ORIGINAL C-#120

Station= PW-18

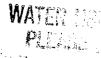
WATER USE PERMIT APPLICATION

and

SUPPLEMENTARY ENGINEERING REPORT

for

ACME IMPROVEMENT DISTRICT



#50-00464-W



WATER USE PERMIT APPLICATION and SUPPLEMENTARY ENGINEERING REPORT for ACME IMPROVEMENT DISTRICT

December 8, 1980

2019 OKEECHOBEE BOULEVARD, WEST PALM BEACH, FLORIDA . . . 33409 . . . 305 - 683-3301

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H.C. GEE, P.E. THEODORE B. JENSON, P.E.

December 8, 1980

Dr. Patrick Gleason South Florida Water Management District Post Office Box V West Palm Beach, Florida

Re: Water Use Permit Application for Acme Improvement District

Dear Pat:

Four copies of the above-referenced Application and Supplemental Engineering Report are being submitted as required by SFWMD on this date.

Generally, it was found that the proposed wellfield in Section 25 would produce water of adequate quantity and quality, without causing adverse impacts, to meet 1988 projected demands.

If you or your staff have any questions regarding this application, please contact me at your earliest convenience. As described in the report, Acme is in urgent need of supplementing their existing raw water supply system and obtaining the necessary approvals to do so.

Your cooperation and assistance in this matter is appreciated.

Yours sincerely,

Shidi Vandor

GEE & JENSON Engineers-Architects-Planners, Inc.

Heidi Vandor Hydrogeologist

HV/de

cc: Edward C. Lowder Fred A. Greene Cotter Christian

APPLICATION FOR WATER USE PERMIT ACME IMPROVEMENT DISTRICT

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PART II

Supplemental Engineering Report

Gee & Jenson, November 1980 "Water Supply Development - Section 25 for the Acme Improvement District."

PART I APPLICATION FOR WATER USE PERMIT for ACME IMPROVEMENT DISTRICT

December 8, 1980

CHECKLIST FOR INDIVIDUAL PERMITS

This checklist is for use under either of two conditions: a) for either existing or proposed water usage in excess of 100,000 gpd in most areas of the District except those designated under (b); b) for either existing or proposed water usage greater than 10,000 gpd on an average day or greater than 20,000 gpd on a maximum day in two distinct geographic areas. These two areas are, first, in the vicinity of the City of Stuart comprising the peninsular land area north of Indian Street, and, second, the land areas of Sanibel and Captiva Islands.

A. General

- Name, address and telephone number of corporation, individual or municipality requesting a permit. Name of person responsible for obtaining a permit.
- 2. Name, address and telephone number of Engineering Firm submitting the application (if applicable). Name of engineer responsible for obtaining the permit.
- 3. Describe the purpose of the application.
- 4. Indicate the quantity of water applied for as an annual allocation (gals/year). This quantity may equal the annual quantity which will be pumped at a future point in time, or may equal the applicant's existing pumpage if no future increases in pumpage are anticipated. The requested allocation should equal average daily pumpage multiplied by 365 days.

The most common mistake made in applying for an allocation is that the maximum daily pumpage is multiplied by either 365 days/year or the number of days per year pumpage is performed. The requested allocation applied for is based on an average daily withdrawal. Make sure that the allocation you requested is equal to your projected average day pumpage multiplied by 365 days per year.

Example: A new utility is presently serving 5000 persons at an average use of 100 GPCD.* Current average daily use is therefore 500,000 gallons per day.

*GPCD - Gallons per Capita Day.

In 1987 this utility expects to serve 15,000 persons at 100 GPCD which is equal to an average day use of 1.5 MGD. Thus the requested annual allocation is:

- 1.5 MGD x 365 days = 548 MG/year
- 5. Explain briefly the derivation of annual allocation.
 - a. Indicate the projected population used in determining the annual allocation.
 - b. Indicate the per capita consumption used in determining the annual allocation.

6. Indicate the maximum daily pumpage associated with your projected average day pumpage.

The applicant should note that the water treatment capacity that is capable of treating the maximum day should be described as part of the answer to "3. Proposed Treatment Facilities" in Section C.

- Indicate the maximum day to average day demand ratio used in calculating the projected maximum day pumpage. Explain briefly the basis for using this number.
- 8. List the future year in which the quantity of water applied for will be used.
- 9. Indicate if SFWMD permits for water use have been issued (Yes or No).
- 10. Map Location of Existing Facilities: Attach a (or a copy of a) USGS Topographic Map (use additional maps if all of the information cannot be clearly indicated) showing:
 - a. the location of all wells.
 - the area served by the applicant's wells.
 - c. location of existing water treatment facilities and wastewater treatment facilities.
- 11. Map Location of Proposed Facilities: Attach a (or a copy of a) USGS Topographic map (use additional maps if all of the information cannot be clearly indicated) showing:
 - a. additional land area, if any, which will be served.
 - b. proposed well locations.
 - c. location of proposed water treatment facilities.
- 12. Indicate on a map or sketch of the applicant's property and surrounding area:
 - a. Location of other wells not owned by the applicant including domestic wells, irrigation wells, etc. within 300' of the applicant's wells.
 - b. Location of pollution sources within 300' of the applicant's wells such as percolation ponds, sewage mains, etc. (septic tanks excluded).
 - Location of nearest saline water or salinity control structure (if the distance is less than one mile).
 - d. Location of any existing or proposed wastewater treatment and disposal facilities that will recharge the aquifer in the vicinity of the applicant's wellfield(s).

13. If the applicant is a private corporation, attach an affidavit of incorporation.

B. Existing Facilities and Pumpage

- 1. EXISTING FACILITIES DESCRIPTION:
 - a. Describe existing wells: fill out Table A as complete as possible; attach driller's log, specific capacity data or aquifer performance test data, if available.
 - b. Describe existing treatment plant: treatment plant capacity (potential capacity and capacity as rated by DER), and method of treatment.
 - c. For surface water systems, indicate source of water, and the name, address and telephone number of either the local drainage or local water management district having jurisdiction over maintenance of the surface water system.
 - d. Describe existing fire flow and standby well capacity. Calculate the existing capacity for each.
 - e. Describe the existing well or wellfield operation schedule. Include in the description:
 - i. Which wells are primary.
 - ii. Which wells are stand-by.
 - iii. Well rotation schedule, if any.
 - iv. Which wells will be pumped simultaneously, if any.
 - v. The order of preference in turning-on wells.
 - f. Describe the location of existing flow meters, i.e., on individual wells, before treatment, after treatment and/or at customer's connections.
- POPULATION: Indicate the number of people and number of connections served by existing wells at the present time.
- 3. SERVICE AREA: Indicate size of area served in acres.
- 4. IRRIGATION: Estimate the percentage of existing withdrawals used for irrigation.
- 5. INTERCONNECTIONS: Explain in detail any interconnections with other suppliers. Indicate maximum amount of water which can be supplied via the interconnect.

- 6. INTERFERENCE: Describe any interference between existing wells or interference with a well on an adjacent landowner's property.
- 7. PAST WATER USE: Fill out Table B with data, if available, on water use during the past 10 years.
- 8. MOST RECENT WATER USE: Fill out Table C using the most recent 12 months of daily pumpage records, if available. If possible, obtain data from DER's monthly operating reports. Attach a list of the ten largest users of water that are currently served by the applicant. Indicate maximum monthly water usage for each user.
- 9. RAW WATER QUALITY: Attach raw water quality information.
- 10. SERVICE AREA: Indicate number of Public Service Commission (PSC) certificate if applicant is regulated by the PSC.
- 11. WATER PROBLEMS: Explain any problems the utility is currently experiencing or causing as a consequence of withdrawals, such as drawdowns of adjacent water bodies, saline water intrusion, adverse impact on adjacent land use, water quality problems, etc.

C. Future Facilities and Pumpage

1. PROJECTED ANNUAL ALLOCATION: Show how projected annual pumpage was determined if different from existing pumpage.

2 INSTALLED CAPACITY:

- a. Detail the installed capacity which will be required to supply the quantity of water requested above.
- Give details on location, size (diameter), length of casing, and total depth of proposed wells, if information available.
- c. Explain choice of well sites.
- d. Describe proposed fire flow and stand-by well capacity.
- 3. PROPOSED WATER TREATMENT FACILITIES: The annual allocation requested within this application should equal the sum of the capacity of existing and proposed treatment facilities. Therefore, the sum of the capacities of existing and proposed treatment plants should not be less than the maximum day withdrawals associated with the projected annual allocation.
 - a. Describe additional treatment plant construction (include treatment capacities).
 - b Projected completion date of proposed construction.
- 4. PER CAPITA DAILY USE: Indicate proposed consumption of water per capita (on a permanent population basis) or per equivalent residential connection; give estimated number of persons/unit. If proposed per capita consumption is greater than existing per capita consumption then explain difference.

- 5. POPULATION PROJECTION: Project population for the future service area for the next ten years, and explain source for information. Fill in Table D with the projected populations for each year of the next ten years.
- 6. WATER USE PROJECTION: Fill out Table D. The origin of the projection should be explained.
- 7. EXTRAPOLATION OF PAST WATER USE: Extrapolate past total annual pumpages to a date which is ten years into the future on semi-log paper.
- 8. IRRIGATION: If any of the projected water use will be for irrigation of golf courses or park areas, please indicate the following:
 - a. Area in acres which will be irrigated.
 - b. Type of vegetation which will be irrigated, i.e., grasses, etc.
 - c. Approximate maximum monthly water use.
 - d. Approximate average annual water use.
 - e. Show irrigated area on USGS Topographic map.

Withdrawal may be calculated by multiplying pump size (gpm) by the amount of time the pump is run.

9. SERVICE AREA EXPANSION:

- a. For Public Utilities If the service area will be expanded in the future by annexation, attach a copy of expansion plans.
- b For Private Utilities If the service area will be expanded in the future, attach a copy of any correspondence to the Public Service Commission (PSC) concerning an expanded service area if the utility is located in a County regulated by the PSC.
- c. For County Franchised Service Areas If the service area is franchised by county government, then attach any correspondence with the county regarding a proposed expansion of the service area.
- d. For Dade County Utilities Submit a letter from the Miami-Dade Water and Sewer Board approving any proposed increase in service area.
- 10. IMPACT ON OTHER USES OF WATER: Indicate any possible interference with other wells not owned by the applicant (including domestic and irrigation wells) as a result of increases in withdrawals.
- 11. SURFACE WATER IMPACT: Detail any impact on surface water bodies (such as ponds, lakes, etc.) that the increased withdrawals may have.
- 12. ENVIRONMENTAL IMPACT: Describe any possible adverse environmental impact on environmentally sensitive areas that the increased withdrawals may cause.
- 13. WASTEWATER RECYCLING: Describe plans to recycle wastewater and indicate volumes with time.

D. Surface Water Use

- 1. Describe existing system including pumps, intakes, and location.
- 2. Describe proposed facilities.
- 3. Show locations of existing and proposed facilities on a (or a copy of a) USGS Topographic Map.
- 4. Indicate any requirement for water from District canals or other works.

E. Reverse Osmosis Treatment

Indicate:

- a. Withdrawal capacity.
- b. Potable water supply capacity.
- c. Reject water discharge capacity.

2. Treatment plant process:

- a. Indicate the treatment efficiency ratio.
- b. Indicate the amount of raw water that can be blended with the R. O. permeate.
- c. Attach correspondence from the appropriate regulatory agency giving approval of raw water/R.O. permeate blending.
- d. Indicate the highest level of total dissolved solids (TDS) or chlorides that can be efficiently and economically treated using the currently installed membranes.
- 3. Indicate the level of chloride ions of both the reject water and the receiving water body.
- 4. Show location of effluent discharge on a USGS topographic map. Will effluent be discharged through a manifold? Show outlets of manifold.
- 5. Indicate any environmental impact that effluent discharge may have.

F. New Wellfield

- 1. If a new wellfield is proposed, please explain:
 - a. Why new wellfield is needed.
 - b. Choice of the specific site.
 - Hydrogeologic information on the site.
 - d. Ownership of the site.
 - e. Distance from nearest saline water source and nearest inland salinity control structure.

G. Affidavit for Proposed Facilities

The applicant should attach an affidavit indicating that the applicant has obtained a legal right to use the proposed sites for wells, treatment plants, and facilities in the locations designated within the application.

ANSWERS TO CHECKLIST FOR WATER USE PERMIT

A. GENERAL

1. Acme Improvement District P. O. Box 248

Loxahatchee, F1 33470

Person Responsible: Edward C. Lowder, Business Manager Phone 305/793-0866

2. Gee & Jenson Engineers-Architects-Planners, Inc.

2019 Okeechobee Boulevard West Palm Beach, Fl 33409

Person Responsible: Heidi Vandor, Hydrogeologist,

Phone 305/683-3301

- 3. The purpose of the application is to obtain an increase in allocation to the existing Water Use Permit for Acme Improvement District for a public water supply system through 1991.
- 4. The quantity of water applied for as an annual allocation is 910 mgy. (2.49 mgd).
- 5. The requested annual allocation is based on the available projected demands to the year 1988, using data for residential, under-construction, and commercial units. See Table 1.
 - a. The projected population for 1988 is 15,746.
 - b. The per capita consumption used in determining the annual allocation is 158 gpcd.
- 6. Projected maximum daily pumpage is 3.76 mgd.
- 7. Maximum day to average day ratio is 1.51, based upon existing pumpage records for the 12-month period, November 1979 through October 1980. See Table 2.
- 8. The quantity of water applied for will be used in 1988.
- 9. Acme Improvement District has an existing Water Use Permit and Surface Water Management Permit.
- 10. See Figure 1 for the following information:
 - a. Location of existing supply wells.
 - b. Present service area.
 - c. Existing raw water and wastewater treatment facilities.

- 11. See Figure 1 for the following information:
 - a. Additional service area.
 - b. Proposed well locations.
 - c. Proposed water treatment facilities (Expansion II).
- 12. Not applicable.
- 13. Not applicable.

B. EXISTING FACILITIES AND PUMPAGE

- 1. Existing facilities description:
 - a. See Table 3 for well construction data.

 See Appendix A for step-drawdown data.

 See Supplemental Engineering Report for aquifer performance test data.
 - b. The existing water treatment plant serving the Acme Improvement District has the capability of producing 1,650,000 gallons of treated water daily. This includes Expansion I. The facility also provides storage for 1,250,000 gallons. It utilizes the lime softening treatment process in addition to aeration, chlorination, and filtration before distribution.
 - c. Acme Improvement District has an existing Surface Water Management Permit.
 - d. A minimum fire flow of 500 gpm can be provided in the single-family residential areas, 1000 gpm can be provided in the vicinity of high density apartments, and 2000 gpm can be provided in major commercial areas.
 - e. Of the 14 existing supply wells, 9 were in service as of November 14, 1980. At present, wells are pumped on a demand basis. Additional supply wells are needed to implement an efficient wellfield operating program.
 - f. Each well is equipped with a totalizing flowmeter and a Clayton control valve. A telemetering control system is also provided so that the operators at the treatment plant can start and stop all well pumps in accordance with water requirements. Individual meters are present at each customer's connection.
- 2. A population of approximately 4,000 is served at present, with 2,466 connections in service as of the end of October 1980.
- 3. Acme Improvement District covers an area of approximately 18,200 acres. The present Water Use Permit serves an area of 7,375 acres (Unit Development 1-Wellington). Future development will include an additional 1,694 acres at the Landings (west of the existing service area) and 958 acres at Country Place (south of the existing service area). See Figure 1.
- 4. An estimated 10% of the existing withdrawals is used for irrigation.

- 5. There are no interconnections with other suppliers.
- 6. There is no known interference to adjacent wells.
- 7. See Table 4 for past water use data.
- 8. See Table 2 for most recent water use data.
- 9. See attached Supplemental Engineering Report for raw water quality information for Section 25 (Appendix C), and a previous report prepared by Gee & Jenson, October 1979, "Summary Report for Acme Improvement District Test Well Program" for available water quality data on Wells 1 through 17.
- 10. Not applicable.
- 11. Acme Improvement District is currently experiencing severe problems with their existing raw water supply wells (Wells 1 to 17). These include water quality problems, short life expectancy of wells, diminishing pumping rates, and inadequate capacity and low pumping rates from the existing wellfield locations.

The existing areas (Wells 1 to 6, 7 to 17) are prone to natural saltwater contamination at shallow depths due to the existence of connate sea water in the region. This problem led to the necessity of extensive exploration for a better raw water supply. The proposed Section 25 wellfield, described in depth in the attached Supplementary Engineering Report, proved to be an area most likely to supply a reliable long-term supply of adequate quality water to Acme Improvement District. Extensive testing of Test Well No. 18 verified this.

The present pumping capacity is 1.03 mgd when all wells are pumping (Table 3). The present average day and maximum day demand is about 0.7 mgd and 1.07 mgd, respectively. This data shows that immediate action needs to be taken to supplement the existing raw water supply.

C. FUTURE FACILITIES AND PUMPAGE

1. The projected annual allocation, 910 mgy, was determined using unit projections for residential, builder-owned, and commercial units and their corresponding consumption rates for 1988. See Table 1.

2. Installed capacity:

a. Listed below is a summary of requirements:

| 1988 maximum da | demand | 3.76 mgd |
|-----------------|-----------------|-----------|
| 1980 maximum da | demand | 1.07 .ngd |
| Additional | required demand | 2.69 mgd |

For an efficient wellfield operating program 100% standby capacity is required = 2.69 mgd

Total capacity required for meet 1988 demands 5.38 mgd

- b. Proposed sites for new supply wells are located in Section 25, Township 44 South, Range 41 East. The 10 proposed wells will be constructed similiarly to Test Supply Well No. 18 already drilled in this area. See table 3 and Supplemental Engineering Report (Figure 4) for construction details. It is estimated each proposed well will have a capacity of about 750 gpm (about 1 mgd).
- c. After an extensive site selection process and test well drilling program, Section 25 was selected as the most feasible in terms of water quality, water availability, location, and legal aspects. The Supplementary Engineering Report provides additional details. Gee & Jenson also prepared a Summary Report for the Test Well Program, 1979, that provides additional background data.
- d. The recommended wellfield operation program for Section 25 wellfield would have 5 of the 10 proposed wells operating at any one time, alternating with the other 5 every 24 hours. See the Supplemental Engineering Report for recommendations and further details.

3. Proposed Water Treatment Facilities:

a. Construction is underway for Expansion II, which will provide an additional capacity of 2.0 mgd, for a total plant capacity of 3.65 mgd.

- b. The projected completion date for Expansion II is October 1981.
- 4. The proposed per capita daily use is 158 gpcd. The estimated number of persons per unit is 2.61, based upon data from Gee & Jenson, March 1980., "Water and Wastewater Facilities Expansion Program." See also Table 1.
- 5. Population Projection: See Table 1.
- 6. Water Use Projection: See Table 1.
- 7. Not applicable. Past water use was used primarily for construction and only five complete years of pumpages are available.
- 8. Not applicable.
- 9. Not applicable.
- 10. Impact on other users of water: An in-depth hydrogeologic analysis was performed on Test Supply Well No. 18 in Section 25 to determine aquifer parameters and impacts associated with pumping. The Supplementary Engineering Report discusses this in detail. In summary, no noticeable impact was found to occur as a result of pumping on shallow wells in the area. Aquifer coefficients of T=32,000 gpd/ft and S=0.1 were used for design purposes. A minimum spacing of 1600 feet between wells and a pumping rate of 750 gpm was found to cause neglible impact under a proper wellfield operation and management program.
- 11. None
- 12. None
- 13. None

D. SURFACE WATER USE

Not Applicable.

E. RESERSE OSMOSIS TREATMENT

Not Applicable.

F. NEW WELLFIELD

 a. New wellfield is needed to supplement existing raw water supply system. Refer to the following for additional information:

> Section C. 2.a. Section C. 2.c. Supplementary Engineering Report

b. Choice of Specific Site:

See: Section C. 2.c.
Supplementary Engineering Report

- c. Hydrogeologic information on the site is contained in the Supplymentary Engineering Report
- d. The site is located within Acme Improvement District boundaries.
- e. The site is located at least 10 miles from the intracoastal waterway.

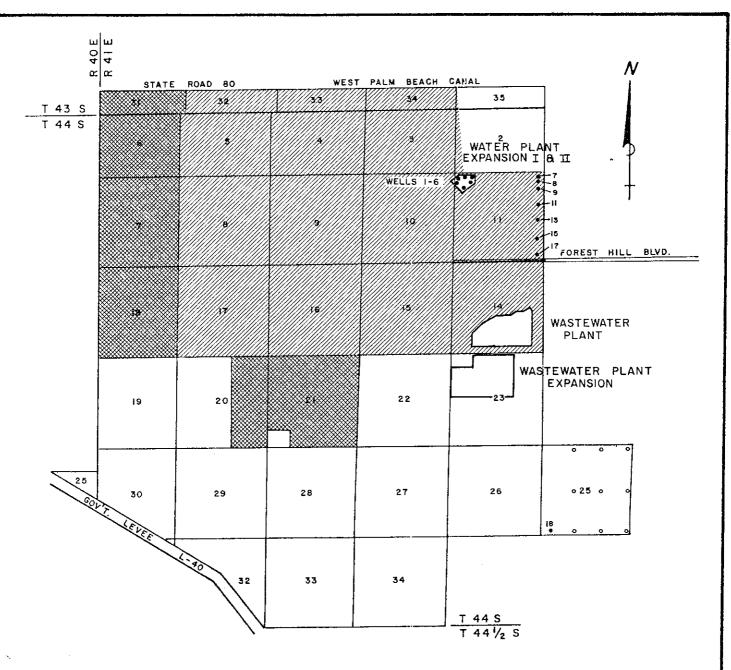
G. AFFIDAVIT FOR PROPOSED FACILITIES

Not Applicable.

REFERENCES

Gee & Jenson, October 1979, "Summary Report for Acme Improvement District Test Well Program."

Gee & Jenson, Revised March 1980, "Water and Wastewater Facilities Expansion Program."





LEGEND

- EXISTING WELL
- PROPOSED WELL(Tentative Location)
- EXIS

EXISTING SERVICE AREA

PROPOSED SERVICE AREA

EXISTING AND PROPOSED SERVICE AREA AND FACILITIES

GEE & JENSON ENGINEERS-ARCHITECTS-PLANNERS,INC.
WEST PALM BEACH, FLORIDA

TABLE 1
PROJECTED WATER USE

| | ACTIVE (1) | RESIDENTIAL (2) | (3) | UNDER C | ONSTRUCTION (5) | | (ERCIAL | TOTAL WATER | (7) USE |
|------|----------------|-----------------|-----------|---------|-----------------|--------------|------------------|-------------|------------|
| YEAR | DWELLING UNITS | POPULATION | WATER USE | UNITS | WATER USE | (1) UNITS | (6) WATER USE | AVERAGE DAY | YEARLY |
| 1980 | 1,533 | 4,001 | 600 | 300 | 79 | 23 | 22 | 0.701 | 255.9 |
| 1981 | 2,133 | 5,567 | 835 | 300 | 79 | 28 | 26 | 0.940 | 343.1 |
| 1982 | 2,733 | 7,133 | 1,070 | 300 | 79 | 33 | 31 | 1.180 | 430.7 |
| 1983 | 3,333 | 8,699 | 1,305 | 300 | 79 | 38 | 36 | 1,420 | 518.3 |
| 1984 | 3,933 | 10,265 | 1,540 | 300 | 79 | 43 | 40 | 1.659 | 605.5 |
| 1985 | 4,533 | 11,831 | 1,775 | 300 | 79 | 48 | 45 | 1.899 | 693.1 |
| 1986 | 5,133 | 13,397 | 2,010 | 300 | 79 | 53 | 50 | 2.139 | 780.7 |
| 1987 | 5,733 | 14,963 | 2,244 | 300 | 79 | 54 | 51 | 2.374 | 866.5 |
| 1988 | 6,033 | 15,746 | 2,362 | 300 | 79 | 55 | 52 | 2.493 | 909.9 |

⁽¹⁾ Gee & Jenson, March 1980, "Water & Wastewater Facilities Expansion Program." (Growth rate data supplied by Developer.)

⁽²⁾ Based upon 2.61 persons per unit.

⁽³⁾ In thousands of gallons for an average day, based upon an average daily consumption of 150 gpcd.

⁽⁴⁾ Includes builder owned and under construction, Gee & Jenson, March 1980.

⁽⁵⁾ In thousands of gallons for an average day, based upon an average daily consumption of 263 gpd, Gee & Jenson, March 1980.

⁽⁶⁾ In thousands of gallons for an average day, based upon an average daily consumption of 940 gpd, Gee & Jenson, March 1980.

⁽⁷⁾ In millions of gallons.

TABLE 2

RECENT WATER USE

NOV. 1979 TO OCT. 1980

| Year | Month | Raw Water Average Day * | Pumpage Maximum Day* | Total Raw Water Pumpage_* | Total Water Treated* |
|--------------|-----------|----------------------------|-------------------------|------------------------------|-------------------------|
| | | | | | 16 500 |
| 197 9 | November | 567 | 931 | 17,002 | 16,582 |
| 1979 | December | 611 | 1,011 | 18,947 | 19,346 |
| 1980 | January | 728 | 1,045 | 22,572 | 24,267 |
| 1980 | February | 703 | 955 | 20,379 | 21,428 |
| 1980 | March | 923 | 1,413 | 28,626 | 29,909 |
| 1980 | April | 834 | 1,280 | 25,030 | 25,746 |
| 1980 | May | 993 | 1,481 | 30,797 | 30,428 |
| 1980 | June | 1,135 | 1,579 | 34,062 | 32,378 |
| 1980 | July | 851 | 1,482 | 26,376 | 26,727 |
| 1980 | August | 878 | 1,315 | 27,223 | 27,105 |
| 1980 | September | 7 95 | 1,273 | 23,863 | 23,234 |
| 1980 | October | 840 | 1,132 | 26,034 | 27,678 |
| | Total | 9,848 | | 300,911 | 304,828 |
| | Average | 821 | | 25,076 | 25,402 |

* In thousands of gallons

Ratio of water pumped to water treated 0.99.

Maximum day pumpage was 1.579 mgd and occurred on June 16, 1980.

Ratio of maximum day pumpage to average day pumpage was 1.51.

TABLE 3

DESCRIPTION OF EXISTING SUPPLY WELLS

| Well No. | Total Depth (feet) | Casing Diameter (inches) | Casing Depth (feet) | Year Drilled | Design Pumping Rate (gpm) | Present Pumping Rate(3) (GPM) | Remarks |
|----------|--------------------------|--------------------------------|---------------------------|---------------------|---------------------------------|-------------------------------|---------------------------------------|
| _1 | 35 | 6 | 20 | 1972 | 100 | 71 | |
| 2 | 45 | 6 | 20 | 1972 | 100 | 64 | |
| 3 | 45 | 6 | 20 | 1972 | 100 | 52 | |
| 4 | 50 | 6 | 25 | 1972 | 100 | _ | Out of service. |
| 5 | 45 | 6 | 20 | 1972 | 100 | - | Out of service. |
| 6 | 45 | 6 | 20 | 1972 ⁽²⁾ | 100 | _ | Out of service. |
| 7 | 40 | 14/6 ⁽¹⁾ | 20 | 1978 | 125 | 67 | |
| 8 | 80 | 14/6 | 20 | 1978 | 250 | 107 | **** |
| 9 | 40 | 14/6 | 20 | 1978 | 125 | 77 | |
| 11 | 40 | 14/6 | 20 | 1978 | 75 | 51 | |
| 13 | 40 | 14/6 | 20 | 1978 | 100 | 98 | |
| 15 | 40 | 14/6 | 20 | 1978 | 100 | 126 | |
| 17 | 80 | 14/6 | 20 | 1978 | 250 | - | Temp. out of service |
| 18* | 90 | 18/12 | 70 | 1980 | N/A | N/A | New test supply wel |
| | | | | TOTAL | 1,625 | 713 | |
| | | | | (2 | 2.34 mgd) | (1.03 mgd) | · · · · · · · · · · · · · · · · · · · |

⁽¹⁾ Outer casing/inner casing.

⁽²⁾ Put in service in 1978.

⁽³⁾ As of November 14, 1980.

N/A Not applicable.

^{*} Lithology log included in Supplementary Engineering Report.

TABLE 4
PAST WATER USE

| | Number (1) of | Average (2) | Maximum (2) | Total (2) |
|------|------------------|-----------------------|-------------|-----------|
| Year | Connections | Day | Day | Annual |
| 1973 | | Records not available | | |
| 1974 | | Records not available | | |
| 1975 | 87 | 52.1 | 231.8 | 19,030 |
| 1976 | 27 0 | 135.0 | 544.7 | 49,291 |
| 1977 | 540 | 221.5 | 486.5 | 80,860 |
| 1978 | 994 | 381.5 | 699.6 | 139,255 |
| 1979 | 1,966 | 638.9 | 1,250.0 | 233,201 |

NOTE: 1973-1976 water used primarily for construction.

- (1) Total metered services at end of year.
- (2) In thousands of gallons.

PART II

SUPPLEMENTARY ENGINEERING REPORT

WATER SUPPLY DEVELOPMENT SECTION 25

for

ACME IMPROVEMENT DISTRICT

November 1980

WATER SUPPLY DEVELOPMENT SECTION 25

FOR THE

ACME IMPROVEMENT DISTRICT

NOVEMBER 1980

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November 17, 1980

Acme Improvement District Post Office Box 248 Loxahatchee, Florida 33470

Attention: Mr. Edward C. Lowder

Business Manager

Re: Acme Test Supply Well #18 - Section 25

Gentlemen:

The report entitled "Water Supply Development - Section 25" for Acme Improvement District is being submitted at this time. It is to act as a required supplementary engineering report for the forthcoming Water Use Permit Application to be submitted to the South Florida Water Management District.

The results of the testing indicated a sustained yield of about 5 mgd may be attainable from Section 25 as described in the report.

Yours sincerely,

GEE & JENSON Engineers-Architects-Planners, Inc.

Heidi Vandor Hydrogeologist

HV/de 80-196

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EXECUTIVE SUMMARY

The following report was prepared to supplement the application for modification of the existing Water Use Permit to be issued by the South Florida Water Management District (SFWMD).

Gee and Jenson Engineers-Architects-Planners, Inc., contracted with Acme Improvement District on July 30, 1979 to provide professional services in connection with hydrologic testing of a test supply well and preparation of SFWMD Water Use Permit.

Acme Improvement District is in urgent need of supplementing its existing raw water supply. After a lengthy site selection process, Section 25 was selected as being the most feasible.

A test well program defining the geology and water quality was performed to verify the feasibility of Section 25 prior to implementing the more costly Test Supply Well No. 18 Program described in this report. These studies provided the necessary lithologic and hydrogeologic data necessary for the interpretation of the subsurface strata.

An aquifer test was conducted to define the aquifer parameters necessary for the planning and management of the water

resources of the area. A transmissivity and storage coefficient of 34,000 gpd/ft and 0.1, respectively, was used as a conservative estimate for design purposes.

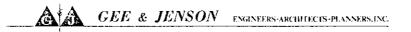
It was found that based on these estimates, Section 25 could support ten wells, each with a capacity in the range of 750 gpm, causing negligible impact. That is, approximately 5 MGD could be withdrawn from the area under a wellfield operating program where five wells would be pumped at any one time.

Recommendations

1. A network of ten supply wells should be constructed in Section 25 of the Acme Improvement District generally in the locations specified. These wells should be spaced approximately 1,600 feet apart. Recommended withdrawal rates are 750 gpm per well which will be dependent upon site specific variations in lithology and hydrology. It is recommended that implementation of well construction be phased starting with the southern wells first.

- 2. A wellfield operating and management program for these wells is required to minimize withdrawal impacts and retain the integrity of the well construction. The recommended operating program is:
 - a. Pump only five wells at a time using alternately spaced wells.
 - b. Duration of pumping each bank of wells should not exceed 24 hours.
- 3. A specific capacity test should be performed on each supply well on completion of construction.
- 4. A monitoring program should be instituted in Section 25 to determine the sustained yield. The data generated from the monitoring may indicate the potential for increased withdrawals from Section 25 or may indicate a reduction in withdrawals. The monitoring should include recording rainfall, groundwater levels in observation wells, pumping water levels in supply wells, well withdrawals and canal stage.
- 5. Additional potable water supply of comparable quantity and quality can be anticipated to the

south of Section 25 and to the east of SR 7 as stated in Gee and Jenson's Test Well Summary Report, 1979.



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1.0 INTRODUCTION

The following report was prepared to supplement the application for modification of the existing Water Use Permit to be issued by the South Florida Water Management District (SFWMD). The results and conclusions generated are based upon prior discussions with SFWMD staff on the feasibility of implementing a program as described in this report. The staff was in agreement that the proposed use would be reasonable and not cause significant impact on adjacent users.

2.0 PURPOSE AND SCOPE

Gee and Jenson Engineers-Architects-Planners, Inc., contracted with Acme Improvement District on July 30, 1979 to provide professional services in connection with hydrologic testing of a test supply well and preparation of SFWMD Water Use Permit.

Acme Improvement District is in urgent need of supplementing its existing raw water supply. After a lengthy site selection process, Section 25 was selected as being the most feasible.

Most other areas under consideration were found to have inadequate water quality, could not be developed quickly enough, or had legal problems associated with their development.

A test well program defining the geology and water quality was performed to verify the feasibility of Section 25 prior to implementing the more costly Test Supply Well No. 18 Program described in this report.

The three test wells constructed as part of Test Well Program - Section 25, in addition to the four observation wells and test supply well of the Test Supply Well No. 18 program provided the necessary lithologic and hydrogeologic data necessary for the interpretation of the subsurface strata. In addition, they can serve as permanent observation wells for water levels and water quality.

