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Hydrologic Data from a Lower Floridan Aquifer Well, Central Orange County, Florida

by

Brian McGurk, P.G. John Sego



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St. Johns River Water Management District Palatka, Florida

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EXECUTIVE SUMMARY

This report presents data collected from the Orlando Utilities Commission (OUC) Southeast test well, located near Lake Nona in south-central Orange County, Florida. The data were collected as part of an agreement between the St. Johns River Water Management District (SJRWMD) and OUC to deepen the existing test well and collect hydrogeologic information in addition to that already collected at the site by OUC.

The project was initiated to obtain information on (1) the thickness of the transition zone between freshwater (chloride concentration of less than 250 milligrams per liter [mg/L]) and salt water (chloride concentration of approximately 19,000 mg/L), (2) relative differences in permeability between different vertical intervals within the Lower Floridan aquifer, and (3) the thickness of the Lower Floridan aquifer.

OUC constructed and performed testing in the original test well between July 11, 1995, and March 29, 1996. The well was cased to a depth of approximately 1,084 feet below land surface (ft bls) and completed with an open borehole to approximately 2,005 ft bls. The additional drilling and testing under the direction of SJRWMD occurred between July 8, 1996, and September 29, 1996. Drilling ceased on July 16, 1996, at a depth of approximately 2,443 ft bls. Upon completion of testing, the borehole was backplugged to a final depth of 1,399 ft bls.

Data collected during drilling included lithologic data, drilling time data, water quality data, and water level data. Geophysical and video logging were conducted upon completion of drilling. Caliper, natural gamma, formation resistivity, fluid resistivity, temperature, flow, and acoustic velocity logs were run in the open borehole. Water quality samples were collected for laboratory analysis at discrete depths within the open borehole using a thief sampler. Nine distinct borehole zones were delineated based upon borehole characteristics and lithologic descriptions.

Straddle-packer testing was conducted at five different depth intervals in order to (1) collect water quality data from discrete zones to better characterize the freshwater/saltwater transition zone, (2) measure hydraulic head in discrete zones so that the vertical hydraulic gradient could be estimated, and (3) estimate the variation in permeablility with depth.

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Results from the various tests indicate that the Lower Floridan aquifer can be roughly divided into three hydrostratigraphic layers:

- An upper permeable layer (the main production zone used for water supply development in the Orlando area) composed primarily of hard dolomitic rocks in which flow is dominated by solution cavities and fractures
- A semiconfining layer composed primarily of relatively soft limestone with little fracture flow
- A lower permeable layer similar in character to the upper permeable layer. Water quality throughout most of its thickness is fresh but slightly more mineralized than the upper permeable layer. Hydraulic head is probably higher than in the overlying layers.

The top of the lower confining unit (the base of the Floridan aquifer system) was found at approximately -2,000 ft National Geodetic Vertical Datum, a depth significantly higher than previously mapped in regional water resource assessment reports. There is little difference in the magnitude of hydraulic head between the lower confining unit and the lower permeable layer of the Lower Floridan aquifer. The thickness of the Lower Floridan aquifer at the Southeast test well site is approximately 980 ft.

The top of the freshwater/saltwater transition zone (equivalent to the 250-mg/L isochlor) was found within the Lower Floridan aquifer near the base of the lower permeable layer and estimated at a depth of approximately 2,050 ft bls.

The bottom of the freshwater/saltwater transition zone was estimated to be at a depth of approximately 2,330 ft bls. The resulting thickness of the transition zone is approximately 280 ft.

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ACRONYMS AND ABBREVIATIONS

(used in figures)

ad	above datum
API	American Petroleum Institute [unit]
bd	below datum
bls	below land surface
bmp	below measuring point
d	datum
deg. C	degrees Celsius
FGS	Florida Geological Survey
ft	foot
ft bls	feet below land surface
ft NGVD	feet National Geodetic Vertical Datum
g/mL	grams per milliliter
gpd/ft	gallons per day per foot
gpm	gallons per minute
in.	inch
mg/L	milligrams per liter
microsec/ft	microseconds per foot
µS/cm	microsiemens per centimeter
mp	measuring point
ohm-m	ohm-meter
OUC	Orlando Utilities Commission
psi	pounds per square inch
rpm	revolutions per minute
SJRWMD	St. Johns River Water Management District
USGS	United States Geological Survey

INTRODUCTION

Orlando, centered within Orange County in east-central Florida (Figure 1), has been experiencing a significant amount of population and commercial growth in recent years. Vergara (1998) projected an increase of more than 50% between 1995 and 2020 in the average amount of water withdrawn by municipalities in this area for public supply use. Most of this water is projected to be withdrawn from the Lower Floridan aquifer. Hydrologic data from the Lower Floridan aquifer are extremely limited, however. The St. Johns River Water Management District (SJRWMD), in cooperation with local governments, has expanded its network of deep observation and test wells in order to gain a better understanding of the lower parts of the Floridan aquifer system.

This report presents and describes data collected from the Orlando Utilities Commission (OUC) Southeast test well, located near Lake Nona in south-central Orange County, Florida (Figure 2). The data were collected as part of an agreement between SJRWMD and OUC to deepen the existing test well and collect hydrogeologic information in addition to that already collected from the well by OUC. Conclusions regarding the hydrogeology of the lower portions of the Floridan aquifer system are also presented.

PURPOSE AND SCOPE

The purpose of this drilling project was to obtain information on (1) the thickness of the transition zone between freshwater (chloride concentration of less than 250 milligrams per liter [mg/L]) and salt water (chloride concentration of approximately 19,000 mg/L), (2) relative differences in permeability between different vertical intervals within the Lower Floridan aquifer, and (3) the thickness of the Lower Floridan aquifer. This information is needed to gain a better understanding of groundwater flow within the Floridan aquifer system in Orange County. The knowledge obtained will aid SJRWMD and the South Florida Water Management District in making resource management decisions for the east-central Florida region.



Figure 1. The St. Johns River Water Management District



St. Johns River Water Management District

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Data from the lower parts of the Floridan aquifer system are extremely limited. Although OUC and other utilities withdraw, on average, approximately 75 million gallons per day from the Lower Floridan aquifer, the entire Floridan aquifer system has been penetrated by a test well at only two sites in southern Orange County. Both sites (the Sand Lake injection test well and the Southern Regional test well) are west of the Southeast test well site (Figure 2) and contain freshwater throughout the Lower Floridan aquifer. Even though the Southeast test well is located outside the boundaries of SJRWMD, it is situated almost midway between the Sand Lake and Southern Regional wells and the test wells to the east (Cocoa C, Cocoa R, and Cocoa S), where very brackish water exists within the main Lower Floridan aquifer production zone. It is therefore an excellent location from which to obtain the needed data.

PREVIOUS WELL DRILLING AND TESTING AT THE SITE

OUC constructed and performed testing in the original test well between July 11, 1995, and March 29, 1996. The well was cased to a depth of approximately 1,084 feet below land surface (ft bls) and completed with an open borehole to approximately 2,005 ft bls. Drilling, geologic and water quality sampling, geophysical logging, and hydraulic testing activities were described in a report prepared by Barnes, Ferland and Associates (1996). That report presents a detailed description of the test well site and a general description of the hydrogeology of south-central Orange County.

DRILLING, TESTING, AND WELL COMPLETION

SJRWMD's project involved deepening the OUC Southeast test well by approximately 450 feet (ft) and conducting additional geologic and water quality tests. Two Cooperative Agreements between OUC and SJRWMD governed the drilling activities. Agreement 96D172, dated December 27, 1995, and Agreement 96J274, dated July 2, 1996, established drilling, sampling, and well-plugging procedures. The latter agreement specified that OUC's drilling contractor, Meredith Associates, would perform the additional work.

INITIAL GEOPHYSICAL AND VIDEO LOGGING

Prior to commencement of drilling and sampling activities, the United States Geological Survey (USGS) conducted geophysical logging of the Southeast test well (SJRWMD well OR0636) on January 18 and 19, 1996. SJRWMD also obtained a borehole video log on January 22, 1996. These logs revealed a borehole depth of 1,997 ft bls, which is considered to be OUC's project completion depth and the SJRWMD project starting point. The video log also revealed a 4–5-ft length of steel casing in the borehole at a depth of approximately 1,125 ft that had separated from the main body of the casing. Consequently, an additional purpose of the project was to grout the loose casing in place or otherwise stabilize the loose casing to the satisfaction of OUC.

DRILLING AND SAMPLING

Meredith Associates remobilized at the site during the first week of July 1996 and began inserting drill pipe with a 7.875-inch (in.) diameter bit into the open hole on July 8, 1996. Reverse-air rotary drilling of the nominal 8-in.-diameter borehole resumed on July 9, 1996. The maximum planned target depth was 2,500 ft bls or a depth at which drill cuttings revealed vertically persistent beds of evaporitic carbonates (limestone or dolostone containing gypsum and/or anhydrite). Drilling ceased on July 16, 1996, at a depth of approximately 2,443 ft bls because lithologic samples from the drill cuttings indicated the consistent presence of gypsiferous carbonate rock below 2,310 ft bls.

Data collected during drilling included lithologic data, drilling time data, water quality data, and water level data. Sampling methods are discussed in the following section.

Lithologic Samples

Lithologic samples were collected from the drill cuttings every 10 ft. The samples were stored in airtight Ziploc plastic bags for shipment to the Florida Geological Survey (FGS) for analysis (Appendix A). The drilled section generally consists of light gray, moderately indurated microcrystalline dolostone and dolomitic limestone to a depth of 2,420 ft bls. The bottom 90 ft (2,330–2,420 ft bls) of this interval consists of gypsiferous dolostone. Minor amounts of gypsum were present in the cuttings below a depth of approximately 2,240 ft bls, however. White, moderately indurated, highly recrystallized gypsiferous limestone was found from 2,420 ft bls to total depth. Analysis by FGS indicated that the dolostone and dolomitic limestone above 2,420 ft bls is part of the Oldsmar Formation and that the limestone of the bottom approximately 23 ft belongs to the Cedar Keys Formation. [Oldsmar Formation and Cedar Keys Formation are equivalent to Oldsmar Limestone and Cedar Keys Limestone, as used in Appendix A.]

Drilling Time Data

The length of time taken to advance the drillstem the length of each drill rod (30 ft) was recorded. Drilling times ranged between 2.2 and 4.3 ft/minute and averaged 2.8 ft per minute from 1,997 to 2,293 ft bls. Below this depth, drilling times increased slightly, ranging from 3.3 to 6.7 ft/minute.

Water Quality Data

Specific conductance of water from the reverse-air discharge line was monitored at intervals of approximately every 10 ft of hole depth. In addition, field water quality samples were collected every 30 ft. Each water quality sample was collected from the reverse-air discharge line after 15 minutes of circulation/development and analyzed in the field by SJRWMD staff for specific conductance, temperature, and chloride concentration (Figure 3; Appendix B). The field analyses indicate a relatively abrupt increase in conductance and chloride concentration between 2,061 and 2,083 ft bls. Conductance increased from 915 to



Figure 3. Data on water quality and depth to water level collected during additional drilling and testing of the Orlando Utilities Commission Southeast test well

St. Johns River Water Management District 7 2,298 microsiemens per centimeter (μ S/cm, equivalent to micromhos per centimeter) and chloride concentration increased from 61 to 372 mg/L. During drilling, the values of these two parameters increased only slightly below 2,083 ft. However, on the day following completion of drilling (July 17, 1996), a slug of very brackish water (chloride concentration of approximately 17,800 mg/L) was discharged after approximately 25 minutes of development using reverse-air circulation. This slug was followed by discharge of increasingly less-saline water during the remaining period of development (Appendix B).

Water quality samples were collected for major-ion analysis from the reverse-air discharge line at depths of 2,083 ft bls and 2,352 ft bls. These samples were preserved, stored in ice, and transported to the SJRWMD laboratory. Results of all laboratory analyses are listed in Table 1.

