.4266	0.0115	22.407	2.033	15.546	0.023
8.500319	7.4266	0.0115	22.407	2.033	15.523	0
8.516160	7.4266	0.0115	22.407	2.033	15.546	0.023
8.533439						
	7.4266	0.0115	22.407	2.033	15.546	0.023
8.549280	7.4266	0.0115	22.384	2.01	15.523	0
8.566559	7.4266	0.0115	22.407	2.033	15.546	0.023
8.583840	7.4151	0	22.407	2.033	15.546	0.023
8.598239	7.4266	0.0115	22.407	2.033	15.546	0.023
8.616960	7.4266	0.0115	22.407	2.033	15.546	0.023
8.632799	7.4266	0.0115	22.407	2.033	15.523	0
8.650079	7.4151	0.0113	22.407	2.033	15.546	0.023
8.665920	7.4266	0.0115	22.407	2.033	15.546	0.023
8.683199	7.4266	0.0115	22.407	2.033	15.546	0.023
8.700480	7.4266	0.0115	22.407	2.033	15.546	0.023
8.716319	7.4266	0.0115	22.407	2.033	15.523	0
8.733600	7.4266	0.0115	22.407	2.033	15.546	0.023
8.749439	7.4266	0.0115	22.407	2.033	15.546	0.023
-8.765280	7.4151	0	22.407	2.033	15.546	0.023
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	9.683999	7.4266	0.0115	22.407	2.033	15.546	0.023
•9.699840 7.4266 0.0115 22.407 2.033 15.523 O	•9,699840	7.4266	0.0115	22.407	2.033	15.523	Q

9.717119	7.4266	0.0115	22.407	2.033	15.546	0.023
9.800639	7.4151	0	22.407	2.033	15.546	0.023
9.882720	7.4266	0.0115	22.407	2.033	15.546	0.023
9.966240	7.4151	0	22.43	2.056	15.523	0
10.04975	7.4266	0.0115	22.43	2.056	15.546	0.023
10.13328	7.4266	0.0115	22.407	2.033	15.523	0
10.21680	7.4266	0.0115	22.43	2.056	15.523	O
10.30031	7.4266	0.0115	22.407	2.033	15.546	0.023
10.38383	7.4266	0.0115	22.43	2.056	15.546	0.023
10.46592	7.4266	0.0115	22.43	2.056	15.523	0
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10.54943	7.4266	0.0115	22.43	2.056	15.546	0.023
10.71648	7.4266	0.0115	22.43	2.056	15.523	0
10.88351	7.4266	0.0115	22,43	2.056	15.546	0.023
11.05056	7.4266	0.0115	22.43	2.056	15.546	0.023
11.21616						
	7.4266	0.0115	22.43	2.056	15.523	0
11.38319	7.4266	0.0115	22.43	2.056	15.546	0.023
11.55024	7.4266	0.0115	22.43	2.056	15.546	0.023
11.71727	7.4266	0.0115	22.43	2.056	15.546	0.023
11.88287	7.4266	0.0115	22.43	2.056	15.546	0.023
12.04992	7.4266	0.0115	22.43	2.056	15.546	0.023
12.21695	7.4266	0.0115	22.43	2.056	.15.546	0.023
12.71663	7.4266	0.0115	22.453	2.079	15.546	0.023
13.21632	7.4266	0.0115	22.43	2.056	15.546	0.023
13.71600	7.4266					
		0.0115	22.453	2.079	15.523	0
14.21712	7.4266	0.0115	22.453	2.079	15.546	0.023
14.71679	7.4266	0.0115	22.43	2.056	15.546	0.023
15.21647	7.4266	0.0115	22.453	2.079	15.546	0.023
15.71615	7.4151	0	22.453	2.079	15.546	0.023
		=				
16.21728	7.4266	0.0115	22.453	2.079	15.546	0.023
16.71696	7.4151	0	22.453	2.079	15.546	0.023
17.21664	7.4151	0	22.453	2.079	15.546	0.023
18.21599	7.4151	0	22.453	2.079	15.546	0.023
19.21679	7.4151	Ö	22.476	2.102	15.546	
		=				0.023
20.21616	7.4266	0.0115	22.453	2.079	15.546	0.023
21.21695	7.4266	0.0115	22.476	2.102	15.546	0.023
22.21631	7.4266	0.0115	22.476	2.102	15.546	0.023
23.21712	7.4266	0.0115	22.476	2.102	15.546	0.023
24.21648	7.4266	0.0115	22.476	2.102	15.546	0.023
25.21727	7.4151	0	22.476	2.102	15.546	0.023
26.21664	7.4266	0.0115	22.476	2.102	15.546	0.023
27.21600	7.4151	0	22.476	2.102	15.546	0.023
29.21616	7.4151	0	22.476	2.102	15.546	0.023
31.21631	7.4151					
		0	22.476	2.102	15.546	0.023
33.21648	7.4151	0	22.476	2.102	15.546	0.023
35.21663	7.4151	0	22.499	2.125	15.546	0.023