The location of the aquifer test is in the southwest quarter of Section 25, T 44 S, R 16 E in Palm Beach County (Figure 1). Additional locations of test wells and observation wells are shown in Figures 2 and 3.

3.0 WELL CONSTRUCTION SCOPE AND METHODOLOGY

A total of seven observation wells and one test supply well were constructed within the Acme Improvement District Section 25 between July 28 and September 18, 1980.

The first three wells drilled were TW 13, TW 14 and TW 15, as part of Test Well Program - Section 25. They were drilled on July 28th, 30th and 31st, respectively.

On August 15, 1980, construction of Test Supply Well No. 18 was commenced and finished on September 10, 1980. Upon completion, one shallow and three deep observation wells were drilled. They were 18-1S, 18-1D, 18-2D and 18-3D (also designated as 1S, 1D, 2D and 3D). Locations of the observation wells and Test Supply Well No. 18 (PW #18) are shown in Figures 2 and 3. Refer to Table 1 and Figure 4 for a summary of well construction specifications.

All wells were constructed using the mud rotary drilling method. During construction of each well, cutting samples were collected at five feet intervals and described according to lithology. These descriptions can be found in Appendix A.

3.1 Test Well and Observation Well Construction

A total of seven, 2 inch P.V.C. wells were constructed. A 7-7/8 inch hole was drilled to the designated well depth. Well construction consisted of 2 inch Schedule 40 P.V.C. casing from land surface to the designated casing depth.

Two inch Schedule 40, #40 slot P.V.C. screen was installed below the casing to the bottoms of the wells. Silica sand (0.75 mm) was installed as annular gravel pack between the casing and the formation from the base of the screens up to approximately ten feet above the screen. The remaining annulus was backfilled with native sediments. The wells were developed by pumping compressed air at a rate of 100 cfm through an air line until a sediment free sample was obtained. On completion of development, a 30 inch x 30 inch x 4 inch reinforced concrete pad was constructed around each well and finished with threaded caps.

3.2 Test Supply Well (PW #18) Construction

Construction began by drilling a 7-7/8 inch pilot hole to act as a guide for the larger 24 inch bit and also to provide information as to the optimum depth for setting the casing in the formation. The hole was then reamed out to a diameter of 24 inches from the surface down to 71 feet followed by the installation of 18 inch diameter steel casing. The annulus was grouted with cement to 71 feet. After the cement had hardened, a nominal 18 inch diameter hole was drilled from the bottom of the steel casing to a depth of 90 feet. Due to the abundance of unconsolidated carbonate sand surrounding the limestone, 20 feet of 12 inch telescope size

#100 slot stainless steel well screen was installed from 70 to 90 feet and 12 inch Schedule 40 P.V.C. inner casing from 70 feet to the surface. The annular space from 90 feet up to the surface was gravel packed with 1/8 to 1/4 inch graded silica gravel. The well was then developed by air lifting with a 600 cfm compressor until the discharge was clear of sediment and mud. A 6 feet x 6 feet x 12 inch concrete pad was constructed around the well. A 4 inch gravel tube for addition of gravel to the annulus was welded onto the outer casing. The well was finished by capping and welding a steel plate between the outer and inner casing.

4.0 LITHOLOGY

Detailed lithologic descriptions are provided in Appendix A of the report. In general, the upper five feet are composed of silica sand. It is white, fine to very fine-grained, with a trace of shell and organics. From 5 to 15 feet, a lithified, intrasparite limestone is encountered. It is composed of a high percentage of medium to fine-grained silica sand with abundant shell fragments and varies from light grey to light brown. Underlying the limestone is a silica sand unit of about 45 to 55 feet thick. It is phosphatic, fine to very fine-grained, and varies from light brown to light grey. At about 60 to 65 feet, a well-lithified

limestone occurs as thin, discontinuous lenses interlayered with a silty grey carbonate sand. The limestone is a intrabiosparite which is grey to dark grey in color and contains silica sand, shell fragments and phosphate. The unit ranges in thickness from 40 to 55 feet. A silty grey carbonate clayey sand unit starts at 100 to 130 feet below the surface. This unit was only fully penetrated in two wells (TW 13 and TW 8) and its thickness was 10 feet. This unit appears to act as a confining or semi-confining bed. Above this unit potable water exists, below the unit highly mineralized water under artesian pressure is encountered. A micritic limestone was encountered at 110 feet. It is light brown with abundant shell fragments, poorly lithified and contains some silty clay and highly mineralized water. This information supplements a previous report prepared by Gee and Jenson in defining the areas with water supply development potential (Gee and Jenson, October 1979, Summary Report for Acme Improvement District, Test Well Program).

5.0 AQUIFER TEST

5.1 General Description

An aquifer test was conducted for Acme Improvement District to determine aquifer parameters necessary for the planning

and management of the water resources of the area. The test was started on September 24, 1980. It involved pumping one well at a constant rate of 900 gpm for a duration of 72 hours and observing resulting drawdowns and changes in water levels in nearby observation wells and canals. The site of the aquifer test was in the southwest corner of Section 25 as shown in Figure 1. Figure 3 shows the configuration of the wells and instrumentation used, and Figure 5 the distances between wells. The pumping well (PW #18) was 12 inches in diameter and screened from 70 to 90 feet. Four 2 inch diameter wells were installed as observation wells of which three were deep (18-1D, 182D, 18-3D) and one shallow (18-1S). Methods of well construction are described in Section 3.0 and generally depicted in Figure 5. Staff gages were installed in nearby canals (SG-1, SG-2, SG-3) to measure stages (Figure 3). A temporary rain gage was installed at the site to measure any rainfall. Water was discharged from the site into a canal flowing away from the site about 450 feet from the pumped well. The data from the test was analyzed using analytical techniques to obtain aquifer parameters. The conjunctive use of drilling data and analytical solutions of the test results were used to determine the values of these aguifer parameters and to interpret the results. The Boulton Method for aquifer analysis has been utilized and included in this report as the methods of

analysis to determine the coefficients of transmissivity and storage. After trying several methods of analysis and comparing the underlying assumptions associated with each method with field conditions, the Boulton Method was found to be the most representative. The coefficients of transmissivity and storage are essential in determining the characteristics of the aquifer in this region.

Transmissivity (T) is defined as the rate of flow of water at prevailing water temperature, in gallons per day per foot through a vertical strip of aquifer one foot wide extending the full saturated thickness of the aquifer under a hydraulic gradient of 100 percent. A hydraulic gradient of 100 percent means a one foot drop of water level in one foot of flow distance.

The coefficient of storage (S) of an aquifer is the volume of water released from storage per unit of surface area of the aquifer, per unit change in head. In water table aquifers, the storage coefficient is the same as the specific yield of the material dewatered during pumping. In confined aquifers it is the result of compression of the aquifer and expansion of the contained water when the head (pressure) is reduced during pumping.

5.2 Method of Data Analysis

The Boulton Delayed Yield method has been utilized and included in this report as the primary method of analysis since the subsurface conditions most closely resemble the basic assumptions.

Boulton Method of Analysis

Boulton (1963) produced a semi-empirical solution that reproduces all three segments of the time-drawdown curve in an unconfined aquifer. During the first segment, covering a short period of pumping, an unconfined aquifer reacts in the same manner as a confined aquifer. Water is released instantaneously from storage by the compaction of the aquifer and by the expansion of water. This portion of the curve is identical to the Theis-type curve. During the second segment, the effects of gravity drainage are felt. The slope of the time-drawdown curve decreases relative to the Theis curve due to dewatering of the falling water table which is greater than that which would be delivered by an equal decline in a confined potentiometric surface. The third segment occurring at later times once again conforms to the Theis-type curve.

Boulton's solution required the definition of an empirical "delay index" that is related to the vertical components of flow that are induced in the flow system and is a function of radius and time.

The following assumptions apply when using the Boulton Method:

- aquifer has seemingly infinite areal extent
- the aquifer is homogenous, isotropic, and of uniform thickness over the area influenced by the pumping test.
- prior to pumping, the phreatic surface is horizontal over the area influenced by the pumping test.
- the discharge rate is constant from the pumped well.
- the pumped well penetrates the entire thickness of the aquifer and receives water by horizontal flow.
- the aquifer is unconfined but showing delayed yield phenomena or the aquifer is semi-unconfined.
- the flow to the well is in an unsteady state.
- the diameter of the well is small, ie. the storage in the well can be neglected.

To calculate the aquifer parameters, drawdown is plotted against time on double logarithmic graph paper. By curve matching the Boulton Delayed Yield Type Curves, match points are determined allowing the following equations to be used to calculate the transmissivity and storage coefficient for early time and late time data:

$$T = \frac{114.6Q}{s} \quad \text{W(u}_{AY}, r/B) \qquad \text{and S} = \frac{Tt}{2693r^2} \quad u_{AY}$$

where:

T = transmissivity (gpd/ft)

S = storage coefficient (dimensionless)

Q = discharge from pumping well (qpm)

r = distance of observation wells from pumped well (ft)

s = drawdown in the observation well (ft)

t = time since pumping started (min)

W(u, r/B) = "well function of Boulton"

subscript A = early time

subscript Y = late time

This method permits analysis for semi-unconfined and unconfined aquifers with delayed yield from storage. It was found that the results generated by the Boulton Method is most representative of actual subsurface conditions and is therefore the method included in this report.

5.3 Results

Observed water levels in the observation wells were collected, reduced and plotted on double logarithmic drawdown vs. time plots for matching the Boulton type curves (Figures 6, 7, and 8). All raw field data has been included in Appendix B. Transmissivity and storage coefficient determinations were made for each of the deep observation wells. Table 2 summarizes the results. Early time results show confined and semiconfined storage coefficient values with an average value of 5.4×10^{-2} due to incomplete dewatering. During this early period of pumping, water is released instantaneously from storage by the compaction of the water and the curve conforms to the Theis curve. During the second segment, the effects of gravity drainage are felt and the slope of the curve decreases relative to the Theis curve due to dewatering of the falling water table. The third segment occurring at later times, once again conforms to the Theis curve. Late time data gave average storage coefficient values of 0.23 which is as expected for an unconfined system. The average transmissivity value for all analyses is about 46,000 gpd/ft. It must be recognized that a considerable range may exist, between 34,000 gpd/ft and 50,000 gpd/ft depending on specific conditions and the method of analysis utilized.

Drawdowns can be calculated based upon the calculated values of $T=46,000~\rm{gpd/ft}$ and S=0.23. These drawdowns were found to be a poor match with the actual drawdowns measured in the field. The lithology in the area indicated water table conditions (refer to Section 4.0 and Appendix A for descriptions). In designing well field systems, conservative values for the aquifer parameters are generally chosen. In this case $T=34,000~\rm{gpd/ft}$ and S=0.1 were found to give reasonably close approximations to field data after three days of pumping. Table 3 shows a comparison of the calculated vs. field drawdowns.

Carrying the analysis further, drawdowns for various intervals of time were calculated. The intervals used were 1 day, 3 days and 30 days, assuming continuous pumping at 900 gpm and no recharge to the system. This extrapolated data is used in a later section to design the wellfield and determine impacts. The drawdown vs. distance data is then plotted in Figure 9 giving a graphical representation of the cone of influence at 900 gpm. In Table 3 it should be noted that although the calculated data after three days of pumping closely resembles the field drawdown data, the system appears to have reached near equilibrium after one day of pumping according to the field data. This is further indication that the projected drawdowns are very conservative and represent worst case conditions for design purposes.

6.0 WATER QUALITY

Four test wells (Test Wells 8, 13, 14 and 15) had been drilled in Section 25 prior to construction of Test Supply Well No. 18. Each of these wells showed potable water extending to a depth of approximately 120 feet. Below 120 feet, these test wells produced highly mineralized water under artesian pressure. A low permeability clayey sand (at 100 to 120 feet below 1sd appears to act as a confining or semi-confining bed, maintaining this highly mineralized water below it. To avoid vertical migration of this saline water, each of these wells were plugged with grout to 100 feet. Conductivities of 500 to 700 umhos/cm was produced from each of these wells after plugging.

PW 18 was constructed with screen from 70 to 90 feet. Water quality samples were collected from the discharge during the 72 hour aquifer performance test and analyzed for standard potable mineral concentrations (Appendix C). One sample was taken one hour after pumping began at a rate of 900 gpm.

The second sample was taken after 72 hours of pumping, just prior to cessation of the test. These water quality analyses showed no significant change in water quality during the Vertical migration of the highly mineralized water test. below 120 feet of depth was not evident in the production well. Wells in Section 25 can be expected to produce hard water (in the 300 mg/l range) with high concentrations of dissolved solids (500 mg/l range), excessive potable color (30 to 40 NTU's), and fluoride (0.21 mg/l). Concentrations of chloride, sulfate and nitrate are low (60 mg/l, 6 mg/l, <0.1 mg/l, respectively). The chloride concentrations are in the same range as the test wells constructed along Lake Worth Road as presented in Gee and Jenson's report "Summary Report for Acme Improvement District Test Well Program", October 1979. Groundwater of potable quality is present in Section 25. Thickness of potable water ranges from a low of 100 feet in the northwest corner (TW 15) to 120 feet along the south border (TW 13 and TW 14), and to a high of 130feet in the northeast corner (TW 8).

7.0 WATER SUPPLY DEVELOPMENT POTENTIAL FOR SECTION 25

Development of water supply from the aquifer underlying Section 25 involves determining impacts that the proposed system will have on the water resources and users in the area.

7.1 Projected Cone of Depression

The cone of depression around a pumping well is dependent upon the transmissivity, storage coefficient and pumping rate. Given these variables, the shape and extent of the cone of depression may be predicted. Maintaining T = 34,000qpd/ft and S = 0.1, and varying the pumping rate, the drawdown with distance from the pumped well is determined. The drawdown versus distance graph for selected pumping rates after 30 days of continuous pumping is shown in Figure The distance of the one foot drawdown contour from the 10. pumping well at varying pumping rates may be determined from the graphs. For example, at a pumping rate of 750 gpm, the one foot drawdown contour would extend a distance of about 1,600 feet from the pumping well after 30 days of continuous pumping and no recharge. See Figure 11 for a schematic representation of the cones of influence. It is felt that the calculated cones of influence are a sufficiently conservative estimate for wellfield design and planning.

7.2 Wellfield Design

The geology, hydrology and water quality of the aquifer indicate that Section 25 of Acme Improvement District has

the capability to support a total of ten supply wells, each with a pumping capacity of about 750 gpm. These locations have been established in Section 25 as indicated in the tentative wellfield configuration shown in Figure 12. A well spacing of at least 1,600 feet should be maintained between wells at the suggested pumping rate of 750 gpm. The exact location and capacity of each well will be subject to site-specific variations in the lithology and hydrology of each location. This is determined during supply well construction and specific capacity testing at each site. It should be noted that a wellfield operating program should be developed as stated in the recommendations.

8.0 RECOMMENDATIONS

1. A network of ten supply wells should be constructed in Section 25 of the Acme Improvement District generally in the locations specified. These wells should be spaced approximately 1,600 feet apart. Recommended withdrawal rates are 750 gpm per well which will be dependent upon site specific variations in lithology and hydrology. It is recommended that implementation of well construction be phased starting with the southern wells first.

- 2. A wellfield operating and management program for these wells is required to minimize withdrawal impacts and retain the integrity of the well construction. The recommended operating program is:
 - a. Pump only five wells at a time using alternately spaced wells.
 - b. Duration of pumping each bank of wells should not exceed 24 hours.
- 3. A specific capacity test should be performed on each supply well on completion of construction.
- 4. A monitoring program should be instituted in Section 25 to determine the sustained yield. The data generated from the monitoring may indicate the potential for increased withdrawals from Section 25 or may indicate a reduction in withdrawals. The monitoring should include recording rainfall, groundwater levels in observation wells, pumping water levels in supply wells, well withdrawals and canal stage.

5. Additional potable water supply of comparable quantity and quality can be anticipated to the south of Section 25 and to the east of SR 7 as stated in Gee and Jenson's Test Well Summary Report, 1979.

TABLES

TABLE 1
WELL CONSTRUCTION DATA

| Well No. | Diamete (in.) | Cased er Depth (ft.) | n Interval | Total Depth (ft.) | Date Drilled |
|----------|----------------------|----------------------------|------------|-------------------------|-----------------|
| TW 13 | 2 | 60 | 60-130 | 100* | 7-28-80 |
| TW 14 | 2 | 60 | 60-130 | 100* | 7-30-80 |
| TW 15 | 2 | 55 | 55-130 | 100* | 7-31-80 |
| 18-1S | 2 | 10 | 10-60 | 60 | 9-12-80 |
| 18-1D | 2 | 70 | 70-90 | 90 | 9-11-80 |
| 18-2D | 2 | 70 | 70-90 | 90 | 9-15-80 |
| 18-3D | . 2 | 70 | 70-90 | 90 | 9-16-80 |
| PW-18 | outer 18 inner 12 | outer 71 inner 70 | 70-90 | 90 | 9-10-80 |

^{*} grouted up to 100 feet

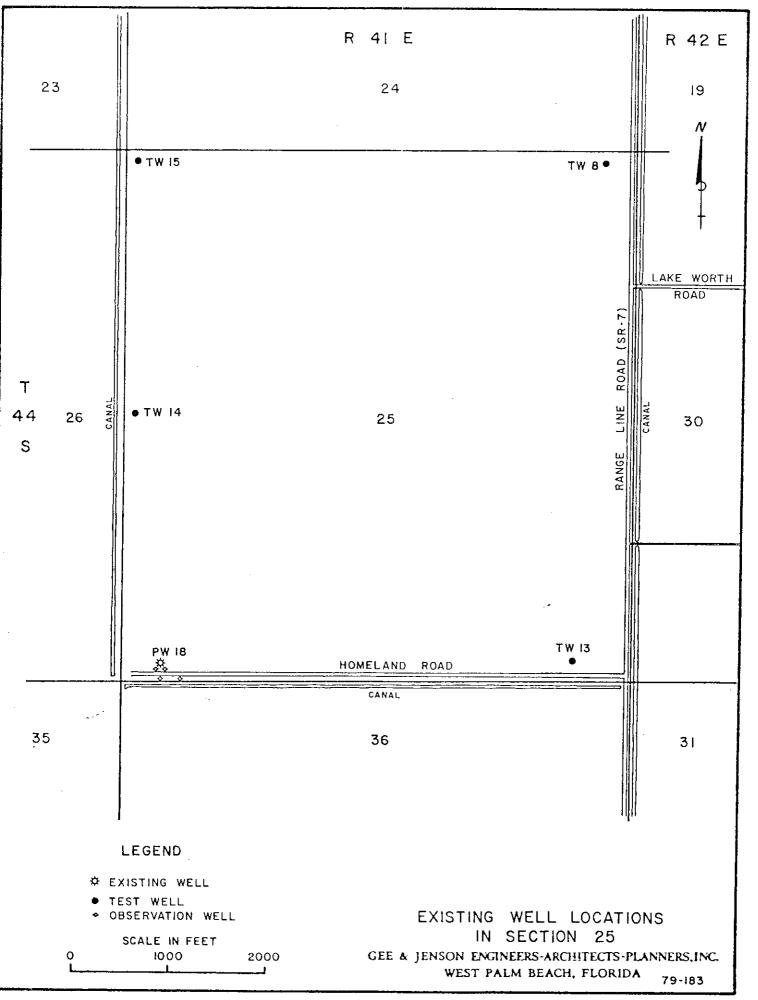
TABLE 2
SUMMARY OF AQUIFER PARAMETERS

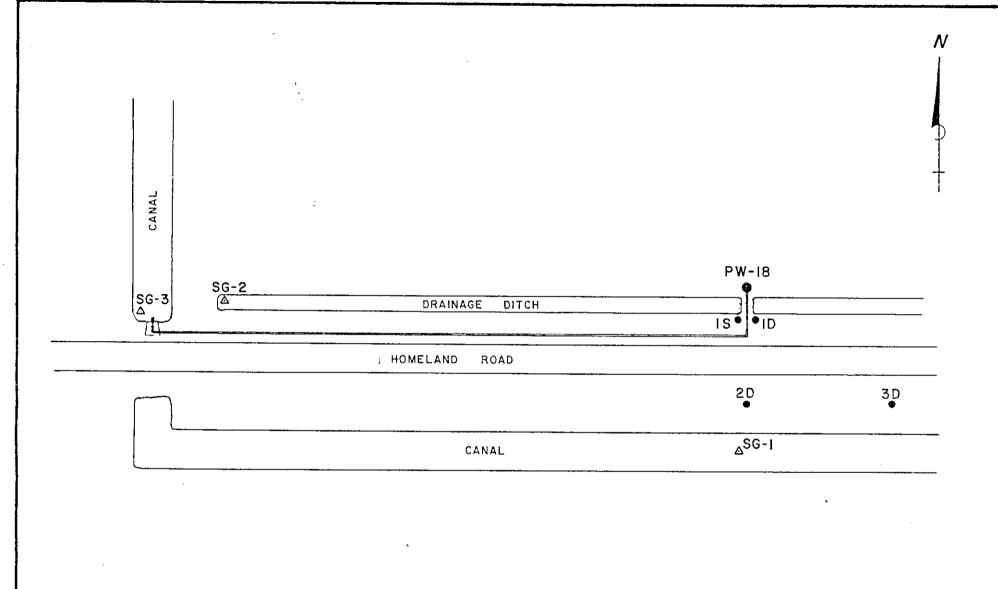
Boulton Method of Analysis

| | Early T | ime |
|----------|----------------------------|------------------------|
| Well No. | Transmissivity (gpd/ft) | Storage Coefficient |
| 18-1D | 33,816 | 1.6×10^{-2} |
| 18-2D | 49,114 | 2.5×10^{-4} |
| 18-3D | 49,114 | 1.1×10^{-5} |
| Average | 44,015 | 5.4×10^{-3} |

| | Late Time | | |
|----------|----------------------------|------------------------|--|
| Well No. | Transmissivity (gpd/ft) | Storage Coefficient | |
| 18-1D | * | * | |
| 18-2D | 46,881 | 0.26 | |
| 18-3D | 49,114 | 0.21 | |
| Average | 47,998 | 0.23 | |

Average transmissivity (Early Time and Late Time) = 46,000 gpd/ft *Late Time could not be calculated





LEGEND

● DISCHARGING WELL

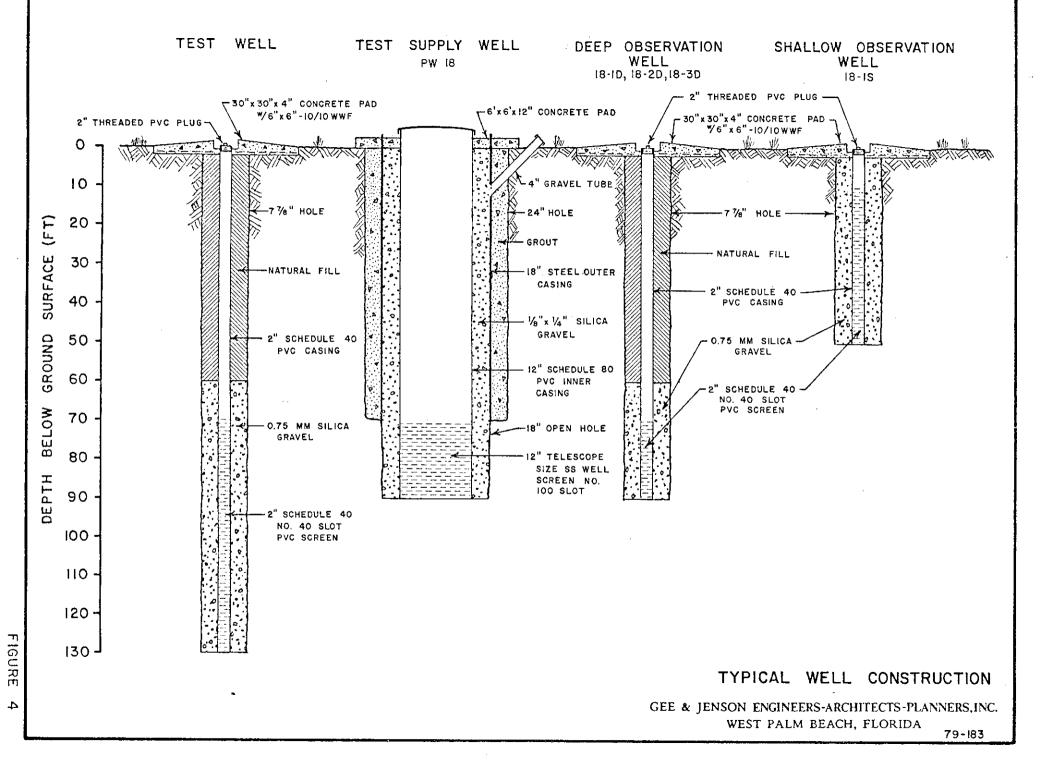
OBSERVATION WELL
(D=DEEP, S=SHALLOW)

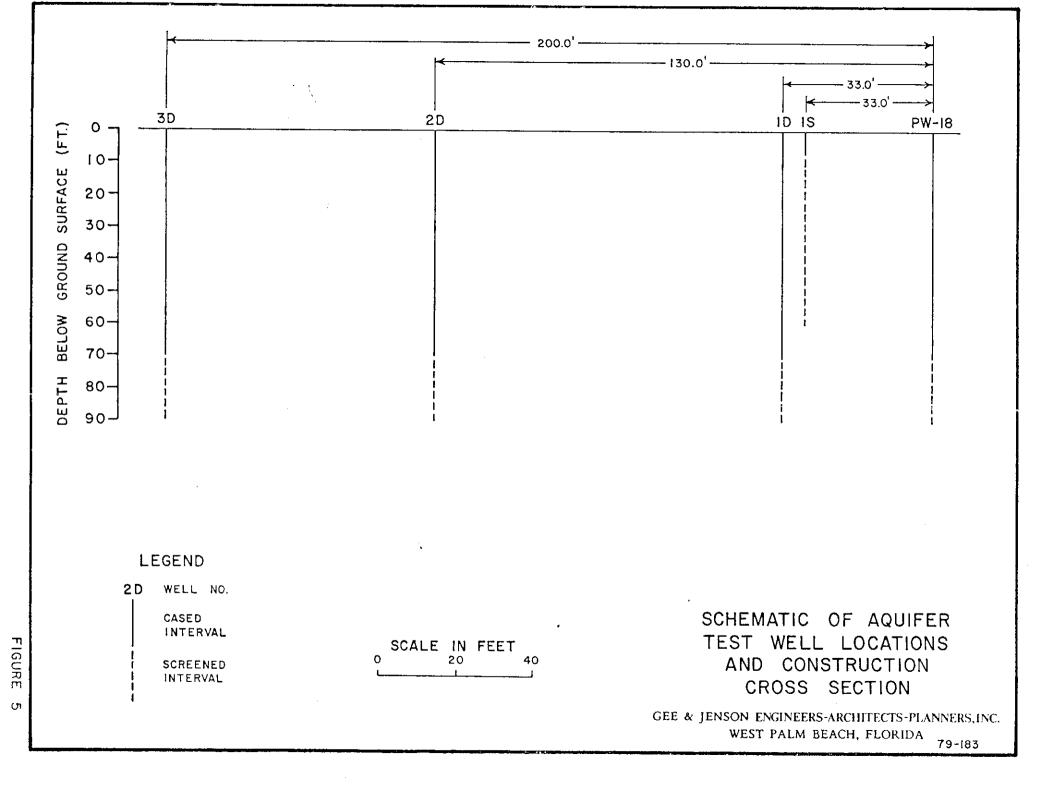
SCALE IN FEET
O 100 200

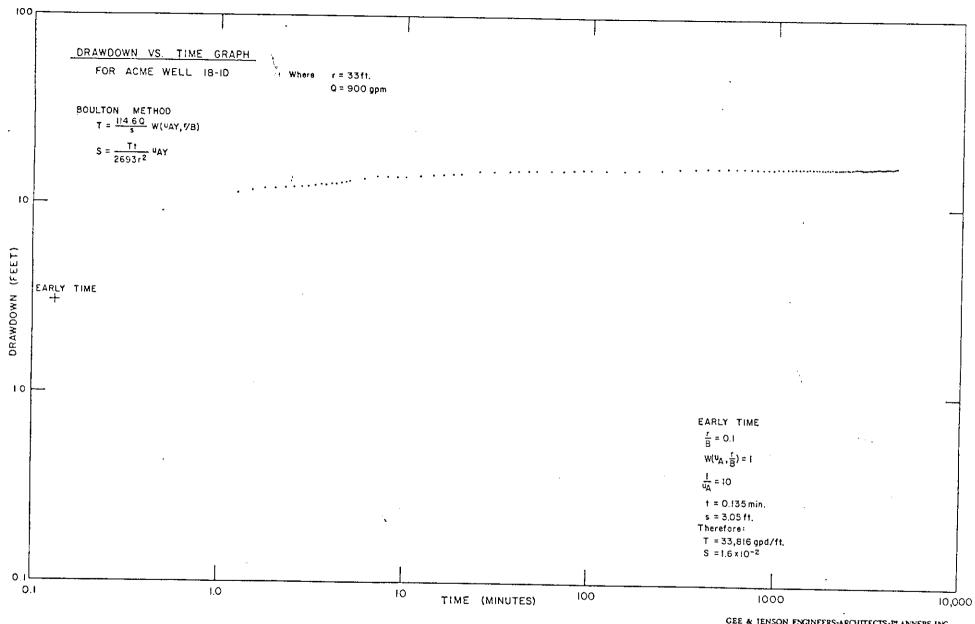
AQUIFER TEST INSTRUMENTATION
LAYOUT - PLAN VIEW

GEE & JENSON ENGINEERS-ARCHITECTS-PLANNERS,INC.
WEST PALM BEACH, FLORIDA
79-183

FIGURE

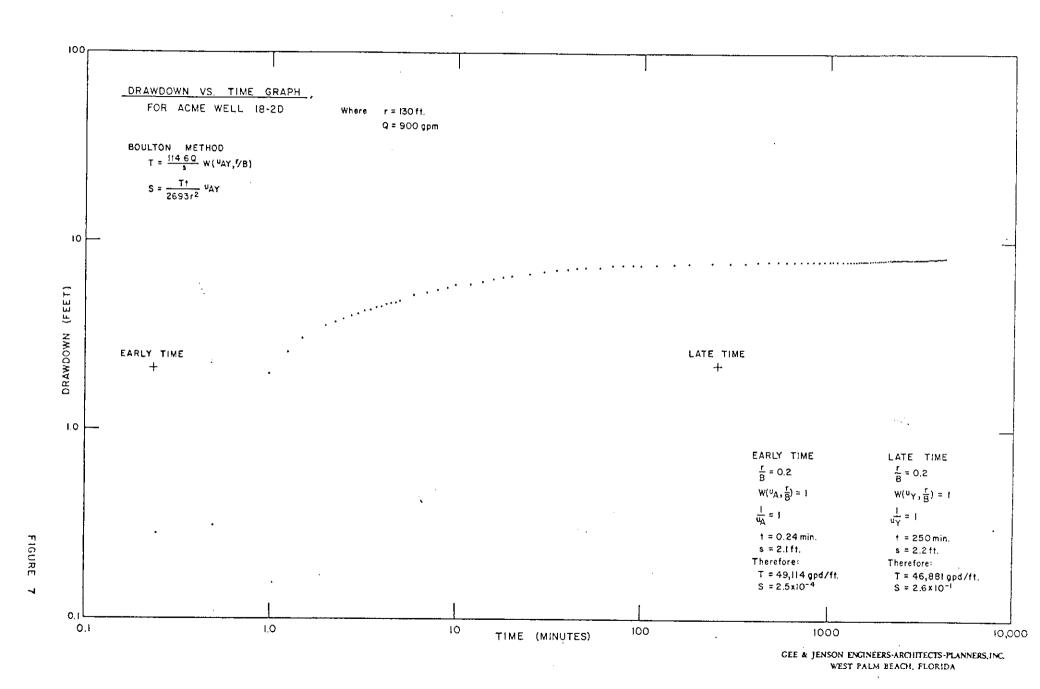


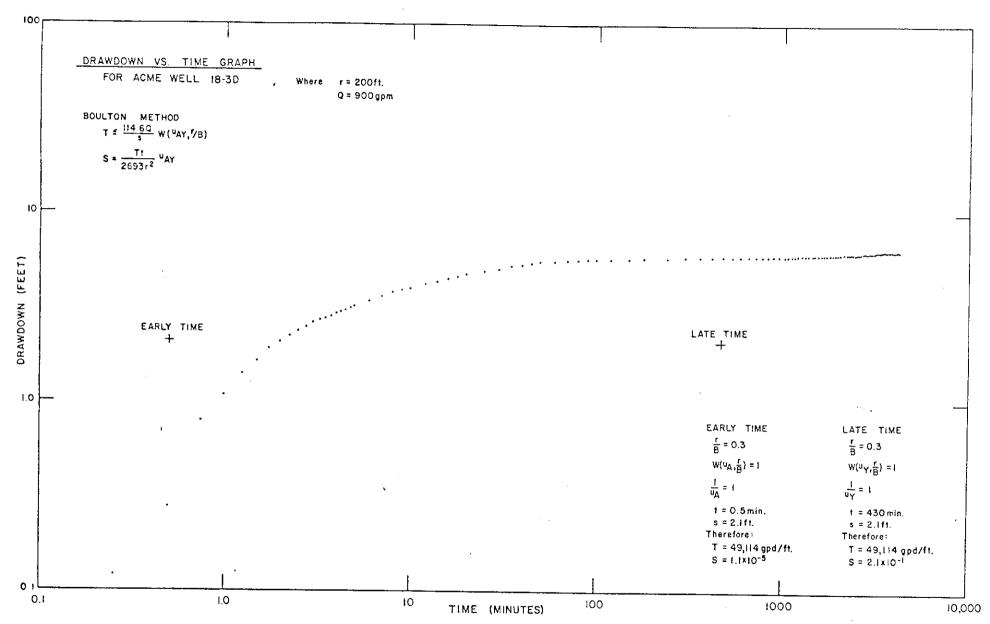




FIGURE

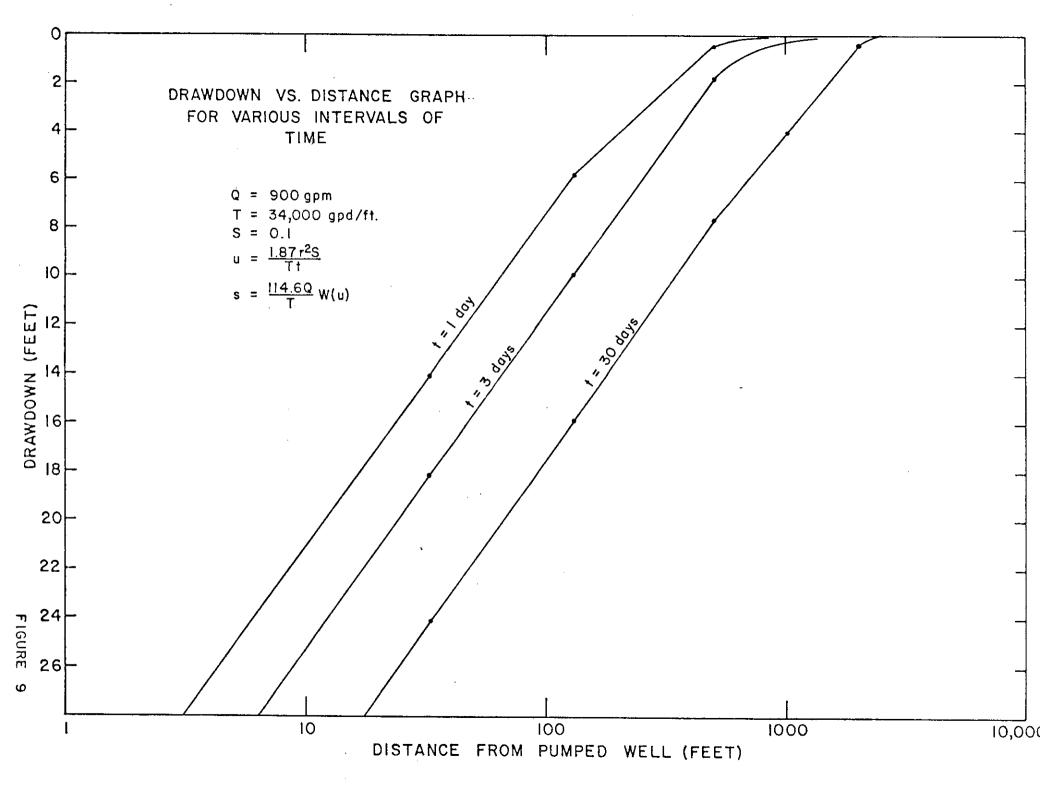
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WEST PALM BEACH, FLORIDA