Water Level Measurements

Measurements of the depth to water level within the drillstem and within the open borehole outside the drillstem were taken periodically as the total depth increased during drilling. Depth to water level in the open borehole was measured from the top of the 16-in. casing beneath the drilling platform (approximately 0.5 ft above land surface). Depth to water level inside the drillstem was measured from the top of the uppermost drill rod and then corrected to represent depth below the 16-in. casing near land surface. Drillstem water level measurements were made periodically between addition of rods to the drillstem and also at the beginning of each day before drilling commenced. Borehole water levels and the initial daily drillstem water levels represent the average head of the entire open hole interval (below the bottom of the 8-in. casing at 1,084 ft bls to total depth). These readings were consistently between 39 and 43 ft bls (Figure 3; Appendix B). If the elevation of the top of the 16-in. casing is assumed to equal 90.00 ft National Geodetic Vertical Datum (NGVD), then the average hydraulic head of the open hole interval ranges between 47 and 51 ft NGVD. Drillstem water level readings taken during drilling were always at least several feet lower than borehole water level readings taken at the same depth (Figure 3; Appendix B). At depths of 2,412 ft bls and 2,443 ft bls (final depth), the drillstem water level

Sample Number*	Date Collected	Time Collected	Depth (ft bis) ¹	Temperature, Field (°C)	pH, Field	Ca (mo/L)	Na (ma/L)	K (ma/L)	Mg (mg/L)	Fe (ug/L)	Ba (uo/L)	Sr (ua/L)	Si, Total (mo/L)
D1	7/11/96	1415	2.083	28.50	N/A	198	219	10.7	94	1.630	42	3.500	6
D2	7/15/96	1702	2.352	29.50	N/A	597	180	9.1	91.5	2.510	50	9.820	6
P2	8/23/96	1716	2.200	28.00	6.91	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
P3	8/26/96	1500	2,086	28.00	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	
P4	8/27/96	1615	2,015	28.68	7.34	96	22	2.2	24.5	126	50	2,531	N/A
P5	8/28/96	2000	1,793	28.06	7.53	84	21	2	21.9	246	45	2,370	N/A
Sample Number*	Date Collected	Time Collected	Depth (ft bls)*	Alkalinity Laboratory	Cl (mg/L)	SO, (mg/L)	F (mg/L)	Density (a/mL) ⁶	Specific Conductance,	Total Dissolved Solids		SiO, (dissolved) (mg/L)	
				(mg/L)*				10 ·	Field (µS/cm)	(mg/L)			
D1	7/11/96	1415	2,083	118	380	474	0.59	N/A	2,298	1,460		N/A	
D2	7/15/96	1702	2,352	197	362	1,340	0.57	N/A	2,390	2,490		N/A	
T1	7/23/96	1705	2,390	N/A	1,480	322	N/A	N/A	N/A	N/A		N/A	
T2	7/23/96	1838	2,350	N/A	1,940	374	N/A	N/A	N/A	N/A		N/A	
Т3	7/23/96	1925	2,150	N/A	44	204	N/A	N/A	N/A	Ń/A		N/A	
T4	7/24/96	0810	2,050	N/A	38	202	N/A	N/A	N/A	N/A		N/A	
T5	7/24/96	1014	2,420	N/A	112	213	N/A	N/A	N/A	N/A		N/A	
T6	7/24/96	1128	1,995	N/A	38	199	N/A	N/A	N/A	N/A		N/A	
T7	7/24/96	1215	1,750	N/A	37	200	N/A	N/A	N/A	N/A		N/A	
P2	8/23/96	1716	2,200	138	3,790	3,710	3.58	1.007	15,190	10,	900	N/A	
P3	8/26/96	1500	2,086	208	2,010	1,940	2.04	1.004	9,494	6,090		N/A	
P4	8/27/96	1615	2,015	117	44	229	0.19	0.999	749	506		13	
P5	8/28/96	2000	1,793	122	39	192	0.2	0.997	632	4	463		4

Table 1. Laboratory analyses of water samples collected from the Orlando Utilities Commission Southeast test well

Note: ft bis = feet below land surface

N/A = not available

g/mL = grams per milliliter mg/L = milligrams per liter μ g/L = micrograms per liter μ S/cm = microsiemens per centimeter

*Sample numbers preceded by "D" indicate samples collected from reverse-air discharge during drilling; sample numbers preceded by "P" indicate samples collected during packer testing; sample numbers preceded by "T" indicate samples collected via thief sampler after geophysical logging. [†]For packer test samples, depth listed equals bottom of isolated interval

[‡]As CaCO₃.

^{\$}Measured at 20°C.

depths exceeded 50 ft and 70 ft below the measuring point, respectively.

BOREHOLE LOGGING

Hydrologic features of the borehole were documented using geophysical logging, sonic televiewer logging, and video logging methods. The logs were used to determine the borehole characteristics and flow at various depths. Borehole logging activities are described separately in the next section; the log results are compared in a subsequent section.

Geophysical Logging and Sampling

As noted previously, geophysical logging was conducted in the open borehole by USGS on January 18 and 19, 1996, prior to commencement of additional drilling and testing. Digital files from seven logs were supplied by USGS (Figure 4).

Additional geophysical logging was conducted upon completion of drilling, on July 18 and 22, 1996, by Southern Resources Exploration of Gainesville, Florida. Caliper, natural gamma, formation resistivity, fluid resistivity, temperature, and acoustic velocity logs were run in the open borehole between approximately 1,084 and 2,443 ft bls on July 18 (Figure 5). On July 22, a flowmeter log was run while the well was pumped at a rate of approximately 1,450 gallons per minute (gpm). Water quality samples were collected for laboratory analysis by the SJRWMD geophysical logger. Samples were taken at discrete depths within the open borehole using a thief sampler on July 23 and 24, 1996. The samples were preserved, stored in ice, and transported to the SJRWMD laboratory for analysis of chloride and sulfate (Table 1).

Video Logging

Borehole video logs were run in color by Deep Venture Logging of Perry, Florida, on three separate occasions. The first, as previously mentioned, was on January 22, 1996. The second was obtained on July 18, 1996, shortly after completion of drilling, and the third was run on September 3, 1996, after completion of straddle-packer testing and prior to backplugging.



Drilling, Testing, and Well Completion

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No significant differences were observed among the three video logs in the condition of the borehole wall. Movement or change in position of the separated piece of casing (which appears to be wedged tightly against the borehole wall in all three videos) was not discernible in the later two video logs relative to the position of the separated piece of casing in the first video log. In the later two video logs, the total differences in recorded depth to (1) the bottom of the grouted casing and (2) the top of the separated piece of casing were, in each case, approximately 2 ft. These small differences may be due to one of more of the following:

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- Slight differences in determining the exact location of the measurement datum (top of 16-in. casing) between different video log operators
- Depth measurement error by the video logging equipment or the operator, or both
- Movement of the separated piece of casing caused by drilling and testing operations.

Appendix C contains a description of the July 18, 1996, video log, including comparisons between it and the other two video logs.

Log Interpretation

The two sets of geophysical logs were plotted at the same vertical scale and compared with those described by Barnes, Ferland and Associates (1996). All of the logs in each set were examined and interpreted collectively. Collective interpretation is important because there can be significant borehole-diameter effects upon the signatures of gamma, resistivity, acoustic velocity, and flowmeter logs (Keys 1988). Note that although a spontaneous potential log was run by Southern Resources Exploration, it was not used in this analysis. Use of the spontaneous potential curve requires a sand-shale baseline from which to compare deflections in the curve, limiting the log's utility in carbonate lithology sequences like the Floridan aquifer system (MacCary 1980).

Over the depth interval that the three sets of logs overlap (approximately 1,000–2,000 ft bls), the logs obtained for this project are very similar to those described by Barnes, Ferland and Associates (1996). The caliper, unpumped heat-pulse flowmeter, temperature,

fluid resistivity, and video logs (Figures 4 and 5; Appendix C) substantiate the presence of significant upward borehole flow originating from cavities between 1,974 and 2,000 ft bls. The pumped flowmeter log (Figure 5) also indicates that approximately 50% of flow originates from the 1,974–2,000-ft bls interval, with the remainder coming from above 1,320 ft bls. A large percentage of flow in the pumped flowmeter log apparently comes from a cavity zone at approximately 1,150–1,180 ft bls. The unpumped heat-pulse flowmeter log (Figure 4) shows significant flow (indicated by an increase in velocity) entering the formation at this depth interval and at approximately 1,320 ft bls. The video logs indicate upward movement of particles between approximately 1,350 and 1,970 ft bls, but no significant borehole flow is apparent in either direction deeper than 2,000 ft bls. Below 2,330 ft bls, the dense evaporitic rocks cause an increase in formation resistivity and a decrease in acoustic velocity.

Nine distinct borehole zones were delineated, based primarily upon similar borehole characteristics—as indicated by geophysical and video logs—and secondarily upon geologic descriptions from Barnes, Ferland and Associates (1996) and FGS (Appendix A).

Borehole Zone 1. Approximately 1,084–1,140 ft bls. Borehole wall smooth to rough, relatively soft rock (limestone) and hard, fractured rock (dolostone) with little borehole inflow or outflow.

Borehole Zone 2. Approximately 1,140–1,320 ft bls. Borehole wall rough, relatively hard rock (dolostone) with abundant fractures and/or cavities; significant inflow to the borehole from the formation.

Borehole Zone 3. Approximately 1,320–1,630 ft bls. Borehole wall rough, predominantly hard rock (dolostone) with numerous fractures but no significant borehole inflow or outflow.

Borehole Zone 4. Approximately 1,630–1,840 ft bls. Borehole wall smooth, predominantly soft rock (limestone) with thin layers of harder rock; no significant borehole inflow or outflow.

Borehole Zone 5. Approximately 1,840–1,970 ft bls. Borehole wall rough, predominantly hard rock (dolostone) with numerous fractures but no significant borehole inflow or outflow (similar to borehole zone 3).

Borehole Zone 6. Approximately 1,970–2,000 ft bls. Rough borehole wall, hard rock (dolostone) with fractures and/or cavities; significant inflow to the borehole from the formation.

Borehole Zone 7. Approximately 2,000–2,080 ft bls. Borehole wall rough, predominantly hard rock (dolostone) with numerous fractures but no significant borehole inflow or outflow (similar to borehole zones 3 and 5).

Borehole Zone 8. Approximately 2,080–2,330 ft bls. Borehole wall very smooth, predominantly soft rock (dolostone and dolomitic limestone containing minor gypsum below approximately 2,240 ft bls) with no borehole inflow or outflow.

Borehole Zone 9. Approximately 2,330–2,443 ft bls. Borehole wall very smooth, relatively hard rock (dolostone and limestone containing significant amounts of gypsum) with no borehole inflow or outflow.

PACKER TESTING

Packer testing consists of isolating part of an open borehole using an inflatable packer assembly suspended on the drillstem in order to measure or estimate that portion's water quality characteristics and hydraulic properties. Straddle-packer testing (in which packers are placed above and below the zone of interest) was chosen for this project so that discrete intervals could be isolated. Specific goals were as follows:

- To isolate intervals above and below the changes in water quality observed during drilling in order to characterize the transition zone between freshwater and salt water within the Floridan aquifer system.
- To obtain discrete measurements of hydraulic head at different vertical locations for comparison with previous water level measurements. The previous measurements represent composite hydraulic head values for the entire portion of the aquifer penetrated by the well. Discrete measurements allow estimation of any vertical hydraulic gradient that may exist within the aquifer.

• To estimate the variation in permeability with depth within and/or below the Floridan aquifer system.

Selection of Test Intervals

Straddle-packer testing was conducted at five different depth intervals within the lower part of the borehole:

Packer Interval 1—2,316 to 2,386 ft bls Packer Interval 2—2,130 to 2,200 ft bls Packer Interval 3—2,016 to 2,086 ft bls Packer Interval 4—1,945 to 2,015 ft bls Packer Interval 5—1,722 to 1,792 ft bls

The depths and thicknesses of the packer intervals were selected based upon the following criteria, using the available water quality, lithologic, geophysical, and video log information:

- Round borehole shape with a diameter of less than 10 in.
- Smooth borehole walls with no linear fractures or large vugs for a minimum distance of 3 ft (the approximate length of an inflatable packer sized for a nominal 8-in. borehole)
- Test interval thicknesses *of equal length* so that the drillstem-packer assembly would be lowered into the well only once (to the deepest interval) then raised for each subsequent test.

Packer Test Methodology

Preparation for straddle-packer testing consisted of attaching a packer string assembly to the bottom of the drillstem and lowering the assembly into the borehole to the first desired test interval (Figure 6). The two packers were then inflated by forcing water downhole under pressure (through plastic tubing) to the packer assembly. Installation of the assembly began initially on July 25, 1996. However, packer failures during test inflation delayed setup at packer interval 1 until August 19, 1996.



The testing plan for each interval consisted of the following steps:

- 1. Purge the drillstem of all water remaining from before inflation so that the water inside is derived only from the isolated interval.
- 2. Collect water quality samples from either the reverse-air discharge line or the submersible pump discharge for field analysis of specific conductance and chloride concentration during drillstem purging.
- 3. Monitor the water level inside the drillstem using either an electric water level meter or a 50 pounds per square inch (psi) pressure transducer to obtain a static water level of the isolated interval. Also, monitor the water level in the annulus between the well casing and the drillstem, using an electric water level meter. (Abrupt changes in annulus water level during packer testing would indicate possible packer failure.)
- 4. Conduct a constant-rate specific-capacity test using a 4-in. submersible pump capable of producing between approximately 5 and 70 gpm.
- 5. Collect water quality samples from the submersible pump discharge for laboratory analysis at the end of pumping for the specific-capacity test.
- 6. Measure the rate of water level recovery in the drillstem after pumping, using a 50 psi transducer and a data logger.
- 7. Download and analyze the water level data to estimate the specific capacity and transmissivity of each packer interval.