37.21679	7.4151	0	22.499	2.125	15.546	0.023
39.21696	7.4151	Ō	22.499	2.125	15.546	0.023
41.21711	7.4151	0	22.499	2.125	15.546	0.023
43.21728	7.4151	0	22.499	2.125	15.546	0.023
45.216	7.4151	0	22.499	2.125	15.546	0.023
47.21615	7.4151	0	22.499	2.125	15.546	0.023
52.21728	7.4151	ō	22.499	2.125	15.546	0.023
57.21695	7.4151	0	22.499	2.125	15.546	
62.21664	7.4151	0	22.499	2.125	15.546	
67.21631	7.4151	0	22.522	2.148	15.546	0.023
.72.21600	7.4035	-0.0116	22.522	2.148	15.546	0.023
						J. 422

77.21712	7.4151	0	22.522	2.148	15.546	0.023	
82.21679	7.4151	0	22.522	2.148	15.523	0	
87.21648	7.4035	-0.0116	22.522	2.148	15.546	0.023	
92.21615	7.4035	-0.0116	22.522	2.148	15.523	0	
97.21728	7.4035	-0.0116	22.522	2.148	15.523	0	
107.2166	7.4035	-0.0116	22.522	2.148	15.523	0	
117.2160	7.392	-0.0231	22.522	2.148	15.5	-0.023	
127.2167	7.392	-0.0231	22.522	2.148	15.5	-0.023	
137.2161	7.4035	-0.0116	22.522	2.148	15.5	-0.023	
147.2169	7.392	-0.0231	22.522	2.148	15.5	-0.023	
157.2163	7.392	-0.0231	22.522	2.148	15.477	-0.046	
167.2171	7.4035	-0.0116	22.522	2.148	15.5	-0.023	
177.2164	7.4035	-0.0116	22.522	2.148	15.477	-0.046	
187.2172	7.392	-0.0231	22.522	2.148	15.477	-0.046	
197.2166	7.3804	-0.0347	22.522	2.148	15.477	-0.046	
217.2167	7.3804	-0.0347	22.522	2.148	15.454	-0.069	
237.2169	7.3804	-0.0347	22.522	2.148	15.408	-0.115	

ATTACHMENT D

Groundwater Flow Model Output

```
NUMBER OF COLUMNS = 43 NUMBER OF ROWS = 49 NUMBER OF LAYERS = 2
NUMBER OF TIME STEPS = 6 DELTA=
                                    .33 ERROR= 10.0 XGRID= 165. YGRID= 165.
                                  LAYER
TT= .2250E+04 S1= .7000E-01 HH=
                                .000000 QQ=
                                              .0000E+00
RR= .0000E+00 RRH= .0000E+00 RRD=
                              .0000E+00 BOTT= -.1500E+02 PP= .1500E+03
                                 LAYER
TT= .3000E+06 S1= .2000E-02 HH=
                                .000000 QQ= .0000E+00
RR= .4000E-01 RRH= .0000E+00 RRD= -.1500E+02 BOTT= -.1000E+03 PP= .3000E+04
NUMBER OF PUMPS =
                  11
NUMBER OF STEPS PER RATE =
NUMBER OF RATES PER PUMP =
                           1
I J K RATEI
                  RATE2
                           RATE3
                                   RATE4
                                                      RATE6
                                                                       RATE8
                                                              RATE7
                                                                               RATE9
                                                                                       RATE10
                                                                                                RATE11 RATE12
26 15 2 .00E+00
26 20 2 .00E+00
15 17 2 .00E+00
13 12 2 .00E+00
26 26 2 .86E+06
26 33 2 .00E+00
26 37 2 .00E+00
16 14 2 .00E+00
26 24 2 .00E+00
19 34 1 .00E+00
26 24 1 .00E+00
                         X GRID SPACING
         2640.
                 2
                        2640.
                               3
                                      2640.
                                                     1320.
                                                           5
  6
         660.