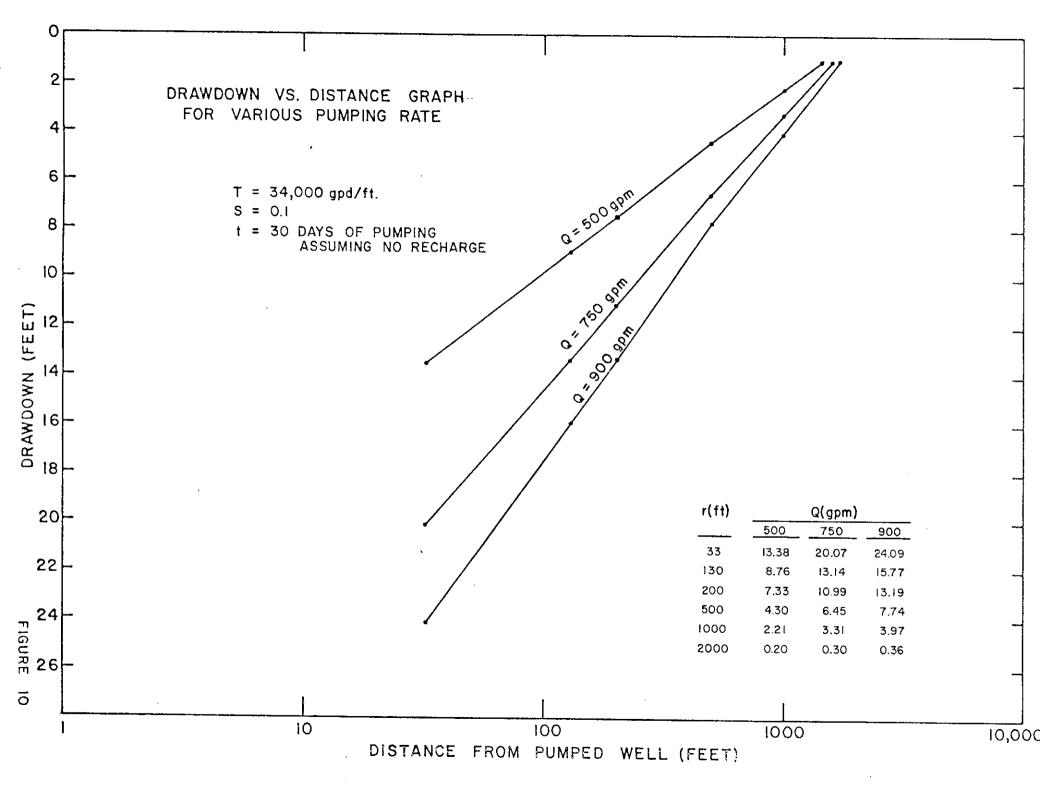


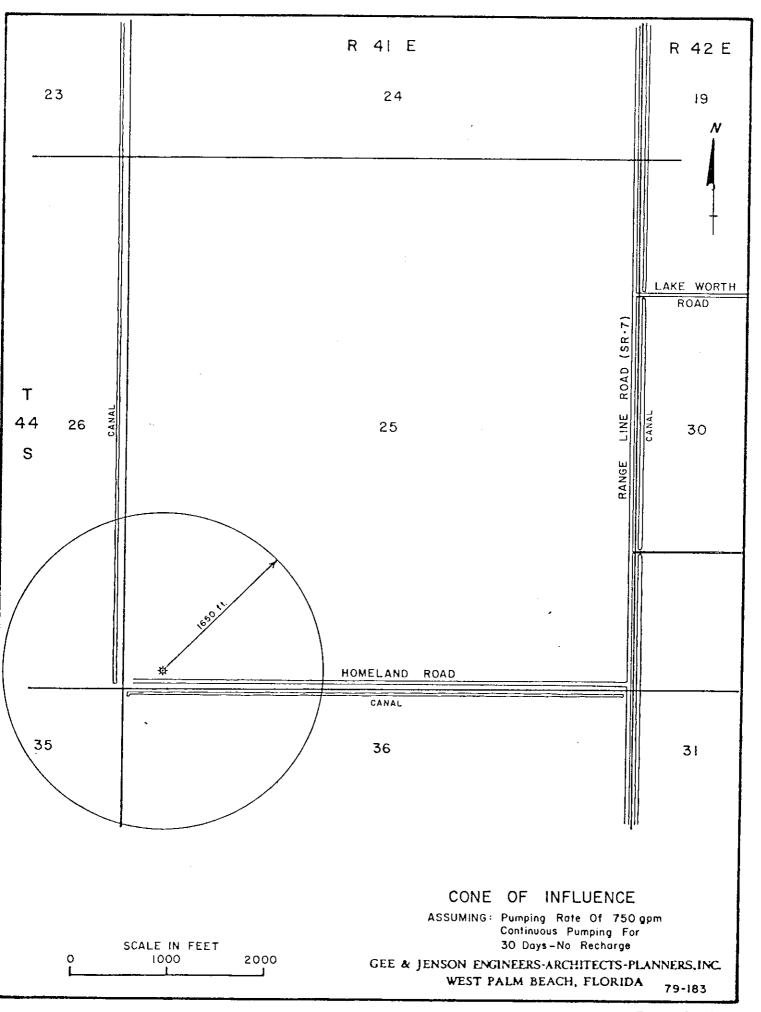


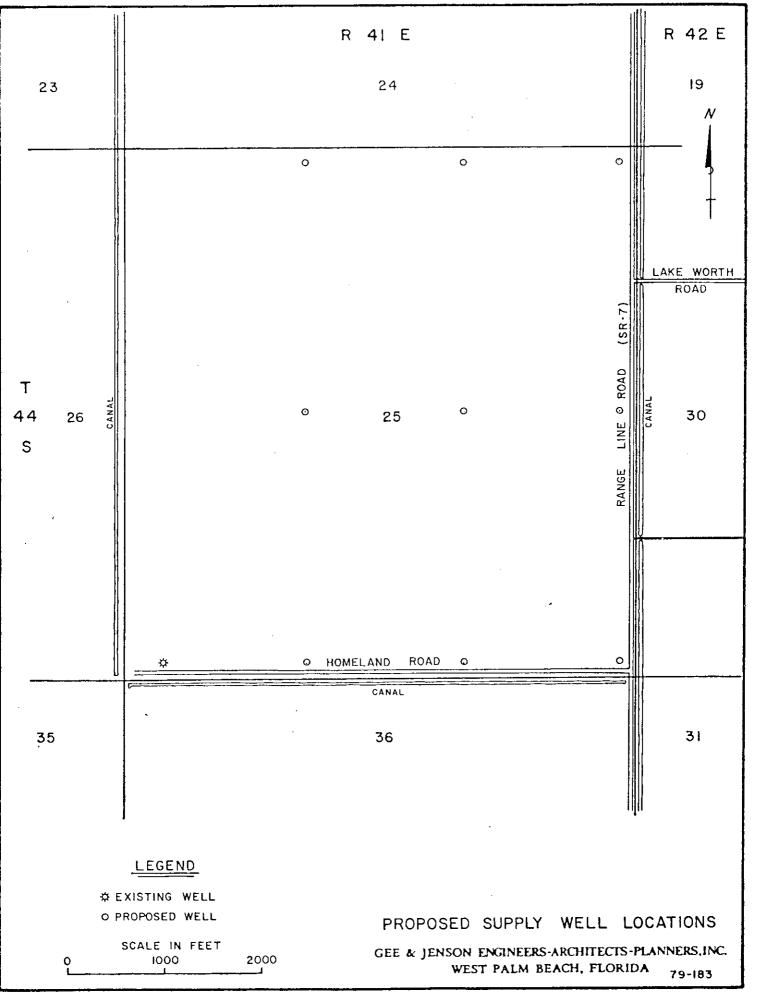
FIGURE

GEE & JENSON ENGINEERS-ARCHITECTS-PLANNERS, INC.
WEST PALM BEACH, FLORIDA









APPENDIX A

WELL CONSTRUCTION

| Well No. PW 18 (Test Supply Well #18) | Location: Acme Improvement Distric |
|---|------------------------------------|
| Driller: Alsay-Pippin | Recorded by: GR |
| Samples: Cuttings X , Core | Date Drilled: August 15, 1980 |
| Casing: Depth 70 feet | Screen: Depth 70-90 feet |
| Outer - 18 inches Diameter Inner - 12 inches | Diameter 12 inches |
| Outer - Steel Material Inner - Schedule 80 | PVC Material Telescope Size |
| | SS #100 S1ot |

| | 55, #IUU SIOL |
|---------------------------------|---|
| DEPTH BELOW LAND SURFACE (FEET) | LITHOLOGY DESCRIPTION |
| 0-5 | Sand-silica, white, very fine to silt sized grains, trace of organics, unconsolidated. |
| 5-10 | Limestone-intrasparite, light gray, cemented fine grained silica sand with pelecypod fragments, abundant, consolidated. |
| 10-15 | Limestone-same as above but increase in unconsolidated sand fraction and calcite crystals. |
| 15-20 | Sand-silica light brown very fine grained, abundant white pelecypod shellds, 15% intraspartie limestone. |
| 20-25 | Same as above. |
| 25-60 | Sand-silica, light brown, fine to silt sized grains, trace of white shell fragments, unconsolidated. |
| 60-62 | Sand-silica, and intramicritic limestone, white, consolidated and unconsolidated layers. |
| 62-66 | Limestone-intrabiosparite, gray, phosphatic, trace of shell fragments, well lithified. |
| 66-68 | Limestone-intrabiosparite, gray, mixed with a intra- micrite, much softer, poorly lithified. |
| 68-85 | Limestone-intrabiosparite, gray, phosphatic, hard, trace of shell fragments, trace of dolomitic lime-stone, increase in hardness at 80 feet, well lithified. |
| 85-90 | Limestone and shell-intrabiosparite, gray with shell lenses, shell is composed of pelecypods and gastropods, trace of medium grained silica sand, limestone is lithified and shell if poorly consolidated. |

WELL CONSTRUCTION

| Well No. | Observation Well 18-1D | Location: Acme Improvement District |
|----------|--------------------------|-------------------------------------|
| Driller: | Alsay-Pippin | Recorded by: GR |
| | Cuttings X , Core | Date Drilled: September 15, 1980 |
| | Depth 70 feet | Screen: Depth 70-90 feet |
| _ | Diameter 2 inches | Diameter 2 inches |
| | Material Schedule 40 PVC | Material Schedule 40 PVC,#40 |

| - Material | Schedule 40 PVC Material Schedule 40 PVC,#4 |
|---------------------------------|---|
| DEPTH BELOW LAND SURFACE (FEET) | LITHOLOGY DESCRIPTION |
| 0-2 | Sand-silica, light brown, fine grained, trace of very fine grained shell fragments, unconsolidated. |
| 2-10 | Limestone-intrabiomicrite, grayish brown, fine grained silica sand and micritic cement matrix surrounding abundant pelecypods and gastropods, poorly lithified. |
| 10-20 | Sand-silica, brown, fine to very fine grained, subangular, unconsolidated, 70%. |
| | Shell-white pelecypods and gastropods, large to small, whole and fragmented, 30%. |
| 20-35 | Sand-silica, light brown, fine to very fine grained, subangular, abundant pelecypod fragments, uncon-solidated. |
| 35-60 | Sand-silica, very light brown, fine to very fine grained, subangular to subrounded, trace of white shell fragments, unconsolidated. |
| 60-65 | Sand-silica, very light gray brown, fine to very fine grained, subangular to subrounded, trace of black fine grained phosphate particles, unconsolidated. |
| 65–70 | Limestone-intrabiosparite, dark gray, pelecypod fragments incorporated in limestone, very fine grained phosphate particles present in silica sand matrix, lithified. |
| 70-85 | Limestone-intrabiosparite, same as above but minor large (less than 1 mm) calcite crystals present. |
| 85-90 | Limestone-intrabiosparite, light gray, same as 65-70 but surrounded by a matrix of pelecypod and gastropod fragments and carbonate sand, the limestone occurs as individual concretionary bodies, limestone is lithified but the sand and shell matrix is consolidated. |

WELL CONSTRUCTION

| Well No. Observation 18-2D | Location: Acme Improvement District |
|----------------------------|-------------------------------------|
| Driller: Alsay-Pippin | Recorded by: GR |
| Samples: Cuttings x , Core | Date Drilled: September 15, 1980 |
| Casing: Depth 70 feet | Screen: Depth 70-90 feet |
| Diameter 2 inches | Diameter 2 inches |
| Material Schedule 40 | Material Schedule 40, PVC #40 Slot |
| | |

| DEPTH BELOW LAND SURFACE (FEET) | LITHOLOGY DESCRIPTION |
|---------------------------------|--|
| 0-15 | Shell-white, gastropods and pelecypods, whole fragmental, poorly consolidated, 80%. |
| | Sand-silica, light brown, fine grained, 10%. |
| | Limestone-intrabiosparite, light gray to gray, composed of medium to fine grained silica sand and shell fragments, lithified, 10%. |
| 15-45 | Sand-silica, light brown, fine to very fine grained, trace of fine fragmented white shell fragments, unconsolidated. |
| 45-62 | Sand-silica, brownish white, fine grained to silt sized grains, trace of black fine grained phosphate particles, unconsolidated. |
| 62-80 | Limestone-intrabiosparite, dark gray, composed of fine grained silica sand and white shell fragments, lithified concretions, 60%. |
| | Sand-silica and carbonate, very fine to fine grained, abundant, very fine grained, black phosphate particles, unconsolidated, 40%. |
| 80-90 | Limestone-intrabiosparite, dark gray, composed of fine grained silica sand and white shell fragments with a sparry calcite cement, lithified, 70%. |
| | Sand and Shell-fine grained silica and carbonate sand, and light brown pelecypod fragments, unconsolidated, 30%. |

| Driller: Samples: | Cuttings X Depth 70 fe Diameter 2 i | , Coreeet | Location Acme Improvement District Recorded by: GR Date Drilled: September 16, 198 Screen: Depth 70-90 feet Diameter 2 inches Material Schedule 40 PVC, | | | |
|--------------------------------|---------------------------------------|--|---|--|--|--|
| | Material Sch | ledule 40 PVC | material stream 40 1.0; | | | |
| DEPTH BE LAND SUF (FEET) | RFACE | LITHOLOGY DESCR | IPTION | | | |
| 0-15 | | and fragmental, | tropods and pelecypods, whole poorly consolidated, 80% the brown, fine grained, 10%. | | | |
| | | Limestone - intra | biosparite, light gray to gray, um to fine grained silica and lithified, 10%. | | | |
| 15-45 | | Sand-silica, lig trace of fine fr unconsolidated. | tht brown, fine to very fine grained, agmented white shell fragments, | | | |
| 45–62 | | Sand-silica, bro sized grains, tr particles, uncon | wnish white, fine grained to silt cace of black fine grained phosphate asolidated. | | | |
| 62-80 | | Limestone-intrab fine grained sil lithified concre | piosparite, dark gray, composed of ica sand and white shell fragments, etions, 60%. | | | |
| | | Sand-silica and abundant very fi unconsolidated 4 | carbonate, very fine to fine grained ne grained black phosphate particles, | | | |
| 80-90 | · | fine grained sil | piosparite, dark gray, composed of lica sand and white shell fragments alcite cement, lithified 70%. | | | |
| | | Sand and Shell-fi sand and light b solidated 30%. | Fine grained silica and carbonate prown pelecypod fragments, uncon- | | | |

| Well No. | Test Well | #13 (TW-13) | Location: Acme Improvement District | | | |
|--|-----------|--|---|--|--|--|
| Driller: | Alsav-P | ippin | Recorded by: GR | | | |
| Samples: Cuttings Casing: Depth 130 f Diameter 2 | | Date Drilled: July 28, 1980 | | | | |
| Casing: | Depth 13 | 30 filled to 100 feet | Screen: Depth 60-130 feet | | | |
| • | Diameter_ | 2 inches | Diameter 2 inches | | | |
| | Material | Schedule 40 PVC | Material Schedule 40 PVC #40 | | | |
| | | | | | | |
| | FACE | LITHOLOGY DESCR | IPTION | | | |
| 0-20 | | white pelecypods | wn, fine grained, abundant and gastropods, some small nts, unconsolidated. | | | |
| 20-30 | | | ht brown, fine to medium grained, , trace of white shell fragments, | | | |
| 30-50 | | | y fine to fine grained, light white shell fragments, uncon- | | | |
| 50-62 | | brown, off white | y fine to fine grained, light shell fragments, unconsolidated, ne grained phosphate sand. | | | |
| 62-68 | | of micrite, dark | atic intrabiosparite with lenses gray to very light brown, some and trace of white shell fied. | | | |
| 68-79 | | gray abundant re | atic intrabiosparite, dark crystalization, abundant stropod fragments, well | | | |
| 79 –95 | | Limestone-same a | s above, but no gastropods and more | | | |
| 95–110 | | abundant recrystand gastropod from lens of micrite | atic intrabiosparite, dark gray, alization, abundant pelecypod agments, well lithified, with (3') at 100 feet and an increase tion of pelecypods. | | | |

| Well No. Tes | t Well 13 (TW-13) | Location: Acme Improvement District |
|--------------------------------------|---|--|
| Driller: | Alsay-Pippin | Recorded by: GR |
| Samples: Cu Casing: De | pth 130 filled to 100 feet ameter 2 inches terial Schedule 40 PVC | Date Drilled: July 28, 1980 Screen: Depth 60-130 feet Diameter 2-inches Material Schedule 40 PVC |
| DEPTH BELOW LAND SURFAC (FEET) | E LITHOLOGY DESCRI | |
| 110-120 | with micrite, abu | ray intrabiosparite interbedded undant shell and silty white clay, ts, coral polyps and Echinoderm |
| 120-130 | Silty clay, lime | mud, carbonate sand, grayish |

sparite and micrite.

white, trace of phosphate particles with some

| Well No. | Test Well #14 (TW-14) | Location: Acme Improvement District | | | | |
|----------|------------------------------|-------------------------------------|--|--|--|--|
| Driller: | Alsay-Pippin | Recorded by: GR | | | | |
| Samples: | Cuttings , Core | Date Drilled: July 30, 1980 | | | | |
| Casing: | Depth 130 filled to 100 feet | Screen: Depth 60-130 feet | | | | |
| • | Diameter 2 inches | Diameter 2 inches | | | | |
| | Material Schedule 40 PVC | Material Schedule 40 PVC #40 Slot | | | | |

| DEPTH BELOW LAND SURFACE | |
|--------------------------|---|
| (FEET) | LITHOLOGY DESCRIPTION |
| 0-26 | Sand-silica, shell, white, fine grained, abundant carbonate sand, 60 percent pelecypods, minor gastropods, fill from adjacent ditch, unconsolidated. |
| 26-40 | Sand-silica, brown, fine to very fine grained, minor fine grained shell fragments, unconsolidated. |
| 40-67 | Sand-silica, light brown, fine to very fine grained, minor fine grained shell fragments, unconsolidated. |
| 67–69 | Dolomitic limestone and limestone, brown and gray, some silica sand. |
| 69-75 | Limestone-intrabiosparite, gray, phosphatic grains, hardness increases, well lithified. |
| 7 5–80 | Limestone-same as above, but calcite crystals and calcite replacement in pelecypods is minor, also had an increase in fluid loss. |
| 80-85 | Limestone-same as above, but harder and fluid loss. |
| 85–90 | Limestone-same as above, but hit a 2 foot seam of micrite. |
| 90-109 | Limestone-same as above, but a little darker due to phosphate in a few spots. |
| 109-120 | Limestone-biosparite, shell fragments and Echinoderm fragments lithified with a sparite/calcite cement, white, density increases and much less fluid loss; abundant white silty clay and micrite. |
| 120-130 | Sand-silty, lime mud, shell fragments (mainly pele- cypods) minor phosphate and micrite and sparite, loosely consolidated, in places. |

| Well No. | Test Well #15 (TW-15) | Location: Acme Improvement District |
|----------|------------------------------|-------------------------------------|
| Driller: | Alsay-Pippin | Recorded by: GR |
| Samples: | Cuttings, Core | Date Drilled: July 31, 1980 |
| Casing: | Depth 130 filled to 100 feet | Screen: Depth 60-130 feet |
| | Diameter 2 inches | Diameter 2 inches |
| | MaterialSchedule 40 PVC | Material Schedule 40 PVC #40 Slot |

| DEPTH BELOW LAND SURFACE (FEET) | LITHOLOGY DESCRIPTION |
|---------------------------------------|---|
| 0-14 | Sand-silica, dolomitic limestone and micrite and abundant shell, light brown, (fill from adjacent canal). |
| 14-50 | Sand-silica, light brown, fine to very fine grained, trace of fine to medium grained shell fragments, unconsolidated. |
| 50-56 | Sand-silica, light gray, fine to very fine grained, abundant fine grained phosphate, trace of shell fragments, unconsolidated. |
| 56-70 | Limestone-gray intrabiosparite, phosphatic, trace of micritic limestone, (bio), lithified. |
| 70-79 | Limestone-gray intrabiosparite, phosphatic, trace micritic limestone (bio), lithified; trace of silty white clay and micrite. |
| 80- | Shell-lense, gastropods, pelecypods and abundant clay. |
| 81-90 | Limestone: gray intrabiosparite, phosphatic, trace of micritic limestone lithified, with a trace of shell fragments. |
| 90-98 | Same as above with an increase in shell fragments, pelecypods and gastropods. |
| 98-100 | Sand-silica, carbonate sand, fine grained shell fragments, abundant phosphate, light gray, trace of silty clay, unconsolidated. |
| 100-107 | Sand-silica, some carbonate, fine grained shell fragments, abundant phosphate, light gray, trace of silty clay, unconsolidated. |
| 107-110 | Shell-white to light brown, pelecypod and gastropod fragments, poorly consolidated. |

| Well No. Test Well #15 (TW-15) | Location: Acme Improvement District |
|--------------------------------------|-------------------------------------|
| Driller: Alsay_Pippin | Recorded by: GR |
| Samples: Cuttings , Core | Date Drilled: July 31, 1980 |
| Casing: Depth 130 filled to 100 feet | Screen: Depth 60-130 feet |
| Diameter 2 inches | Diameter 2 inches |
| Material Schedule 40 PVC | Material Schedule 40 PVC #30 |

| DEPTH BELOW LAND SURFACE (FEET) | LITHOLOGY DESCRIPTION |
|---------------------------------|--|
| 110-120 | Limestone-biointramicrite, light brown, abundant pelecypods and gastropods, abundant silty clay, poorly lithified, trace of phosphate. |
| 120-132 | Limestone-intrabiomicrite, light gray, abundant phosphate and silty white clay, trace of pelecypods, poorly lithified. |

APPENDIX B

2019 OKEECHOBEE BOULEVARD, WEST PALM BEACH, FLORIDA. . . 33409. . . 305 - 683-3301

FRED A. GREENE, P.E.
RICHARD M. MILLER P.E.
WALTER O. STEPHERS, JR., P.E.
WILLIAM G. WALLACE, JR., P.L.S.
PHILIP A. CRANGELU JR., A.I.A.
JOHN C. WISE, P.E.

Director Emerities H. C. GEE, P.E. THEODORE B. JENSON, P.E.

RECORD OF WATER LEVELS

| Well | No. | PW-18 |
|------|-----|-------|
|------|-----|-------|

| Proj | ect | /9-183 A | .cme we | | | Locat | tion_Hom_ | neland koad | · · · · · · · · · · · · · · · · · · · | |
|------|--------|----------|---------------------------------------|-------------|--------------|--------|-----------|---------------------------|---------------------------------------|-----------------|
| Elev | ation | | | | MSL | Measu | iring Po | oint Top o | f Casing | ·· - |
| Dist | ance 1 | to Pump | ed Wel | 110 | | feet D | oischarg | je <u>90</u> 0 | | GPM |
| Tota | l Dept | _h90 | fe | eet C | ased De | epth |)-70 f | eet Dia | meter <u>12</u> | |
| Star | ting [| Date of | Test_ | 9/24 | /80 @ | 1000 | | · | , | |
| Time | | Wate | r Leve | 1 (ft) | Draw - | Mea- | Adjust | ments | Remarks | |
| | | Held | Wet | Below MP | Down (ft) | | | Back- ground Levels | | - |
| 7: | 50 | | | 4.20 | | | | | M-Scope | |
| | | | - | 4.23 | | | | | Tape | |
| 9: | 17 | | | 4.20 | | | - | | | |
| 9 : | 47 | | | 4.21 | | | | - | | |
| 9 : | 59 | | • | 4.21 | | KD | STATIC | | | |
| | . 25 | | · · · · · · · · · · · · · · · · · · · | | | | , | | | |
| | .50 | | | 30.46 | 26.25 | KD | | | | |
| | .75 | | | 36.20 | 31.99 | KD | | | | |
| | 1.00 | | | | | | | | | |
| | 1.25 | | | 37.20 | 32.99 | KD | | | | |
| | 1.50 | , | | 37.70 | 33.49 | KD | | | | |
| | 1.75 | | | 37.05 | 32.84 | KD | | | | |
| | 2.00 | | | 36.40 | 32.19 | KD | | | | |
| | 2.29 | | | 36.35 | 32.14 | KD | | | | |
| | 2.50 | | | 36.40 | 32.19 | KD | | | | |
| | 2.75 | | | | 00 07 | | | | | |

GEE & JESSON MANIER AROHITECOMERCIA

RECORD OF WATER LEVELS

Well No. PW-18

| mi | | Water | Level | (£t.) | Draw- | Mea- | Adjustma | ents | | |
|-----------|---------|-------|---------------|-------|-------|-------|----------|--------|--------------|--------------|
| rime (hr) | (min) | | Wet | Below | Down | sured | De- | Back- | ••• |] |
| ''' / | (10.21) | | · | MP | (ft) | by | water- | | | Remarks |
| | | | | | | | ing | Levels | | |
| | 3.00 | | | | | | į | | | |
| | 3.00 | | | | 22 27 | | | | | |
| | 3.25 | | | 36.58 | 32.37 | KD | | | | |
| | 3.50 | | | 36.66 | 32.45 | KD | | | | |
| | 3.75 | | | 36.72 | 32.51 | KD | | | | |
| | 4.00 | | | 36.84 | 32.63 | KD | | | | |
| | 4,25 | | | 36,86 | 32.65 | KD | | | | |
| | 4.50 | | | 36.92 | 32.71 | KD | | | ···· | |
| | 4.75 | | | 37.02 | 32.81 | KD | | | | |
| | 5 | | | 37.12 | 32.91 | KD | | | | |
| | 6 | | | 39.20 | 34.99 | KD | | | | |
| | 7 | | | 39.10 | 34.89 | KD | | | | · |
| | 8 | | | 38.54 | 34.33 | KD | | | | |
| | 9 | | | 38.33 | 34.12 | KD | | | | |
| | 10 | | | 38.44 | 34.23 | KD | | | | |
| | 12 | | | 38.68 | 34.51 | KD | | | | |
| | 14 | | | 38.94 | 34.73 | KD | | | | |
| | 16 | | | 39.08 | 34.87 | KD | | | | |
| | 18 | | · | 39.30 | 35.09 | KD | | | | |
| | 20 | | | 39.44 | 35.23 | KD | | | | |
| | 25 | | | 39.64 | 35.43 | KD | | | | |
| | 30 | | | 39.79 | 35.58 | KD | | | | |
| | 35 | | | 40.18 | 35.97 | KD | | | | , |