Packer Test Results

The results of packer testing for each interval are discussed below. Water level and field-analyzed water quality data are presented in both tabular and graphic formats (Appendix D). Specific-capacity (ratio of discharge rate to steady drawdown) estimates were calculated using averages of measured discharge rates and drawdown values from a relatively constant part of the drawdown curve. The Jacob straight-line recovery method (Driscoll 1986) was used to graphically estimate transmissivity according to the following equation:

$$T = (264Q) / \Delta s$$

where

- T = transmissivity (gallons per day per foot)
- Q = discharge (gallons per minute)
- Δs = the change (in feet) in residual drawdown (s) over 1 log cycle in a graph of s vs. t/t', where t = time (days) since pumping started and t' = time (days) since pumping stopped

Packer Interval 1. Purging began on August 19, 1996, with the injection of compressed air into the drillstem through a 1.5-in.diameter PVC air line. In this process, water is ejected along with the released air, usually at rates of approximately 50 to 100 gpm. Purging resulted in extreme drawdown and very slow recovery of the water level inside the drillstem after each purge (Table D1). On the second day of purging, after only about 360 gallons of the estimated 1,050 gallons needed to purge one well volume had been removed, SJRWMD staff decided to abandon further testing of packer interval 1. Static water level measurements, specific-capacity estimates, and a water quality analysis of water derived from packer interval 1 are therefore not available.

Packer Interval 2. The packers were set and inflated on August 22, 1996. Purging of the drillstem was conducted using the same air-line method used for packer interval 1. Approximately 1,200 gallons were removed on August 22, 1996, and another 1,500 gallons were removed during the morning of August 23, 1996. The specific conductance of the purged water on August 23, 1996, ranged from 12,000 to 16,000 μ S/cm. The pumping apparatus and water level transducers were installed as shown on Figure 6. One pump test (consisting of a specific-capacity test and corresponding recovery period) was run at a nearly constant rate of 50 gpm (Figure D1). The resulting specific capacity and transmissivity (calculated from the recovery data) were calculated to be 0.5 gpm/ft and 143 gallons per day per foot (gpd/ft), respectively (Figures D2 and D3). The specific conductance of water discharged during testing remained relatively constant at about 16,000 μ S/cm (Table D2; Figure D1). Laboratory analysis of the water quality sample taken near the end of the pumping period indicates that packer interval 2 contains brackish water (Table 1, sample P2),

(1)

with a chloride concentration of 3,790 mg/L and a density of 1.007 grams per milliliter (g/mL).

Packer Interval 3. The packers were set and inflated on August 25, 1996. Purging was accomplished using the air-line method used for packer intervals 1 and 2. Approximately 1,500 gallons were removed from the drillstem on August 25, 1996, and approximately 1,575 gallons were purged during the morning of August 26, 1996. Two pump tests were conducted, each consisting of a specific-capacity test and a corresponding recovery period (Table D3; Figure D4). The first test was run with a pumping rate of approximately 83 gpm, the second with a rate of approximately 37.5 gpm. The resulting specific capacities are 2.8 gpm/ft and 2.7 gpm/ft, respectively (Figures D5 and D6). Transmissivity estimates calculated from the corresponding recovery data equal 730 gpd/ft and 707 gpd/ft (Figures D7 and D8). Specific conductance throughout purging and testing on August 26, 1996, ranged from 8,500 to 10,000 μ S/cm until after deflation (pumping was continued during packer deflation), when conductance dropped to approximately $2,600 \,\mu\text{S/cm}$ (Figure D4). Laboratory analysis of the water quality sample taken near the end of the second pumping period indicates that packer interval 3 contains brackish water (Table 1, sample P3), with a chloride concentration of 2,010 mg/L and a density of 1.004 g/mL. Note that cation analyses are not listed on Table 1 for packer intervals 2 and 3. An equipment malfunction in the field made it impossible to preserve those samples properly for cation analysis.

Packer Interval 4. The packers were set and inflated and the interval was tested on August 27, 1996. The submersible pump and transducers were installed prior to inflation and purging. Purging was accomplished by pumping at rates between 85 and 101 gpm for approximately 80 minutes after the packers were inflated (Table D4; Figure D9). Recovery data were collected at the end of this pumping period, then a specific-capacity test was conducted, followed by an additional recovery period. The resulting specific capacity is 3.6 gpm/ft (Figure D10), and the transmissivity estimates are 1,067 gpd/ft and 837 gpd/ft (Figures D11 and D12). Periodic specific-conductance readings taken throughout purging and testing on August 26, 1996, ranged from 747 to 899 μS/cm (Figure D9). Laboratory analysis of the water quality sample taken near the end of the specific-capacity test indicates that packer interval 4 contains fresh,

potable water with a chloride concentration of 44 mg/L and a density of 0.999 g/mL (Table 1, sample P4).

Packer Interval 5. The packers were set and inflated, and the interval was tested on August 28, 1996. The submersible pump and transducers were also installed prior to inflation and purging. However, for this interval, purging was accomplished by pumping at rates varying between 1.5 and 80 gpm before and during the two pump test periods (Figure D13). The pumping periods were planned as step-drawdown tests, each with at least three successive periods of increased, constant withdrawal rates. However, during both tests, problems were encountered in recording and maintaining a constant withdrawal rate because of sediment clogging the flowmeter. Specific capacity was estimated using data from step 1 of step-drawdown test 1. (Figure D14) and steps 1–3 of step-drawdown test 2 ((Figure D15). The resulting specific-capacity values range from 0.1 to 0.2 gpm/ft. The transmissivity estimates are 59 gpd/ft and 61 gpd/ft (Figures D16 and D17). Specific-conductance values during pumping ranged from 690 to $1,800 \,\mu\text{S/cm}$ (Figure D13). However, most readings were close to the low end of this range. The higher values correspond to relatively turbid water produced at the beginning of the first test. The laboratory analysis of water sampled near the end of pumping indicates that packer interval 5 produces water slightly fresher than packer interval 4. The chloride concentration from the sample tested is 39 mg/L, and the measured density is 0.997 g/mL (Table 1, sample P5).

BACKPLUGGING

After removal of the packer string and drillstem, a video log was run on September 3, 1996, as previously described. This log indicated that the separated piece of steel casing at a depth of approximately 1,125 ft bls had not moved measurably, if at all, during testing and is apparently wedged tightly against the borehole wall. The separated casing was deemed to be stabilized, and preparations were then made to backplug the open borehole from total depth (2,443 ft bls) to approximately 1,410 ft bls. Backplugging was accomplished between September 5, 1996, and September 29, 1996, using neat cement grout and pea gravel (Figure 7), bringing the final depth to 1,399 ft bls. Grout was mixed off site by a commercial supplier and pumped



Not to scale

Note: ft bls = feet below land surface

Figure 7. Final well depth and backplugging stages

through a tremie pipe that extended to within approximately 60 to 90 ft above the borehole bottom. Grout samples were periodically collected and weighed by the SJRWMD site representative to ensure an appropriate water/cement mix. A minimum cure time of 8 hours separated successive grout lifts pumped during the same day. Gravel was emplaced via gravity feed. The well was backplugged using a total of 18 cubic yards of cement grout and 7 cubic yards of pea gravel.

DISCUSSION OF TEST RESULTS

Drilling samples, borehole logs, and straddle-packer/pump test results were used to determine the water quality and hydrologic characteristics of the test well. Combined with water level data, these results can help assess the thickness of the freshwater/saltwater transition zone, the thickness of the Lower Floridan aquifer, and the relative permeabilities of the various zones identified within the borehole. These results are discussed in the following sections.

WATER QUALITY

Water quality results indicate a significant discrepancy between samples collected during drilling and those collected during packer testing of intervals 2 and 3 (Figure 3; Table 1). Specific conductance and chloride values from the two packer tests are nearly an order of magnitude higher than those derived from corresponding depths from the reverse-air discharge during drilling and from thief samples collected after geophysical logging.

Other evidence, from both the geophysical and video logs and the packer tests, indicates that the analyses derived from the packer test samples are representative of formation water quality. The reverse-air discharge data and the thief sample values represent water that was pulled downward from above 2,000 ft bls by the drilling process. The geophysical and video logs indicate no borehole inflow or outflow below 2,000 ft bls. During drilling below 2,000 ft bls, the water flowing quickest to the drill bit was from the flow zone located between 1,970 and 2,000 ft bls (borehole zone 6). Because of the lack of natural borehole flow, the diluted water remained in the borehole. Consequently, the thief samples collected on July 23 and 24, 1996—one week after the cessation of drilling—were relatively fresh.

Evidently, some brackish water did collect near the bottom of the borehole after drilling ceased, however, because field analysis during development indicated discharge of water with a chloride concentration of approximately 17,800 mg/L, followed by lessbrackish water (Appendix B). The less-brackish water was probably a mixture of salty water derived from near the bottom of the borehole and freshwater from the flow zone above. Static water elevations (Table 2) indicate that a downward gradient may exist between packer CONTRACTOR &

interval 3 and packer interval 2. If these elevations represent typical conditions, then the buoyancy force resulting from density differences may not be sufficient to overcome this pressure gradient and force the diluted water upward.

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If the water quality analyses from the packer tests are representative of formation conditions, then the upper boundary of the freshwater/saltwater transition zone (the 250-mg/L isochlor) must lie within packer interval 3. It is reasonable to assume that the water sample collected at the end of this packer test represents a mixture of the water withdrawn from the 70-ft interval isolated by the straddle packers (2,016–2,086 ft bls), with freshwater coming from the upper part and brackish water coming from the lower part. The fluid resistivity log begins to decrease at a depth of about 2,070 ft bls (Figure 5), which indicates increasing salinity of the borehole fluid. However, the borehole fluid was apparently diluted by the drilling process. The data available are not sufficient to delineate the upper boundary further. Therefore, the top of the transition zone is assumed to be at 2,050 ft bls (Figure 8), which is approximately the midpoint of packer interval 3.

The bottom of the freshwater/saltwater transition zone is the boundary between brackish water and salt water (chloride concentration of approximately 19,000 mg/L). If the water discharged during well development is considered salt water, then the base of the transition zone is between packer interval 2 (2,130–2,200 ft bls) and 2,443 ft bls (total depth drilled). The available data do not allow further delineation of the base of the transition zone with a great deal of certainty. However, the geophysical log data, as well as the presence of evaporitic minerals below 2,330 ft bls, suggest that little, if any, groundwater circulation occurs below this depth. It is thus reasonable to assume that salt water is present in the rocks below 2,330 ft bls (Figure 8). According to these assumptions, then, the thickness of the freshwater/saltwater transition zone is approximately 280 ft (2,330–2,050 ft bls).

PERMEABILITY ESTIMATES

The specific capacity and transmissivity estimates (Table 3) are much lower than typical values calculated for the Floridan aquifer system. This is because most of the drawdown observed during the packer tests
is due to head loss within the well, rather than within the aquifer. An attempt was made with the drawdown data from packer interval 5 to estimate that portion of the drawdown that may be due to turbulent well loss. However, because specific capacity increased (rather than decreased) between steps 1 and 2 of step-drawdown test 2, the calculated well-loss coefficient was negative. This indicates that most, if not all, of the well loss is due to laminar flow (Driscoll 1986). According to Driscoll, a well with little or no turbulent well loss can still be very inefficient. The packer string design, with a 5-ft-long perforated section placed at the bottom of a 70-ft packer interval (Figure 6), probably contributes to the inefficiency. In fact, additional well loss may also have been caused by sediment settling within the bottom portion of the perforated pipe and partially closing some of the perforations, further restricting flow into the well. Sediment was observed plugging the bottom few perforations upon removal of the packer string. (This may also explain the difficulty in maintaining a constant flow rate during pumping of packer interval 5.) The specific capacity and transmissivity estimates should therefore be interpreted only as relative to one another. That is, packer interval 4 is apparently the most permeable interval and packer intervals 2 and 5 are apparently less permeable than packer intervals 3 and 4. The extremely slow water level recovery observed after purging of packer interval 1 indicates that this interval is the least permeable.

The decrease in drawdown that occurred during pumping of packer intervals 3 and 4 may indicate leakage of water around the packers. Sampling of packer intervals 2, 3, and 4 produced waters of very different quality. However, because no significant change in water quality was observed during pumping, the decrease in drawdown was probably not due to packer failure in the borehole. It was more likely caused by some degree of hydraulic connection through fractures in the formation between packer intervals 3 and 4.