               7
                        660.
                              8
                                      660.
                                              9
                                                      330. 10
                                                                   165.
 11
         165.
               12
                        165.
                                      165. 14
                              13
                                                     165.
                                                            15
                                                                    165.
 16
         165.
               17
                        165.
                               18
                                      165.
                                             19
                                                     165.
                                                            20
                                                                   165.
 21
                22
         165.
                        165.
                                      83.
                               23
                                            24
                                                     41.
                                                            25
                                                                    21.
 26
          21.
               27
                         21.
                               28
                                       21.
                                            29
                                                      41.
                                                            30
                                                                    83.
 31
         165. 32
                        165.
                               33
                                      165.
                                             34
                                                     165.
                                                            35
                                                                    165.
 36
         330. 37
                        660.
                               38
                                      660. 39
                                                                 1320.
                                                     660. 40
 41
         1320. 42
                        2640. 43
                                      2640. 44
                                                     2640.
                               Y GRID SPACING
         2640.
               2
                        2640.
                               3
                                      2640.
                                              4 .
                                                     1320.
                                                            5
                                                                   1320.
  6
         660.
               7
                        660.
                              8
                                       660.
                                              9
                                                      330.
                                                            10
                                                                   330.
 11
          330.
              12
                        330.
                             13
                                       330. 14
                                                      165.
                                                            15
                                                                    165.
                                     330.
 16
         165. 17
                        330.
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                                                      165.
                                                            20
                                                                    330.
 21
          330.
               22
                        165.
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 26
          21.
               27
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21.

165.

330.

330. 43

1320. 48

31

36

41

46

165.

330.

330. 42

1320. 47

32

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2640. 49

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2640.

		• • • • • • • • •			. 64.5	P.L	Ç. :	remi.i	renno
1 9 1.7500E+0	3 .7500E+03 .1000E+02 13 .7500E+03 .1000E+02 13 .7500E+03 .1000E+02 CATEGORY CHARACTER	0. 0. 0.	.000E+00 .000E+00 .000E+00	.150E-02 .150E-02 .150E-02	0. 0. 0.	0. 0. 0.	-15.	.5000E+02 .5000E+02 .5000E+02	.5000E+02
.000	0								
050	1								
500	2								
-1.000	3								
-2.000	4								
-3.000	5								
-5,000	6	•							
-8.000	7								
TIME =	.33 DAYS								

ERROR = .9376155E+00 FEET NUMBER OF ITERATIONS = 88

GLOBAL INPUTS = 779328.6 GLOBAL OUTPUTS = 864000.0 WATER BALANCE = -9.79993 %

TIME = .67 DAYS

ERROR = .1042833E+01 FEET NUMBER OF ITERATIONS = 76

GLOBAL INPUTS = 957371.9 GLOBAL OUTPUTS = 864000.0 WATER BALANCE = 9.75294 %

TIME = 1.00 DAYS

ERROR = .1058256E+01 FEET NUMBER OF ITERATIONS = 19

GLOBAL INPUTS = 957687.9 GLOBAL OUTPUTS = 864000.0 WATER BALANCE = 9.78271 %

TIME = 1.33 DAYS

ERROR = .8222610E+00 FEET NUMBER OF ITERATIONS = 5

GLOBAL INPUTS = 934363.8 GLOBAL OUTPUTS = 864000.0 WATER BALANCE = 7.53067 %

TIME = 1.67 DAYS

ERROR = .4180179E+00 FEET NUMBER OF ITERATIONS = 5

GLOBAL INPUTS = 901205.1 GLOBAL OUTPUTS = 864022.0 WATER BALANCE = 4.12593 X

TIME = 2.00 DAYS

ERROR = .1740249E+00 FEET NUMBER OF ITERATIONS = 5

GLOBAL INPUTS = 877534.9 GLOBAL OUTPUTS = 864748.4 WATER BALANCE = 1.45709 %

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NUMBER OF COLUMNS = 43 NUMBER OF ROWS = 49 NUMBER OF LAYERS = 2
NUMBER OF TIME STEPS = 10 DELTA= 3.00 ERROR= 1.0 XGRID= 165. YGRID= 165.