GEE & JENSON INGINERS ARCHITECTS PLANNERS INC

RECORD OF WATER LEVELS

Well No. PW-18

| Nr Nr Held Net Below Down Sured Dewater Ground Levels | · · · | | 1 | | (5) | 1 12 | 1 11000 | 3 2 2 2 2 2 2 2 | | | · · · · · · · · · · · · · · · · · · · |
|--|-------|------------|-------------|---------------|-------|----------------|---|-----------------|--------------|-------------|---------------------------------------|
| NP | ime | (p) = \ | | | | | ذ ا | | | | |
| A0 | nr) | (min) | nera | wer | | | 1 1 | | , , | | Remarks |
| 40 | ļ | |] | | 1.17 | 1+6/ | | | | | |
| 45 | | • | | | | | | | | | |
| 1 60 40.23 36.02 KD 1 60 40.46 36.25 KD 70 40.51 36.30 KD 80 40.59 36.38 KD 90 40.70 36.49 KD 100 40.64 36.43 KD 2 120 40.74 36.53 KD 150 - 40.87 36.66 KD 3 180 40.97 36.76 JE 5 300 41.14 36.93 JE 6 360 41.23 37.02 JE 7 420 41.46 37.25 JE 8 480 41.47 37.26 KD/JF 9 540 41.47 37.26 KD/JF 10 600 41.54 37.24 KD/JF 11 660 41.50 37.29 KD/JF 12 720 41.54 37.33 KD/JF | | 40 | | | 40.26 | 36.05 | KD | | | | |
| 1 60 40.23 36.02 KD 1 60 40.46 36.25 KD 70 40.51 36.30 KD 80 40.59 36.38 KD 90 40.70 36.49 KD 100 40.64 36.43 KD 2 120 40.74 36.53 KD 150 - 40.87 36.66 KD 3 180 40.97 36.76 JE 5 300 41.14 36.93 JE 6 360 41.23 37.02 JE 7 420 41.46 37.25 JE 8 480 41.47 37.26 KD/JF 9 540 41.47 37.26 KD/JF 10 600 41.54 37.24 KD/JF 11 660 41.50 37.29 KD/JF 12 720 41.54 37.33 KD/JF | 1 | <i>1</i> C | | | 10.00 | 24 25 | | | | | |
| 1 60 40.46 36.25 KD 70 40.51 36.30 KD 80 40.59 36.38 KD 90 40.70 36.49 KD 100 40.64 36.43 KD 2 120 40.74 36.53 KD 150 - 40.87 36.66 KD 3 180 40.97 36.76 JE 5 300 41.14 36.93 JE 6 360 41.23 37.02 JE 7 420 41.46 37.25 JE 8 480 41.47 37.26 KD/JF 9 540 41.47 37.26 KD/JF 10 600 41.50 37.29 KD/JF 11 660 41.50 37.29 KD/JF 12 720 41.54 37.33 KD/JF 13 780 41.66 37.35 KD/JF | | 45 | | | 40.26 | 36.05 | $\left\{\begin{array}{c} KD \\ \end{array}\right\}$ | | | | |
| 1 60 40.46 36.25 KD 70 40.51 36.30 KD 80 40.59 36.38 KD 90 40.70 36.49 KD 100 40.64 36.43 KD 2 120 40.74 36.53 KD 150 40.87 36.66 KD 3 180 40.87 36.66 JE 4 240 40.97 36.76 JE 5 300 41.14 36.93 JE 6 360 41.23 37.02 JE 7 420 41.46 37.25 JE 8 480 41.47 37.26 KD/JF 9 540 41.47 37.26 KD/JF 10 600 41.45 37.24 KD/JF 11 660 41.50 37.33 KD/JF 13 780 41.66 37.35 KD/JF | | 50 | | | 40.23 | 36,02 | KD | | İ | | |
| 70 | | | | | | | | | | | |
| 80 | 1 | 60 | | | 40.46 | 36.25 | KD | | | | |
| 80 | | 70 | | | 40 51 | 26 20 | l MD | İ | | | |
| 90 | | | | | 40.01 | <u> 30.</u> 30 | עא | | | | |
| 100 | | 80 | | | 40.59 | 36.38 | KD | | | | |
| 100 | | 0.0 | | | | | | | | | |
| 2 120 40.74 36.53 KD 150 - 40.87 36.66 KD 3 180 40.87 36.66 JE 4 240 40.97 36.76 JE 5 300 41.14 36.93 JE 6 360 41.23 37.02 JE 7 420 41.46 37.25 JE 8 480 41.47 37.26 KD/JF 9 540 41.47 37.26 KD/JF 10 600 41.45 37.24 KD/JF 11 660 41.50 37.29 KD/JF 12 720 41.54 37.33 KD/JF 13 780 41.66 37.35 KD/JF | | 90 | | | 40.70 | 36.49 | KD | | | | |
| 2 120 40.74 36.53 KD 150 - 40.87 36.66 KD 3 180 40.87 36.66 JE 4 240 40.97 36.76 JE 5 300 41.14 36.93 JE 6 360 41.23 37.02 JE 7 420 41.46 37.25 JE 8 480 41.47 37.26 KD/JF 9 540 41.47 37.26 KD/JF 10 600 41.45 37.24 KD/JF 11 660 41.50 37.29 KD/JF 12 720 41.54 37.33 KD/JF 13 780 41.66 37.35 KD/JF | | 100 | | | 40.64 | 36.43 | KD | ļ | | | |
| 150 | | | | - | | 30.73 | - KD | | | | |
| 150 | 2 | 120 | | | 40.74 | 36.53 | KD | | | | |
| 3 180 40.87 36.66 JE 4 240 40.97 36.76 JE 5 300 41.14 36.93 JE 6 360 41.23 37.02 JE 7 420 41.46 37.25 JE 8 480 41.47 37.26 KD/JF 9 540 41.47 37.26 KD/JF 10 600 41.45 37.24 KD/JF 11 660 41.50 37.29 KD/JF 12 720 41.54 37.33 KD/JF 13 780 41.66 37.35 KD/JF | | 150 | | _ | 40.07 | 26.66 | *** | | ļ | } | |
| 4 240 40.97 36.76 JE 5 300 41.14 36.93 JE 6 360 41.23 37.02 JE 7 420 41.46 37.25 JE 8 480 41.47 37.26 KD/JF 9 540 41.47 37.26 KD/JF 10 600 41.45 37.24 KD/JF 11 660 41.50 37.29 KD/JF 12 720 41.54 37.33 KD/JF 13 780 41.66 37.35 KD/JF | | 1.20 | | | 40.87 | 36.66 | KD | | | | |
| 4 240 40.97 36.76 JE 5 300 41.14 36.93 JE 6 360 41.23 37.02 JE 7 420 41.46 37.25 JE 8 480 41.47 37.26 KD/JF 9 540 41.47 37.26 KD/JF 10 600 41.45 37.24 KD/JF 11 660 41.50 37.29 KD/JF 12 720 41.54 37.33 KD/JF 13 780 41.66 37.35 KD/JF | 3 | 180 | | , | 40.87 | 36.66 | JE | | İ | | • |
| 5 300 41.14 36.93 JE 6 360 41.23 37.02 JE 7 420 41.46 37.25 JE 8 480 41.47 37.26 KD/JF 9 540 41.47 37.26 KD/JF 10 600 41.45 37.24 KD/JF 11 660 41.50 37.29 KD/JF 12 720 41.54 37.33 KD/JF 13 780 41.66 37.35 KD/JF | | | | | | | | | | | |
| 6 360 41.23 37.02 JE 7 420 41.46 37.25 JE 8 480 41.47 37.26 KD/JF 9 540 41.47 37.26 KD/JF LO 600 41.45 37.24 KD/JF L1 660 41.50 37.29 KD/JF L2 720 41.54 37.33 KD/JF L3 780 41.66 37.35 KD/JF | 4 | 240 | | | 40.97 | 36.76 | JE | | | | |
| 6 360 41.23 37.02 JE 7 420 41.46 37.25 JE 8 480 41.47 37.26 KD/JF 9 540 41.47 37.26 KD/JF LO 600 41.45 37.24 KD/JF L1 660 41.50 37.29 KD/JF L2 720 41.54 37.33 KD/JF L3 780 41.66 37.35 KD/JF | 5 | 300 | | | 41 14 | 36 03 | TE | [| | | |
| 7 420 41.46 37.25 JE 8 480 41.47 37.26 KD/JF 9 540 41.47 37.26 KD/JF LO 600 41.45 37.24 KD/JF L1 660 41.50 37.29 KD/JF L2 720 41.54 37.33 KD/JF L3 780 41.66 37.35 KD/JF | | | | | 71.14 | 30.93 | JE | | | | |
| 8 480 41.47 37.26 KD/JF 9 540 41.47 37.26 KD/JF L0 600 41.45 37.24 KD/JF L1 660 41.50 37.29 KD/JF L2 720 41.54 37.33 KD/JF L3 780 41.66 37.35 KD/JF | 6 | 360 | | | 41.23 | 37.02 | JE | | | | - |
| 8 480 41.47 37.26 KD/JF 9 540 41.47 37.26 KD/JF L0 600 41.45 37.24 KD/JF L1 660 41.50 37.29 KD/JF L2 720 41.54 37.33 KD/JF L3 780 41.66 37.35 KD/JF | _ | 100 | | | | | | | |] | |
| 9 540 41.47 37.26 KD/JF 10 600 41.45 37.24 KD/JF 11 660 41.50 37.29 KD/JF 12 720 41.54 37.33 KD/JF L3 780 41.66 37.35 KD/JF | | 420 | | | 41.46 | 37.25 | JE _ | | | | |
| 9 540 41.47 37.26 KD/JF 10 600 41.45 37.24 KD/JF 11 660 41.50 37.29 KD/JF 12 720 41.54 37.33 KD/JF L3 780 41.66 37.35 KD/JF | 8 | 480 | | | 41,47 | 37,26 | KD/JE | | ļ | | |
| L0 600 41.45 37.24 KD/JF L1 660 41.50 37.29 KD/JF L2 720 41.54 37.33 KD/JF L3 780 41.66 37.35 KD/JF | | | | | | - | 10,01 | | · · | | |
| L1 660 41.50 37.29 KD/JF L2 720 41.54 37.33 KD/JF L3 780 41.66 37.35 KD/JF | 9 | 540 | | | 41.47 | 37.26 | KD/JF | | | | |
| L1 660 41.50 37.29 KD/JF L2 720 41.54 37.33 KD/JF L3 780 41.66 37.35 KD/JF | 10 | 600 | | | /1 /5 | 27.27 | WD / TT | | | | |
| L1 660 41.50 37.29 KD/JF L2 720 41.54 37.33 KD/JF L3 780 41.66 37.35 KD/JF | - | 600 | | | 41.45 | 37.24 | KD/JF | | | | |
| L2 720 41.54 37.33 KD/JF L3 780 41.66 37.35 KD/JF | l. 1 | 660 | | | 41.50 | 37.29 | KD/JE | ĺ | | | 1 |
| L3 780 41.66 37.35 KD/JF | | | | | | | | | | | |
| | 12 | 720 | | | 41.54 | 37.33 | KD/JR | | | | |
| | 13 | 780 | | - | 41 66 | 37 35 | מז/מע | | | ĺ | |
| | - | | | | 71.00 | | עה/ או | | | | |
| | 14 | 840 | | | 41.69 | 36.38 | KD/JH | | | | |

GEE & JENSON INDIVIDUALISMENTE PLANTESING

RECORD OF WATER LEVELS

Well No. PW-18

| Time | | Water | Level | (ft.) | Draw- | Mea- | Adjustm | nents | | |
|------|-------------|-------------|------------------|-------|--------------|--------------|---------|--------|-------|---------|
| (hr) | (min) | | Wet | Below | Down | sured | De- | Back- | |] |
| | |] | | MP | (ft) | by | water- | | | Remarks |
| | | | | ļ | | | ing | Levels | | |
| 15 | 900 | | | 41.73 | 37.52 | KD/JF | | | | |
| 16 | 960 | | | 41.55 | 37.34 | KD/JF | | | | |
| 17 | 1020 | | — ; — | 41.62 | 37.41 | KD/JF | | | | |
| 18 | 1080 | | | 41.64 | 37.43 | KD/JF | | | | |
| 19 | 1140 | | | 41.70 | 37.49 | KD/JF | | | · · · | |
| 20 | 1200 | | | 41.80 | 37.59 | KD/JF | | | | |
| 21 | 1260 | | | 41.91 | 37.70 | GR | | | | |
| 22 | 1320 | | | 41.82 | 37.61 | GR | | | | - |
| 23 | 1380 | | | 41.98 | 37.77 | GR | | | | |
| 24 | 1440 | | | 41.72 | 37.51 | GR | | | | |
| 25 | 1500 | | | 41.94 | 37.73 | GR | | | | |
| 26 | 1560 | | | 41.93 | 37.72 | GR | | | | |
| 27 | 1620 | | | 41.99 | 37.78 | GR | | | | |
| 28 | 1680 | | | 41.97 | 37.76 | GR | | | | · • |
| 29 | 1740 | | | 42.18 | 37.97 | GR | | | | |
| 30 | 1800 | | | 42.23 | 38.02 | GR | | | | |
| 31 | 1860 | | | 42.04 | 37.83 | GR | | | | |
| 32 | 1920 | | | 42.05 | 37.84 | GR | | | | |
| 33 | 1980 | | | 42.07 | 37.86 | JF/KD | | | | |
| 34 | 2040 | | | 42.20 | 37.99 | JF/KD | | | | |
| 35 | 2100 | | | 45.40 | 41.19 | JF/KD | | | | |
| 36 | 2160 | | | 42.31 | 38.10 | JF/KD | | | | • |

Well No. PW-18

| rime | · · · · · · · · · | Water | Leve | (f.t.) | Draw- | Mea- | Adjustm | ents | | |
|--------|-------------------|-----------------|------|--|--------|--------------|---------|--------|-------------|---------------------------------------|
| (hr) | (min | | | Below | | sured | De- | Back- | | |
| (111.) | (111.11) | , nera | 1 | MP | (ft) | by | water- | 1 | | Remarks |
| | | | | *** | 1 1207 | ~1 | ing | Levels | | 1.0.1.01.12 |
| | | | | | | | | | | |
| 37 | 2220 | | | 42.32 | 38.11 | JF/KD | } | | - | |
| | <u> </u> | i | | <u> </u> | | 1 32 / 122 | | | | |
| 38 | 2280 | } | | 42.20 | 37.99 | JF/KD | | ľ | ļ | |
| | | | | | | 1 | | | | |
| 39 | 2340 | | | 42.22 | 38.01 | JF/KD | | | | |
| | | | | | | 1 | | | | · · · · · · · · · · · · · · · · · · · |
| 40 | 2400 | | | 42.27 | 38.06 | JF/KD | ~ | | | |
| | · | | | | | | | | | |
| 41 | 2460 | | | 42.30 | 38.09 | JF/KD | | Ì | | |
| | | | | | | | | İ | | |
| 42 | 2520 | | | 42.31 | 38.10 | JF/KD | | | | |
| | | | | | | | | | | |
| 4.3 | 2580 | | | 42.37 | 38.16 | JF/KD | | | | |
| | | | | 10 10 | _ | | | | | |
| 44 | 2640 | | | 42.40 | 38.19 | JF/KD | | | | |
| | 0.7.0.0 | | | (0.07 | | | | Ì | | |
| 45 | 2700 | | | 42.87 | 38.66 | JF/KD | | | | |
| 4.5 | 2760 | | | (2 50) | | | | 1 | } | |
| 46 | 2760 | | | 42.50 | 38.29 | JF/KD | | | | |
| 47 | 2020 | Ì | | 42 52 | 20.01 | | ļ. | • | | |
| 47 | 2820 | | | 42.52 | 38.31 | JF/KD | | | | |
| 40 | 2000 | | | 42.30 | 20.00 | | 1 | | | 1 |
| 48 | 2880 | <u> </u> | | 42.30 | 38.09 | JF/KD | | | | |
| 49 | 2940 | | | 42.40 | 20.10 | (| | | | |
| 49 | 2940 | | | 42.40 | 38.19 | JF/KD | | | | |
| 50 | 3000 | 1 | ł | 42.47 | 38.26 | TD / | | | | |
| 30 | 3000 | | | 72.47 | 30.20 | JF/KD | | | | |
| 51 | 3060 | | | 42.48 | 38.27 | TE /YE | ļ | | | |
| 31 | .5000 | | | 72.70 | 30.27 | JF/KD | | | | |
| 52 | 3120 | | 1 | 42.54 | 38.33 | JF/KD | | | | |
| | 3120 | | | | 30.33 | Jr/KD | | | | |
| 53 | 3180 | | | 42.59 | 38.38 | JF/KD | | | ŀ | |
| -35 | 2100 | | | | | JI/KD | | | | |
| 54 | 3240 | ļ | . | 42.61 | 38.40 | JF/KD | | } | ļ | |
| | 32.10 | | | | - | JI/KD | | | | |
| 55 | 3300 | - | - 1 | 42.56 | 38.35 | JF/KD | Ì | | | |
| | | | | | | 01 / RB | | | | |
| 56 | 3360 | , | [| 42.45 | 38.24 | JF/KD | | | | |
| | | | | | | / 10 | | | | |
| 57 | 3420 | | | 42.53 | 38.32 | GR/MK | 1 | | | |
| | | - - | | | | | | | | |
| 58 | 3480 | ļ | | 42.65 | 38.44 | GR/MK | |] | - | |
| | | | | | | - | | | | |

Well No. PW-18

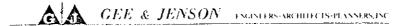
| | | | | | | | 1 | | _ | |
|------|-------|------------------|------------|----------------|----------|--------------|-------------|--|---------------|--|
| Time | | Water | | | Draw- | | | | ļ | _ |
| (hr) | (min) | Held | Wet | Below | Down | sured | | Back- | | Doma visa |
| | |] | | MP | (ft) | by | water- | ground Levels | | Remarks |
| | | | ļ | - | | | ing_ | 1 revers | | |
| 59 | 3540 | ļ | 42 72 | 30 50 | on Imp | | į | | | |
| | 2240 | | 42.73 | 38.52 | GR/MK | <u> </u> | | | 1 | |
| 60 | 36.00 | | 42.88 | 38.67 | GR/MK | | | | ļ | |
| | | | | | | | | | | |
| 61 | 3660 | | 42.63 | 38.42 | GR/MK | <u> </u> | <u> </u> | | ļ | 1 |
| 60 | 2724 | | | 00.00 | an ! | | - | | | |
| 62 | 3720 | | 42.42 | 38.21 | GR/MK | ! | | | | - |
| 63 | 3780 | | 42.62 | 38.41 | GR/MK | | | | | <u> </u> |
| | | ļ - - | -T C + U Z | 20.41 | 21//111/ | | | | | |
| 64 | 3840 | | 42.71 | 38.50 | GR/MK | | ļ | | | |
| | 3000 | | | | | | | | | |
| 65 | 3900 | | 42.68 | 38.47 | GR/MK | <u></u> | - | | ļ | - |
| 66 | 3960 | | 42.65_ | 20 11 | GR/MK | | | · | } | |
| | 2200 | | 44.00 | 38.44 | GU/LIV | | | | | |
| 67 | 4020 | } | 42.73 | 38.52 | GR/MK | | | | · | |
| | | | | | . [| | | | | |
| 68 | 4080 | | 42:82 | 38.61 | GR/MK | | | | · | |
| 69 | 4140 | ŀ | ,, ,, | 20 50 | on har | | | | | |
| 09 | 4740 | | 42.73 | 38.52 | GR/MK | | | | | |
| 70 | 4200 | | 42.66 | 38.45 | GR/MK | . | | | | |
| | | | | | | | | | | |
| 71 | 4260 | | 42.80 | 38.59 | GR/MK | | | | | |
| 72 | 4320 | | | 00 == | | İ | | | | - |
| 72 | 4320 | | 42.73 | 38.52 | GR/MK | | | | | |
| - | 1 | - | j | [| 1 | | | | | |
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Well No. PW-18

| 'ime | | Water | Level | (ft.) | | Mea- | Adjustme | ents . | |
|------|-------------|-------|-------|-------|-------------|-------------|----------------------|---------------------------|---------|
| hr) | (min) | | | | Recovery | sured by | De- water- ing | Back- ground Levels | Remarks |
| DEC | 9:58 | | | 42.73 | 38.52 | JF | | | |
| RECL | OVERY | | | | | | | | |
| | | | | | | | | | |
| | .25 | | | 13,90 | 9.69 | JF | | | |
| | .50 | | | | | - | - | | |
| | .75 | | | 11.65 | 7.44 | ,IF | | | |
| | 1.00 | | | | | | | | |
| | | | | 11.50 | 7.29 | JF | | | |
| | 1.25 | | | | | | | | |
| | 1.50 | | | 10.28 | 6.07 | JF | | | |
| | 1.75 | | Į | | | | | | |
| | 2.00 | | , | | | | | | |
| | 2.25 | | | 9.26 | 5.05 | JF | | | |
| | 2.50 | | | | | | - | | |
| | 2.75 | | | 8.70 | 4.49 | JF | | | |
| | 3.00 | | | 8.47 | 4.21 | JF | | | • |
| | 3.25 | | | 8.30 | 4.09 | JF | | | |
| | 3.50 | | | 8.16 | 3.95 | JF | | | |
| | 3.75 | | | 8.02 | 3.81 | JF | | | |
| | 4.00 | | | 7.92 | 3.71 | JF | | | |
| | 4.25 | | | 7.86 | 3.65 | JF | | | |
| | 4.50 | | | 7.77 | 3.56 | JF | | | |
| | 4.75 | | | 7.68 | 3,47 | JF | | | |
| | 5.00 | | | 7.59 | 3.38 | JF | | | · |

Well No. PW-18

| Tim | | Water | Leve | (ft.) |] | Mea- | | | |
|----------|-------------|----------|-------------|----------|----------|------|--------------|-------------|-----------|
| (hr | | | Wet | | Recovery | | | Back- | |
| Ì | | | | MP | 1 | by | water- | | Remarks |
| R | COVER' | <u> </u> | | <u> </u> | | | ing | Levels | |
| | | | | 20 | 2 20 | JF | | | |
| | 6 | | | 7.30 | 3.09 | | | | |
| ļ | 7 | ł | | 7.08 | 2.87 | JF | | | |
| | + | | | | | | | | |
| | 8 | | | 6.90 | 2.69 | JF | | | |
| | | | | 6.75 | 2.54 | JF | = | | |
| | 9 | | | 0.75 | 2.54 | | | | |
| | 10 | | | 6.60 | 2.39 | JF | | | |
| | | | | (/) | | JF | | | |
| | 12 | | | 6.41 | 2.20 | | | | |
| | 14 | | | 6.24 | 2.63 | JF | . | | } |
| | 1 | | | | 2.03 | | _ | | |
| _ | 16. | | | 6.17 | 1.96 | JF | | | |
| | 1,0 | | | 6.04 | 1 00 | JF | | ĺ | |
| <u> </u> | 18 | | | 0.04 | 1.83 | | - | | |
| | 21 | ļ | , | 5.91 | 1.70 | JF | | | |
| | | | | | | | | | |
| | 25 | | | 5.75 | 1.54 | JF | | · | |
| | 30 | | | 5.61 | 1.40 | · JF | | } | _ |
| · | 30 | | | 3.01 | 1.40 | | | | |
| | 35 | | | 5.50 | 1.29 | JF | | | |
| | | | -, | | 1.00 | | | | _ |
| | 40 | | | 5.41 | 1.20 | JF | | | |
| | 45 | İ | 1 | -5.34 | 1.13 | JF | | , | |
| | | | | | | | | | |
| | 50 | | | 5.29 | 1.08 | JF | | | • |
| 1 | 60 | | | 5.13 | 0.92 | JF | | | |
| <u> </u> | 60 | | | 3.13 | 0.92 | | | | |
| | 70 | | | 5.10 | 0.89 | JF | | | |
| | | | | 7.10 | | | | | |
| | 80 | | | 5.10 | 0.89 | JF | | | |
| | 90 | | 1 | 5.04 | 0.83 | JF | | 1 | |
| | | | · · | | 3.03 | | | | |
| | 100 | | ŀ | 5.00 | 0.79 | JF | | | |
| | 300 | | | 4 05 | 0.7/ | TD | | | |
| 2 | 120 | | | 4.95 | 0.74 | JF | | | |
| 1 | 150 | į | į | 4.88 | 0.67 | JF | | | |
| | | | | 4.85 | | | | | M-Scope 2 |
| 3 | 180 | l | ļ | 4.91 | 0.64 | JF | 1 |] | Таре |



Well No. PW-18

| lima | | Water | Level | (ft.) | T | Mea- | Adjustme | ante | 1 | |
|------------|----------|----------|-------------|---------------------------------------|---------------------------------------|--------------|----------|---------------------------------------|--|---------------------------------------|
| ime hr) | (min) | | | L Bolon | Recovery | sured | De- | Back- | | 1 |
| ,nr) | (101711) | neru | wel | MP | Recovery | by | water- | | | Remarks |
| | | | | MP | | l ny | | Levels |] | Kemarks |
| | | <u> </u> | | | | | ing | revers | <u> </u> | |
| , : | 2/0 | | | , ,, | 0.55 | | | | | |
| 4 | 240 | | | 4.82 | 0.55 | JF | | · · · · · · · · · · · · · · · · · · · | | |
| 0.0 | 7.5.60 | | | , ., | | | | | | |
| 26 | 1560 | | | 4.74 | 0.47 | JF | | | | |
| | 0000 | | | , | | | | | | |
| 0.5 | 3030 | | _ | 4.74 | 0.47 | JF | | | | |
| | | | į | | | | ſ | | i | |
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2019 OKEECHOBEE BOULEVARD, WEST PALM BEACH, FLORIDA. . . 33409. . . 305 - 683-3301

FRED A. GREENE, P.E.
RICHARD M. MILLER, P.E.
WALTER D. STEPHENS, JR., P.E.
WILLIAM G. WALLACE, JR., P.L.S.
PHILIP A. CRANDELL JR., A.I.A.
JOHN C. WISE, P.E.

Director Emercial
H. C. GEE, P.E.
THEODORE B. JENSON, P.E.

RECORD OF WATER LEVELS

Well No. 18-18

| Proj | ect | 79-183 | Acme V | Vell 18 | | Locat | tion Ho | meland Ro | ad | | |
|------|--------|---------|-------------|---------|--------------|---------------|---------------|---------------------------|---------------------------------------|-------------|-----|
| Elev | ation_ | | | | MSL | Measu | uring Po | oint_Top | of Cas | ing | |
| Dist | ance t | to Pump | ed Wel | .1 | | feet D | oischarg | je | 900 | | GPM |
| Tota | l Dept | h 60 | fe | et C | ased D | epth <u>0</u> | -10f | eet Di | ameter | 2 | |
| Star | ting [| Date of | Test_ | 9/24/ | 80 @ 10 | 000 | | · · · | | | |
| Time | | Water | Leve | 1 (ft) | Draw - | Mea- | Adjust | ments | | Remarks | |
| | } | Held | | | Down (ft) | sured by | De- water- | Back- ground Levels | Correc Drawdo | n | |
| 755 | | | | 3.83 | | | | | · · · · · · · · · · · · · · · · · · · | M-Scope B | -, |
| | | | , | 3.85 | | | | | | Таре | |
| 091 | 5 | | | 3.83 | | | | | | | |
| 094 | 6 | | | 3.84 | | | | | i | | |
| 095 | 9 | | | 3.83 | | HV | | | | | |
| | .25 | | | 3.86 | 0.03 | ни | | | | | |
| | .50 | | | 3.91 | 0.08 | ну | | | | | |
| | .75 | | | 3.99 | 0.16 | HV | | | | | |
| | 1.00 | | | 4.04 | 0.21 | HV | | | | | |
| | 1.25 | | | | 0.27 | нν | | | | | |
| | 1.50 | • | | | 0.31 | HV | | | | | |
| | 1.75 | | | 4.18 | 0.35 | HV | | | | | |
| | 2.00 | | | 4.22 | 0 · 39 | н٧ | | | | | |
| | 2.25 | | | 4.25 | 0.42 | н٧ | | | | | |
| | 2.50 | | | 4.27 | 0.44 | ни | | | | | |
| | 2.75 | | | 4.29 | 0.46 | HV | | | | | |

Well No. <u>18-15</u>

| | | T2 | _ | | 1 10 | 1-1 | Adjustm | onic | 1 | |
|----------------|-------------|----------|---------------|----------|--------------|--------------|----------|-------------|-------------|--------------------------|
| Time | | Water | | (ft.) | | | | L Back- | Corrected | 1 |
| (hr) | (min) | Held | Wet | Below | Down (ft) | sured by | water- | | | Remarks |
| | | | | MP | (10) | l ny | ing | Levels | | 1.0 |
| ļ | | <u> </u> | | <u> </u> | | | <u> </u> | 20,010 | | - |
| | 3.00 | | | 4.33 | 0.50 | HV | | | | |
| | 3.00 | | | | | | | | | - |
| | 3.25 | | | 4.36 | 0.53 | HV | | | | |
| | | | | 4 27 | 0.54 | 7117 | | | | |
| | 3.50 | | | 4.37 | 0.54 | HV | | | | |
| | 3.75 | | | 4.39 | 0.56 | HV | | | | |
| | 3.13 | | | | | | | | | |
| | 4.00 | } | ı | 4.41 | 0.58 | HV | | | | |
| | | | | | | | | | | |
| | 4.25 | | | 4.42 | 0.59 | HV | | | | |
| | 1 50 | į | | 4.44 | 0.61 | HV | | | İ | |
| | 4.50 | | | 7.74 | 0 + OT | 11.4 | | | | |
| | 4.75 | | | 4.46 | 0.63 | HV | | | | |
| | | | | | | | | | | |
| | 5 | | | 4.48 | 0.65 | HV | | | | |
| | | | | , 53 | 0.70 | 1177 | ļ | | | |
| | 6 | | | 4.53 | 0.70 | HV | | | | |
| | 7 | | | 4.59 | 0.76 | нv | ļ | Ì | | |
| | | | | | | | | | | |
| | 8 | | | 4.64 | 0.81 | нν | | | | |
| | | | | | | | | | | |
| | 9 | | | 4.67 | 0.84 | HV | | | | |
| | | T | | 4.70 | 0.87 | ни | ļ | | | - |
| <u> </u> | 10 | | | 7.70 | 0.07 | 11 V | | | | |
| | 12 | | | 4.75 | 0.92 | HV | | | | |
| | | | | | | | | | | |
| | 14 | | | 4.80 | 0.97 | НΛ | | | | |
| | | | | / 00 | 7 00 | | | | | |
| | 16 | | | 4.83 | 1.00 | HV | | | | <u> </u> |
| 1 | 10 | | } | 4.86 | 1.03 | HV | 1 | | | |
| | 18 | | | | | | | | | |
| | 20 | | ŀ | 4.89 | 1.06 | ни | [| • | | |
| - | | | | | | | | | | |
| 1 | 25 | ŀ | | 4.95 | 1.12 | HV | | | | |
| | | | | 4 00 | 1 16 | 1117 | | | | |
| | 30 | | | 4.99 | 1.16 | HV | | | | |
| | 25 | | | 5.02 | 1.19 | н٧ | | | | • |
| | 35 | | | 3.02 | | | | | | |

Well No. <u>18-18</u>

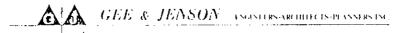
| | | 1.1 - 1 - 1 | 1 01:01 | / E I- \ | Draw- | Mea- | Adjustme | ents | | <u> </u> |
|------|----------|---------------|--------------|---------------------|-------|-----------|----------|--------|--------|-----------------|
| 'ime | (min) | Water Held | <u>rever</u> | (ft.) Below | | sured | De- | | Correc | ted |
| hr) | (111111) | nerd | WEC | MP | (ft) | by | water- | ground | Drawdo | wn Remarks |
| | ì | | | 1 | , , | | ing | Levels | (ft.) | |
| | | | | | | | | | | |
| | 40 | | · <u>-</u> | 5.05 | 1.22 | HV | | | | |
| | 4.5 | | | F 07 | 1 2/ | HV | Ì | | | |
| | 45 | | | 5.07 | 1.24 | nv | | | | |
| | 50 | | | 5.09 | 1.26 | ΗV | | | | |
| | | | | , | | | | ĺ | į | |
| 1 | 60 | | | 5.11 | 1.28 | HV | | | | |
| 1 | . 70 | | | 5.14 | 1.31 | нν | | | } | • |
| | 70 | | | J.14 | 1.71 | 11.4 | | | | |
| ĺ | 80 | } | | 5.16 | 1.33 | HV | | | | |
| | | | | | | | | |] | |
| | 90 | | | 5.17 | 1.34 | ΗV | | | | |
| 1 | 100 | | | 5.18 | 1.35 | ну | | | | |
| | 100 | | | 3.10 | 1.55 | 11 9 | | | | |
| 2 | 120 | | | 5.20 | 1.37 | HV | | | | |
| | | | | | | | | | Ì | |
| | 150 | | | 5.23 | 1.40 | GR | | | | M-Scope |
| _ | 100 | | j | 5.25 5.27 | 1.42 | JE/KD | -0.01 | - | | м-ѕсоре Таре |
| 3 | 180 | | | 3.21 | 1.72 | JE/RD | | | L. 41 | Tupe |
| 4 | 240 | | | 5.31 | 1.46 | JЕ | -0.01 | | .45 | |
| | | | | | | | | | | |
| 5 | 300 | | | 5.34 | 1.49 | JE | -0.01 | | L.48 | |
| | 360 | } | | 5.37 | 1.52 | JE | -0.01 | | L.51 | - |
| 6 | 360 | | | 3.37 | 1.52 | | -0.01 | | 1.071 | |
| 7 | 420 | | | 5.40 | 1.55 | JE | -0.01 | | 1.54 | |
| | | | | | | _ , _ | | | | Ì |
| 8 | 480 | | | 5.42 | 1.57 | JF/KD | -0.01 | | L.56 | |
| 9 | 540 | | | 5.42 | 1.57 | JF/KD | -0.01 | } | 1.56 | į |
| 9 | 340 | | | 7.42 | 1.57 | | 0.01 | | . 30 | |
| 10 | 600 | | | 5.46 | 1.61 | JF/KD | -0.01 | | L.60 | |
| | | | | | | (| | | | |
| 11 | 660 | | | 5.50 | 1.65 | JF/KD | -0.01 | | 1.64 | |
| 12 | 720 | | | 5.51 | 1.66 | JF/KD | -0.01 | | 1.65 | |
| | 120 | | | | | 52710 | | | | - |
| 13 | 780 | | | 5.51 | 1.66 | JF/KD | -0.01 | - | 1.65 | |
| | | | | | 7 (7 | III / III | 0.07 | | | • |
| 14 | 840 | | | 5.52 | 1.67 | JF/KD | -0.01 | | 1.66 | |

GEE & JENSON - MINITION ARCHITECTS OF ANNIHALING

RECORD OF WATER LEVELS

Well No. <u>18-15</u>

| Time | | Water | | (ft.) | Draw- | 1 | | ents . | Corrected |
|-------------|---------|----------|-----|-------|-------|------------|--------|--------------------|------------------|
| (hr) | (min | Held | Wet | Below | | sured | | | Corrected |
| | | | | MP | (ft) | рÀ | water- | ground Levels | Drawdown Remarks |
| <u> </u> | · | ! | | | | | ing | PEAGIS | (10.) |
| 15 | 900 | | | 5.54 | 1.69 | JF/KD | -0.01 | | 1.68 |
| | | | | | | | | | |
| 16 | 960 | | | 5.54 | 1.69 | JF/KD | -0.01 | | 1.68 |
| 7 -7 | 1020 | | | | 1 70 | יע/ער | 0.01 | | 1 60 |
| 17 | 1020 | <u> </u> | | 5.55 | 1.70 | JF/KD | -0.01 | | 1.69 |
| 18 | 1080 | | | 5.56 | 1.71 | JF/KD | -0.01 | | 1.70 |
| | | | | | | | | | |
| 19 | 1140 | | | 5.55 | 1.70 | JF/KD | -0.01 | | 1.69 |
| 20 | 1.200 | | , | 5.56 | 1.71 | JF/KD | -0.01 | | 1.70 |
| 20 | 1.200 | | | 3.30 | 1.11 | UI/KD | J.01 | | |
| 21 | 1260 | | | 5.57 | 1.72 | GR | -0.01 | | 1.71 |
| | 1222 | | | 5.50 | 7 7/ | a n | | | . 70 |
| 22 | 1320 | · · | | 5.59 | 1.74 | GR | -0.01 | | 1.73 |
| 23 | 1380 | ļ | | 5.59 | 1.74 | GR | -0.01 | | 1.73 |
| | | | | | : | | | | |
| 24 | 1440 | | | 5.60 | 1.75 | GR . | -0.01 | | 1.74 |
| 25 | 1500 | | • } | 5.60 | 1.75 | GR | -0.01 | ļ | 1.74 |
| 25 | 1200 | | | 3.00 | 1.75 | GIV | -0.01 | | 1. 1. 1. 4 |
| 26 | 1560 | | | 5.61 | 1.76 | GR | -0.01 | | 1.75 |
| | | | | | | | _ | | |
| 27 | 1620 | | | 5.62 | 1.77 | GR | -0.01 | | 1.76 |
| 28 | 1680 | 1 | | 5.63 | 1.78 | GR | -0.01 | . | 1.77 |
| | | | | | | J. | 0.01 | | |
| 29 | 1740 | | | 5.64 | 1.79 | GR | -0.01 | | 1.78 |
| 20 | 1800 | | | E 61 | 1 70 | CD. | 0.01 | • | 1 70 |
| 30 | T800 | | | 5.64 | 1.79 | GR | -0.01 | | 1.78 |
| 31 | 1860 | | | 5.62 | 1.77 | GR | -0.01 | | 1.76 |
| | | | | | | | | | |
| 32 | 1920 | | . | 5.65 | 1.80 | GR | -0.01 | | 1.79 |
| 33 | 1980 | | | 5.66 | 1.81 | JF/KD | -0.01 | | 1.80 |
| | T 9 0 0 | | | 7.00 | 1.0T | Jr/KU | -0.01 | | 1.00 |
| 34 | 2040 | | | 5.68 | 1.83 | JF/KD | -0.01 | | 1.82 |
| | - | | | | | | | | |
| 35 | 2100 | | | 5.72 | 1.87 | JF/KD | -0.01 | | 1.86 |
| 36 | 2160 | | | 5.70 | 1.85 | JF/KD | -0.01 | | 1.84 |
| 30 | 2100 | | | 3.70 | 1.00 | JI/KD | 0.01 | | J. 6 12-4 3 |