STATIC WATER ELEVATIONS AND HYDRAULIC GRADIENTS

Static water elevations were calculated assuming that the top of the 16-in. casing near land surface equals an elevation of 90.00 ft NGVD. These elevations (Table 2) represent the hydraulic head of water in the interval isolated by the straddle packers. Because the packers isolate intervals with waters of differing density (Table 1), the static water elevations from packer intervals 2, 3, and 4 were adjusted to account for density differences. The adjusted head values (defined as

environmental-water heads by Lusczynski [1961]) are calculated using a weighted average density for the distance between the datum and the midpoint of the packer interval.

To estimate the weighted average density of water above each packer interval, the measured density values derived from water quality samples collected during packer testing were first assumed to represent particular depth intervals of constant density. The density value derived from the packer interval 5 sample (0.997 g/ml, Table 2) was used to represent the zone of freshwater that extends from the datum (0 ft NGVD) to the top of packer interval 4 (1,945 ft bls). The packer interval 4 density value (0.999 g/ml, Table 2) represents the slightly mineralized water found between 1,945 ft bls and 2,015 ft bls. The density values derived from the two deeper packer tests samples (intervals 2 and 3) were assigned to depths ranging from the base of the overlying packer interval to the base of the packer interval from which the sample was collected. Therefore, a density value of 1.004 g/ml represents the interval between 2,015 ft bls and 2,086 ft bls, and a density value of 1.007 g/ml represents the interval between 2,086 ft bls and 2,200 ft bls. The weighted average density for the water column above the midpoint of each packer interval was estimated using the following equation:

$$\rho_{\rm a} = \Sigma \left\{ \frac{(\rho_{\rm int} d_{\rm int})}{d} \right\}$$

(2)

where

- ρ_a = the weighted average density (g/ml)
- ρ_{int} = the assigned constant density within a particular depth interval (g/ml)
- d_{int} = the thickness of a particular depth interval of constant density (ft)
- d = the total thickness of the water column between the datum (NGVD) and the midpoint of the packer interval (where the environmental-water head is to be calculated) (ft)

The environmental-water head values (Table 2) were estimated using Equation 4a from Lusczynski (1961):

$$H_{\rm in} = \frac{\left[\rho_{\rm i} H_{\rm ip} - \{Z_{\rm i}(\rho_{\rm i} - \rho_{\rm a})\}\right]}{\rho_{\rm f}}$$
(3)

where

 H_{in} = environmental-water head at point *i* (ft NGVD)

- H_{ip} = point-water head (measured static water level elevation) at point *i* (ft NGVD)
- Z_i = vertical distance between point *i* and NGVD (ft)
- ρ_i = density of water at point *i* (g/ml)
- ρ_a = the weighted average density of water between NGVD and point *i* (g/ml)
- $\rho_{\rm f}$ = density of freshwater (0.997 g/ml)

For example, the environmental-water head value of 53.17 ft NGVD listed for packer interval 2 on the first row of Table 2 was calculated using other values from the same row in the following manner:

$$H_{\rm in} = \frac{\left[(1.007)(33.27) - \{ (-2075)(1.007 - 0.9976) \} \right]}{0.997}$$

The environmental-water heads can be used to estimate vertical gradients that are based solely upon pressure differences, rather than both pressure and density differences (Lusczynski 1961).

Average values of the environmental-water heads (Table 2) were used to estimate vertical hydraulic gradients between the intervals isolated by packers within the Southeast test well. For example, an upward gradient of 0.038 between packer intervals 4 and 5 results from dividing the average environmental-water head difference (53.51 ft minus 45.06 ft) by the distance between the midpoints of the two packer intervals (1,980 ft bls minus 1,757 ft bls). A much smaller upward gradient of 0.002 was calculated for the interval between the midpoints of packer intervals 3 and 4. A small downward gradient of 0.004 was calculated between packer interval 3 and packer interval 2. These computed gradients may not be precise for the following reasons:

• Depth to water level measurements were not made on the same day.

- Depth to static water level measurements were made (except for packer interval 5) using an electric water level meter through the open top of the drillstem alongside the submersible pump column and transducer cable. These measurements are probably accurate to approximately 0.05 ft at best.
- The weighted-average density estimates used to calculate environmental-water head may be in error because the true, continuous density distribution is unknown.
- Static water levels for packer interval 5 were taken from transducer readings which, upon calibration with water level meter measurements, are apparently only accurate to within several tenths of a foot.
- The gradients were calculated using the midpoint of each packer interval.

The upward gradient between packer intervals 4 and 5 is substantiated by the observance of upward flow between those portions of the borehole during logging. However, the static water elevations in packer interval 5 may be underestimated because measurements of depth to water level were made after pumping that resulted in relatively large drawdowns; also, as demonstrated by the graph of recovery test 2 (Figure D13), complete recovery of water levels in this interval required more than 60 minutes. If the actual static water level in packer interval 5 is higher than recorded, then the magnitude of the upward hydraulic gradient is less than that shown in Table 2.

The average environmental-water heads computed for packer intervals 2, 3, and 4 are very similar. Given the uncertainty in precision because of the factors listed above, hydraulic pressure within these two intervals may be approximately equal.

HYDROSTRATIGRAPHIC LAYERS WITHIN THE LOWER FLORIDAN AQUIFER

Five hydrostratigraphic layers (Figure 8) can be identified at the Southeast test well site based upon a comparison of the packer test results with the borehole zones listed on page 17. There are two relatively permeable layers separated by three less-permeable layers. The two highly permeable layers consist primarily of fractured dolostone and dolomitic limestone and contain the borehole zones in which inflow or outflow was noted during logging. The borehole zones that contain fractured dolomite but no observed inflow or outflow were combined with the fractured dolomite zones in which borehole flow was observed. The assumption was that the fractured dolomitic rocks are more likely to contain interconnected water-bearing solution cavities or fractures at some distance from the borehole than the softer limestone intervals in which no fractures were observed. The less-permeable layers consist of either limestone or evaporitic carbonates and are characterized by smooth borehole walls with no significant amount of observed fractures.

The uppermost hydrostratigraphic layer depicted on Figure 8 is the lowermost portion of the middle semiconfining unit described by Miller (1986) and Tibbals (1990). At this site, only the top 16 ft (1,084–1,100 ft bls) of the open hole interval is within this layer. Underneath the middle semiconfining unit lies the main Lower Floridan aquifer production zone described by Barnes, Ferland and Associates (1996) and by Lichtler et al. (1968). This layer lies within the lower part of the Avon Park Formation. An interval of relatively high gamma ray activity occurs near the base of this layer (between approximately 1,560 and 1,600 ft bls; see Figures 4 and 5). This interval appears to correlate with a similar gamma response in logs of the Lower Floridan aquifer at injection wells in Brevard County. According to Duncan et al. (1994), this distinctive gamma signature represents glauconite beds that mark the top of the Oldsmar Formation. A lower semiconfining layer separates the upper permeable layer from the lower permeable layer. This semiconfining interval is similar in character to the middle semiconfining unit. Packer interval 5 is located within this lower semiconfining layer. Packer interval 4 and most of packer interval 3 are within the lower permeable layer. The bottom layer (borehole zones 8 and 9)—the top of which occurs at about 2,080 ft bls-contains increasing amounts of gypsum with depth and is believed to be equivalent to the lower confining unit that underlies the Floridan aquifer system. Therefore, the thickness of

the Lower Floridan aquifer at the Southeast test well site is approximately 980 ft (1,010–1,990 ft bls).

Miller (1986) and Tibbals (1990) mapped the top of the lower confining unit (and therefore the base of the Floridan aquifer system) at approximately -2,500 ft NGVD in south-central Orange County. The lower confining unit at this site is therefore approximately 500 ft higher than previously mapped. Boyle Engineering Corporation (1994) identified the base of the Floridan aquifer system at approximately the same elevation (-2,000 ft NGVD) at the Orange County Southern Regional Wellfield test well.

Discussion of Test Results



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Figure 8. Hydrostratigraphic layers and location of the freshwater/saltwater transition zone in the Lower Floridan aquifer, Orlando Utilities Commission Southeast test well

Packer Interval Number	Interval Depth (ft bis)	Date	Time	Depth to Water Level (ft bmp)*	Depth to Water Level (ft below datum) [†]	Static Water Elevation (NGVD)	Density of Water in Packer Interval (o/mL)	Average Density (g/mL) [‡]	Elevation of Midpoint of Packer Interval (NGVD)	Environmentäl- Water Head (NGVD) [‡]	Hydraulic Gradient**	Comments
2	2,130 2,200	8/23/96	1628	64.68	56.73	33.27	1.007	0.9976	-2,075	53.17		After purging, before test pumping
2	2,130– 2,200	8/23/96	1825	64.45	56.50	33.50	1.007	0.9976	-2,075	53.40		Before specific- capacity tes
2	2,130 2,200	8/23/96	1942	64.74	56.79	33.21	1.007	0.9976	-2,075	53.11		After recovery
											0.004 (downward)	
3	2,016– 2,086	8/26/96	1039	54.95	50.34	39.66	1.004	0.9972	-1,961	53.31		After purging, before test pumping
3	2,016– 2,086	8/26/96	1604	54.23	49.62	40.38	1.004	0.9972	-1,961	54.04		After recovery test 2
											0.002 (upward)	× .
4	1,945 2,015	8/27/96	1406	50.50	41.16	48.84	0.999	0.997	-1,890	52.73		After recovery test 1
4	1,945– 2,015	8/27/96	1714	48.95	39.61	50.39	0.999	0.997	- 1,890	54.28		After recovery test 2
											0.038 (upward)	

Table 2—Continued

Packer Interval Number	Interval Depth (ft bis)	Date	Time	Depth to Water Level (ft bmp)*	Depth to Water Level (ft below datum) ¹	Static Water Elevation (NGVD)	Density of Water in Packer Interval (g/mL)	Average Density (g/mL) [‡]	Elevation of Midpoint of Packer Interval (NGVD)	Environmental- Water Head (NGVD) ⁵	Hydraulic Gradiont**	Comments
5	1,722– 1,792	8/28/96	1641	51.66	44.06	45.94	0.997	0.997	-1,667	45.94		Before step- drawdown test 1
5	1,722 1,792	8/28/96	1853	53.43	45.83	44.17	0.997	0.997	-1,667	44.17		Before step- drawdown test 2

Note: ft = foot

ft bls = feet below land surface

g/mL = grams per milliliter

bmp = below measuring point

NGVD = National Geodetic Vertical Datum

*Feet below measuring point equals feet below top of drillstem.

[†]Datum equals top of 16-inch casing (assumed to be at an elevation of 90.00 ft NGVD).

*Weighted average density of water between NGVD and midpoint of packer interval.

⁸Environmental-water head equals static water elevation corrected for density using Equation 4a of Lusczynski (1961).

**Hydraulic gradient equals difference between average environmental-water head for each interval divided by distance between midpoint of each interval.

Table 3. S	Summary of packer test	results from the (Orlando Utilities	Commission	Southeast test w	ell
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Packer Interval Number	Interval Depth (ft bis)	Date	Test Period (pumping and recovery)	Time Interval	Specific Capacity (gpm/ft)	Transmissivity Estimated From Recovery Tests (gpd/ft)	Comments
1	2,316–2,386	8/19/96	1	1100-1102	NA	N/A	Purging of drillstem with air line
1	2,316–2,386	8/19/96	2	1354–1357	NA	N/A	Purging of drillstem with air line
1	2,316–2,386	8/19/96	3	1505–1510	NA	N/A	Purging of drillstem with air line
2	2,130-2,200	8/23/97	1	1835-1942	0.5	143	
3	2,016-2,086	8/26/96	1	1118-1243	2.8	730	
3	2,016-2,086	8/26/96	2	1322-1604	2.7	707	
4	1,945–2,015	8/27/96	1	13521406	N/A	1,067	Packers inflated during pumping period
4	1,945-2,015	8/27/96	2	1425-1714	3.6	837	
. 5	1,722–1,792	8/28/96	1	16421749	0.2	59	Step-drawdown test 1, step 1—average pump rate of 10.7 gpm used for recovery analysis
5	1,722–1,792	8/28/96	2	1854–1859	0.1	NA	Step-drawdown test 2, step 1
5	1,722-1,792	8/28/96	2	18591904	0.2	NA	Step-drawdown test 2, step 2
5	1,722–1,792	8/28/96	2	1912–2128	0.2	61	Step-drawdown test 2, step 3—average pump rate of 14.9 gpm used for recovery analysis

Note: ft bls = feet below land surface gpd/ft = gallons per day per foot gpm = gallons per minute gpm/ft = gallons per minute per foot N/A = not available

CONCLUSIONS

The conclusions developed as a result of SJRWMD's additional drilling and testing of the Southeast test well are presented below.