                              LAYER I
TT= .2250E+04 S1= .7000E-01 HH= .000000 QQ= .0000E+00
RR= .0000E+00 RRH= .0000E+00 RRD= .0000E+00 BOTT= -.1500E+02 PP= .1500E+03
                             LAYER 2
TT= .3000E+06 S1= .2000E-02 HH=
                            .000000 QQ= .0000E+00
RR= .4000E-01 RRH= .0000E+00 RRD= -.1500E+02 BOTT= -.1000E+03 PP= .3000E+04
NUMBER OF PUMPS = 11
NUMBER OF STEPS PER RATE =
                      10
NUMBER OF RATES PER PUMP =
                       1
I J K RATEI
                RATE2
                        RATE3
                                RATE4
                                       RATE 5
                                                RATE6
                                                       RATE7
                                                               RATE8
                                                                      RATE9
                                                                             RATE10
                                                                                     RATELL RATEL2
26 15 2 .11E+06
26 20 2 .11E+06
15 17 2 .18E+05
13 12 2 .11E+06
26 26 2 .11E+06
26 33 2 .18E+06
26 37 2 .18E+06
16 14 2 .00E+00
. 26 24 2 .00E+00
19 34 1 .00E+00
26 24 1 .00E+00
                             X GRID SPACING
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                                 660. 39
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    1320. 42
                   2640. 43
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                             Y GRID SPACING
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        330. 37
                    330. 38
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660. 45
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 41
        330. 42
                    330. 43
                                 660. 44
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                                 2640. 49
        1320, 47
                   1320. 48
                                              2640.
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1 41		1.	.7500E+03 .7500E+03	.7500E+03	.1000E+02 .1000E+02 .1000E+02 CHARACTER	0. 0. 0.	.000E+00 .000E+00 .000E+00	.150E-02 .150E-02 .150E-02	0. 0. 0.	0. 0. 0.	-15.	.5000E+02 .5000E+02 .5000E+02	.5000E+02
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			-1.000	3	I								
			-2.000	4									
			-3.000	5									
			-5.000	6									
		,	-8.000	7									
11)	4F -		2	aa nave									

TIME = 3.00 DAYS

ERROR = .2120441E+00 FEET NUMBER OF ITERATIONS = 173

GLOBAL INPUTS = 805844.6 GLOBAL OUTPUTS = 822000.0 WATER BALANCE = -1.96538 %

TIME = 6.00 DAYS

ERROR = .2191280E+00 FEET NUMBER OF ITERATIONS = 164

GLOBAL INPUTS = 838686.9 GLOBAL OUTPUTS = 822000.0 WATER BALANCE = 1.98964 %

TIME = 9.00 DAYS

ERROR = .2162483E+00 FEET NUMBER OF ITERATIONS = .34

GLOBAL INPUTS = 805649.8 GLOBAL OUTPUTS = 822000.0 WATER BALANCE = -1.98907 %

TIME = 12.00 DAYS

ERROR = .2137690E+00 FEET NUMBER OF ITERATIONS = 59

GLOBAL INPUTS = 805674.0 GLOBAL OUTPUTS = 822000.0 WATER BALANCE = -1.98613 % ERROR = .2000437E+00 FEET NUMBER OF ITERATIONS = 5

GLOBAL INPUTS = 826244.3 GLOBAL OUTFUTS = 822000.0 WATER BALANCE = .51368 %

TIME = 18.00 DAYS

ERROR • .2172808E+00 FEET NUMBER OF ITERATIONS = 65

GLOBAL INPUTS = 838631.5 GLOBAL OUTPUTS = 822000.0 WATER BALANCE = 1.98317 %

TIME = 21.00 DAYS

ERROR = .2588207E+00 FEET NUMBER OF ITERATIONS = 7

GLOBAL INPUTS = 837843.5 GLOBAL OUTPUTS = 822000.0 WATER BALANCE = 1.89099 %

TIME = 24.00 DAYS

ERROR = .2163294E+00 FEET NUMBER OF ITERATIONS = 5

GLOBAL INPUTS = 824529.9 GLOBAL OUTPUTS = 822000.0 WATER BALANCE = .30683 %

TIME = 27.00 DAYS

ERROR = .2114981E+00 FEET NUMBER OF ITERATIONS = 11

GLOBAL INPUTS = 805735.9 GLOBAL OUTPUTS = 822000.0 WATER BALANCE = -1.97860 %

TIME = 30.00 DAYS

ERROR = .2124619E+00 FEET NUMBER OF ITERATIONS = 29

GLOBAL INPUTS = 805875.9 GLOBAL OUTFUTS = 822000.0 WATER BALANCE = -1.96157 %