Well No. 18-15

| | | T | | | | | | | |
|-------------|-------|--------------|---------------------------------------|--------------|-------|--------------|----------|-------------------|------------------|
| lime | | Water | | | Draw- | 1 | Adjustme | | |
| (hr) | (min) | Held | Wet | Below | | sured | 1 | | Corrected |
| | 1 | | | MP | (ft) | by | water- | | Drawdown Remarks |
| | - | | | | | - | ing | Levels | (ft.) |
| 37 | 2220 | | | 5.69 | 1.84 | JF/KD | -0.01 | | 1.83 |
| | | | | 7.09 | 1.04 | 31 / KD | -0.01 | | 1.00 |
| 38 | 2280 | | | 5.70 | 1.85 | JF/KD | -0.01 | | 1.84 |
| | | | · · · · · · · · · · · · · · · · · · · | | | , , , , , , | | | |
| 39 | 2340 | | | 5.72 | 1.87 | JF/KD | -0.01 | | 1.86 |
| 40 | 2400 | | | | | | 1 | | |
| 40 | 2400 | | | 5.73 | 1.88 | JF/KD | -0.0l | | 1.87 |
| 41 | 2460 | | | | . 07 | TR/mp | | | 1 00 |
| | 2400 | | | 5.72 | 1.87 | JF/KD | -0.01 | | 1.86 |
| 42 | 2520 | | | 5.72 | 1.87 | JF/KD | -0.01 | | 1.86 |
| | | | | | 1.07 | 02/KB | -0.01 | | 1.00 |
| 43 | 2580 | • | | 5.73 | 1.88 | JF/KD | -0.01 | j | 1.87 |
| | | | | | | | | | |
| 44 | 2640 | | ······ | 5.75 | 1.90 | JF/KD | -0.02 | | 1.88 |
| 4.5 | 2700 | ľ | | | | | | | |
| 45 | 2700 | | | 5.76 | 1.91 | JF/KD | -0.02 | | 1.89 |
| 46 | 2760 | | | E 75 | 1.90 | 7112 / 1275 | 0.00 | | 7 00 |
| -40 | 2700 | | | 5.75 | 1.90 | JF/KD | -0.02 | | 1.88 |
| 47 | 2820 | } | | 5.78 | 1.93 | JF/KD | -0.02 | | 1.91 |
| - | | | | 3.,0 | | J., ILD | | | |
| 48 | 2880 | | | 5.78 | 1.93 | JF/KD | -0.02 | | 1.91 |
| | | | | | | | | | |
| 49 | 2940 | | | 5.78 | 1.93 | JF/KD | -0.02 | | 1.91 |
| | 2000 | | | | | | | | |
| 50 | 3000 | | | 5.78 | 1.93 | JF/ KD | -0.02 | | 1.91 |
| 51 | 3060 | | | 5.80 | 1.95 | JF/KD | 0.00 | | 1 03 |
| | 3000 | - | } | 3.00 | 1.93 | JF/KD | -0.02 | | 1.93 |
| 52 | 3120 | |] | 5.79 | 1.94 | JF/KD | -0.02 | | 1.92 |
| | | | - | | | | | | 1.02 |
| 53 | 3180 | | | 5.80 | 1.95 | JF/KD | -0.02 | | 1.93 |
| | | | | | | | | | |
| 54 | 3240 | | | 5.81 | 1.96 | JF/KD | -0.02 | | 1.94 |
| | 2200 | ļ | 1 | £ 0.1 | 1 06 | | | | |
| 55 | 3300 | | | 5.81 | 1.96 | JF/KD | -0.02 | | 1.94 |
| 56 | 3360 | | | 5.81 | 1.96 | JF/KD | -0.02 | | 1 04 |
| | 7300 | | | J. UI | | 21/KD | -0.02 | | 1.94 |
| 57 | 3420 | | 1 | 5.81 | 1.96 | GR/MK | -0.02 | } | 1.94 |
| | | | | | | -, -11 | | | |
| 58 | 3480 | | | 5.83 | 1.98 | GR/MK | -0.02 | | 1.96 |
| | ~ | | | | | | | _ l _ | |



Well No. <u>18-18</u>

| | | | | | | | | | + | | | |
|---------------|-------|--|-------|-------------|--------|----------|--------|-------------|-----------------|----------------|-------------|---------------------------------------|
| Time | | Water | Level | (ft.) | Draw- | l . | | ents . | | | | |
| (hr) | | Held | Wet | Below | | sured | | Back- | porrec | tea | _ | , |
| 1 | | | | MP | (ft) | by | water- | ground | \t+ / htamac | WII | Rema | rks |
| | | | | <u> </u> | | | ing | Levels | (IC.) | | • | <u> </u> |
| 50 | 25.42 | | | 5.83 | 1 00 | OD 1201 | 0.00 | | 1 04 | 1 | | |
| 59 | 3540 | ļ - - | | 7.05 | 1.98 | GR/MK | -0.02 | | 1.96 | +- | | |
| 60 | 3600 | | | 5.83 | 1.98 | GR/MK | -0.02 | | 1.96 | 1 | | |
| - 00 | 2000 | | | | T • 30 | GR/ FIX | 0.02 | | 1.70 | 1 | | · · · · · · · · · · · · · · · · · · · |
| 61 | 3660 | | | 5.83 | 1.98 | GR/MK | -0.02 | | 1.96 | | | |
| <u> </u> | | | | | | , | - | | | | | |
| 62 | 3720 | | , | 5.83 | 1.98 | GR/MK | -0.02 | | 1.96 | | | •• |
| | | | | | 1 | | | | | | | |
| 63 | 3780 | | | 5.83 | 1.98 | GR/MK_ | -0.02 | | 1.96 | | | |
| | | | | 5 02 | | <i>!</i> | | | 1 01 | 1 | | |
| 64 | 3840 | | | 5.83 | 1.98 | GR/MK | -0.02 | | 1.96 | ļ | | |
| | 2000 | | | 5.84 | 1 00 | OD /364 | | | 1 07 | | | |
| 65 | 3900 | | | 3.04 | 1.99 | GR/MK | -0.02 | | 1.97 | ├ | | |
| 66 | 3960 | | | 5.85 | 2.00 | GR/MK | -0.02 | | 1.98 | | | |
| 00 | טסענ. | | | | 2.00 | GR/ PIR | -0.02 | | 1.70 | - | | |
| 67 | 4020 | | | 5.85 | 2.00 | GR/MK | -0.02 |] | 1.98 | Į | | |
| - 7 | 1020 | | | | -2.55 | | | | | | | |
| 68 | 4080 | | - [| 5.85 | 2.00 | GR/MK | -0.02 | | 1.98 | [| | |
| - | | | - | | | | | | | | | |
| 69 | 4140 | | [| 5.85 | 2.00 | GR/MK | -0.02 | | 1.98 | | | |
| | | | | | | | | | - | | | |
| 70 | 4200 | - | | 5.86 | 2.01 | GR/MK | -0.02 | | 1.99 | | | |
| | | | | 5 94 | | | | | | | | |
| 71 | 4260 | | | 5.86 | 2.01 | GR/MK | -0.02 | | 1. 99 | V - | | TA |
| 7. | 4220 | | | 5.85 | 0.00 | an /sar | 0.02 | | 2 00 | | cope 1 | A. |
| 72 | 4320 | | | 5.87 | 2.02 | GR/MK | -0.02 | | 2.00 | Tap | e | |
| | ł | | | | | | j | | - | | | |
| | | | | | | | | | | | | |
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| 1 | | | | } | - | | | | | | | |
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Well No. 18-1S

| Time | | Water | Level | (ft.) | | Mea- | Adjustme | | | |
|------|-------|----------|-------|-------|----------|-------|-------------|--------|------|---|
| (hr) | (min) | | Wet | | Recovery | sured | De- | Back- | | |
| (/ | (,, | | | MP | | by | water- | ground | | y Remarks |
| ļ | | | | | | | ing | Levels | (ft) | |
| DEC | OVERY | | | | | | | | | |
| REC | JVERI | | | | | | | | | |
| ł | | | | 5.85 | 2.02 | . HA | -0.02 | | 2.00 | M-Scope #A |
| | 2.5 | | | | 0.04 | | -0.02 | | 2 22 | |
| | .25 | | | 5.91 | 2.04 | HV | | | 2.02 | <u>, </u> |
| | .50 | 1 | | 5.84 | 1.97 | HV | -0.02 | ļ | 1.95 | |
| | | | | | | | -0.01 | | | |
| | .75 | | | 5.76 | 1.89 | HV | | | 1.88 | |
| | 1.00 | 1 | | 5.68 | т от | 1777 | -0.01 | 1 | 1.80 | |
| | 1.00 | | | 3.00 | 1.81 | HV | | | 1.80 | |
| 1 | 1.25 | 1 | | 5.62 | 1.75 | HV | -0.01 | | 1.74 | |
| | | | | | | | -0.01 | | | |
| | 1.50 | | | 5.58 | 1.71 | HV | | | 1.70 | |
| | 1.75 | } | ļ | 5.52 | 1.65 | HV | -0.01 | | 1.64 | |
| | 1.75 | | | 3.52 | 1.00 | 11.0 | | | 1.04 | |
| | 2.00 | | - | 5. 48 | 1.61 | НV | -0.01 | | 1.60 | |
| | | | | | | | 0.01 | | | |
| | 2.25 | | | 5.44 | 1.57 | HV | -0.01 | | 1.56 | |
| | 2.50 | 1 | | 5.42 | 1.55 | ни | -0.01 | | 1.54 | |
| - | 2.50 | | | | 1.33 | | | | | · · · · · · · · · · · · · · · · · · · |
| ļ | 2.75 | 1 | Ī | 5.39 | 1.52 | HV | -0.01 | | 1.51 | |
| | | | | 5 0.5 | | | -0.01 | | 7 10 | • |
| | 3.00 | | | 5.37 | 1.50 | HV | | | 1.49 | |
| 1 | 3.25 | | | 5.35 | 1.48 | HV | -0.01 |] | 1.47 | |
| | | | | | | - | | | | |
| | 3.5d | | | 5.33 | 1.46 | HV | -0.01 | | 1.45 | |
| | 2 7 5 | | | 5.31 | 1 // | 1177 | -0.01 | 1 | 1.43 | |
| | 3.75 | | | 3.31 | 1.44 | HV | | | 1.43 | |
| ļ | 4.00 | | | 5.30 | 1.43 | HV | -0.01 | | 1.42 | |
| | | | | | | | 2 2- | | | |
| | 4.25 | | | 5.28 | 1.41 | HV | -0.01 | | 1.40 | |
| | 4 5 0 | [. | | 5.27 | 1.40 | ни | -0.00 | | | |
| | 4.50 | | | 3.21 | 1.40 | | | | | |
| | 4.75 | ĺ | ļ | 5.25 | 1.38 | нv | 1 | | | |
| | | | | - | | | | | | |
| | 5.00 | | | 5.24 | 1.37 | HV | | | | · . |

Well No. <u>18-18</u>

| | | | | | | | | | |
|-------------|---------|--------------|-------|--------------|-------------|-------|---------------|-----------------|-----------|
| Tim | | | Level | (ft.) | | Mea- | | | |
| (hr |) (min | Held | Wet | | Recovery | sured | De- water- | Back- ground | Remarks |
| 1 0 | RECOVER | \ | | MP | | pλ | ing | Levels | Remains |
| | LICOVEX | | | | | | | | |
| | 6 | | | 5.20 | 1.33 | HV | | | |
| | . 7 | | | 5.17 | 1.30 | н٧ | | | |
| | 8 | | | 5.14 | 1.27 | HV | | | |
| | 9 | | | 5.11 | 1.24 | HV | - | | |
| | 10 | | | 5.09 | 1.22 | HV. | | | |
| | 12 | | | 5.07 | 1.20 | HV | | | |
| <u> </u> | 14 | | | 5.03 | 1.16 | HV | | | |
| | 16 | | | 5.01 | 1.14 | HV | - | | |
| ļ | 18 | | | 4.99 | 1.12 | HV | | | |
| | 20 | | | 4.96 | 1.09 | HV | | | |
| | 25 | | | 4.91 | 1.04 | HV | | | |
| | 30 | | | 4.88 | 1.01 | · HV | | | |
| | 35 | | | 4.85 | 0.98 | HV | | | |
| | 40 | | | 4.83 | 0.96 | HV | | | - |
| | 45 | | | 4.80 | 0.93 | ΗV | | | |
| | 50 | | | 4.77 | 0.90 | н۷ | | | |
| 1 | 60 | | | 4.73 | 0.86 | ни | | | |
| | 70 | | | 4.69 | 0.82 | HV | | | |
| | 80 | | | 4.65 | 0.78 | н۷ | | | · |
| | 90 | | | 4.62 | 0.75 | н۷ | | | |
| | 100 | | | 4.59 | 0.72 | н۷ | | | |
| - 2 | 120 | | | 4.54 | 0.67 | нν | | | |
| - | 150 | | | 4.48 | 0.61 | ни | | | |
| 3 | 180 | | | 4.41 4.46 | 0.61 | нν | | | M-Scope A |

Well No. 18-1S

| Time | · · · · · · | Water | Level | (ft.) | | Mea- | Adjustm | ents | ì | |
|------|-------------|-------|-------|---------------|---------------------------------------|---------------|--------------|--------------|-------------|--------------|
| (hr) | (min) | | Wet | Below | Recovery | sured | De- | Back- | | |
| ``' | , | | | MP | | by | water- | | | Remarks |
| | | | | | | 1 | ing | Levels | | |
| | | | | | | | | | 1 | |
| 4 | 240 | | | 4.33 | 0.48 | HV | | [| | |
| | | | | ۲۰۰۰ | 0.40 | | | | | |
| 26 | 1560 | | | 4.20 | 0.35 | ну | | ŀ | | |
| | | | | 4.20 | | | | | | |
| 50.5 | 3030 | | | 4.20 | 0.35 | HV | ! | | | • |
| 30.3 | 5030 | · | | 4.20 | | | | | | |
| | : | · . | | | | | | | | |
| | | | | ··· | · | I | | | | |
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2019 OKEECHOBEE BOULEVARD, WEST PALM BEACH, FLORIDA... 33409,... 305 - 683-3301

FRED A. GREENE, P.E.
RICHARD M. MILLER, P.E.
WALTER D. STEPHENS, JR., P.E.
WILLIAM G. WALLACE, JR., P.E.S.
PHILIP A. GRANNELL JR., A.I.A.
JOHN C. WISE, P.E.

Project 79-183 Acme Well 18

Director Emeritus
H. C. GEE, P.E.
THEODORE B. JENSON, P.E.

RECORD OF WATER LEVELS

| Well | No. | 18-1D | |
|------|-----|-------|--|
|------|-----|-------|--|

Location Homeland Road

| Elev | ation_ | | | | MSL | Measi | uring Po | oint Top | of Casi | ng | |
|------|--------|---------|--------|-------------|--------------|---------------|---------------|---------------------------|---------|---------------------------------------|----------|
| Dist | ance t | to Pump | ed Wel | .13 | 33.0 | feet I | Dischar | ge | 90 | | GPM |
| Tota | l Dept | .h 90 | fe | et C | ased D | epth <u>0</u> | - 70 f | feet Di | ameter | 2" | I |
| Star | ting D | ate of | Test_ | 9/24/ | 80 @100 | 00 | <u> </u> | = , | | | · |
| Time | | Water | Leve | 1 (ft) | | Mea- | Adjust | ments | İ | Remarks | |
| (hr) | (min) | Held | Wet | Below MP | Down (ft) | by | water- | Back- ground Levels | Drawdow | ed n | |
| 7:5 | 3.a.m. | | | 3.30 | | | | | | Таре | |
| | | | | 3.27 | | | | | | M-Scope A | |
| 9:1. | a.m. | | | 3.27 | | | | - | | · | <u> </u> |
| 9:4 | a.m. | | | 3.28 | | | | | | | |
| 9:4 | a.m. | | | 3.28 | | | | | | · · · · · · · · · · · · · · · · · · · | |
| | .25 | | | | | | | Ì | | | |
| | -50 | | | 12.82 | 9.59 | | ¬0.47 | | 9.07 | | |
| | .75 | | | | | | | | | | |
| | 1.00 | | | | | | | | | | |
| | 1.25 | | | 15.55 | 12.27 | | -0.79 | | 11.48 | | |
| | 1.50 | • | | 16.10 | 12.82 | | -0.87 | | 11.95 | | |
| | 1.75 | | | 16.33 | 13.05 | | -0.90 | | 12.15 | • | |
| | 2.00 | | | 16.36 | 13.08 | | -0.91 | | 12.17 | | |
| | 2.25 | | | 16.45 | 13.17 | | -0.92 | | 12.25 | ~ | |
| | 2.50 | | | 16.57 | 13.29 | | 0.94 | | 12.35 | | |
| | 2.75 | | | 16.68 | 13.40 | | 0.95 | | 12.45 | | |

GEE & JESSON ENGINEERS ARCHITECTS PLANNERS AND

RECORD OF WATER LEVELS

Well No. <u>18-1D</u>

Project 79-183 Acme Well 18

Starting date of Test 9/24/80 @ 1000

| Nate Nate Level (Et.) Draw Sured Sured Dar Water HP Sured Dar Water Sured Dar Water Sured Dar Water Sured Dar Water Sured Dar Water Sured Sured Dar Water Sured | | | | | | | | | | | | |
|--|----------|-------------|----------|-------|---------------|--------|---------|---------|--------------|---------|----------|-------------|
| Chicago Chic | Time | | Water | Level | (ft.) | Draw- | Mea- | Adjustm | | | _ | |
| MP | | (min) | | | | | 1 | | Back- | Correc | ted | |
| 16.82 13.54 JF/KD -0.98 12.56 | (ur) | (111.111) | neru | nec | i i | | L | water- | ground | Drawdo | wn Rer | narks |
| 3.00 | | | | | *** | (20) | -1 | 1 | | | | |
| 3.25 | | | <u> </u> | | | | | | | | | |
| 3.25 | | 2 00 | | | 16.82 | 13.54 | TF/KD | -0.98 | | 12.56 | | |
| 3.75 | . | 3.00 | | | 10.02 | | 01710 | | | | | |
| 3.50 | .] | 2 25 | | | 16 92 | 13.64 | IE/KD | -0.99 | | 12.65 | | |
| 3.50 | | 3.25 | | | 10.72 | | SITED | | | | <u> </u> | - |
| 3.75 | | 2 50 | | | 17 03 | 13.75 | וב/גם | -1.01 | | 12.74 | | |
| 3.75 | | 3.50 | | | 17.00 | | SITKD | | | | | |
| | | 2 25 | | | 17 13 | 13.85 | וא/או | -1.02 | | 12.83 | | |
| 4.00 | | 3.75 | | | 17.13 | 13.03 | SITKD | | | | | |
| 4.25 | | 4 00 | . ' | | 17 22 | 13.94 | מא/אז | -1.04 | | 12.90 | | |
| 4.25 17.32 14.04 JF/KD -1.06 13.04 4.50 17.38 14.10 JF/KD -1.06 13.04 4.75 17.47 14.19 JF/KD -1.08 13.11 5 17.54 14.26 JF/KD -1.09 13.17 6 18.27 14.89 JF/KD -1.19 13.70 7 18.53 15.31 JF/KD -1.26 14.05 8 18.54 15.30 JF/KD -1.26 14.04 9 18.56 15.28 JF/KD -1.25 14.03 10 18.67 15.39 JF/KD -1.27 14.12 12 18.91 15.63 JF/KD -1.31 14.32 14 19.12 15.84 JF/KD -1.35 14.49 16 19.28 16.00 JF/KD -1.38 14.62 18 19.45 16.17 JF/KD -1.41 14.76 20 19.58 16.30 JF/KD -1.43 14.87 25 19.79 <td></td> <td>4.00</td> <td></td> <td></td> <td></td> <td></td> <td>JI/KD</td> <td></td> <td></td> <td></td> <td></td> <td></td> | | 4.00 | | | | | JI/KD | | | | | |
| 4.50 17.38 14.10 JF/KD -1.06 13.04 4.75 17.47 14.19 JF/KD -1.08 13.11 5 17.54 14.26 JF/KD -1.09 13.17 6 18.27 14.89 JF/KD -1.19 13.70 7 18.53 15.31 JF/KD -1.26 14.05 8 18.54 15.30 JF/KD -1.26 14.04 9 18.56 15.28 JF/KD -1.25 14.03 10 18.67 15.39 JF/KD -1.27 14.12 12 18.91 15.63 JF/KD -1.31 14.32 14 19.12 15.84 JF/KD -1.35 14.49 16 19.28 16.00 JF/KD -1.38 14.62 18 19.45 16.17 JF/KD -1.41 14.76 20 19.58 16.30 JF/KD -1.43 14.87 25 19.79 16.51 JF/KD -1.47 15.04 30 19.98 | | 4 25 | | | 17.32 | 14.04 | מא/אז | -1.05 | | 12.99 | | - |
| 4.75 17.47 14.19 JF/KD -1.08 13.11 5 17.54 14.26 JF/KD -1.09 13.17 6 18.27 14.89 JF/KD -1.19 13.70 7 18.53 15.31 JF/KD -1.26 14.05 8 18.54 15.30 JF/KD -1.26 14.04 9 18.56 15.28 JF/KD -1.25 14.03 10 18.67 15.39 JF/KD -1.27 14.12 - 12 18.91 15.63 JF/KD -1.31 14.32 14 19.12 15.84 JF/KD -1.35 14.49 16 19.28 16.00 JF/KD -1.38 14.62 18 19.45 16.17 JF/KD -1.41 14.76 20 19.58 16.30 JF/KD -1.43 14.87 25 19.79 16.51 JF/KD -1.47 15.04 30 19.98 16.70 JF/KD -1.51 15.35 Stool tride <td><u> </u></td> <td>4.25</td> <td></td> <td></td> <td>17.32</td> <td>2.110</td> <td>JF/KD</td> <td></td> <td></td> <td></td> <td></td> <td></td> | <u> </u> | 4.25 | | | 17.32 | 2.110 | JF/KD | | | | | |
| 4.75 17.47 14.19 JF/KD -1.08 13.11 5 17.54 14.26 JF/KD -1.09 13.17 6 18.27 14.89 JF/KD -1.19 13.70 7 18.53 15.31 JF/KD -1.26 14.05 8 18.54 15.30 JF/KD -1.26 14.04 9 18.56 15.28 JF/KD -1.25 14.03 10 18.67 15.39 JF/KD -1.27 14.12 - 12 18.91 15.63 JF/KD -1.31 14.32 14 19.12 15.84 JF/KD -1.35 14.49 16 19.28 16.00 JF/KD -1.38 14.62 18 19.45 16.17 JF/KD -1.41 14.76 20 19.58 16.30 JF/KD -1.43 14.87 25 19.79 16.51 JF/KD -1.47 15.04 30 19.98 16.70 JF/KD -1.51 15.35 Stool tride <td></td> <td>4 50</td> <td></td> <td></td> <td>17 38</td> <td>14.10</td> <td>זה/עה</td> <td>-1.06</td> <td></td> <td>13.04</td> <td></td> <td>•</td> | | 4 50 | | | 17 38 | 14.10 | זה/עה | -1.06 | | 13.04 | | • |
| 5 17.54 14.26 JF/KD -1.09 13.17 6 18.27 14.89 JF/KD -1.19 13.70 7 18.53 15.31 JF/KD -1.26 14.05 8 18.54 15.30 JF/KD -1.26 14.04 9 18.56 15.28 JF/KD -1.25 14.03 10 18.67 15.39 JF/KD -1.27 14.12 12 18.91 15.63 JF/KD -1.31 14.32 14 19.12 15.84 JF/KD -1.35 14.49 16 19.28 16.00 JF/KD -1.38 14.62 18 19.45 16.17 JF/KD -1.41 14.76 20 19.58 16.30 JF/KD -1.43 14.87 25 19.79 16.51 JF/KD -1.47 15.04 30 19.98 16.70 JF/KD -1.51 15.19 | | 4.50 | | | 17.50 | | JI/KD | | | | ļ | |
| 5 17.54 14.26 JF/KD -1.09 13.17 6 18.27 14.89 JF/KD -1.19 13.70 7 18.53 15.31 JF/KD -1.26 14.05 8 18.54 15.30 JF/KD -1.26 14.04 9 18.56 15.28 JF/KD -1.25 14.03 10 18.67 15.39 JF/KD -1.27 14.12 12 18.91 15.63 JF/KD -1.31 14.32 14 19.12 15.84 JF/KD -1.35 14.49 16 19.28 16.00 JF/KD -1.38 14.62 18 19.45 16.17 JF/KD -1.41 14.76 20 19.58 16.30 JF/KD -1.43 14.87 25 19.79 16.51 JF/KD -1.47 15.04 30 19.98 16.70 JF/KD -1.51 15.19 | 1 | | | | 17 47 | 14.19 | מע/עז | -1.08 | | 13.11 | | |
| 6 18.27 14.89 JF/KD -1.19 13.70 7 18.53 15.31 JF/KD -1.26 14.05 8 18.54 15.30 JF/KD -1.26 14.04 9 18.56 15.28 JF/KD -1.25 14.03 10 18.67 15.39 JF/KD -1.27 14.12 12 18.91 15.63 JF/KD -1.31 14.32 14 19.12 15.84 JF/KD -1.35 14.49 16 19.28 16.00 JF/KD -1.38 14.62 18 19.45 16.17 JF/KD -1.41 14.76 20 19.58 16.30 JF/KD -1.43 14.87 25 19.79 16.51 JF/KD -1.47 15.04 30 19.98 16.70 JF/KD -1.51 15.19 | | 4./5 | | | 17.77 | | JF/KD | | | | | |
| 6 18.27 14.89 JF/KD -1.19 13.70 7 18.53 15.31 JF/KD -1.26 14.05 8 18.54 15.30 JF/KD -1.26 14.04 9 18.56 15.28 JF/KD -1.25 14.03 10 18.67 15.39 JF/KD -1.27 14.12 12 18.91 15.63 JF/KD -1.31 14.32 14 19.12 15.84 JF/KD -1.35 14.49 16 19.28 16.00 JF/KD -1.38 14.62 18 19.45 16.17 JF/KD -1.41 14.76 20 19.58 16.30 JF/KD -1.43 14.87 25 19.79 16.51 JF/KD -1.47 15.04 30 19.98 16.70 JF/KD -1.51 15.19 | | _ | | | 17 54 | 14.26 | יוא/או | -1.09 | | 13.17 | | |
| 7 18.53 15.31 JF/KD -1.26 14.05 8 18.54 15.30 JF/KD -1.26 14.04 9 18.56 15.28 JF/KD -1.25 14.03 10 18.67 15.39 JF/KD -1.27 14.12 12 18.91 15.63 JF/KD -1.31 14.32 14 19.12 15.84 JF/KD -1.35 14.49 16 19.28 16.00 JF/KD -1.38 14.62 18 19.45 16.17 JF/KD -1.41 14.76 20 19.58 16.30 JF/KD -1.43 14.87 25 19.79 16.51 JF/KD -1.47 15.04 30 19.98 16.70 JF/KD -1.51 15.19 | | 5 | | | 17.57 | | JI/KD | | | | | |
| 7 18.53 15.31 JF/KD -1.26 14.05 8 18.54 15.30 JF/KD -1.26 14.04 9 18.56 15.28 JF/KD -1.25 14.03 10 18.67 15.39 JF/KD -1.27 14.12 12 18.91 15.63 JF/KD -1.31 14.32 14 19.12 15.84 JF/KD -1.35 14.49 16 19.28 16.00 JF/KD -1.38 14.62 18 19.45 16.17 JF/KD -1.41 14.76 20 19.58 16.30 JF/KD -1.43 14.87 25 19.79 16.51 JF/KD -1.47 15.04 30 19.98 16.70 JF/KD -1.51 15.19 | | | | | 18 27 | 14.89 | ו מא/צו | -1.19 | | 13.70 | | |
| 7 18.53 -1.26 14.04 9 18.54 15.30 JF/KD -1.26 14.03 10 18.56 15.28 JF/KD -1.25 14.03 10 18.67 15.39 JF/KD -1.27 14.12 12 18.91 15.63 JF/KD -1.31 14.32 14 19.12 15.84 JF/KD -1.35 14.49 16 19.28 16.00 JF/KD -1.38 14.62 18 19.45 16.17 JF/KD -1.41 14.76 20 19.58 16.30 JF/KD -1.43 14.87 25 19.79 16.51 JF/KD -1.47 15.04 30 19.98 16.70 JF/KD -1.51 15.19 | | 6 | | | 10.27 | | - Jr/KD | | | | | |
| 7 18.53 -1.26 14.04 9 18.54 15.30 JF/KD -1.26 14.03 10 18.56 15.28 JF/KD -1.25 14.03 10 18.67 15.39 JF/KD -1.27 14.12 12 18.91 15.63 JF/KD -1.31 14.32 14 19.12 15.84 JF/KD -1.35 14.49 16 19.28 16.00 JF/KD -1.38 14.62 18 19.45 16.17 JF/KD -1.41 14.76 20 19.58 16.30 JF/KD -1.43 14.87 25 19.79 16.51 JF/KD -1.47 15.04 30 19.98 16.70 JF/KD -1.51 15.19 | | | | | | 15 31 | מע/עם | -1.26 | | 14.05 | | |
| 9 18.56 15.28 JF/KD -1.25 14.03 10 18.67 15.39 JF/KD -1.27 14.12 12 18.91 15.63 JF/KD -1.31 14.32 14 19.12 15.84 JF/KD -1.35 14.49 16 19.28 16.00 JF/KD -1.38 14.62 18 19.45 16.17 JF/KD -1.41 14.76 20 19.58 16.30 JF/KD -1.43 14.87 25 19.79 16.51 JF/KD -1.43 15.19 19.98 16.70 JF/KD -1.51 15.19 | | 7 | | · | 18.53 | 15.51 | JF/KD | | | | | |
| 9 18.56 15.28 JF/KD -1.25 14.03 10 18.67 15.39 JF/KD -1.27 14.12 12 18.91 15.63 JF/KD -1.31 14.32 14 19.12 15.84 JF/KD -1.35 14.49 16 19.28 16.00 JF/KD -1.38 14.62 18 19.45 16.17 JF/KD -1.41 14.76 20 19.58 16.30 JF/KD -1.43 14.87 25 19.79 16.51 JF/KD -1.43 15.19 19.98 16.70 JF/KD -1.51 15.19 | | _ | | | 10 5/ | 15 30 | ומא/שנו | -1.26 | | 14.04 | | |
| 10 | | - 8 | | | 10.34 | 13.30 | JI/KD | | | | | |
| 10 | 1 1 | _ | | | | | ומע/עם | -1.25 | | 14.03 | • | |
| 10 18.67 15.39 JF/KD -1.27 14.12 12 18.91 15.63 JF/KD -1.31 14.32 14 19.12 15.84 JF/KD -1.35 14.49 16 19.28 16.00 JF/KD -1.38 14.62 18 19.45 16.17 JF/KD -1.41 14.76 20 19.58 16.30 JF/KD -1.43 14.87 25 19.79 16.51 JF/KD -1.47 15.04 30 19.98 16.70 JF/KD -1.51 15.19 | | 9 | | | <u> 18.56</u> | _15.28 | JF/KD | | | | | |
| 10 | 1 | | | į | 70.57 | 15.00 | מע/שו | -1.27 | | 14.12 | | |
| 12 18.91 15.63 37/kb -1.35 14.49 14 19.12 15.84 JF/KD -1.35 14.49 16 19.28 16.00 JF/KD -1.38 14.62 18 19.45 16.17 JF/KD -1.41 14.76 20 19.58 16.30 JF/KD -1.43 14.87 25 19.79 16.51 JF/KD -1.47 15.04 30 19.98 16.70 JF/KD -1.51 15.19 | | 10 | | | 18.67 | 15,39 | JE/KD | | | | | |
| 12 18.91 15.63 37/kb -1.35 14.49 14 19.12 15.84 JF/KD -1.35 14.49 16 19.28 16.00 JF/KD -1.38 14.62 18 19.45 16.17 JF/KD -1.41 14.76 20 19.58 16.30 JF/KD -1.43 14.87 25 19.79 16.51 JF/KD -1.47 15.04 30 19.98 16.70 JF/KD -1.51 15.19 | | | | } | | | ופ/עם | -1.31 | j | 14.32 | | • |
| 14 19.12 15.84 37/kb -1.38 14.62 18 19.45 16.17 JF/KD -1.41 14.76 20 19.58 16.30 JF/KD -1.43 14.87 25 19.79 16.51 JF/KD -1.47 15.64 30 19.98 16.70 JF/KD -1.51 15.19 | | 12 | | | 18.91 | 15.63 | OF/KD | | - | | | |
| 14 19.12 15.84 37/kb -1.38 14.62 18 19.45 16.17 JF/KD -1.41 14.76 20 19.58 16.30 JF/KD -1.43 14.87 25 19.79 16.51 JF/KD -1.47 15.64 30 19.98 16.70 JF/KD -1.51 15.19 | 1 | | . | İ | | | ובי/אט | -1.35 | | 14.49 | | |
| 18 | | 1.4 | | | 19.14 | 15.84 | OF/KD | | | / | | |
| 18 | 1 1 | 10 | | . | 10 00 | | ומא/פון | -1.38 | l | 14.62 | | |
| 20 | | T.0 | | | 19.28 | 16.00 | 21/10 | | | | | |
| 20 | | 10 | | | | | מא/מו | -1.41 | | 14.74 | | |
| 20 | | TR | | | 19.45 | 16.17 | JI/KD | | | | | |
| 25 19.79 16.51 JF/KD -1.47 15.04 30 19.98 16.70 JF/KD -1.51 15.19 | 1 1 | | ļ | | 1 | | מע/פון | -1.43 | | 14.87 | • • | |
| 30 19.98 16.70 JF/KD -1.51 15.19 | | 20 | ,, | | 19.58 | 16.30 | JI/KD | | | | | |
| 30 19.98 16.70 JF/KD -1.51 15.19 | | | | | | | ומע/עה | - 1.47 | | الم. 15 | • | |
| 30 19.98 16.70 37.55 15.25 Stool tage | | 25 | | | 19.79 | 16.51 | 3F/KU | | | | | |
| 30 19.98 16.70 37.55 15.25 Stool tage | T | | | | 1 | | 15/170 | -1 51 | 1 | 15.19 | | |
| 35 20.20 16.89 JF/KD -1.54 15.35 Steel tape | | 30 | | | 19.98 | 16.70 | Jr/KD | 1.1 | | | | |
| 35 20.20 16.89 JF/KD 1.34 1 1333 Section Corp. | | - | | | | | 77 /200 | -15/ | | 15.35 | Stee1 | tape |
| | | 35 | | | 20.20 | 16.89 | JF/KD | 1,04 | 1 | | | [- |

GEE & JENSON MAINTERS ARCHITECTS PLANNERS, INC.