- 1. The Lower Floridan aquifer can be roughly divided into three hydrostratigraphic layers, as follows:
 - An upper permeable layer (the main production zone used for water supply development in the Orlando area) composed primarily of hard dolomitic rocks in which flow is dominated by solution cavities and fractures.
 - A semiconfining layer composed primarily of relatively soft limestone with little fracture flow.
 - A lower permeable layer similar in character to the upper permeable layer. Water quality throughout most of its thickness is fresh but slightly more mineralized than the upper permeable layer. Hydraulic head is probably higher than in the overlying layers.
- 2. The top of the lower confining unit (the base of the Floridan aquifer system) was found at approximately -2,000 ft NGVD, a depth significantly higher than previously mapped in regional water-resource assessment reports. There is little difference in the magnitude of hydraulic head between the lower confining unit and the lower permeable layer of the Lower Floridan aquifer. The thickness of the Lower Floridan aquifer at the Southeast test well site is approximately 980 ft.
- 3. The top of the freshwater/saltwater transition zone (equivalent to the 250-mg/L isochlor) was found within the Lower Floridan aquifer near the base of the lower permeable layer and estimated at a depth of approximately 2,050 ft bls.
- 4. The bottom of the freshwater/saltwater transition zone was estimated to be at a depth of approximately 2,330 ft bls. The resulting thickness of the transition zone is approximately 280 ft.

REFERENCES

- Barnes, Ferland and Associates, Inc. 1996. Results of Construction and Testing of the Southeast and Orange Test Wells, Orlando Utilities Commission. Appendix in *Construction and Testing of the Orange and Southeast Test Wells*, by CH2M HILL, Inc. Orlando, Fla.
- Boyle Engineering Corporation. 1994. Interim Report on the Results of Investigations, Orange County Public Utilities Division Southern Regional Wellfield. Orange County Public Utilities Division.
- Driscoll, F.G. 1986. *Groundwater and Wells*. 2d edition. St. Paul, Minn.: Johnson Division.
- Duncan, J.G., W.L. Evans III, and K.L. Taylor. 1994. Geologic Framework of the Lower Floridan Aquifer System, Brevard County, Florida. Bulletin No. 64. Tallahassee, Fla.: Florida Geological Survey.
- Keys, W.S. 1988. Borehole Geophysics Applied to Ground Water Investigations. Open File Report 87-539. Denver, Colo.: U.S. Geological Survey.
- Lichtler, W.F., W. Anderson, and B.F. Joyner. 1968. *Water Resources of Orange County, Florida*. Report of Investigations 50. Tallahassee, Fla.: Florida Bureau of Geology.
- Lusczynski, N.J. 1961. Head and Flow of Ground Water of Variable Density. Journal of Geophysical Research 66:4,247–56.
- MacCary, L.M. 1980. Use of Geophysical Logs to Estimate Water-Quality Trends in Carbonate Aquifers. Water Resources Investigations 80-57. Denver, Colo.: U.S. Geological Survey.
- Miller, J.A. 1986. Hydrogeologic Framework of the Floridan Aquifer System in Florida and in Parts of Georgia, Alabama, and South Carolina. Professional Paper 1403-B. Washington, D.C.: U.S. Geological Survey.
- Tibbals, C.H. 1990. Hydrology of the Floridan Aquifer System in East-Central Florida. Professional Paper 1403-E. Washington, D.C.: U.S. Geological Survey.
- Vergara, B.A., ed. 1998. Water Supply Assessment, 1998: St. Johns River Water Management District. Technical Publication SJ98-2. Palatka, Fla.: St. Johns River Water Management District.

APPENDIX A—LITHOLOGIC DESCRIPTIONS PROVIDED BY THE FLORIDA GEOLOGICAL SURVEY

Appendix A

Lithologic Well Log Printout		Source:	FGS
Well Number: W-17480 Total [Drilled] Depth: 2,443 ft 46 Samples from 2,000 to 2,450	ft	County: Location:	Orange T.24S R.30E S.12 Lat = 28D 25M 15S Lon = 81D 16M 26S
Completion Date: 08/24/96 Other Types of Logs Available: 1	None	Elevation:	90 ft
Owner/Driller: St. John's River V	Vater Management District (OR-0636)		
Worked by: Tom Miller 2/97	46 Bags of Washed Cuttings		
0–2,000 000NOSM 2,000–2,420 124OLDM 2,420–2,450 125CDRK	No Samples Oldsmar Limestone Cedar Keys Limestone		Ч. Ч.
2,000–2,010 Dolos 15% g 50–90 Grain Rango Ceme Access Other	tone; dark gray to moderate gray porosity: intergranular, intercrystalline 0% altered; euhedral size: microcrystalline e: microcrystalline to fine; moderate indu nt type(s): dolomite cement ssory minerals: iron stain—02% features: sucrosic	ration	
Fossil 2,010–2,020 Dolos 15% J 50–90 Grain Range Ceme Other Fossil	s: no fossils tone; moderate gray to light gray porosity: intergranular, intercrystalline)% altered; euhedral size: microcrystalline e: microcrystalline to fine; moderate indu nt type(s): dolomite cement features: sucrosic s: no fossils	ration	
2,020–2,030 Dolos 15% j 50–90 Grain Range Ceme Acces Other Fossil	stone; very light gray to light gray porosity: intergranular, intercrystalline 0% altered; euhedral size: microcrystalline e: microcrystalline to fine; moderate indu nt type(s): dolomite cement ssory minerals: iron stain—02% features: sucrosic s: no fossils	ration	
2,030–2,040 Dolos 15% j 10–50 Grain Range Ceme Acces Fossil	tone; very light gray to light gray porosity: intergranular, intercrystalline 0% altered; subhedral size: microcrystalline e: microcrystalline to fine; moderate indu nt type(s): dolomite cement sory minerals: limonite—04%, iron stain s: no fossils	ration 1-02%	

	Moderately to highly altered dolostone
2,040-2,050	Dolostone; light gray to moderate light gray
	15% porosity: intergranular, intercrystalline
	50-90% altered; subhedral
•	Grain size: microcrystalline
	Range: microcrystalline to fine; moderate induration
	Cement type(s): dolomite cement
	Accessory minerals: iron stain-02%
	Fossils: no fossils
2 050-2 060	Dolostone: light gray to moderate light gray
2,000 2,000	15% porosity: intergranular intercrystalline
	50_90% altered: subhedral
	Grain size: microcrystalline
	Bange: microcrystalline to fine: moderate induration
	Cement type(s): dolomite cement
	Accessory minerals: limonite_05% iron stain_02%
	Equally no fossile
2 060 2 070	Possils. no lossils
2,000-2,070	15% perositivi intergravular intergravitalling
	50, 00% altered, such a dral
	Su-90% altered; subheural
	Grain size: microcrystalline
	Range: microcrystalline to line; moderate induration
	Cement type(s): dolomite cement
	Accessory minerals: limonite-02%, iron stain-02%
	Fossils: no fossils
2,070-2,080	Dolostone; very light gray to moderate gray
	15% porosity: intergranular, intercrystalline
	50–90% altered; subhedral
	Grain size: microcrystalline
	Range: microcrystalline to fine; moderate induration
	Cement type(s): dolomite cement
	Accessory minerals: limonite-02%, iron stain-02%
	Fossils: no fossils
2,0802,090	Dolostone; very light gray to moderate gray
	15% porosity: intergranular, intercrystalline
	50–90% altered; euhedral
	Grain size: microcrystalline
	Range: microcrystalline to fine; moderate induration
	Cement type(s): dolomite cement
	Other features: sucrosic
	Fossils: no fossils
2,090-2,100	Dolostone; moderate light gray to grayish brown
	15% porosity: intergranular, intercrystalline
	50–90% altered; euhedral
	Grain size: microcrystalline
	Range: microcrystalline to fine; moderate induration
	Cement type(s): dolomite cement
	Accessory minerals: limonite-05%, iron stain-01%
	Other features: sucrosic
	Fossils: no fossils

2,100-2,110	Dolostone; moderate light gray to very light gray
	15% porosity: intergranular, intercrystalline
	50–90% altered; euhedral
	Grain size: microcrystalline
	Range: microcrystalline to fine; moderate induration
	Cement type(s): dolomite cement
	Accessory minerals: limestone-20% limonite-05%
	Iron stoin 01%
	Other features success
	Esserile no fossile
	FOSSIIS: NO TOSSIIS
	Accessory [minerals]: highly recrystallized limestone
2,110–2,120	Limestone; white to very light gray
	20% porosity: intergranular
	Grain type: biogenic, calcilutite
	80% allochemical constituents
	Grain size: medium; range: microcrystalline to medium
	Moderate induration
	Cement type(s): calcilutite matrix
	Accessory minerals: dolomite-30% iron stain-02%
	Other features: high recrystallization
	Equiles no fossile
	russiis, ilu iussiis A aaaaaami [minanala], himbly altered delectore
0 100 0 100 ¹	Accessory [minerals]: mgnly altered dolostone
2,120-2,130	Limestone; white to grayish brown
· · · · · · · · · · · · · · · · · · ·	20% porosity: intergranular
	Grain type: biogenic, calcilutite
	90% allochemical constituents
	Grain size: very fine; range: microcrystalline to fine
	Moderate induration
	Cement type(s): calcilutite matrix
	Accessory minerals: dolomite—50%, limonite—10%
	Iron stain—02%
	Other features: high recrystallization
	Fossils: no fossils
2 130-2 140	Limestone: very light gray
2,130-2,140	2007 porosity interconvolor
	Crain turna historia calailutita
	Oran type: biogenic, calchutte
	90% allochemical constituents
	Grain size: very fine; range: microcrystalline to fine
	Moderate induration
	Cement type(s): calcilutite matrix
	Accessory minerals: dolomite—10%, limonite—04%
	Iron stain—01%, calcite—01%
	Other features: high recrystallization
	Fossils: no fossils
2.140-2.150	Dolostone: very light gray to gravish brown
, · · · · _ , ·	15% porosity: intergranular, intercrystalline
	50–90% altered: eubedral
	Grain size: microcrystalline
	Range: microcrystalline to fine: moderate induction
	Cament type(a): dolomite comment
	Accessory minorales limenite 0500 increates 0500
	Accessory minerals: himonite-25%, iron stain-05%

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·	Fossils: no fossils
2,150-2,160	Dolostone; very light gray to grayish brown
	15% porosity: intergranular, intercrystalline
	50–90% altered: euhedral
	Grain size: microcrystalline
	Range: microcrystalline to fine: moderate induration
	Coment type(s): delemite coment
	A second minimum la limenta 100 inter stain 020
	Accessory minerals: hmonite—10%, iron stain—02%
	Fossils: no fossils
2,160–2,170	Dolostone; very light gray to grayish brown
	15% porosity: intergranular, intercrystalline
	10–50% altered; subhedral
۰.	Grain size: microcrystalline
	Range: microcrystalline to fine; moderate induration
	Cement type(s): dolomite cement
	Accessory minerals: limonite—04%, iron stain—02%
	Fossils: no fossils
2 170-2 180	Dolostone: very light gray to gravish brown
2,170-2,100	15% porosity: intergranular intergravetalline
	10, 50% altered, subhedral
	10–50% altered; subledral
	Grain size: microcrystalline
	Range: microcrystalline to fine; moderate induration
	Cement type(s): dolomite cement
	Accessory minerals: limonite—05%, iron stain—01%
	Fossils: no fossils
2,180-2,190	Limestone; very light gray to light gray
	20% porosity: intergranular
	Grain type: biogenic, calcilutite
	80% allochemical constituents
	Grain size: very fine: range: microcrystalline to fine
	Moderate induration
	Coment type(s): calcilutite matrix
	Other factures, high recruite lightion
	Family no family
0 100 0 000	Fossiis: no fossiis
2,190–2,200	Limestone; very light gray to light gray
	20% porosity: intergranular
	Grain type: biogenic, calcilutite
	70% allochemical constituents
	Grain size: very fine; range: microcrystalline to fine
· · · ·	Moderate induration
	Cement type(s): calcilutite matrix
	Accessory minerals: dolomite-15%, limonite-04%
	Iron stain—01%
	Other features: high recrystallization
	Fossils: no fossils
2 200-2 210	Dolostone: very light gray to gravish brown
<i>2,200 -2,21</i> 0	15% norosity: intergranular intergravitalling
	50.00% altered aubedral
	Sumon size: microarrightalling
	Oram Size. Inicroci ystalling to finge and denote in the st
	Range: microcrystalline to fine; moderate induration
	Cement type(s): dolomite cement

Appendix A

 2,210–2,220 Dolostone very light gray to grayish brown 15% porosity: intergranular, intercrystalline S0–90% altered; euhedral Grain size: microcrystalline to fine; moderate induration Cement type(s): dolomite cement Accessory minerals: limestone—15%, limonite—04% Fossils: no fossils 2,220–2,230 Dolostone; very light gray to grayish brown 15% porosity: intergranular, intercrystalline S0–90% altered; euhedral Grain size: microcrystalline to fine; moderate induration Cement type(s): dolomite cement Accessory minerals: limonite—05% Fossils: no fossils 2,230–2,240 Limestone; white to very light gray 20% porosity: intergranular 2,230–2,240 Limestone; white to very light gray 20% porosity: intergranular 2,230–2,240 Limestone; white to very light gray 20% porosity: intergranular 30% allochemical constituents Grain size: very fine; range: microcrystalline to fine Moderate induration Cement type(s): calcilutite 80% allochemical constituents 3100 Fossils: no fossils 2,240–2,250 Limestone; very light gray to light gray 20% porosity: intergranular Grain type: biogenic, calcilutite 70% allochemical constituents 32,240–2,250 Limestone; very light gray to light gray 20% porosity: intergranular Grain type; biogenic, calcilutite 70% allochemical constituents 32,240–2,250 Limestone; very light gray to light gray 20% porosity: intergranular Grain type; biogenic, calcilutite 70% allochemical constituents 32,250–2,260 Limestone; very light gray to light gray 20% porosity: intergranular Grain type; biogenic, calcilutite 70% allochemical constituents 32,250–2,260 Limestone; very light gray to light gray 20% porosity: intergranular Grain type; biogenic, calcilutite 70% allochemical constituents 32,250–2,260 Limestone; very light gray to light gray 20% porosity: intergranular Grain type; biogenic, calcilutite 70% allochemical constituents 32,250–2,260 Limest		Accessory minerals: limestone—20%, limonite—04% Iron stain—02% Fossils: no fossils
Grain size: microcrystalline Range: microcrystalline to fine; moderate induration Cement type(s): dolomite cement Accessory minerals: limestone—15%, limonite—04% Fossils: no fossils 2,220–2,230 Dolostone; very light gray to grayish brown 15% porosity: intergranular, intercrystalline 50–90% altered; euhedral Grain size: microcrystalline to fine; moderate induration Cement type(s): dolomite cement Accessory minerals: limonite—05% Fossils: no fossils 2,230–2,240 Limestone; white to very light gray 20% porosity: intergranular Grain type: biogenic, calcilutite 80% allochemical constituents Grain size: very fine; range: microcrystalline to fine Moderate induration Cement type(s): calcilutite matrix Accessory minerals: lolomite—15% Other features: high recrystallization Fossils: no fossils 2,240–2,250 Limestone; very light gray to light gray 20% porosity: intergranular Grain type: biogenic, calcilutite 70% allochemical constituents Grain size: very fine; range: microcrystalline to fine Moderate induration Cement type(s): calcilutite 70% allochemical constituents Grain type: biogenic, calcilutite 70% allochemical constituents Grain size: very fine; range: microcrystalline to fine Moderate induration Cement type(s): calcilutite 70% allochemical constituents Grain size: very fine; range: microcrystalline to fine Moderate induration Cement type(s): calcilutite 70% allochemical constituents Grain size: very fine; range: microcrystalline to fine Moderate induration Cement type(s): calcilutite 70% allochemical constituents Grain size: very fine; range: microcrystalline to fine Moderate induration Cement type(s): calcilutite 70% allochemical constituents Grain size: very fine; range: microcrystalline to fine Moderate induration Cement type(s): calcilutite matrix Accessory minerals: dolomite—05%, limonite—05% Iron stain—01% Other features: high recrystallization	2,210–2,220	Highly altered dolostone with recrystallized limestone Dolostone; very light gray to grayish brown 15% porosity: intergranular, intercrystalline 50–90% altered; euhedral
Accessory minerals: limestone—15%, limonite—04% Fossils: no fossils 2,220-2,230 Dolostone; very light gray to grayish brown 15% porosity: intergranular, intercrystalline 50-90% altered; euhedral Grain size: microcrystalline to fine; moderate induration Cement type(s): dolomite cement Accessory minerals: limonite—05% Fossils: no fossils 2,230-2,240 Limestone; white to very light gray 20% porosity: intergranular Grain type: biogenic, calcilutite 80% allochemical constituents Grain size: very fine; range: microcrystalline to fine Moderate induration Cement type(s): calcilutite matrix Accessory minerals: dolomite—15% Other features: high recrystallization Fossils: no fossils 2,240-2,250 Limestone; very light gray to light gray 20% porosity: intergranular Grain size: very fine; range: microcrystalline to fine Moderate induration Cement type(s): calcilutite 70% allochemical constituents Grain size: very fine; range: microcrystalline to fine Moderate induration Cement type(s): calcilutite 70% allochemical constituents Grain size: very fine; range: microcrystalline to fine Moderate induration Cement type(s): calcilutite matrix Accessory minerals: dolomite—10%, iron stain—01% Other features: high recrystallization Fossils: no fossils 2,250-2,260 Limestone; very light gray to light gray 20% porosity: intergranular Grain type: biogenic, calcilutite 70% allochemical constituents Grain size: very fine; range: microcrystalline to fine Moderate induration Fossils: no fossils 2,250-2,260 Limestone; very light gray to light gray 20% porosity: intergranular Grain type: biogenic, calcilutite 70% allochemical constituents Grain size: very fine; range: microcrystalline to fine Moderate induration Cement type(s): calcilutite matrix Accessory minerals: dolomite—05%, limonite—05% Iron stain—01% Other features: high recrystallization		Grain size: microcrystalline Range: microcrystalline to fine; moderate induration Cement type(s): dolomite cement
Fossils: no fossils 2,220–2,230 Dolostone; very light gray to grayish brown 15% porosity: intergranular, intercrystalline S0–90% altered; euhedral Grain size: microcrystalline to fine; moderate induration Cement type(s): dolomite cement Accessory minerals: limonite—05% Fossils: no fossils 2,230–2,240 Limestone; white to very light gray 20% porosity: intergranular Grain type: biogenic, calcilutite 80% allochemical constituents Grain size: very fine; range: microcrystalline to fine Moderate induration Cement type(s): calcilutite matrix Accessory minerals: dolomite—15% Other features: high recrystallization Fossils: no fossils 2,240–2,250 Limestone; very light gray to light gray 20% porosity: intergranular Grain size: very fine; range: microcrystalline to fine Moderate induration Cement type(s): calcilutite 70% allochemical constituents Grain size: very fine; range: microcrystalline to fine Moderate induration Cement type(s): calcilutite 70% allochemical constituents Grain size: very fine; range: microcrystalline to fine Moderate induration Cement type(s): calcilutite matrix Accessory minerals: dolomite—10%, iron stain—01% Other features: high recrystallization Fossils: no fossils 2,250–2,260 Limestone; very light gray to light gray 20% porosity: intergranular Grain size: very fine; range: microcrystalline to fine Moderate induration Cement type(s): calcilutite 70% allochemical constituents Grain size: very fine; range: microcrystalline to fine Moderate induration Cement type(s): calcilutite 70% allochemical constituents Grain size: very fine; range: microcrystalline to fine Moderate induration Cement type(s): calcilutite matrix Accessory minerals: dolomite—05%, limonite—05% Iron stain—01% Other features: high recrystallization		Accessory minerals: limestone-15%, limonite-04%
 2,220-2,230 2,220-2,230 2,220-2,230 2,30-2,240 2,230-2,240 2,230-2,250 2,230-2,250 2,240-2,250 2,250-2,260 2	2 220-2 230	Fossils: no fossils Delestone: very light gray to gravish brown
 S0-90% altered; euhedral Grain size: microcrystalline Range: microcrystalline to fine; moderate induration Cement type(s): colomite cement Accessory minerals: limonite05% Fossils: no fossils 2,230-2,240 Limestone; white to very light gray 20% porosity: intergranular Grain type: biogenic, calcilutite 80% allochemical constituents Grain size: very fine; range: microcrystalline to fine Moderate induration Cement type(s): calcilutite matrix Accessory minerals: dolomite15% Other features: high recrystallization Fossils: no fossils 2,240-2,250 Limestone; very light gray to light gray 20% porosity: intergranular Grain size: very fine; range: microcrystalline to fine Moderate induration Cement type(s): calcilutite 2,240-2,250 Limestone; very light gray to light gray 20% porosity: intergranular Grain size: very fine; range: microcrystalline to fine Moderate induration Cement type(s): calcilutite 70% allochemical constituents Grain size: very fine; range: microcrystalline to fine Moderate induration Cement type(s): calcilutite matrix Accessory minerals: dolomite10%, iron stain01% Other features: high recrystallization Fossils: no fossils 2,250-2,260 Limestone; very light gray to light gray 20% porosity: intergranular Grain type: biogenic, calcilutite 70% allochemical constituents Grain size: very fine; range: microcrystalline to fine Moderate induration Cement type(s): calcilutite 70% allochemical constituents Grain size: very fine; range: microcrystalline to fine Moderate induration Cement type(s): calcilutite matrix Accessory minerals: dolomite05%, limonite05% Iron stain01% Other features: high recrystallization 	2,220-2,230	15% porosity: intergranular, intercrystalline
Grain size: microcrystalline Range: microcrystalline to fine; moderate induration Cement type(s): dolomite cement Accessory minerals: limonite—05% Fossils: no fossils 2,230–2,240 Limestone; white to very light gray 20% porosity: intergranular Grain type: biogenic, calcilutite 80% allochemical constituents Grain size: very fine; range: microcrystalline to fine Moderate induration Cement type(s): calcilutite matrix Accessory minerals: dolomite—15% Other features: high recrystallization Fossils: no fossils 2,240–2,250 Limestone; very light gray to light gray 20% porosity: intergranular Grain type: biogenic, calcilutite 70% allochemical constituents Grain size: very fine; range: microcrystalline to fine Moderate induration Cement type(s): calcilutite 70% allochemical constituents Grain size: very fine; range: microcrystalline to fine Moderate induration Cement type(s): calcilutite matrix Accessory minerals: dolomite—10%, iron stain—01% Other features: high recrystallization Fossils: no fossils 2,250–2,260 Limestone; very light gray to light gray 20% porosity: intergranular Grain type: biogenic, calcilutite 70% allochemical constituents Grain size: very fine; range: microcrystalline to fine Moderate induration Cement type(s): calcilutite 70% allochemical constituents Grain size: very fine; range: microcrystalline to fine Moderate induration Cement type(s): calcilutite 70% allochemical constituents Grain size: very fine; range: microcrystalline to fine Moderate induration Cement type(s): calcilutite matrix Accessory minerals: dolomite—05%, limonite—05% Iron stain—01% Other features: high recrystallization		50–90% altered; euhedral
Range: microcrystalline to fine; moderate induration Cernent type(s): dolomite cement Accessory minerals: limonite—05% Fossils: no fossils 2,230-2,240 Limestone; white to very light gray 20% porosity: intergranular Grain type: biogenic, calcilutite 80% allochemical constituents Grain size: very fine; range: microcrystalline to fine Moderate induration Cernent type(s): calcilutite matrix Accessory minerals: dolomite—15% Other features: high recrystallization Fossils: no fossils 2,240-2,250 Limestone; very light gray to light gray 20% porosity: intergranular Grain type: biogenic, calcilutite 70% allochemical constituents Grain size: very fine; range: microcrystalline to fine Moderate induration Cernent type(s): calcilutite matrix Accessory minerals: dolomite—10%, iron stain—01% Other features: high recrystallization Fossils: no fossils 2,250-2,260 Limestone; very light gray to light gray 20% porosity: intergranular Grain size: very fine; range: microcrystalline to fine Moderate indu		Grain size: microcrystalline
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Accessory minerals: limonite—05% Fossils: no fossils 2,230–2,240 Limestone; white to very light gray 20% porosity: intergranular Grain type: biogenic, calcilutite 80% allochemical constituents Grain size: very fine; range: microcrystalline to fine Moderate induration Cement type(s): calcilutite matrix Accessory minerals: dolomite—15% Other features: high recrystallization Fossils: no fossils 2,240–2,250 Limestone; very light gray to light gray 20% porosity: intergranular Grain type: biogenic, calcilutite 70% allochemical constituents Grain size: very fine; range: microcrystalline to fine Moderate induration Cement type(s): calcilutite matrix Accessory minerals: dolomite—10%, iron stain—01% Other features: high recrystallization Fossils: no fossils 2,250–2,260 Limestone; very light gray to light gray 20% porosity: intergranular Grain size: very fine; range: microcrystalline to fine Moderate induration Cement type(s): calcilutite matrix Accessory minerals: dolomite—10%, iron stain—01% Other features: high recrystallization Fossils: no fossils 2,250–2,260 Limestone; very light gray to light gray 20% porosity: intergranular Grain size: very fine; range: microcrystalline to fine Moderate induration Cement type(s): calcilutite 70% allochemical constituents Grain size: very fine; range: microcrystalline to fine Moderate induration Cement type(s): calcilutite 70% allochemical constituents Grain size: very fine; range: microcrystalline to fine Moderate induration Cement type(s): calcilutite matrix Accessory minerals: dolomite—05%, limonite—05% Iron stain—01% Other features: high recrystallization		Cement type(s): dolomite cement
2,230–2,240 Limestone; white to very light gray 20% porosity: intergranular Grain type: biogenic, calcilutite 80% allochemical constituents Grain size: very fine; range: microcrystalline to fine Moderate induration Cement type(s): calcilutite matrix Accessory minerals: dolomite—15% Other features: high recrystallization Fossils: no fossils Fossils: no fossils 2,240–2,250 Limestone; very light gray to light gray 20% porosity: intergranular Grain type: biogenic, calcilutite 70% allochemical constituents Grain size: very fine; range: microcrystalline to fine Moderate induration Cement type(s): calcilutite 70% allochemical constituents Grain size: very fine; range: microcrystalline to fine Moderate induration Cement type(s): calcilutite matrix Accessory minerals: dolomite—10%, iron stain—01% Other features: high recrystallization Fossils: no fossils Fossils 2,250–2,260 Limestone; very light gray to light gray 20% porosity: intergranular Grain size: very fine; range: microcrystalline to fine Moderate induration Grain size: very fine; range: microcrystalline to fine Moderate induration Cement type(s): calcilutite 70% allo		Accessory minerals: limonite05%
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Iron stain—01% Other features: high recrystallization		Cement type(s): calcilutite matrix
Other features: high recrystallization		1000 1000
		Other features: high recrystallization
Fossils: no fossils		Fossils: no fossils