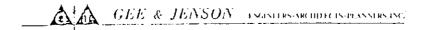
RECORD OF WATER LEVELS

Well No. 18-1D

roject 79-183 Acme Wells 18

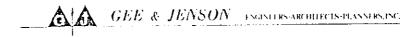
Starting date of Test 9/24/80 @ 1000

| 13.2 | | [1/2 + 22- | Lorral | (ft.) | l Draw- | Mea- | Adjustme | ante | |
|-----------------|-------|----------------|--------|-------|---------|-------|-------------------|--------|-----------------|
| ime | (min) | Water Held | Met | Below | 1 | sured | | Back- | Corrected |
| hr) | (min) | nera | wet | MP | (ft) | by | water- | | Drawdown Remark |
| | | | | 1,11 | (10) | | ing | Levels | (ft.) |
| | | [] | | | | | | | |
| | 41 | | | 20.30 | 16.99 | JF | ⁻ 1.56 | | 15.43 |
| | | | 1 | | | JF | | | ļ. |
| | 46 | | | 20.33 | 17.02 | J1 | ⁻ 1.57 | | 15.45 |
| | 51 | | | 20.37 | 17.06 | JF | -1 57 | | 15.49 |
| | | | | 20.37 | 17.00 | | -1.57 | | 10.49 |
| 1 | 61 | | | 20.58 | 17.27 | JF | -1.61 | | 15.66 |
| | | | | | | T77 | | | |
| | 71 | | | 20.58 | 17.27 | JF | -1.61 | · . | 15.66 |
| | 81 | İ | - | 20.65 | 17 2/ | JF | 1 (0 | | 15 74 |
| | OT | | | 20.03 | 17.34 | | -1.63 | | 15.71 |
| - 1 | 90 | 1 | [| 20.71 | 17.40 | JF | -1.64 | ļ | 15.76 |
| | | | | | | | 1:07 | | 13.10 |
| | 100 | | | 20.72 | 17.41 | JF | -1.64 | | 15.77 |
| _ | 100 | | | | | JF | | , | |
| 2 | 120 | · . | | 20.78 | 17.47 | Jr | -1.65 | | 15.82 |
| 1 | 150 | ļ | _ | 20.84 | 17.53 | JF | -1 (7 | | 15 06 |
| | 130 | | | 20.04 | 17.55 | | -1.67 | | 15.86 |
| 3 | 180 | | - | 20.86 | 17.55 | JE/KD | -1.67 | . } | 15.88 |
| | | | | | · | | | | |
| 4 | 240 | | | 20.95 | 17.64 | JE | -1.69 | | 15.95 |
| _ | 200 | | ļ | 21 05 | 177/ | | | 1 | |
| 5 | 300 | | | 21.05 | 17.74 | JE | -1.71 | | 16.03 |
| 6 | 360 | | | 21.11 | 17.80 | JE | -1.72 | | 16.08 |
| - | - 300 | | | | | 32 | 1./2 | | 10.00 |
| 7 | 420 | | | 21.22 | 17.91 | JE | -1.74 | | 16.17 |
| | | | | 21.00 | | | | | , |
| 8 | 480 | | | 21.23 | 17.92 | JF/KD | -1.74 | | 16.18 |
| 9 | 540 | | | 21.23 | 17.92 | | -1.74 | | 16.18 |
| - - | 340 | | | | 17.72 | JF/KD | 1.74 | | 10.10 |
| 0 | 600 | ŀ | | 21.22 | 17.91 | JF/KD | -1.74 | | 16.17 |
| | | | | | | | | | |
| 1 | 660 | | | 21.24 | 17.93 | JF/KD | -1.74 | | 16.19 |
| $\overline{1}$ | 200 | | | | 17.06 | | | | |
| 2 | 720 | | | 21.27 | 17.96 | JF/KD | -1.75 | | 16.21 |
| 3 | 780 | | | 21 20 | 17.98 | to | -1.75 | | 16.23 |
| | | | | 21.29 | | JF/KD | | | 10.23 |
| 4 | 840 | | | 21.32 | 18.01 | JF/KD | -1.76 | | 16.25 |



Well No. 18-1D

| | | | | | | _ | | | · |
|--|-------------|---------------|-------------|--------|---|--------------|-------------------|----------------|------------------|
| Time | | Water | Level | (ft.) | Draw- | Mea- | Adjustm | ents . | |
| (hr) | (min) | · | Wet | Below | l | sured | | Back- | Corrected |
| \\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\ | (1111) | | | MP | (ft) | by | water- | | Drawdown Remarks |
| | | | | | • | } ~~~ | ing | Levels | (ft.) |
| | <u></u> | | | | | | | | |
| 15 | 900 | ļ | | 01 26 | 18.05 <u>.</u> | KD/JF | -1.77 | | 16.28 |
| - | | | <u> </u> | 21.36 | 10.05 | KD/ 51 | 1 | | |
| 16 | 960 | | | | 17.96 | KD/JF | -1.75 | | 16.11 |
| 10 | 500 | - | | 21.27 | 17.90 | KD/ J1 | 1.5.7. | | |
| 17 | 1020 | | | | 17.99 | KD/JF | -1.76 | | 16.23 |
| | 1020 | | | 21.30 | 17.77 | KD/JT | 1.70 | | |
| 18 | 1080 | | | | 18.02 | KD/JF | -1.76 | | 16.26 |
| 10 | 1000 | | | 21.33. | 10.02 | KD/31 | 1.70 | | |
| 19 | 1140 | | | | 10.06 | KD/JF | -1.77 | | 16.29 |
| 19 | 1140 | | | 21_37 | 18.06 | VD/ 3.E | 1.// | | |
| 20 | 1200 | | | | 10.06 | un/te | _1 77 | | 16.29 |
| 20 | 1200 | | | 21.37 | 18.06 | KD/JF_ | -1.77 | - - | 10.25 |
| 1 ,, 1 | 3260 | | | | | O.D. | _1 70 | | 16.34 |
| 21 | 1260 | | | 21.43 | 18.12 | GR | -1.78 | - | 10.54 |
| | 1220 | | | | | | 1 70 | | 16.32 |
| 22 | 1320 | | | 21.41 | 18.10 | GR | - 1.78 | | 10.32 |
| 22 | 1200 | | } | İ | | | 1 | ļ | 16.38 |
| 23 | 1380 | · · · | | 21.48 | 18.17 | GR | - 1.79 | | 10.30 |
| | 7.40 | | | | j | ì | | İ | 16.34 |
| 24 | 1440 | | | 21.43 | 18.12 | GR . | -1.78 | | 10.34 |
| | | Ì | | | | | | 1 | 76 20 |
| 25 | 1500 | | | 21.48 | 18.17 | GR | -1.79 | | 16.38 |
| | _ | | | | 1 | | ļ | i | 16 20 |
| 26 | 1560 | | | 21.48 | 18.17 | GR | <u>-1.79</u> | | 16.38 |
| | | | | · | | ļ | | . | 26.42 |
| 27 | 1620 | | | 21.52 | 18.21 | GR | 1.80 | | 16.41 |
| | | | | | | | | , | |
| 28 | 1680 | | | 21.51 | 18.20 | GR | 1.80 | | 16.40 |
| | | | | | | | i | | |
| 29 | 1740 | | } | 21.58 | 18.27 | GR | 1.81 | | 16.46 |
| | | | | | | | | . • | |
| 30 | 1800 | | | 21.61 | 18.30 | GR | 1.82 | | 16.48 |
| | - | | 1 | | | | | | |
| 31 | 1860 | | | 21.57 | 18.26 | GR | 1.81 | | 16.45 |
| | | | | | | | | | |
| 32 | 1920 | | | 21.59 | 18,28 | GR | 1.82 | | 16.46 |
| - | | | | | | | | | |
| 33 | 1980 | | 1 | 21.65 | 18.34 | JF/KD | 1.83 | 1 | 16.51 |
| | - | | | | | | | 1. | |
| 34 | 2040 | ļ | | 21.62 | 18.31 | JF/KD | 1.82 | | 16.49 |
| | | } | | 21.02 | ±0.31 | | | | . |
| 35 | 2100 | . [| • | 22.89 | 19.58 | JF/KD | -2.09 | | 17.49 |
| | | | - | 24.07 | 17,70 | | | - | |
| 36 | 2160 |] | | 21 62 | 10 21 | JF/KD | -1.82 | | 16.49 |
| | | | | 21.63 | 18.31 | | ~,02 | | |



Well No. 18-1D

| rime | | Water | Level | (ft.) | .1 | i | | | |
|------|-------|--|-------|----------|-------|--------------|---------------|--------|----------------------------|
| (hr) | (min) | | Wet | Below | | sured | | | Corrected Drawdown Remarks |
| | | | | MP | (ft) | by | water- ing | Levels | pranacti |
| | | | | <u> </u> | | | | | |
| 37 | 2220 | | | 21.70 | 18.39 | JF/KD | -1.84 | | 16.55 |
| 38 | 2280 | | | 21.70 | 18.39 | JF/KD | -1.84 | | 16.55 |
| 39 | 2340 | | · | 21.73 | 18.42 | JF/KD | -1.84 | | 16.58 |
| 40 | 2400 | | | 21.76 | 18.45 | JF/KD | -1.85 | | 16.60 |
| 41 | 2460 | | | 21.75 | 18.44 | JF/KD | -1.85 | · | 16,59 |
| 42 | 2520 | | | 21.72 | 18.42 | JF/KD | -1.84 | | 16.58 |
| 43 | 2580 | · | | 21.75 | 18.44 | JF/KD | -1.85 | | 16.59 |
| 44 | 2640 | | | 21.82 | 18.51 | JF/KD | -1.86 | | 16.65 |
| 45 | 2700 | | | 21.83 | 18.52 | JE | -1.86 | | 16.66 |
| 46 | 2760 | | | 21.83 | 18.52 | JE | -1.86 | | 16.66 |
| 47 | 2820 | | | 21.86 | 18.55 | JE | -1.87 | | 16.68 |
| 48 | 2880 | | | 21.78 | 18.47 | JE | -1.85 | | 16.62 |
| 49 | 2940 | | | 21.80 | 18.49 | JE | -1.86 | | 16.63 |
| 50 | 3000 | | | 21.88 | 18.57 | JE | -1.88 | | 16.69 |
| 51 | 3060 | | | 21.86 | 18.55 | JE | -1.87 | | 16.68 |
| 52 | 3120 | | | 21.85 | 18.54 | JE | -1.87 | | 16.67 |
| 53 | 3180 | | | 21.88 | 18.57 | JE | -1.88 | | 16.69 |
| 54 | 3240 | | | 21.90 | 18.59 | JE | -1.88 | | 16.71 |
| 55 | 3300 | | | 21.91 | 18.60 | JE | -1.88 | | 16.72 |
| 56 | 3360 | | | 21.89 | 18.58 | JE | -1.88 | | 16.70 |
| 57 | 3420 | | | 21.90 | 18.59 | GR/MK | -1.88 | | 16.71 |
| 58 | 3480 | · _ | | 21.92 | 18.61 | GR/MK | -1.88 | | 16.73 |

Well No. <u>18-1D</u>

| | | | | | | | | | | _ |
|--|-------|-------------|-------|-------------|-------|----------|-------------|-------------|-------|---------------|
| Time | | Water | Level | (ft.) | Draw- | Mea- | | | ļ | |
| (hr) | (min) | | | Below | | sured | | Back- | Corre | |
| | | | | MP | (ft) | by | water- | | | wn Remarks |
| | | | | <u> </u> | | | ing | Levels | (ft. | |
| | | | | 23 04 | 19 63 | GR/MK | _ 1.89 | | 16.74 | |
| 59 | 3540 | | | 21.94 | 18.63 | GR/MK | - 1.09 | | 10.74 | |
| | 2600 | | | 21.97 | 18.66 | GR/MK | _1.89 | | 16.77 | |
| 60 | 3600 | | | 41.7/ | 10.00 | OIC/III | -1.0/ | | | |
| 61 | 3660 | | | 21.92 | 18.61 | GR/MK | _1.88 | | 16.73 | |
| -0.7 | 3000 | | | | | | | | | |
| 62 | 3720 | | | 21.92 | 18.61 | GR/MK | _1.88 | | 16.73 | |
| | | | | | | | | | | |
| 63 | 3780 | | | 21.91 | 18.60 | GR/MK | _1.88 | | 16.72 | |
| | | | | 01 00 | 10.50 | on har | 1.00 | | 16 72 | 1 |
| 64 | 3840 | | | 21.90 | 18.59 | GR/MK | _1.88 | | 16.71 | |
| | 2022 | | | 21.93 | 18.62 | GR/MK | _1.89 | | 16.73 | |
| 65 | 3900 | | | | 10.02 | , GR/FIR | - 1.09 | | 20.75 | |
| 1 | 2060 | ļ | | 21.95 | 18.64 | GR/MK | -1.89 | | 16.75 | |
| 66 | 3960 | | | 21.77 | 70.04 | OIC/ FIX | 1.07 | | -0.75 | |
| 67 | 4020 | ļ | | 21.96 | 18.65 | GR/MK | -1.89 | | 16.76 | |
| | | | | , | | | | | | |
| 68 | 4080 | | - | 21.97 | 18.66 | GR/MK | -1.89 | | 16.77 | |
| | | | | | | | | | | |
| 69 | 4140 | | | 21.97 | 18.66 | GR/MK | -1.89 | | 16.77 | |
| | 1000 | | | 22 22 | 10.60 | OD Age | 1.00 | . | 16 70 | |
| 70 | 4200 | | | 22.00 | 18.69 | GR/MK | -1.90 | | 16.79 | 22.04 Tape |
| 71 | 4260 | } | 1 | 22.02 | 18.71 | GR/MK | -1.90 | - 1 | 16.81 | 22.11 M-Scope |
| - ' - | 4200 | | · | | | | | | | |
| 72 | 4320 | 1 | - | 22.08 | 18.70 | GR/MK | -1.90 | | 16.80 | M-Scope B |
| | | | | | | | | | | |
| | | | | . } | | | | | | |
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Well No. 18-1D

| Cime | | Water | Level | (ft.) | | Mea- | Adjustm | | | |
|------|-------|-------|--------|-------|----------|-------------|---------------|--------|--------|-------------------|
| (hr) | (min) | Held | Wet | Below | Recovery | sured by | De- water- | Back- | Correc | ted wn Remarks |
| | | | | MP | | l by | ing | Levels | | WII Remarks |
| REC | OVERY | 9/2 | 7/80 @ | 1000 | | MK | | | | M-Scope B |
| | | | | 22.08 | 18.70 | MK | -1.90 | | 16.80 | @ 0955 |
| | .25 | | | 14.29 | 10.91 | МК | - 0.62 | | 10.29 | |
| | .50 | | | 12.26 | 8.88 | MK . | -0.40 | | 8.48 | |
| | .75 | | .,, | 10.65 | 7.27 | MK | -0.26 | | 7.01 | _ |
| | 1.00 | | | 10.10 | 6.72 | MK | -0.22 | | 6.50 | |
| | 1.25 | | | 9.38 | 6.00 | MK | -0.17 | | 5.83 | |
| | 1.50 | | | 8.98 | 5.60 | MK | -0.15 | | 5.45 | |
| | 1.75 | | | 8.60 | 5.22 | MK | -0.13 | | 5.09 | |
| | 2.00 | | , | 8.38 | 5.00 | MK | -0.11 | | 4.89 | : |
| | 2.25 | | | 8.26 | 4.88 | MK | -0.11 | | 4.77 | |
| | 2.50 | | | 8.09 | 4.71 | MK | -0.10 | | 4.61 | |
| | 2.75 | | | 7.85 | 4.47 | MK | -0.09 | | 4.38 | |
| | 3.00 | | | 7.60 | 4.22 | MK | -0.08 | | 4.14 | - |
| | 3.25 | | | 7.51 | 4,13 | MK | -0.07 | | 4.06 | |
| | 3.50 | | | 7.35 | 3,97 | MK | - 0.07 | | 3.90 | |
| | 3.75 | | | 7.24 | 3.86 | MK | -0.06 | | 3.80 | |
| | 4.00 | | | 7.16 | 3.78 | MK | -0.06 | | 3.72 | |
| | 4.25 | | | 7.03 | 3.65 | МК | - 0.06 | | 3.59 | |
| | 4.50 | | | 6.96 | 3.58 | MK | - 0.05 | | .3,53 | |
| | 4.75 | | | 6.88 | 3.50 | MK | - 0.05 | | 3.45 | |
| | 5,00 | | | 6.77 | 3,39 | MK | -0.05 | | 3.34 | |

Well No. 18-1D

| Time Water Level (ft.) | | | | | | Mea- | | ents . | | | | |
|--------------------------|--------|----------|-------------|--------------|----------|-------|--------|--------|--------|---------------------------------------|--|--|
| (hr | | | | Below | Recovery | | | Back- | Correc | ted | | |
| | | | | MP | | by | water- | | | ry Remarks | | |
| R | #COVER | <u> </u> | | | | | ing_ | Levels | (It) | | | |
| | 6 | | | 6.52 | 3.14 | MK | -0.04 | | 3.10 | | | |
| | 7 | | | 6.30 | 2.92 | MK | -0.03 | | 2.89 | · | | |
| | 8 | | - | 6.09 | 2.71 | MK | -0.03 | | 2.68 | | | |
| | | | | 5.93 | 2.55 | MK | -0.02 | | 2.53 | | | |
| | 9 | | | 13.93 | | TIK | | | | | | |
| | 10 | | | 5.82 | 2.44 | MK | -0.02 | | 2.42 | | | |
| | 12 | | | 5.61 | 2.23 | MK | -0.02 | | 2.21 | · · · · · · · · · · · · · · · · · · · | | |
| | 14 | | | 5.43 | 2.05 | MK | -0.01 | | 2.04 | | | |
| _ | 16 | | | 5.29 | 1.91 | MK | -0.01 | | 1.90 | | | |
| | 18 | | | 5.15 | 1.77 | MK | -0.01 | | 1.76 | | | |
| | 20 | | | 5.00 | 1.62 | MK | -0,01 | | 1.61 | : | | |
| | 25 | | | 4.83 | 1.45 | MK | | | - | | | |
| | 30 | | | 4.68 | 1.30 | · MK | | | | | | |
| | 35 | | | 4.59 | 1.21 | MK | | | | | | |
| | 40 | | - | 4.50 | 1.12 | MK | | | | | | |
| | 45 | | | - 4.43 | 1.05 | MK | | | | | | |
| | 50 | | | 4.36 | 0.98 | MK | | | | | | |
| 1 | 60 | | | 4.28 | 0.90 | MK | | · | | | | |
| | 70 | | | 4.21 | 0.83 | MK | | | | | | |
| | 80 | | | 4.16 | 0.78 | MK | | | | | | |
| | 90 | | | 4.12 | 0.74 | MK | | | | | | |
| <u> —</u> | 100 | | | 4.10 | 0.72 | MK | | | | | | |
| 2 | 120 | | | 4.02 | 0.64 | MK | | | | | | |
| | 150 | | | 3.99 | 0.61 | MK | | | | | | |
| <u> </u> | 180 | | | 3.94 3.93 | 0.55 | MK MK | | | | 1-Scope B Tape | | |

Well No. 18-1D

| ime | | Water | Level | l (ft.) | 1 | Mea- | Adjustments | | | |
|-------------|--------|----------|-------|---------|-------------|-------|-------------|--------|--|---------|
| nr) | (min) | | Wet | Below | Recovery | sured | De- | Back- | | 7 |
| | - 1 | | | MP | | by | water- | ground | | Remarks |
| | | | | | · · · · · · | | ing | Levels | | |
| 4 | 240 | | | 3.85 | 0.54 | | | | | |
| 26 | 1560 | | | 3.77 | 0.46 | | | | | |
| 50.5 | 3030 | | | 3.78 | 0.47 | | | | | |
| | ! ! | | | | | | | } | | |
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2019 OKEECHOBEE BOULEVARD, WEST PALM BEACH, FLORIDA. . . 33409. . . 305 - 683-3301

FRED A. GREENE, P.E.
RICHARD M. MILLER, P.E.
WALTER O. STEPHENS, JR., P.E.
WILLIAM G. WALLACE, JR., P.L.S.
PHILIP A. CRANIELL JR., A.E.A.
JOHN C. W.SE, P.E.

Director Emerica H. C. GEE, P.E. THEODORE B. JENSON, P.E.

RECORD OF WATER LEVELS

Well No. 18-2D

| PIOJ | ect | 19-103 | Acine we | TT 10 | | roca | tion | | | | |
|-----------|--------|--------|----------|--------|---------|---------------|--------------|-----------------------------|--------------------|------------|-------------|
| Elev | ation_ | | | | MSL | Meas | uring F | oint | Тор о | f Casing | |
| Dist | ance t | o Pump | ed Wel | 1 | 130.0 | feet | Dischar | ge | 900 | | GPM |
| Tota | l Dept | :h | 90f∈ | et C | ased De | epth <u>0</u> | 70 | feet D | iameter | 2 | I |
| Star | ting D | ate of | Test_ | 9/24 | /80 @ | 1000 | | | | | · |
| - Time | | Wate | r Leve | 1 (ft) | Draw- | Mea- | Adjus | tments | 1 | Remarks | |
| | | Held |] | 1 | Down | sured | De- water | Back- - ground Levels | Correct Downdra | ₩ | |
| 740 | | | | 3.22 | | JF | | | | Таре | |
| | | | , | 3.24 | | JF | | | | M-Scope #4 | |
| 091 | | | | 3.24 | | JF | | | | | |
| 094 | | | | 3.24 | | JF | | | | | ٠ - د |
| | | | • | 3.25 | | GR | | | | | |
| | .25 | | | 3.53 | 0.28 | GR | 0.00 | | 0.28 | | • |
| | .50 | | - | 3.56 | 0.31 | GR | 0.00 | | 0.31 | | |
| | .75 | | | | · | | | | | | |
| | 1.00 | | | 5.25 | 2.00 | GR | -0.01 | | 1.99 | | |
| | 1.25 | | | 5.84 | 2.59 | GR | -0.02 | | 2.57 | | |
| | 1.5d | > | | 6.36 | 3.11 | GR | -0.04 | | 3.07 | | |
| | 1.75 | | | | | | | | | | |
| | 2.00 | | | 6.90 | 3.65 | GR | -0.06 | | 3.59 | | |
| | 2.25 | | | 7.05 | 3.80 | GR | -0.06 | | 3.74 | | |
| | 2.50 | | | 7.20 | 3.95 | GR | -0.07 | | 3.88 | | |
| | 2.75 | | | 7.37 | 4.12 | GR | -0.07 | | 4.05 | | |

GEE & JETSON ENGSERGAROUTECTSON INVERSING

RECORD OF WATER LEVELS

Well No. 18-2D____

| Time | | Water | Level | (£t.) | Draw- | Mea- | Adjustme | ents | Correct | ted |
|--------------|-------|-------|---------------|-------|---------------|-------|----------|------------------|--------------|------------|
| (hr) | (min) | | Wet | Below | | sured | De- | Back- ground | Decree | n Remarks |
| | | | | MP | (ft) | рÀ | water- | ground Levels | | |
| | | ļ | | | | | ing | TEAGTR | \ <u>\``</u> | |
| | 2 00 | | | 7 40 | 4.24 | GR | -0.08 | ! | 4.16 | |
| | 3.00 | | | 7.49 | 7 • 4 4 | بيب | | | | - |
| | 3.25 | | | 7.61 | 4.36 | GR | -0.08 | · | 4.28 | |
| | | | | | ; | | | | , | |
| | 3.50 | | | 7.71 | 4.46 | GR | -0.09 | | 4.37 | |
| | 2 7- | | | 7 00 | 4.55 | GR | -0.09 | 1 | 4.46 | |
| | 3.75 | | | 7.80 | | VIV | V. V. | | | |
| | 4.00 | | | 7.89 | 4.64 | GR | -0.10 | | 4.54 | |
| | | | | | | | | | , , , , | - |
| | 4.25 | | | 7.98 | 4.73 | GR | -0.10 | | 4.63 | |
| | 4.50 | | | 8 06 | 4.81 | GR | -0.11 | | 4.70 | |
| | 4.50 | | - | 8.06 | | OI. | | | } | |
| | 4.75 | | ا ا | 8.12 | 4.87 | GR | -0.11 | | 4.76 | |
| | | | | | | | | ļ | , 05 | |
| | 5 | | | 8.21 | 4.96 | GR | -0.11 | | 4.85 | |
| - | | T . | Ì | 8.50 | 5.25 | GR | -0.13 | | 5.12 | |
| | 6 | | | 0.00 | - د ۱۰۰۰ - | | 3,13 | | | |
| | 7 | | | 8.79 | 5.54 | GR | -0.14 | | 5.40 | |
| | | | | | | an l | . 0.16 | | 5 5/ | |
| | 8 | | | 8.97 | 5.72 | GR | -0.16 | | 5,56 | |
| | 9 | | ļ | 9.09 | 5.84 | GR | -0.16 | | 5.68 | |
| | 9 | | | 2.03 | | | | | | |
| | 10 | { | | 9.23 | 5.98 | GR | -0.17 | | 5.81 | |
| | | | | | | an l | 0.10 | | 5 00 | • |
| | 12 | | | 9.42 | 6.17 | GR | -0.18 | | 5.99 | |
| | 14 | | | 9.62 | 6.37 | GR | -0.20 | | 6.17 | · |
| | | | | | | | | | | |
| | 16 | | | 9.77 | 6.52 | GR | -0.21 | | 6.31 | |
| | | | | 2 2 - | | | 0.22 | | 6.44 | |
| | 18 | | | 9.91 | 6.66 | GR | -0.22 | | <u> </u> | |
| | 20 | | | 10.03 | 6.78 | GR | -0.23 | | 6.55 | |
| | 20 | | | 10.03 | | | | | | |
| | 25 | | | 10.25 | 7.00 | GR | -0.24 | | 6.76 | W.C. #1 |
| | | | | 10.46 | 7 10 | an T | 0.00 | | 6 02 | M-Scope #4 |
| | 30 | | | 10.44 | 7.19 | GR | -0.26 | | 6.93 | Tape |
| | 35 | | | 10.53 | 7.28 | GR | -0.26 | | 7.02 | • |
| | رد | | | | | | | . <u></u> | | |

GEE & JENSON ENGINEERS ARCHITECTS PLANSERS INC.

RECORD OF WATER LEVELS

Well No. 18-2D

| ime | | Water | Level | (f.t.); | Draw- | Mea- | Adjustme | ents | |
|-----|-------|----------|-------|---------|-------|--------|----------|--------|-----------|
| hr) | (min) | | | Below | | sured | De- | Back- | Corrected |
| ĺ | | | | MP | (£t) | by | water- | | 1 |
| | | | | | | | ing | Levels | (ft.) |
| | 40 | | • | 10.64 | 7.39 | GR | 0.27 | | 7.12 |
| | | | | | | | j | | |
| | 45 | <u> </u> | | 10.74 | 7.49 | GR | -0.28 | | 7.21 |
| | 50 | | | 10.77 | 7.52 | _GR | 0.28 | | 7.24 |
| 1 | 60 | | | 10.88 | 7.63 | _GR | -0.29 | | 7.34 |
| | 70 | | | 10.96 | 7.71 | GR | -0.30 | | 7.41 |
| | 80 | | | 11.00 | 7.75 | _GR | 0.30 | | 7.45 |
| | 90 | | | 11.04 | 7.79 | GR | -0.30 | | 7.49 |
| | 100 | | | 11.08 | 7.83 | GR | -0.31 | | 7.52 |
| 2 | 120 | | | 11.12 | 7.87 | GR | 0.31 | | 7.56 |
| | 150 | | | 11.18 | 7.93 | GR | 0.32 | | 7.61 |
| 3 | 180 | | | 11.21 | 7.96 | JE/KD | -0.32 | - | 7.64 |
| 4 | 240 | | | 11.24 | 7.99 | JE | -0.32 | | 7.67 |
| 5 | 300 | | | 11.32 | 8.07 | JE | -0.33 | | 7.74 |
| 6 | 360 | | | 11.35 | 8.10 | JE | -0.33 | | 7.77 |
| 7 | 420 | | | 11.39 | 8.14 | JE | -0.33 | | 7.81 |
| 8 | 480 | | | 11.41 | 8.16 | _JF/KD | _0.34 | | 7.82 |
| 9 | 540 | | | 11.41 | 8.16 | JF/KD | -0.34 | | 7.82 |
| .0 | 600 | | | 11.43 | 8.18 | JF/KD | 0.34 | | 7.84 |
| .1 | 660 | | | 11.42 | 8.17 | JF/KD | -0.34 | | 7.83 |
| .2 | 720 | | | 11.43 | 8.18 | JF/KD | -0.34 | | 7.84 |
| .3 | 780 | | | 11.44 | 8.19 | JF/KD | -0.34 | | 7.85 |
| . 4 | 840 | | | 11.46 | 8.21 | JF/KD | -0.34 | | 7.87 |

____ & GEE & JENSON | DESCRIBE ARCHITECTS DE ASSURS AND

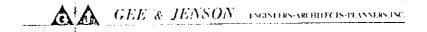
RECORD OF WATER LEVELS

Well No. <u>18-2D</u>

| Time | | Water | | | Draw- | | Adjustm | ents |
|------|-------|-------|-----|-------|-------|-------|---------------|---|
| (hr) | (min) | Held | Wet | Below | Down | sured | De- water- | Back- Corrected ground Drawdown Remarks |
| | • | | | MP | (ft) | by | ing | Levels (ft.) |
| | | | | | | | | |
| 15 | 900 | | | 11.48 | 8.23 | JF/KD | -0.34 | 7.89 |
| 16 | 960 | | | 11.41 | 8.16 | JF/KD | -0.34 | 7.82 |
| 17 | 1020 | | | 11.44 | 8.19 | JF/KD | -0.34 | 7.85 |
| 18 | 1080 | | | 11.46 | 8.21 | JF/KD | -0.34 | 7.87 |
| 19 | 1140 | | | 11.47 | 8.22 | JF/KD | -0.34 | 7.88 |
| 20 | 1200 | | | 11.50 | 8.25 | JF/KD | -0.34 | 7.91 |
| 21 | 1260 | | | 11.51 | 8.26 | GR | -0.34 | 7.92 |
| 22 | 1320 | | | 11.52 | 8.27 | GR | -0.35 | 7.92 |
| 23 | 1380 | | | 11.53 | 8.28 | GR | -0.35 | 7.93 |
| 24 | 1440 | | , | 11.56 | 8.31 | GR | -0.35 | 7.96 |
| 25 | 1500 | | | 11.55 | 8.30 | GR | -0.35 | 7.95 |
| 26 | 1560 | | | 11.53 | 8.28 | GR | -0.35 | 7.93 |
| 27 | 1620 | | | 11.56 | 8.31 | GR | -0.35 | 7.96 |
| 28 | 1680 | | | 11.57 | 8.32 | GR | -0.35 | 7.97 |
| 29 | 1740 | | | 11.58 | 8.33 | GR | -0.35 | 7.98 |
| 30 | 1800 | | | 11.61 | 8.36 | GR | -0.35 | 8.01 |
| 31 | 1860 | | | 11.60 | 8.35 | GR | -0.35 | 8.00 |
| 32 | 1920 | | | 11.59 | 8.34 | GR | -0.35 | 7.99 |
| 33 | 1980 | | | 11.63 | 8.38 | GR | -0.36 | 8.02 |
| 34 | 2040 | | | 11.62 | 8.37 | GR | -0.35 | 8.02 |
| 35 | 2100 | | | 12.14 | 8.89 | GR | -0.40 | 8.49 |
| 36 | 2160 | | | 11.73 | 8.48 | GR | -0.36 | 8.12 |

Well No. 18-2D

| | | 7.7 - 1 | T 1 | 1.61. | | | 1 | | · · · · · · · · · · · · · · · · · · · | |
|----------------|--|--------------|-----|--------|---|-------------|------------------|-------------|---------------------------------------|---------|
| Time | | Water | | | -1 | | | | | |
| (hr) | (min | Held | Wet | Below | 1 | sured | | | Correcte | |
| | | | | MP | (ft) | by | water- | | Drawdown | Remarks |
| | ļ <u>.</u> | | | ļ | | ļ | ing | Levels | (ft.) | |
| 37 | 2220 | | | 17.65 | | | | | | |
| | 2220 | | | 11.65 | 8.40 | JF/KD | -0.36 | l | 8.04 | |
| 38 | 2280 | | | 111 67 | 0.40 | | | | | |
| | 1 2200 | ļ | | 11.67 | 8.42 | JF/KD | -0.36 | · | 8.06 | |
| 39 | 2340 | | • | 11.68 | 0.40 | 777 / 777 | | | | |
| | | | | 111.00 | 8.43 | JF/KD | -0.36 | | 8.07 | |
| 40 | 2400 | | | 11.69 | 8.44 | TE/VD | 5.00 | | 8.08 | |
| | | } | | 11.05 | 0.44 | JF/KD | -0.36 | | 0.00 | |
| 41 | 2460 | | | 11.68 | 8.43 | JF/KD | -0.36 | [| 8.07 | |
| | | | | | 9.75 | JI/KD | -0.36 | | | |
| 42 | 2520 | 1 | | 11.68 | 8.43 | JF/KD | 0.36 | 1 | 8.07 | Ì |
| | | | | | | JI/KD. | -0-30 | <u> </u> | | |
| 43 | 2580 | İ | j | 11.69 | 8.44 | JF/KD | -0.36 | | 8.08 | |
| | | | | | | | -31-311 | | | |
| 44 | 2640 | | | 11.71 | 8.46 | JF/KD | -0, 36 | ľ | 8.10 | |
| | | | | | | | | | | |
| 45 | 2700 | İ | | 11.75 | 8.50 | JE | - 0. 37 | | 8.13 | |
| | - | | |] | | | | | | |
| 46 | 2760 | | , | 11.73 | 8.48 | JE | -0.36 | | 8.12 | |
| | | | | | | | | | | |
| 47 | 2820 | | | 11.75 | 8.50 | JE | -0.37 | | 8.13 | |
| | 0000 | | | | | | | | | |
| 48 | 2880 | | | 11.73 | 8.48 | JE | -0.36 | | 8.12 | |
| 4.0 | 20.40 | | | | | | | | | |
| 49 | 2940 | | | 11.73 | 8.48 | JE | -0.36 | | 8.12 | |
| - | 2000 | j | | | | i | | 1 | _ | |
| 50 | 3000 | | | 11.76 | 8.51 | JE | -0.37 | · | 8.14 | |
| 51 | 3060 | | | ,, ,, | | | | 1 | | |
| | 3000 | | | 11.75 | 8.50 | JE | -0.37 | | 8.13 | |
| 52 | 3120 | | | 11 7/ | 0.40 | | | | 0.10 | |
| | | | | 11.74 | 8.49 | JE | -0.37 | | 8.12 | |
| 53 | 3180 | ļ |] | 11.76 | 8.51 | | _ | | 8.14 | |
| | 27.00 | | | | 0. JT | JE | -0.37 | | 0.14 | |
| 54 | 3240 | | | 11.77 | 8.52 | 717 | | | 8.15 | |
| | 3240 | | | 11.// | 0.32 | JE | -0.37 | | 0.13 | |
| 55 | 3300 | j | 1 | 11.79 | 8.54 | | 0.07 | 1 | 8.17 | |
| | | | | | | JE | -0.37 | | J. 17 | |
| 56 | 3360 | | | 11.78 | 8.53 | JЕ | -0.27 | | 8.16 | |
| | | | | | | 317 | -0.37 | | 0.10 | |
| 57 | 3420 | |] | 11.78 | 8.53 | GR/MK | -0.27 | | 8.16 | |
| } - | | | | | | JI/III | -0.37 | | | |
| 58 | 3480 | } | | 11.82 | 8.57 | GR/MK | -0.37 | | 8.20 | |
| | | | L | 1 | · · - · · · · · · · · · · · · · · · · · | , | 0.37 | | | |



Well No. 18-2D

| | | | | | | | | | T | |
|------|------|-------|----------|----------------|----------|--------------|---------|--------|--------|--------------|
| Time | | Water | | | Draw- | | Adjustm | ents . | 0 | 1 |
| (hr) | | Held | Wet | Below | | sured | | Back- | Decree | rea no 1 |
| | | ! | ţ | MP | (£t) | by | water- | ground | /++/ | own Remarks |
| | 1 | | <u> </u> | | <u> </u> | | ing | Levels | (11) | + |
| 59 | 3540 | | | 11.82 | 8.57 | GR/MK | -0.37 | | 8.20 | |
| 60 | 3600 | | | 11.83 | 8.58 | GR/MK | -0.37 | | 8.21 | |
| 61 | 3660 | | | 11.82 | 8.57 | GR/MK | -0.37 | | 8.20 | |
| 62 | 3720 | | | 11.82 | 8.57 | GR/MK | -0.37 | | 8.20 | |
| 63 | 3780 | · | | 11.82 | 8.57 | GR/MK | -0.37 | | 8.20 | |
| 64 | 3840 | | | 11.81 | 8.56 | GR/MK | -0.37 | | 8.19 | |
| 65 | 3900 | | | 11.81 | 8.56 | GR/MK | -0.37 | | 8.19 | |
| 66 | 3960 | | | 11.81 | 8.56 | GR/MK | -0.37 | | 8.19 | |
| 67 | 4020 | | | 11.81 | 8.56 | GR/MK | -0.37 | _ | 8.19 | |
| 68 | 4080 | | | 11.82 | 8.57 | GR/MK | -0.37 | | 8.20 | |
| 69 | 4140 | | | 11.83 | 8.58 | GR/MK | -0, 37 | | 8.21 | |
| 70 | 4200 | | | 11.84 | 8.59 | GR/MK | -0.37 | - | 8.22 | |
| 71 | 4260 | | | 11.83 | 8.58 | GR/MK | -0.37 | | 8.21 | M-Scope #4 . |
| 72 | 4320 | | | 11.88 11.84 | 8.59 | GR/MK | -0.37 | | 8.22 | Tape |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
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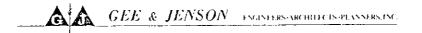


Well No. 18-2D

| | | 177 | T 1 | 161 | | 1 10 | 1 22: | | | · · · · · · · · · · · · · · · · · · · |
|------|-------------|-------------|----------------|--------------|-------------|---------------|--------|-----------------|----------|---------------------------------------|
| rime | | Water | Level Wet | | Recovery | Mea- sured | · | ents Back- | Carros | tod |
| (hr) | (min) | Held | wet | MP | Recovery | by | water- | | | ty Remarks |
| | | | | 1.15 | | Dy. | ing | Levels | | I Kemarks |
| | | | <u> </u> | | | | | | (-4-/ | |
| REC | OVERY | | | 11.88 | | | | | | M-Scope #4 |
| | | | | 11 00 | | | | | | |
| 001. | 10 | | | 11.88 | 8.59 | · | -0.37 | · | 8.22 | |
| | .25 | | | 11.66 | 8.37 | GR | -0.35 | | 8.02 | |
| | . 23 | | | 11.00 | 0.37 | GK | -0.33 | | 0.02 | |
| | .50 | | | 10.79 | 7.50 | GR | -0.28 | | 7.22 | |
| | 2.5 | | | | | , | | | | |
| | .75 | | | 10.10 | 6.81 | GR | -0.23 | | 6.58 | |
| | 1.00 | 1 | | 9.59 | 6.30 | GR | -0.19 | | 6.11 | |
| | | | | 7.37 | 0.30 | GK | -0.19 | | 0.11 | |
| _ [| 1.25 | | | 9.16 | 5.87 | GR | -0.16 | | 5.71 | |
| | | | | | | | - | | | |
| | 1.50 | | | 8.83 | 5.54 | GR | -0.14 | | 5.40 | |
| | 1.75 | | İ | 8.53 | 5.24 | GR | -0.13 | | 5.11 | |
| | /3 | | | 0.55 | 3.24 | GR | 0.15 | | J.TT | |
| | 2.00 | } | - | 8.26 | 4.97 | GR . | -0.11 | } | 4.86 | |
| | | | | | | | | | | |
| | 2.25 | | | 8.04 | 4.75 | GR | -0.10 | | 4.65 | |
| | 2.50 | | 1 | 7.85 | 4.56 | GR | -0.09 | | 4.47 | 1 |
| | | | | 7.03 | | OK . | 0.07 | | 4.4/ | |
| | 2.75 | } | | 7.70 | 4.41 | GR | -0.09 | | 4:47 | j |
| | | | | | | | | | | • |
| | 3.00 | | | 7.54 | 4.25 | GR | -0.08 | | 4.17 | |
| | 3.25 | | | 7.39 | 4.10 | GR | -0.07 | • | 4.03 | |
| | | | | | | OIL - | | | 7.03 | |
| | 3.5d | | | 7.28 | 3.99 | GR | -0.07 | | 3.92 | |
| | 2 7 1 | ĺ | | 7 7 7 | 2 22 | 0.0 | 0.06 | | | |
| | 3.75 | | | 7.17 | 3.88 | GR | -0.06 | | 3.82 | |
| ĺ | 4.00 | | | 7.08 | 3.79 | GR | -0.06 | 1 | 3.73 | |
| | 7.00 | | | | | | - | | 3.73 | |
| 1 | 4.25 | | | 6.96 | 3:67 | GR | -0.06 | | 3.61 | |
| | | | | 6 00 | 2 (0 | G.D. | 0.05 | | <u> </u> | |
| | 4.50 | | | 6.89 | 3.60 | GR | -0.05 | | 3.55 | |
| - | 4.75 | į | } | 6.82 | 3.53 | GR | -0.05 | | 3.48 | |
| - | | | | | | | | | | |
| | 5.00 | ŀ | | 6.70 | 3.41 | GR | -0.05 | | 3.36 | |
| | | | | | | | | | | |

Well No. 18-2D

| | | | | | | | - | - | τ | |
|------|--|--------------|-----|----------------|-------------|-------------|-------------|---------------|----------|-------------|
| Time | 2 | Water | | (ft.) |]_ | Mea- | | <u>ents</u> . | <u> </u> | |
| (hr | | Held | Wet | Below | Recovery | sured | | Back- | | dted |
| | | | | MP | | by | water- | ground | Recov | ery Remarks |
| R | COVER | <u> </u> | | | | | ing | Levels | (ft. | · |
| | | | | | | | | | 3.11 | |
| | 6 | | | 6.44 | 3.15 | GR | -0-04 | | 3.11 | |
| | 7 | 1 | | () | 2.95 | | 0.00 | | 2.92 | |
| | | | | 6.24 | 2.9. | GR—— | -0.03 | | | |
| | 8 | | | 6.05 | 2.76 | GR_ | -0.03 | : | 2.73 | |
| | 1 | | | | | | | | | |
| | 9 | | | 5,89 | 2.60 | GR | -0.02 | | 2.58 | |
| | | | • | | • | • | · | | 2 // | |
| | 10 | | | 5.75 | 2.46 | GR | -0.02 | | 2.44 | |
| | 12 | | | _{= ,} | 2.25 | | 0.00 | | 2.23 | [|
| | TZ | | | 5.54 | L. L. | GR | -0.02 | | | |
| | 14 | | j | 5.36 | 2.07 | GR_ | -0.01 | | 2.06 | |
| | | | | | | | | | | |
| | 16 | | | 5.27 | 1.98 | GR | -0.01 | | 1.97 | |
| | | | | | | | 1 | | 1 05 | |
| | 18 | | | 5.15 | 1.86 | GR | -0.01 | | 1.85 | |
| | 20 | 1 | | r 02 | 1.74 | (In | 0.01 | | 1.73 | |
| | 20 | | | 5.03 | 1.74 | GR | -0.01 | | 3.75 | |
| | 25 | | 1 | 4.77 | 1.48 | GR | 1 | | | |
| | | | | | | | | | | |
| | 30 | | | 4.61 | 1.32 | GR | | | | |
| | _ | | | | ÷ | | | | l | |
| | 35 | | | 4.50 | 1.21 | GR | | | | |
| | 40 | 1 | | . , , , | | CD. | | · | Ì | 1. |
| | 40 | | | 4.40 | 1.11 | GR | <u> </u> | | | |
| | 4.5 | |]. | 4.34 | 1.05 | GR | | | 1 | |
| | | | | 4.24 | 1.95 | | | | | M-Scope #4 |
| | 50 | | | 4.28 | 0.98 | GR | | | | Tape |
| | 60 | | | / 20 | | | | | | |
| 1 | 60 | | | 4.20 | 0.95 | GR | | | | |
| | 70 | | : | 4.11 | 0.06 | GR | | | | |
| | -,- | | | · · · · | 0.86 | GK | | | | |
| | 80 | | - | 4.06 | 0.81 | GR | 1 | } | | |
| | | | | | <u> </u> | | | | | |
| - 1 | 90 | | | 4.01 | 0.76 | GR | | | | |
| | 7.00 | | | 2.00 | | | | | 1 | |
| | 100 | | | 3.98 | 0.73 | GR | | | | |
| 2 | 120 | | | 3.82 | 0.57 | GR | | | | |
| | 120 | | | | 0.57 | GK | | | | |
| .] | 150 | | l | İ | | | ŧ | | 1 | |
| | | | | | | | | | | |
| 3 | 180 | | 1 | 1 | | | 1 | 1 | | |



Well No. 18-2D

| ime | | Water | Level | (ft.) | | . Mea- | Adjustm | ents . | 1 | 1 |
|------|-------|-------|-------|--------------|----------|-------------|---------|--------|---|---------------------------------------|
| hr) | (min) | | Wet | Below MP | Recovery | sured by | | Back- | | Remarks |
| 2.5 | 150 | | | 3.87 3.88 | 0.62 | HV | | | | Tape M-Scope |
| 3 | 180 | | | 3.81 | 0.56 | HV | | | | |
| 4 | 240 | | | 3.73 | 0.48 | JF | | | | |
| 26 | 1560 | | | 3.67 | 0.42 | JF | | | | |
| 50.5 | 3030 | | | 3.78 | 0.53 | JF | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| - | | | | | | | | | | |
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Project 79-183 Acme Well 18 Location Homeland Road

2019 OKEECHOBEE BOULEVARD, WEST PALM BEACH, FLORIDA. . . 33409. . . 305 - 683-3301

FRED A, GREENE, P.E.
RICHARD M, MILLER, P.E.
WALTER D STEPHENS, JR., P.E.
WILLIAM G, WALLACE, JR., P.L.S.
PHILIP A, CRANIELL JR., A.I.A.
JOHN C. WISE, P.E.

Elevation

Director Emeritor
H. C. GEE, P.E.
THEODORE B. JENSON, P.E.

RECORD OF WATER LEVELS

| Well | No. | 18-3D | |
|------|-----|-------|--|
| | | | |

MSL Measuring Point Top of Casing

| Dist | ance t | o Pump | ed Wel | 120 | 00.0 | feet 1 | Dischar | ge | | 900 | GPM |
|------|--------|-------------|--------|-------------|--------------|---------------|---------|-------------------------------|---------|---------|-------------|
| Tota | l Dept | h <u>90</u> | fe | et C | ased De | epth <u>(</u> | 0-702 | feet Di | ameter | 2 | |
| Star | ting D | ate of | Test_ | 9/24 | /80 @ | 1000 | | | | | |
| Time | | Water | Leve | 1 (ft) | | | | tments | | Remarks | |
| (hr) | (min) | Held | Wet | Below MP | Down (ft) | by | water- | Back- ground Levels | Drawdow | | |
| 0745 | | | | 3.08 | | JF_ | | | | Таре | |
| | | <u>-</u> | | 3.15 | | JF | | | | M-Scope | |
| 0911 | | | | 3.15 | | JF | | | | | · |
| 0944 | - | | | 3.15 | | JF | , | | | | |
| | | | | 3.16 | | _ | | | | | |
| | .25 | | | 3.28 | 0.12 | JE | | | 0.12 | | |
| | . 50 | | | 3.95 | 0.28 | JЕ | | | 0.28 | | |
| | .75 | | | 3.45 | 0.79 | JЕ | | | 0.79 | | |
| | 1.00 | | | 4.25 | 1.09 | JE | | | 1.09 | | |
| | 1.25 | | | 4.56 | 1.40 | JE | | | 1.40 | | |
| | 1.50 | • | | 4.81 | 1.65 | JЕ | -0.01 | | 1.64 | | |
| | 1.75 | | | 5.08 | 1.92 | JE | -0.01 | | 1.91 | | |
| | 2.00 | | | 5.25 | 2.09 | JE | -0.01 | | 2.08 | | |
| | 2.25 | | | 5.41 | 2.25 | JE | -0.02 | | 2.23 | | |
| | 2.50 | | | 5.54 | 2.38 | JE | -0.02 | | 2.36 | | |
| | 2.75 | | | 5.66 | 2.50 | JE | -0.02 | | 2.48 | | |

GEE & JEINON MANTER ARCHITECTS PLANS ROLLES

RECORD OF WATER LEVELS

Well No. 18-3D

| | | | | | | | | - | |
|--|-------|-------|-------|-------|-------|----------|---------|----------------|------------------|
| Time | | Water | Level | (ft.) | Draw- | Mea- | Adjustm | | |
| (hr) | (min) | | Wet | Below | | sured | De- | | Corrected |
| \ | • | | | MP | (£E) | рÀ | water- | | Drawdown Remarks |
| | | | | | | | ing_ | Levels | (ft) |
| | | | | | | | | | |
| | 3.00 | | | 5.81 | 2.65 | JE | -0.03 | | 2.62 |
| - | | | | | | | | | |
| | 3.25 | | | 5.89 | 2.73: | JE | -0.03 | | 2.70 |
| | | | | | | | ļ | | |
| 1 | 3.50 | | | 5.98 | 2.82 | JE | -0.03 | | 2.79 |
| | | | | | | | | | |
| | 3.75 | | | 6.05 | 2.89 | JE | -0.03 | | 2.86 |
| | | | | | - | | [| i | |
| | 4.00 | | | 6.15 | 3.00 | JE | -0.03 | | 2.97 |
| | | | | | | | | ĺ | |
| | 4.25 | | | 6.19 | 3.04 | JE | -0.04 | | 3.00 |
| | | | | } | | | | ļ | |
| | 4.50 | | | 6.27 | 3.12 | JE | -0.04 | - | 3.08 |
| | | | | | | | | - | |
| | 4.75 | | | 6.35 | 3.20 | JE | -0.04 | | 3.16 |
| | | | | | | | | | |
| | 5 | | | 6.40 | 3.25 | JE | -0.04 | | 3.21 |
| | } | İ | | | | | | | 2 / 5 |
| | 6 | | | 6.65 | 3.50 | JE | -0.05 | | 3.45 |
| | _ | į | | (00 | 2 72 | . | 0.06 | Ì | 2.67 |
| | 7 | | | 6.88 | 3.73 | JE | -0.06 | | 3.67 |
| | | 1 | - | 7.04 | 3.89 | TE | -0.06 | | 3.83 |
| | 8 | | | 7.04 | 3.09 | JE | -0.00 | | 3.03 |
| | | | | 7.17 | 4.02 | JE | -0.07 | | 3.95 |
| | 9 | | | | 4.02 | - JE | -0.07 | | |
| | 10 | | } | 7.27 | 4.12 | JE | -0.07 | | 4.05 |
| + | 10 | | | | | | | | |
| 1 1 | 12 | - | | 7.46 | 4.31 | JE | -0.08 | | 4.23 |
| | 14 | | | | | | | | |
| | 14 | | | 7.63 | 4.48 | JE | -0.09 | | 4.39 |
| } | | | | | | | | | |
| 1. | 16 | 1 | | 7.78 | 4.63 | JЕ | -0.10 | ţ | 4.53 |
| | | | | | | | | | |
| | 18 | | | 7.90 | 4.75 | JE | -0.10 | | 4.65 |
| | | | | | | | | | |
| | 20 | 1 | ł | 8.02 | 4.88 | JE | -0.11 | | 4.77 |
| | | | | | | | | | İ |
| | 25 | | 1 | 8.23 | 5.09 | JE | -0.12 | | 4.97 |
| | | | | | | | | | |
| | 30 | | | 8.41 | 5.27 | JE | -0.13 | | 5.14 |
| | | | | | | | | | - 0.5 |
| | 35 | | 1 | 8.53 | 5.39 | JE | -0.14 | | 5.25 |
| } | | + | | | | | | | • |

GEE & JENSON INCINIERS ARCHITECTS PLANNERS INC.

RECORD OF WATER LEVELS

Well No. 18-3D

| ime | | Water | Loval | (ft.) | Draw- | Hea- | Adjustmo | onts | | <u> </u> |
|-------|----------|---------------|---|-----------|--------|-----------|-------------|--------|----------|-------------|
| hr) | (min | 4 | | Below | .1 | sured | | | Correcte | ed |
| 111./ | (111.211 | 1,210 | 1 | MP | (ft) | by | water- | ground | Drawdown | Remarks |
| | | | | | | • | ing | Levels | (ft) | |
| | | | | | | | | | | |
| | 40 | | | 8.62 | 5.48 | JE | -0.14 | | 5.34 | |
| | 4.5 |] . | | | | | | | | |
| | 45 | <u> </u> | · · · · · · | 8.70 | 5.56 | JE | 70.15 | | 5.41 | |
| | 50 | | | 8.82 | 5.68 | JE | -0.15 | | 5.53 | |
| | | | - - | 0.02 | J.00 | <u>JE</u> | <u>U•1J</u> | | | |
| 1 | 60 | | | 8.85 | 5.71 | JE | -0.15 | | 5.56 | |
| | | | | | | | | | | |
| | 70 | | | 8.91 | 5.77 | JE | -0.16 | | 5.61 | |
| | 80 | | | 8.98 | F 92 | Yan | 0.16 | | F (3 | |
| | 80 | | | 0.90 | 5.83 | JE | -0.16 | | 5.67 | |
| | 90 | 1 | | 9.00 | 5.86 | . JE | -0.16 | | 5.70 | |
| | | | | | | | | | 3173 | |
| | 100 | | | 9.02 | 5.88 | JE · | -0.16 | | 5.72 | |
| | | | | | | | | | | |
| 2 | 120 | | | 9.06 | 5.92 | JE | -0.17 | | 5.75 | |
| - | 350 | | | 9.10 | 5.96 | 7.50 | 0 17 | Ì | F 70 | |
| | 150 | | | | 3.90 | JE | -0.17 | | 5.79 | |
| 3 | 180 | | 1 | 9.15 9.10 | 6.01 | JE | 70.17 | | T T | M-Scope |
| - | | | | -9.10 | 0.01 | JE _ | | | 2.04 | Tape |
| 4 | 240 | \$ | İ | 9.14 | 6.05 | JE | -0.18 | ļ | 5.87 | |
| | | | | | | | | | | |
| 5 | 300 | | | 9.20 | 6.11 | JE | -0.18 | | 5.93 | |
| | 260 | 1 | | 0.00 | | | | | | |
| 6 | 360 | | | 9.22 | 6.13 | JE | -0.18 | | 5.95 | |
| 7 | 420 | | 1 | 9.25 | 6.16 | JE | -0.18 | | 5.98 | |
| | | | | 7,23 | | <u> </u> | -0.10 | | | |
| 8 | 480 | | | 9.30 | 6.14 | JF/KD | -0.18 | | 5.96 | |
| | | | | | | | | | | |
| 9 | 540 | | | 9.30 | 6.14 | JF/KD | 0.18 | | 5.96 | |
| | 600 | Ì | | 0.00 | | , | | | | |
| LO | 600 | | | 9.30 | 6.14 | JF/KD | 0.18 | | _5.96 | |
| u | 660 | | | 9.28 | 6.12 | JF/KD | -0.18 | | 5.94 | |
| | | | | -7.20 | · V.12 | JE/KD | 0.10 | | J. 74 | |
| L2 | 720 | | | 9.28 | 6.12 | JF/KD | -0.18 | | 5,94 | |
| | | | · • • • • • • • • • • • • • • • • • • • | | | | | | | |
| L 3 | 780 | | | 9.31 | 6.15 | JF/KD | -0.18 | | 5.97 | |
| 14 | 0.40 | | | 0 27 | | | | | | • |
| L 4 | 840 | | | 9.31 | 6.15 | JF/KD | -0.18 | | 5.97 | |

GEE & JEASON INVESTIGATION OF THE STREET

RECORD OF WATER LEVELS

Well No. 18-3D

| Time | | Water | Level | | . / | Mea- | | | | |
|--|-------------|-------------|-------|-------|---------|---------------------------------------|--------|------------------|------------------|--------------|
| (hr) | (min | Held | Wet | Below | | sured | | | Correct | |
| | | | | MP | (ft) | рy | water- | ground Levels | Drawdown (ft) | Remarks |
| | | <u> </u> | | - | <u></u> | | 1119 | Tever2 | (ILC) | |
| 15 | 900 | } | | 9.33 | 6.17 | JF/KD | -0.18 | | 5.99 | |
| | | | | | | | | | | |
| 16 | 960 | | | 9.30 | 6.14 | _JF/KD_ | -0.18 | | 5.96 | |
| 17 | 1020 | | | 0 22 | (16 | · · · · · · · · · · · · · · · · · · · | -0.18 | | 5.98 | |
| 1./ | 1020 | | | 9.32_ | 6.16 | _JF/KD_ | T-V-18 | | 3.98 | |
| 18 | 1080 | } | | 9,33 | 6.17 | _JF/KD | -0.18 | | 5.99 | |
| 7.0 | 2.1.4.0 | | | | | | | | | |
| 19 | 1140 | | | 9.34 | 6.18 | _JF/KD_ | -0.18 | | 6.00 | <u> </u> |
| 20 | 1200 | | | 9.37 | 6.21 | JF/KD | -0.19 | | 6.02 | |
| | | | | | | | | | | |
| 21 | 1260 | | | 9.36 | 6.20 | GR | -0.19 | | _6_01 | |
| 22 | 1320 | | | 9.37 | 6.21 | GR | -0.19 | | 6.02 | |
| | 1020 | | | 7.31 | 0,21 | GR | 0.13 | | | |
| 23 | 1380 | | | 9.37 | 6.21 | GR | -0.19 | | 6.02 | |
| 24 | 1440 | | | | | | | | | |
| 24 | | | | 9.37 | 6.21 | GR | -0.19 | | 6.02 | |
| 25 | 1500 | | | 9.40 | 6.24 | GR | -0.19 | | 6.05 | |
| | 7.5.5 | | | | | | | | | |
| 26 | 1560 | | | 9.40 | 6.24 | GR | -0.19 | | 6.05 | |
| 27 | 1620 | | ľ | 9.41 | 6.25 | GR | -0.19 | } | 6.06 | |
| | | | | | | | | | | |
| 28 | 1680 | | | 9.43 | 6.27 | GR | -0.19 | | 6.08 | |
| 29 | 1740 | | | 9.43 | 6.27 | GR . | -0.19 | | 6.08 | |
| | | | | 7.73 | 0.27 | CIL | 0.17 | | 0.00 | |
| 30 | 1800 | | | 9.45 | 6.29 | GR | -0.19 | | 6.10 | |
| 31 | 1860 | | | 0.75 | 6 20 | an. | 0.10 | | (10 | |
| 21 | 1000 | | | 9.45 | 6.29 | GR | -0.19 | | 6.10 | |
| 32 | 1920 | ľ | | 9.45 | 6.29 | GR | -0.19 | | 6.10 | |
| | 1000 | | | | | | | | | |
| 33 | 1980 | | | 9.48 | 6.32 | JF/KD | -0.19 | | 6.13 | |
| 34 | 2040 | | | 9.48 | 6.32 | JF/KD | -0.19 | | 6.13 | |
| | | | | | | -5-, 10 | | | | ····· |
| 35 | 2100 | | | 9.85 | 6.69 | JF/KD | -0.22 | | 6.47 | |
| 3.0 | 2160 | | | 0 50 | 6 (2) | TD /275 | 0.20 | | 6 22 | • |
| 36 | 2160 | | | 9.58 | 6.42 | JF/KD | -0.20 | | 6.22 | |

Well No. 18-3D

| | | 1.1.2.4.2.15 | Tarral | / E L | J D. | Man | 1 7 3 3 4 5 5 | | | |
|-------------|-------|--------------|--------------|------------------|------------|--------------|---------------|-------------|---|--------------|
| ime | | | Level | (ft.) Below | _ 1 | Mea- sure | | | Correct | ođ |
| (hr) | (min) | пета | Wet | MP | (ft) | by | | i | | n Remarks |
| | | | | FIF | (10) | l by | ing | Levels | | 1 Kemarks |
| | | | | | | | 1,119 | nevers | 110 | |
| 37 | 2220 | | | 9.52 | 6.36 | JF/KD | -0.20 | | 6.16 | , |
| | | | | 7.72 | <u> </u> | J-7KD | 1 0.20 | | | |
| 38 | 2280 | | | 9.53 | 6.37 | JF/KD | _0.20 | l İ | 6.17 | |
| | 0.740 | | | | | | | | | • |
| 39 | 2340 | | <u>.</u> | 9.53 | 6.37 | JF/KD | -0.20 | | 6.17 | |
| 40 | 2400 | | | 0 53 | (27 | TE/VD | 0.20 | | (17 | ; |
| 40 | 2400 | | | 9.53 | 6.37 | JF/KD | -0.20 | | 6.17 | |
| 41 | 2460 | | | 9.53 | 6.37 | JF/KD | -0.20 | | 6.17 | . <u>-</u> . |
| | | | | | 0.37 | O Z / RD | 0.20 | | | |
| 42 | 2520 | | | 9.53 | 6.37 | JF/KD | -0.20 | | 6.17 | |
| | | | | | | | | | | |
| 43 | 2580 | | | 9.53 | 6.37 | JF/KD | -0.20 | | 6.17 | |
| | 2640 | | | ٠., | 6 (0 | / | 2.00 | , | | |
| 44 | 2640 | | | 9.56 | 6.40 | JF/KD | -0.20 | | 6.20 | |
| 45 | 2700 | ĺ | | 9.58 | 6.42 | JE | -0.20 | İ | 6.22 | |
| 4) | 2700 | | | | 0.42 | | -0.20 | | 0.22 | |
| 46 | 2760 | | _ | 9.56 | 6.40 | JE | -0.20 | | 6.20 | |
| | | | | | | | | | | |
| 47 | 2820 | 1 | | 9.56 | 6.40 | JE | -0.20 | | 6.20 | |
| | | | | | | | | | | |
| 48 | 2880 | | | 9.57 | 6.41 | JE | -0.20 | | 6.21 | |
| 4.0 | 2040 | | | 0 56 | 6.40 | TE | -0.20 | ļ | 6.20 | |
| 49 | 2940 | | | 9.56 | 0.40 | JE | 0.20 | | 0.20 | |
| 50 | 3000 | 1 | | 9.58 | 6.42 | JE | -0.20 | | 6.22 | - |
| - | | | | | | | | | | |
| 51 | 3060 | | | 9.59 | 6.43 | JE | -0.20 | | 6.23 | |
| | | | | | | | | | | |
| 52 | 3120 | | | 9.59 | 6.43 | JE | -0.20 | | 6.23 | |
| | | | | 0.50 | 6.40 | TY7 | -0.30 | | ()) | |
| 53 | 3180 | | | 9.59 | 6.43 | JE | -0.20 | | 6.23 | |
| 54 | 3240 | | | 9.60 | 6.44 | JE | -0.20 | į | 6.24 | |
| 34 | 3240 | | | | | | | | | |
| 55 | 3300 | | | 9.62 | 6.46 | JE | -0.20 | | 6.26 | |
| | | | | | | | | | | |
| 56 | 3360 |] | | 9.62 | 6.46 | JE | -0.20 | | 6.26 | |
| | | | | | | 22 (11 | | | () = | |
| 57 | 3420 | | | 9.61 | 6.45 | GR/MK | -0.20 | | 6.25 | |
| ۲,0 | 2400 | | | 9.63 | 6.47 | GR/MK | -0.20 | | 6.27 | |
| 58 | 3480 | | | 7.03 | 0.47 | OW PIK | 0.20 | | 0.21 | |