2,260-2,270	Limestone; very light gray to light gray
	20% porosity: intergranular
	Grain type: biogenic, calcilutite
	80% allochemical constituents
	Grain size: very fine; range: microcrystalline to fine
	Moderate induration
	Cement type(s): calcilutite matrix
	Accessory minerals: limonite—05%
	Other features: high recrystallization
	Fossils: no fossils
2,270-2,280	Limestone; very light gray to very light orange
	20% porosity: intergranular
	Grain type: biogenic, calcilutite
	90% allochemical constituents
	Grain size: very fine; range: cryptocrystalline to fine
	Moderate induration
	Cement type(s): calcilutite matrix
	Accessory minerals: limonite—05%, iron stain—01%
	Other features: medium recrystallization
	Fossils: no fossils
2.280-2.290	Limestone: very light gray to very light orange
-,	20% porosity: intergranular
· .	Grain type: biogenic, calcilutite
	90% allochemical constituents
	Grain size: very fine; range: cryptocrystalline to fine
	Moderate induration
	Cement type(s): calcilutite matrix
	Accessory minerals: limonite—10%, iron stain—02%
	Other features: high recrystallization
	Fossils: no fossils
2.290-2.300	Limestone: very light gray to white
-,,	20% porosity: intergranular
	Grain type: biogenic, calcilutite
	90% allochemical constituents
	Grain size: very fine: range: cryptocrystalline to fine
	Moderate induration
	Cement type(s): calcilutite matrix
	Accessory minerals: limonite-04%
	Other features: medium recrystallization
	Fossils: no fossils
2.300-2.310	Dolostone: very light gray to gravish brown
	15% porosity: intergranular, intercrystalline
	50–90% altered: subhedral
	Grain size: microcrystalline
	Range: microcrystalline to fine: moderate induration
	Cement type(s): dolomite cement
	Accessory minerals: limestone-35%, limonite-05%
	Fossils: no fossils
	Dolostone with accessory highly recrystallized limestone

Appendix A

2,310–2,320	Dolostone; very light gray to grayish brown 15% porosity: intergranular, intercrystalline
	50–90% altered; subhedral
	Grain size: microcrystalline
	Range: microcrystalline to fine; moderate induration
	Accessory minerals: limestone 20% limonite 05%
	Eossils: no fossils
2 320-2 330	Poissins. No rossins Dolostone: very light gray to gravish brown
2,520-2,550	15% porosity: intergranular, intercrystalline
	50–90% altered: subhedral
	Grain size: microcrystalline
	Range: microcrystalline to fine; moderate induration
	Cement type(s): dolomite cement
;	Accessory minerals: limestone-25%, limonite-05%
	Iron stain—02%
	Fossils: no fossils
2,330–2,340	Dolostone; white to very light gray
	15% porosity: intergranular, intercrystalline
	10–50% altered; subhedral
	Grain size: microcrystalline
	Range: microcrystalline to fine; moderate induration
	Cement type(s): dolomite cement
	Accessory minerals: limestone—20%, gypsum—05%, limonite—03%
	Iron stain
	FOSSIIS: NO TOSSIIS
2 240 2 247	Small science gypsum component Delestone: white to very light gray
2,340-2,347	15% porosity: intergranular intergrassialline
	10-50% altered: subbedral
	Grain size: microcrystalline
	Range: microcrystalline to fine: moderate induration
	Cement type(s): dolomite cement
	Accessory minerals: limestone—15%, limonite—05%
	Iron stain-02%
	Fossils: no fossils
2,347-2,350	Dolostone; white to very light orange
	15% porosity: intergranular, intercrystalline
	10-50% altered; subhedral
	Grain size: microcrystalline
	Range: microcrystalline to fine; moderate induration
	Cement type(s): dolomite cement
	Accessory minerals: limestone—10%, gypsum—05%, limonite—05%
	Iron stain—01%
2 250 2 260	Fossils: no fossils
2,350-2,360	15% porosity intergraphic intergraphics
	10-50% altered: subbedral
	Grain size: microcrystalline
	Range: microcrystalline to fine: moderate induration
	Cement type(s): dolomite cement

	Accessory minerals: limonite—05%, gypsum—04%
	Iron stain—01%
	Fossils: no fossils
2,360-2,370	Dolostone; white to very light orange
.,	15% porosity: intergranular, intercrystalline
	10-50% altered; subhedral
	Grain size: microcrystalline
	Range: microcrystalline to fine: moderate induration
	Cement type(s): dolomite cement
	Accessory minerals: limonite-05%, gypsum-05%
	Iron stain—01%
	Fossils: no fossils
2 370-2 380	Dolostone: white to very light orange
2,570-2,500	15% norosity: intergranular intergrystalline
	10-50% altered: subhedral
	Grain size: microorystalline
	Dange: microcrystalline to fine: moderate inducation
	Compart turns(a): dolomite compart
	A concern minorales limenite 05% surgery 02%
	Accessory minerals: milonite-05%, gypsum-02%
	Fron Stain—01%
	Fossils: no fossils
0 000 0 000	Trace iron stains
2,380-2,390	Dolostone; white to very light orange
	15% porosity: intergranular, intercrystalline
	10–50% altered; subhedral
	Grain size: microcrystalline
	Range: microcrystalline to fine; moderate induration
	Cement type(s): dolomite cement
	Accessory minerals: gypsum—10%, limonite—05%
·	Iron stain—02%
	Fossils: no fossils
	Moderately altered iron-stained dolomite
2,390–2,400	Dolostone; white to very light orange
•	15% porosity: intergranular, intercrystalline
	10–50% altered; subhedral
	Grain size: microcrystalline
	Range: microcrystalline to fine; moderate induration
	Cement type(s): dolomite cement
	Accessory minerals: gypsum-10%, limonite-02%
	Iron stain—01%
	Fossils: no fossils
2,400-2,410	Dolostone; white to very light gray
	15% porosity: intergranular, intercrystalline
	10-50% altered; subhedral
	Grain size: microcrystalline
	Range: microcrystalline to fine; moderate induration
	Cement type(s): dolomite cement
	Accessory minerals: gypsum-10%, calcite-04%, limonite-02%
	Iron stain—01%
	Fossils: no fossils
2,410-2,420	Dolostone; white to very light grav
	,

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	15% porosity: intergranular, intercrystalline
	10-50% altered; subhedral
	Grain size: microcrystalline
	Range: microcrystalline to fine; moderate induration
	Cement type(s): dolomite cement
	Accessory minerals: limestone-30%, gypsum-25%, calcite-05%
	Fossils: no fossils
2,420-2,430	Limestone; white
	20% porosity: intergranular
	Grain type: biogenic, calcilutite, skeletal
	90% allochemical constituents
	Grain size: very fine; range: microcrystalline to fine
	Moderate induration
	Cement type(s): calcilutite matrix
	Accessory minerals: gypsum-15%
	Other features: high recrystallization
	Fossils: benthic foraminifera
	Highly recrystallized gypsiferous limestone
2,430-2,440	Limestone; white
	20% porosity: intergranular
	Grain type: biogenic, calcilutite, skeletal
	90% allochemical constituents
	Grain size: very fine; range: microcrystalline to fine
	Moderate induration
	Cement type(s): calcilutite matrix
	Accessory minerals: gypsum—20%
	Other features: high recrystallization
	Fossils: benthic foraminifera
2,440–2,450	Limestone; white
	20% porosity: intergranular
	Grain type: biogenic, calcilutite, skeletal
	80% allochemical constituents
	Grain size: very fine; range: microcrystalline to fine
	Moderate induration
	Cement type(s): calcilutite matrix
	Accessory minerals: gypsum-10%
	Other features: high recrystallization
	Fossils: benthic foraminifera
2,450	Total depth

[Note: Total depth drilled equals 2,443 feet. The lithologic log was primarily described in 10-ft intervals, however. The well was backplugged to a final completion depth of 1,399 feet below land surface.]

APPENDIX B—WATER LEVEL AND WATER QUALITY DATA COLLECTED DURING DRILLING AND DEVELOPMENT

Date-Time	Well Depth	Open	Specific	Chloride,	Thief Sample,	Temperature	Depth to	Depth to Water
	(ft bis)	Hole	Conductance,	Field	Chloride	(°C)	Water Level-	Level-Drilstem
		Interval	Field	(mg/L)	Concentration		Borenole	
00/07/04 4045	4 750		(Lokan)					
96/07/24-1215	1,/50	663			3/			
96/07/24-1128	1,995	908			38			
96/07/09-1536	1,997	910					40.60	
	2,008	921	850					······
	2,018	931	800					
96/07/09-1832	2,025	938	760	34		28		
96/07/09-1850	2,025	938					41.19	44.08
96/07/10-0820	2,025	938					40.88	
	2,030	943	774					
	2,040	953	776					
	2,050	963	987		38	1		
96/07/10-1059	2,054	967	836	53		29		
96/07/10-1115	2,054	967					43.75	47.77
96/07/10-1147	2,061	974					40.78	
96/07/10-1314	2,061	974	915	61		29.5		
	2,070	983	1,785					
	2,080	993	3,194					
96/07/11-1415	2,083	996	2,298	372		28.5		
96/07/11-1433	2,083	996					41.46	45.66
	2.090	1.003	3.300					
	2,100	1.013	2,700					
96/07/11-1715	2.112	1.025	1.858	310		29		
96/07/11-1743	2.112	1.025					41.23	44.22
	2.120	1.033	2.160					
	2,130	1.043	1.973				·	
· · ·	2,140	1.053	1.794					

Table B1. Water level and water quality data collected during drilling and development

Appendix B

Table B1—Continued

Date-Time	Well Depth (ft bis)	Open Hole Interval (ft)	Specific Conductance, Field (µS/cm)	Chloride, Field (mg/L)	Thief Sample, Chloride Concentration (mg/L)	Temperature (°C)	Depth to Water Level— Borehole (ft bmp)	Depth to Water Level—Drillstem During Drilling (ft bmp)
96/07/11-1924	2,141	1,054	1,453	162		28		
96/07/12-0831	2,141	1,054					40.97	
	2,150	1,063	1,764		44			
	2,160	1,073	1,704					
96/07/12-1038	2,172	1,085	1,409	143		28.5		
96/07/12-1106	2,172	1,085					40.61	44.37
	2,180	1,093	1,673					
	2,190	1,103	1,673					
	2,200	1,113	1,849					
96/07/12-1253	2,202	1,115	2,156	371		29		
96/07/12-1322	2,202	1,115					40.78	47.26
	2,210	1,123	2,277					
	2,220	1,133	2,138					
	2,230	1,143	2,834		-			
96/07/12-1600	2,233	1,146	2,114	346		29		
96/07/12-1610	2,233	1,146					40.35	44.76
	2,240	1,153	2,234					
	2,250	1,163	2,345					
	2,260	1,173	2,880			· •		
96/07/12-1740	2,264	1,177	2,509	486		29		
96/07/15-0904	2,264	1,177					41.01	
<u>.</u>	2,270	1,183	2,250					
	2,280	1,193	2,870					
	2,290	1,203	2,211					
96/07/15-1103	2,293	1,206	2,038	338		28.5		
96/07/15-1129	2,293	1,206					40.84	47.62