Well No. <u>18-3D</u>

| Time | | Water | Level | (ft.) | Draw- | Mea- | Adjustm | ents . | | |
|--------------|-----------|--------------|-------------|--------------|--------------|------------|---------|-------------|----------|--------------|
| (hr) | | | | Below | Down | sured | | Back- | Corre | dted |
| 1/117/ | (111,211, | 1 nera | ,,,,,, | MP | (ft) | bу | water- | around | Drawdo | wn Remarks |
| 1 | j | | | 111 | (10) | ω_I | ing | Levels | | |
| | | | | | | | 1119 | nevers | (20) | |
| 1 | | | | | | | | | | |
| 59 | 3540 | ļ . | | 9.65 | 6.49 | GR/MK_ | -0,20 | | 6.29 | |
| | 1 | | | | | | | | | |
| 60 | 3600 | | | 9.67 | 6.51 | GR/MK | -0.21 | | 6.30 | |
| | | | <u> </u> | | | | | | | |
| 6.1 | 3660 | | | 9.65 | 6.49 | CD /MZ | -0.20 | | 6.29 | |
| 61 | 3000 | ļI | | 9.63 | 0.49 | GR/MK | -0.20 | | 0.49 | |
| | 1 | 1 1 | | | | | | ļ | | |
| 62 | 3720 | | | 9.64 | 6.48 | GR/MK | -0.20 | | 6.28 | ļ |
| | | [| | | | ; | | | | |
| 63 | 3780 | | | 9.64 | 6.48 | GR/MK | -0.20 | | 6.28 | |
| | | | | | | | | | | |
| 64 | 3840 |] | | 9.64 | 6.48 | GR/MK | -0.20 | | 6.28 | |
| 04 | 3040 | | | 9.04 | 0.40 | GR/TIK | 0.20 | | <u> </u> | |
| 1 | | | | | | an /an- | | } | | |
| 65 | 3900 | | | 9.64 | 6.48 | GR/MK | -0.20 | | 6.28 | |
| | | | | | | | | · | | |
| 66 | 3960 | 1 | | 9.63 | 6.47 | GR/MK | -0.20 | | 6.27 | |
| | | | | | | | | | | |
| 67 | 4020 | · . | | 9.64 | 6.48 | GR/MK | -0.20 | ļ | 6.28 | |
| <u> </u> | 4020 | - | | 7.07 | 0.40 | ORTH | 0.20 | | 0.20 | |
| | 4000 | | _ | 0 65 | ((0 | OD Arr | 0.00 | ļ | c 20 | |
| 68 | 4080 | | | 9.65 | 6.49 | GR/MK | -0.20 | | 6.29 | |
| | | |] | | | | } | | | |
| 69 | 4140 | | 1 | 9.65 | 6.49 | GR/MK | -0.20 | | 6.29 | · |
| | | | | | | | - | | | |
| 70 | 4200 | 1 | | 9.66 | 6.50 | GR/MK | -0.21 | 1 | 6.29 | |
| | - | | | | | | | | | |
| 71 | 4260 | Į. | | 9.66 | 6.50 | CD /MZ | _0 21 | } | 6.29 | |
| | 4200 | | | | 0.50 | GR/MK | -0.21 | | 0.29 | |
| | | 1 | | 9.67 | | . | | | | Tape - |
| 72 | 4320 | ſ | | 9.73 | 6.51 | GR/MK | -0.21 | | 6.30 | M-Scope - 1 |
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Wel

Well No. 18-3D

| rime | | Water | Level | (ft.) | Ţ <u>.</u> | Mea- | Adjustm | ents . | T | 1 |
|------|-------|-------|-------|-------|------------|------|---------|--------|------|-------------------|
| (hr) | | Held | Wet | | Recovery | i i | | Back- | | ted ry Remarks |
| | | | | | | | ing | Levels | | |
| REC | OVERY | | | | | | | | | |
| 9: | 56 | | | 9.73 | 6.60 | JE | -0.21 | | 6.39 | |
| | .25 | | | 9.60 | 6.47 | JE | -0.20 | | 6.27 | |
| | .50 | | | 9.39 | 6.26 | JE | -0.19 | | 6.07 | |
| | .75 | | | 9.10 | 5.97 | JE . | -0.17 | | 5.80 | |
| | 1.00 | | | 8.76 | 5.63 | JE | -0.15 | | 5,48 | |
| | 1.25 | | | 8.45 | 5.32 | JE | -0.13 | | 5.19 | |
| | 1.50 | | | 8.18 | 5.05 | JE | -0.12 | | 4,93 | |
| | 1.75 | | | 8.01 | 4.88 | JE | -0.11 | | 4,77 | |
| | 2.00 | | - | 7.80 | 4.67 | JE . | -0.10 | | 4.57 | |
| | 2.25 | | | 7.60 | 4.47 | JE | -0.09 | | 4.38 | |
| | 2.50 | | | 7.45 | 4.32 | JE | -0.08 | | 4.24 | <u>.</u> |
| | 2.75 | | - | 7.31 | 4.18 | JE | -0.08 | | 4.10 | |
| | 3.00 | | | 7.16 | 4.03 | JE | -0.07 | | 3.96 | • |
| | 3.25 | | | 7.06 | 3.93 | JE | -0.07 | | 3.86 | |
| | 3.50 | | | 6.95 | 3.82 | JE | -0.06 | | 3.76 | |
| | 3.75 | | | 6.85 | 3.72 | JE | -0.06 | | 3.66 | |
| | 4.00 | | | 6.76 | 3.63 | JE | -0.05 | | 3,58 | |
| | 4.25 | | | 6.67 | 3.54 | JE | -0.05 | | 3.49 | |
| | 4.50 | | | 6.60 | 3.47 | JE | -0.05 | | 3.42 | |
| | 4.75 | | | 6.52 | 3.39 | JE | -0.05 | | 3.34 | |
| | 5.00 | | | 6.45 | 3.32 | JE | -0.04 | | 3.28 | • . |

Well No. <u>18-3D</u>

1

| | | 1 | _ | (F 1 \ | 1 | Mea- | Adjustm | onte | j |
|-------------|-------|-------|---------------|---------|----------|-------------|---------|--------|---------------------|
| Time | | Water | | (ft.) | Recovery | sured | | Back- | Corrected |
| (hr) | (min | Held | wet | MP | Recovery | by | water- | ground | Recovery Remarks |
| D | COVER | ↓ | | 111 | | | ing | Levels | |
| | | | | 6.21 | 3.08 | JE | -0.04 | | 3.04 |
| | 6 | | | - | | | | | |
| | 7 | | · | 6.02 | 2.89 | JE | -0.03 | | 2.86 |
| | 8 | | | 5.86 | 2.73 | JE | -0.03 | | 2.70 |
| | 9 | | | 5.70 | 2.57 | JE | -0.02 | | 2.55 |
| | 10 | | · | 5.59 | 2.46 | JE . | -0.02 | | 2.44 |
| | 12 | | | 5.37 | 2.24 | JE | -0.02 | | 2.22 |
| | 14 | | | 5.22 | 2.09 | JE | -0.01 | | 2.08 |
| | 16. | | | 5.17 | 2.04 | JЕ | -0.01 | | 2.03 |
| | 18 | | | 4.96 | 1.83 | JE | -0.01 | | 1.82 |
| | 20 | | _ | 4.86 | 1.73 | JE | -0.01 | | 1.72 |
| | 25 | | | 4.66 | 1.53 | JE | -0.00 | | 1.53 |
| | 30 | | | 4.51 | 1.38 | JE | - | | |
| | 35 | | | 4.40 | 1.27 | JE | | | |
| | 40 | | • | 4.31 | 1.18 | JE | · | | - |
| | 45 | | | -4.24 | 1.11 | JE | | | |
| | 50 | | | 4.18 | 1.05 | JE | | | · · |
| 1 | 60 | | | 4.11 | 0.98 | JE | : | | |
| | 70 | | | 4.05 | 0.92 | JE | | | |
| | 80 | | | 4.00 | 0.87 | JE | | | |
| | 90 | | | 3.94 | 0.81 | JE | | | |
| | 100 | | | 3.91 | 0.78 | JE | | | |
| 2 | 120 | | | 3.86 | 0.73 | JE | | | |
| | 150 | | | 3.80 | 0.67 | JE | | | |
| 3 | 180 | | | 3.77 | 0.64 | JE | | | M-Scope - 1 Tape |

Well No. 18-3D

| roject | 79-183 | Acme | Well 18 | • | Starting | date | of | Test | 9/24/80 | @ 1000 | |
|--------|--------|------|---------|---|----------|------|----|------|---------|--------|---|
| | | | | | _ | | | _ | | | _ |

| ime | | Water | Level | (ft.) | | Mea- | | ents | 1 | |
|---------------|-------------|-------|-------|-------------|----------|-------------|----------------------|---------------------------------------|---|---------|
| hr) | (min) | | Wet | Below MP | Recovery | sured by | De- water- ing | Back- | | Remarks |
| 4 | 240 | | · | 3.65 | 0.49 | JF | | | | |
| 26 | 1560 | | | 3.57 | 0.41 | JF | | | | |
| 50.5 | 3030 | - | | 3.58 | 0.42 | JF | - :- | | | |
| | ; ; | | | | | | | | | |
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| PROJECT_ | 79-183 | Acme Well 18 | LOCATION Homeland Road |
|----------|--------------|------------------|------------------------|
| | | : | |
| STARTING | DATE OF TEST | r 9/24/80 @ 1000 | |

| ī | ime | SG-1 | SG-2 | SG-3 | | |
|-------|-------|------|------|------|------|---------------------------------------|
| (hr) | (min) | (ft) | (ft) | (ft) | (ft) | Remarks |
| · | | 7.64 | 3.97 | 1,64 | - | @ 0730 |
| | | 7.64 | 3.95 | 1,66 | | @ 0920 |
| : | | 7.64 | 3.95 | 1.67 | | @ 0941 |
| 0 | 0 | | | 1.68 | | @ 1000 Start of Te |
| | 10 | | | 1.68 | | |
| | 35 | 7.65 | 3.94 | 1.70 | | |
| . 1 | 60 + | 7.65 | | 1.70 | | |
| . 2 | 120 | 7.66 | 3.95 | 1.72 | | |
| 3 | 180 | 7.68 | 3.94 | 1.75 | | · · · · · · · · · · · · · · · · · · · |
| 4 | 240 | 7.69 | 3,92 | 1.76 | | |
| 5 | 300 | 7.70 | 3.92 | 1.77 | - | |
| 6 | 360 | 7.71 | 3,92 | 1.79 | | |
| 7 | 420 | 7.72 | 3.92 | 1.80 | | |
| 8 | 480 | 7.73 | 3.92 | 1.81 | | |
| 9 | 540 | 7.74 | 3.92 | 1.82 | | |
| 10 | 600 | 7.75 | 3.92 | 1.83 | | |
| 11 | 660 | 7.76 | 3,92 | 1.85 | | |
| 12 | 720 | 7.77 | 3.92 | 1.85 | | |
| 13 | 780 | 7.78 | 3.92 | 1.85 | | |
| 14 | 840 | 7.78 | 3.92 | 1.84 | | |

| PROJECT | 79-183 | Acme Well | 18 | LOCATION | Homeland Road |
|----------|--------------|-----------|--------|----------|---------------|
| | | | • | | |
| STARTING | DATE OF TEST | 9/24/80 | @ 1000 | | |

| | | | | 99.2 | | |
|------|-----------|--------------|--------------|--------------|------|---------------------------------------|
| (hr) | ime (min) | SG-1 (ft) | SG-2 (ft) | SG-3 (ft) | (ft) | Remarks |
| | | | | | | |
| 15 | 900 | 7.79 | 3.92 | 1.84 | | |
| 16 | 960 | 7.80 | 3,92 | 1.85 | | |
| 17 | 1020 | 7.80 | 3.93 | 1.85 | | |
| 18 | 1080 | 7.81 | 3.93 | 1.86 | | |
| 19 | 1140 | 7.81 | 3.93 | 1.86 | | |
| 20 | 1200 | 7.82 | 3,93 | 1.86 | | |
| 21 | 1260 = | 7.82 | 3.93 | 1.86 | | · · · · · · · · · · · · · · · · · · · |
| 22 | 1320 | 7.82 | 3.93 | 1.87 | | |
| 23 | 1380 | 7.82 | 3,93 | 1.87 | | |
| 24 | 1440 | 7.82 | 3.92 | 1.85 | · | |
| 25 | 1500 | 7.82 | 3.92 | 1.85 | ` . | |
| 26 | 1560 | 7.82 | 3.92 | 1.84 | | |
| 27 | 1620 | 7.82 | 3.92 | 1.84 | | |
| 28 | 1680 | 7.82 | 3.92 | 1.83 | | |
| 29 | 1740 | 7.81 | 3.91 | 1.82 | | |
| 30 | 1800 | 7.80 | 3.90 | 1.82 | | |
| 31 | 1860 | 7.80 | 3.90 | 1.81 | | |
| 32 | 1920 | 7.80 | 3.90 | 1.80 | | |
| 33 | 1980 | 7.80 | 3.90 | 1,80 | | |
| 34 | 2040 | 7.80 | 3.90 | 1.79 | | |

| PROJECT_ | 79-183 | Acme Well | 18 | LOCATION | Homeland | Road | |
|----------|--------------|-----------|--------|----------|----------|------|------|
| | | | 4 | | | | |
| STARTING | DATE OF TEST | 9/24/80 | @ 1000 | | | | |

| | | | · · · · · · · · · · · · · · · · · · · | 1 | 1 | |
|---------|--------------|--------------|---------------------------------------|--------------|------|---------|
| (hr) | ime (min) | SG-1 (ft) | SG-2 (ft) | SG-3 (ft) | (ft) | Remarks |
| 35 | 2100 | 7.79 | 3.90 | 1.80 | 2 | |
| 36 | 2160 | 7.79 | 3.90 | 1.79 | | |
| 37 | 2220 | 7.78 | 3.89 | 1.79 | | |
| 38 | 2280 | 7.78 | 3.89 | 1.78 | | |
| 39 | 2340 | 7.78 | 3.88 | 1.77 | | |
| 40 | 2400 | 7.77 | 3.88 | 1.77 | | |
| 41 | 2460 | 7.77 | 3.88 | 1.77 | | |
| 42 | 2520 | 7.76 | 3.88 | 1.76 | - | |
| 43 | 2580 | 7.76 | 3.87 | 1.76 | | |
| 44 | 2640 | 7.76 | 3.87 | 1.76 | | |
| 45 | 2700 | 7.76 | 3.86 | 1.75 | | |
| 46 | 2760 | 7.75 | 3.86 | 1.75 | | |
| : 47 | 2820 | 7. 75 | 3.85 | 1.75 | | |
| 48 | 2880 | 7.75 | 3.85 | 1.75 | | |
| 49 | 2940 | 7.75 | 3.85 | 1.74 | | |
| 50 | 3000 | 7,75 | 3,85 | 1.74 | | |
| 51 | 3060 | 7,74 | 3.85 | 1.73 | | |
| 52 | 3120 | 7.73 | 3.84 | 1.73 | | |
| 53 | 3180 | 7.73 | 3.84 | 1.73 | | |
| 54 | 3240 | 7.72 | 3.84 | 1.72 | | |

| PROJECT 79-183 Acme Well | 18: | LOCATION Homeland Road | |
|-------------------------------|--------|------------------------|--|
| STADTING DATE OF TEST 9/24/80 | a 1000 | | |

| T | ime | SG-1 | SG-2 | SG-3 | | |
|------|-------|------|------|------|------|----------------|
| (hr) | (min) | (ft) | (ft) | (ft) | (ft) | Remarks |
| 55 | 3300 | 7.72 | 3.84 | 1.72 | • | |
| 56 | 3360 | 7.71 | 3.82 | 1.71 | | |
| 57 | 3420 | 7.71 | 3.82 | 1.73 | _ | |
| 58 | 3480 | 7.74 | 3.82 | 1.74 | | |
| 59 | 3540 | 7.74 | 3.82 | 1.74 | | |
| 60 | 3600 | 7.75 | 3.82 | 1.75 | | |
| 61 | 3660 | 7.75 | 3.82 | 1.76 | · | |
| 62 | 3720 | 7.76 | 3.83 | 1.76 | | |
| 63 | 3780 | 7.77 | 3.83 | 1.76 | | |
| 64 | 3840 | 7.77 | 3.83 | 1.76 | | |
| 65 | 3900 | 7.78 | 3.83 | 1,77 | | |
| 66 | 3960 | 7.78 | 3.83 | 1.77 | | |
| 67 | 4020 | 7.78 | 3.83 | 1.78 | | |
| 68 | 4080 | 7.78 | 3,84 | 1.78 | | |
| 69 | 4140 | 7.78 | 3.84 | 1.78 | | |
| 70 | 4200 | 7.78 | 3.85 | 1.78 | | |
| 71 | 4260, | 7.78 | 3.85 | 1.79 | | |
| 72 | 4320 | | | | | Pump shut off. |
| | | | | | | |
| | | | | | | |

| PROJECT 79-183 Acme Well 18 | LOCATION Homeland Road |
|--------------------------------------|---------------------------|
| METHOD OF MEASURING 5" x 6" orifice | AVERAGE DISCHARGE 900 GPM |
| STARTING DATE OF TEST 9/24/80 @ 1000 | |

| Ti (hr) | me (min) | Inches | Dis- charge (gpm) | Staff* Gage (ft) | Temp | Cond. (umhos/cm) | Mea- sured by | Remarks |
|------------|-------------|--------|-------------------------|------------------------|------|------------------|---------------------|---------|
| 1000 | .5 | | I (Spii) | (10) | (00) | (diaros) ciri) | | , |
| τούο | 1 | | | | | | SN | |
| | | | | | | <u>.</u> | | |
| | 1.5 | 53.5 | 900 | | | . <u> </u> | SN | |
| | 2 | | | | | | | |
| | 2.5 | 53.0 | 896 | | | | SN | |
| | 3.0 | 53.5 | 900 | | | | SN | |
| | 3.5 | 53.5 | 900 | | | | SN | |
| _ | 4.0 | 53.0 . | 896 | | | | SN | |
| | 4.5 | 53.0 | 896 | | | | SN | |
| | 5.0 | 53.5 | 900 | | | | SN | |
| | 6 | 53.5 | 900 | | | | SN | |
| | 7 | 53.5 | 900 | | | | SÑ | |
| | 8 | 53.5 | 900 | | | | SN | |
| | 9 | 53.5 | 900 | | | | SN | |
| | 10 | 53.5 | 900 | | | · | SN | |
| | 12 | 53.5 | 900 | | | | SN | |
| | 14 | 53.5 | 900 | | | | SN | |
| | 16 | 53.5 | 900 | | | | SN | |
| | 18 | 53.5 | 900 | | | | SN | |
| | 20 | _53.5 | 900 | | | | SN | |
| | 25 | | | | | | | |
| | 30 | 53.5 | 900 | | | | SN | |

^{*} See separate sheet for staff gage readings.

| PROJECT 79-183 Acme Well 18 | LOCATION Homeland Road |
|--------------------------------------|---------------------------|
| METHOD OF MEASURING 5" x 6" orifice | AVERAGE DISCHARGE 900 GPM |
| STARTING DATE OF TEST 9/24/80 @ 1000 | |

| Ti | me | | Dis- | Staff Gage | Temp | Cond. | Mea- sured | Remarks |
|------|------|---------|-----------------|---------------|---------|------------|---------------|---------|
| (hr) | | Inches | charge (gpm) | Gage (ft) | (oC) | (umhos/cm) | by | |
| | 35 | 53.5 | 900 | | <u></u> | | SN | |
| | 40 | 53.5 ′. | 900 | | | | SN | |
| | 45 | 53.5 | 900 | | | | SN | |
| | 50 | 53.5 | 900 | | | | SN | |
| 1 | 60 | 53.5 | 900 | | 32.0 | 780 | SN | |
| | 70 | 53.5 | 900 | | | | SN | |
| - | 80 | 53.5 | 900 | | | | SN | |
| | 90 | 53.5 | 900 | | | | SN | |
| | 100 | 53.5 | 900 | | | | SN | |
| 2 | 120 | 53.5 | 900 | | 25.0 | 780 | SN | · · · |
| | 150 | 53.5 | 900 | | | | JF | |
| 3 | 180 | 53.25 | 898 | | | 770 | GR | |
| 4 | 240 | 53.25 | 898 | | 27.2 | 820 | JE | |
| 5 | 300 | 53.5 | 900 | | 28.2 | 820 | JЕ | |
| · 6 | 360 | 53.5 | 900 | | 27.3 | 820 | JE | |
| 7 | 420 | 54.0 | 904 | | 26.8 | 820 | JE | |
| 8 | 480 | 53.5 | 900 | | 24.9 | 815 | JF | |
| 9 | 540 | 53.5 | 900 | | 24.1. | 810 | JF/KD | |
| 10 | 600 | 53.75 | 902 | | 24.0 | 795 | JF/KD | |
| 11 | 660 | 53.5 | 900 | | 24.0 | 795 | JF/KD | |
| 12 | 720_ | 53.75 | 902 | | 24.0 | 780 | JF/KD | |
| 13 | 780 | 53.5 | 900 | | 23.8 | 795 | JF/KD | |

| PROJECT 79-183 Acme Well 18 | LOCATION Homeland Road |
|--------------------------------------|---------------------------|
| METHOD OF MEASURING 5" x 6" orifice | AVERAGE DISCHARGE 900 GPM |
| STARTING DATE OF TEST 9/24/80 @ 1000 | |

| Time (hr) | | Inches | Dis- charge (gpm) | Staff Gage (ft) | Temp (oC) | Cond. (umnos/cm) | Mea- sured by | Remarks |
|------------|------|--------|-------------------------|-----------------------|--------------|---------------------|---------------------|---------|
| 14 | 840 | 53.5 | 900 | | 24.0 | 750 | JF/KD | |
| 15 | 900 | 54.0 | 904 | | 24.0 | 760 | JF/KD | |
| 16 | 960 | 53.0 | 896 | | 24.0 | 750 | JF/KD | |
| 17 | 1020 | 53.5 | 900 | | 23.9 | 720 | JF/KD | |
| 18 | 1080 | 53.5 | 900 | | 23.8 | 710 | JF/KD | |
| 19 | 1140 | 53.5 | 900 | | 23.9 | 720 | JF/KD | |
| 20 | 1200 | 53.5 | 900 | | 23.8 | 720 | JF/KD | |
| 21 | 1260 | 53.5 | 900 | | 23.7 | 720 | GR | |
| 22 | 1320 | 54.0 | 904 | | 24.0 | 715 | GR | |
| 23 | 1380 | 53.5 | 900 | | 25.0 | 710 | GR | |
| 24 | 1440 | 53.5 | 900 | | 25.5 | 720 | GR | |
| 25 | 1500 | 53.5 | 900 | | 26.5 | 720 | GR | |
| 26 | 1560 | 53.5 | 900 | | 27.0 | 760 | GR | |
| 27 | 1620 | 53.5 | 900 | | 27.5 | 7 70 | GR | |
| 28 | 1680 | 53.5 | 900 | | 26.0 | _800 | GR | |
| 29 | 1740 | 53.5 | 900 | | 26.5 | 830 | GR | |
| 20 | 1800 | 53.5 | 900 | | 26.0 | 830 | GR | |
| 31 | 1860 | 53.75 | 902 | | 26.0 | 825 | GR | |
| 32 | 1920 | 53.5 | 900 | | 25.5 | 780 | GR | |
| 33 | 1980 | 54.0 | 904 | - | 25.0 | _750 | GR _ | |
| 34 | 2040 | 53.25 | 898 | | 24.9 | _750 | GR | |
| 3 5 | 2100 | 58.0 | 934 | | | | GR | |

| PROJECT 79-183 Acme Well 18 | LOCATION Homeland Road |
|--------------------------------------|---------------------------|
| METHOD OF MEASURING 5" x 6" orifice | AVERAGE DISCHARGE 900 GPM |
| STARTING DATE OF TEST 9/24/80 @ 1000 | |

| . Ti | me | | Dis- | Staff | Temp | Cond. | Mea- | Remarks |
|------|------|---------------|-------------------------|--------------|--------------|-------------|-------------|---------------------------------------|
| (hr) | | Inches | Dis- charge (gpm) | Gage (ft) | (oC) | (umhos/cm) | sured by | Remarks |
| 36 | 2160 | 54.0 | 904 | | 24.3 | 995 | JF/KD | |
| 37 | 2220 | 53.25 '. | 898 | | 24.3 | 1005 | JF/KD | . <u></u> |
| 38 | 2280 | 53.5 | 900 | | 24.1 | 1000 | JF/KD | |
| 39 | 2340 | 53.5 | 900 | | 24.5 | 830 | JF/KD | · · · · · · · · · · · · · · · · · · · |
| 40 | 2400 | 53.5 | 900 | | 24.0 | 805 | JF/KD | |
| 41 | 2460 | 53.5 | 900 | | 24.1 | 795 | JF/KD | |
| 42 | 2520 | 53.0 | 896 | | 24.0 | 800 | JF/KD | |
| 43 | 2580 | 53.0 | 896 | | 24.0 | 800 | JF/KD | |
| 44 | 2640 | 53.75 | 902 | | 23.9 | 740 | JF/KD | |
| 45 | 2700 | 53.5 | 900 . | | 23.9 | 790 | JE | |
| 46 | 2760 | 53.25 | 898 | | 24.1 | 770 | JЕ | |
| 47 | 2820 | 53.75 | 902 | | 24.9 | 770 | JE` | |
| 48 | 2880 | 53.5 | 900 | | 25.8 | 800 | JE | |
| 49 | 2940 | 53.25 | 898 | | 26.0 | 800 | JE | |
| 50 | 3000 | 53.75 | 902 | | 26.2 | 800 | JE_ | <u> </u> |
| 51 | 3060 | 53.5 | 900 | | 26.2 | 800 | JЕ | |
| 52 | 3120 | 53.25 | 898 | | 26.6 | 810 | JE | |
| 53 | 3180 | 53.5 | 900 | | 27.0 | 810 | JE | |
| 54 | 3240 | 53.25 | 898 | | 28.0 | 810 | JE | <u></u> |
| 55 | 3300 | 53.5 | 900 | | 26.9 | 810 | JE | |
| 56 | 3360 | _53 <u>_0</u> | 896 | | 26.8 | 800 | JF/MK | |
| 57 | 3420 | 53.0. | 896 | | 25.0 | 7 90 | GR/MK | |

| PROJECT 79-183 Acme Well 18 | LOCATION Homeland Road | | | |
|--------------------------------------|---------------------------|--|--|--|
| METHOD OF MEASURING 5" x 6" orifice | AVERAGE DISCHARGE 900 GPM | | | |
| STARTING DATE OF TEST 9/24/80 @ 1000 | | | | |

| Ti | me | | Dis- | Stafi | Temp | Cond. | Mea- | |
|------|------|--------|-----------------|--------------|-------|------------|-------------|----------------|
| (hr) | | Inches | charge (gpm) | Gage (ft) | (oC) | (umhos/cm) | sured by | Remarks |
| 58 | 3480 | 53.5 | 900 | | 24.0 | 780 | GR/MK | |
| 59 | 3540 | 53.5 | 900 | | 24.0 | 980 | GR/MK | |
| 60 | 3600 | 53.5 | 900 | | 24.0 | 780 | GR/MK | |
| 61 | 3660 | 53,5 | 900 | | 24.0_ | 780 | GR/MK | |
| 62 | 3720 | 53.5 | 900 | | 23.5 | 820 | GR/MK | |
| 63 | 3780 | 53.5 | 900 | | 23.8 | 810 | GR/MK | |
| 64 | 3840 | 53.25 | 898 | | 23.5 | 810 | GR/MK | |
| 65 | 3900 | 53.5 | 900 | | 23.5 | 810 | GR/MK | |
| 66 | 3960 | 53.5 | 900 | | 23.5 | 800 | GR/MK | |
| 67 | 4020 | 53.5 | 900 | | 23.5 | 800 | GR/MK | - |
| 68_ | 4080 | 53.5 | 900 | | 23.5 | 780 | GR/MK | |
| 69 | 4140 | 53.5 | 900 | | 23.5 | 780 | GR/MK | |
| 70 | 4200 | 53.5 | 900 | | 23.8 | 780 | GR/ MK | |
| 71 | 4260 | 53.0 | 896 | | 24.9 | 775 | GR/MK | |
| 72 | 4320 | 53.5 | 900 | | | | GR/MK | |
| | | | | | | | | |
| | | | | | | - | | |
| | | | | | | | <u></u>] | |
| | | | | | | | | |
| | | | | | | | | |
| | | | | | | | | |

APPENDIX C

THE WATER WORKS

Complete Water Analysis

634 42nd Street West Palm Beach, Fl. 33407

Phone 842-3332

October 22, 1980

9-27-80

Frederick C. Bothe Chemist

Gee & Jenson Engineers 2019 Okeechobee Boulevard West Palm Beach, Florida

| Water Works Job No. 1808 | 121-80 | 7 - 7 - |
|--------------------------------|-----------------|-----------------------------------|
| | ACME 0900 | ACME 1100 |
| Total Dissolved Solids | $_{488}$ mg/1 | 516 mg/1 |
| Total Hardness | 302 | 294 |
| Total Alkalinity | 321 | 322 |
| Non-Cafbonate Hardness | N/D | N/D |
| Iron | 0.26 | 0.19 |
| Sulfate | 6 | ζ5 |
| Chloride | 66 | 62 |
| Calgium | 109 | 106 |
| Nitrate | 40.1 | 40.1 |
| Fluoride | 0.21 | 0.21 |
| Magnesium | 7 | 7 |
| Turbidity | 0.56 | 0.52 |
| Color | 40 Units | 30 Units |
| Silica | ∠10 mg/l | $\langle 10 \text{ mg/l} \rangle$ |
| Sodium | 38 | 25 |
| рН | 7.3 | 7.3 |
| Bicarbonate as CaCO3 | 321 . | 322 |
| Hydroxide as CaCO ₃ | -0- | -0- |
| Carbonate as CaCO3 | - O- | -0- |
| Carbon Dioxide | 24 | 15 |
| Bicarbonate | 392 | 393 |
| | | |

collected after 72 hrs pumping

1. he pun

9-24-80

Respectfully submitted,

FREDERICK C. BOTHE

FCB:1bt

TABLE 3

COMPARISON OF CALCULATED VERSUS FIELD DRAWDOWN DATA

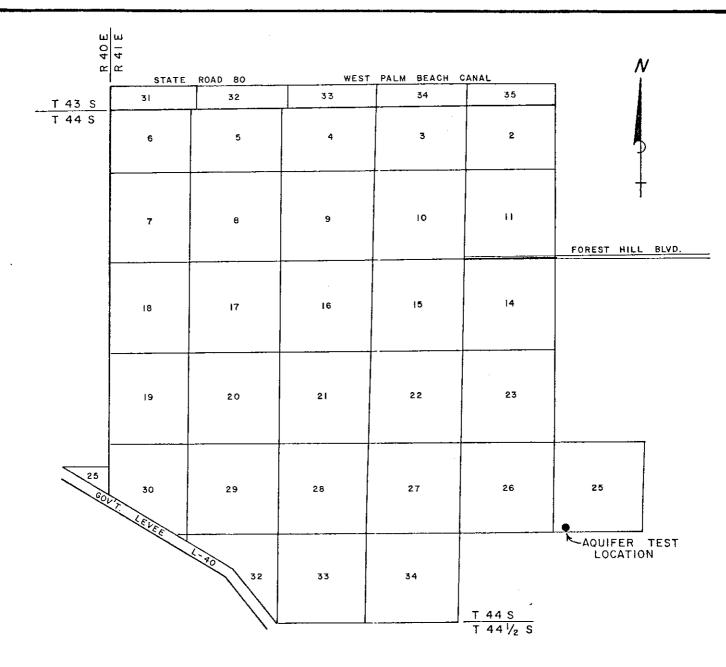
$$u = \frac{1.87^2 S}{Tt}$$
 $s = \frac{114.6 Q}{T}$ $W(u)$

T = 34,000S = 0.1

Q = 900 gpm

| t (days) | 18-1D $r = 33 ft$ | 18-2D $r = 130 ft$ | 18-3D $r = 200 ft$ | r = 500 ft | r = 1,000 ft | r = 2,000 ft |
|-------------|--|--|--|--------------------------------------|---|---------------------------------------|
| 1 | | $u = 9.3 \times 10^{-2}$ $W(u) = 1.89$ $s = 5.73ft(7.96)*$ | $u = 1.6 \times 10^{-1}$ $W(u) = 1.41$ $s = 4.28ft(6.02)*$ | u = 1.38 $W(u) = 0.12$ $s = 0.36$ ft | u = 5.5 W(u) = 0.0006 $s = 1.82 \times 10^{-3}$ | ft - |
| 3 | $u = 1.5 \times 10^{-3}$ $W(u) = 5.93$ $s = 18.00ft(16.80)*$ | W(u) = 3.22 | $u = 5.4 \times 10^{-2}$ $W(u) = 2.40$ $s = 7.28ft(6.30)*$ | W(u) = 0.61 | W(u) = 0.06 | |
| 30 | $u = 2.0 \times 15^{-4}$ W(u) = 7.94 s = 24.09ft | | $u = 7.3 \times 10^{-3}$ $W(u) = 4.35$ $s = 13.19ft$ | W(u) = 2.55 | $u = 1.83 \times 10^{-1}$ $W(u) = 1.31$ $s = 3.97 \text{ ft}$ | u = 1.36 W(u) = 0.12 s = 0.36ft |

^{*} Field drawdown data obtained from data sheets in Appendix B.





ACME IMPROVEMENT DISTRICT LOCATION MAP

GEE & JENSON ENGINEERS-ARCHITECTS-PLANNERS,INC.
WEST PALM BEACH, FLORIDA

- 1