Hydrologic Data from a Lower Floridan Aquifer Well, Central Orange County, Florida

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Table B1—Continued

Date-Time	Well Depth	Open	Specific	Chloride,	Thief Sample,	Temperature	Depth to	Depth to Water
	(ft bis)	Hole	Conductance,	Field	Chloride	-(°C)	Water Level—	Level-Drillstem
		Interval	Field	(mg/L)	Concentration		Borehole	During Drilling
		(ft)	(µS/cm)		(mg/L)		(ft bmp)	(ft bmp)
	2,300	1,213	3,662					
	2,310	1,223	2,733					
	2,320	1,233	2,899					
96/07/15-1309	2,322	1,235	3,364	510		28		
96/07/15-1359	2,322	1,235					40.77	45.42
	2,330	1,243	2,936	-				
	2,340	1,253	3,066					
	2,350	1,263	3,988		1,940			
96/07/15-1702	2,352	1,265	2,390	332		29.5		
96/07/15-1726	2,352	1,265					40.41	43.74
	2,360	1,273	3,636					
96/07/16-0828	2,363	1,276					40.81	
	2,370	1,283	3,296					
	2,380	1,293	3,323					
96/07/16-1057	2,383	1,296	2,611	394		29.5		
96/07/16-1117	2,383	1,296					40.43	46.27
	2,390	1,303	3,418		1,480			
	2,400	1,313	3,531					
	2,410	1,323	3,438					
96/07/16-1458	2,412	1,325	3,438	364		29		
96/07/16-1536	2,412	1,325					40.40	50.37
	2,420	1,333	3,624		112			
	2,430	1,343	3,531					
	2,440	1,353	3,945					
96/07/16-1841	2,443	1,356	4,152	496		28.5		
96/07/17-1851	2,443	1,356	7,749	1,480				

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Table B1—Continued

Date-Time	Well Depth (ft bls)	Open Hole Interval (ft)	Specific Conductance, Field (µS/cm)	Chloride, Field (mg/L)	Thief Sample, Chloride Concentration (mg/L)	Temperature (°C)	Depth to Water Level— Borehole (ft bmp)	Depth to Water Level—Drillstem During Drilling (ft.bmp)
96/07/16-1911	2,443	1,356					40.50	71.05
96/07/17-0759	2,443	1,356					40.78	
96/07/17-0810	2,443	1,356	2,608					
96/07/17-0820	2,443	1,356	2,550					•
96/07/17-0830	2,443	1,356	50,000	17,800				
96/07/17-0833	2,443	1,356	9,595	2,225			,	
96/07/17-0834	2,443	1,356	12,605	2,865				
96/07/17-0837	2,443	1,356	3,103	500				
96/07/17-0930	2,443	1,356	2,091					
96/07/17-1000	2,443	1,356	2,094					

Note: ft = foot

ft bls = feet below land surface

ft bmp = feet below measuring point (top of 16-inch casing)

mg/L = milligrams per liter

 μ S/cm = microsiemens per centimeter

The open hole interval is the interval between the bottom of the original cased well (1,084 feet below land surface) and the well depth. The well depth is the changing total depth of the borehole as drilling occurred.

APPENDIX C—BOREHOLE TELEVISION SURVEY (VIDEO LOG) SUMMARY

Borehole Television Survey (Video Log) Summary Orlando Utilities Commission Southeast Test Well (St. Johns River Water Management District Well OR0636)

Date Logged: July 18, 1996 Depth Logged: 0–2,433 feet below datum (ft bd)

Note: Television surveys were also conducted on January 18, 1996, and September 3, 1996. Borehole conditions appeared, in general, very similar for all three surveys. Differences between the July 18, 1996, survey and the other two video logs are described in this summary.

Land surface datum is top of flange on 16-in. casing (approximately 0.5 ft above land surface). Depths are in feet from this datum.

Casing Data

16-in. diameter casing from land surface to approximately 180 ft bd 8-in. diameter casing from approximately 180 to 1,084 ft bd 7.875-in. borehole from approximately 1,084 to 2,433 ft bd

Note: Visibility in casing is relatively poor due to abundant black precipitate and particles suspended in water column and on casing. Bottom edge of 8-in. casing is jagged and uneven. Black precipitate was not present in January 18, 1996, video.

Borehole Zone 1

Depth: approximately 1,084 to 1,140 ft bd General borehole shape: round to very irregular General borehole wall description: small vugs common, occasional large vugs and vertical fractures

<u>Depth (ft bd)</u>	Notable Features
1,127–1,130	Piece of steel casing tightly wedged against borehole wall. No restriction of less than nominal 8-in. diameter is apparent. At top, piece of casing extends approximately 0.5 ft higher on one side of borehole than it does on other side. Black precipitate covers casing piece.
1,1351,140	Visibility poor due to black precipitate.

1,084–1,140 Black precipitate makes conditions cloudy throughout; precipitate was not visible in January 18, 1996, video.

Borehole Zone 2

Depth: approximately 1,140 to 1,320 ft bd

General borehole shape: round to very angular

General borehole wall description: occasionally smooth, usually rough to very rough; small and large vugs very common

<u>Depth (ft bd)</u> 1,146–1,147	<u>Notable Features</u> Later movement of water visible into small fracture.
1,172–1,176	Large angular fracture and/or cavity on one side of borehole.
1,223–1,225	Cavity on one side of borehole.
1,296–1,299	Full hole cavity.
1,316–1,318	Cavity on one side of borehole.
1,140–1,320	Black precipitate abundant on borehole wall, but not cloudy; white chips (drill cuttings) laying on surfaces of vugs and cavities (not present in January 18, 1996, video).

Borehole Zone 3

Depth: approximately 1,320 to 1,630 ft bd

General borehole shape: round to very angular

General borehole wall description: varies from smooth with abundant small vugs and occasional large vugs to extremely angular with large fractures and broken borehole walls

<u>Depth (ft bd)</u> 1.320–1.348	<u>Notable Features</u> Smooth with few yugs
1 257 1 260	Constructed to 1 250 ft consticulture and flow original in how hole
1,337-1,360	Cavity, full hole to 1,359 ft, vertically upward now visible in borenole.
1,363–1,375	Borehole very irregular with vertically upward flow visible.
1,421–1,422	Full hole cavity.
1,511–1,513	Full hole cavity.
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1,594–1,597	Full hole cavity.
1,320–1,630	Black precipitate and occasional white chips on surfaces of fractures, cavities, and vugs (not present in January 18, 1996, video).
Borehole Zone	4

Depth: approximately 1,630 to 1,840 ft bd General borehole shape: round to semiround General borehole wall description: predominantly smooth; abundant small vugs; few large vugs or fractures

Depth (ft bd)Notable Features1,630–1,840Upward movement of particles (bubbles?) visible throughout interval;
black precipitate not evident.

Borehole Zone 5

Depth: approximately 1,840 to 1,970 ft bd General borehole shape: round to semiround General borehole wall description: smooth to very angular; abundant vugs and fractures;

black precipitate not evident

<u>Depth (ft bd)</u>	<u>Notable Features</u>
1,840–1,842	Full hole cavity.
1,964–1,965	Full hole cavity.

1,840–1,970 Vertically upward movement of particles only occasionally evident.

Borehole Zone 6

Depth: approximately 1,970 to 2,000 ft bd General borehole shape: round to very angular General borehole wall description: very angular; abundant vugs and fractures; black

precipitate not evident

<u>Depth (ft bd)</u> 1,974–1,975	<u>Notable Features</u> Full hole cavity.
1,9951,997	Full hole cavity.
1,970-2,000	Vertically upward borehole flow not visible.

Borehole Zone 7

Depth: approximately 2,000 to 2,080 ft bd General borehole shape: round to angular General borehole wall description: smooth with abundant small vugs to very rough and angular; black precipitate not evident

<u>Depth (ft bd)</u> 2,024–2,026	<u>Notable Features</u> Cavity on one side at 2,024 ft bd, extending all around wall by 2,026 ft bd.
2,034–2,035	Large fracture along one side.
2,0602,062	"Shimmering" effect, with picture slightly out of focus (caused by tool moving through water of different density?). Note: This effect did not occur at this depth in the September 3, 1996, video.
2,0642,065	Full hole cavity.
2,070–2,080	Borehole wall smooth with abundant small and large vugs.
2,030–2,080	Slightly cloudy (not cloudy in September 3, 1996, video).

Borehole Zone 8

Depth: approximately 2,080 to 2,330 ft bd

General borehole shape: round

General borehole wall description: very smooth with no vugs to pitted with occasional large vugs

Depth (ft bd)Notable Features2,080–2,330Slightly cloudy in July 18, 1996, video; not cloudy in September 3, 1996, video.

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2,154–2,156	Borehole wall mottled with white and brown patches.
2,185–2,186	Small fracture on one side of wall.
2,219–2,312	Occasional white patches on borehole wall.
2,224–2,225	"Shimmering" effect, with picture slightly out of focus (caused by tool moving through water of different density?). Note: Only in September 3, 1996, video.
2,273–2,276	"Shimmering" effect again (only in September 3, 1996, video).
2,312–2,330	Abundant white patches on borehole wall.

Borehole Zone 9

Depth: approximately 2,330 to 2,433 ft bd

General borehole shape: round

General borehole wall description: smooth to slightly rough, with marbled white and brown bands; no fractures, few vugs

<u>Depth (ft bd)</u>	<u>Notable Features</u>
2,356	Increase in cloudiness (slightly cloudy in September 3, 1996, video).
2,397–2,420	"Shimmering" effect, with picture slightly out of focus (caused by tool moving through water of different density?). Note: Only in July 18, 1996, video.

APPENDIX D—PACKER TEST DATA AND ANALYSIS

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Key for Appendix D abbreviations and column headings-

ft	foot
ft bls	feet below land surface
ft bmp	feet below measuring point
gpd/ft	gallons per day per foot
gpm	gallons per minute
gpm/ft	gallons per minute per foot
min	minute
µS/cm	microsiemens per centimeter
t	time since pump started [column heading]
ť	elapsed time, recovery [column heading]
t/ť	time since pump started (total time) divided by
	elapsed time, recovery (<i>time since pumping ended</i>)

Date	Time or	Depth to Water Level	Volume	Specific	Comments
	THE TREAM	(ft bmp)	(dallons)*	Field	
			, , , , , , , , , , , , , , , , , , ,	(µS/cm)	
8/19/96	1050			540	
8/19/96	1100-1102		100.2		Purge with air line
8/19/96	1100	49.5			
8/19/96	1110	149.7			
8/19/96	1125	140.7			
8/19/96	1130	137.8			
8/19/96	1145	130.2			
8/19/96	1230	113.2			
8/19/96	1330	98.6			
8/19/96	1352	94.8			
8/19/96	1355			620	
8/19/96	1354-1357		60.9		Purge with air line
8/19/96	1402	155.7			
8/19/96	1403	154.7			
8/19/96	1412	148.2			
8/19/96	1432	139.2			
8/19/96	1442	135.0			
8/19/96	1452	130.2			
8/19/96	1502	127.5			
8/19/96	1505	119.4			
8/19/96	1505-1510		37.1	590	Purge with air line
8/19/96	1512	156.5			
8/19/96	1517		·		Water level meter broken
8/19/96	1623-1626	· · · · ·	31		Purge with air line, volume estimated
8/19/96	1623		· · · · · · · · · · · · · · · · · · ·	590	
8/19/96	1733–1737		30	600	Purge with air line,
8/19/96	1847–1850		30	600	Purge with air line,
					volume estimated
8/20/96	0717-0720		60	580	Purge with air line, volume estimated
8/20/96	08330834		30		Purge with air line, volume estimated

Table D1. Data collected during purging of packer interval 1 (2,316-2,386 ft bls), 8/19/96 and 8/20/96

*Volume estimated by assuming 1 gallon per foot of 5-inch-inside-diameter pipe in which drawdown was measured. Estimated total volume purged equals 364 gallons.

Table D2	Data collected	during testing of	of packer interval 2	2 (2,130–2,200 ft bls)	, 8/23/96
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					Specific-Capacity Test			Recovery Test		
Time	Cumulative	Water	Pump	Specific	Elapsed	Drawdown	Elapsed	Residual	Time since	t/ť
	Time since	Level	Rate	Conductance	Time,	from Static	Time,	Drawdown	Pump	
	Beginning of	Change	(gpm)	(µS/cm)	Pumping	Level	Recovery	(ft)	Started	
	Pumping	(ft)*			— (min)	(ft)	[1]		[1]	
	(min)						(min)		(min)	
1634	0.000		0							
1634	0.000		40							
	4.000	87.25	40							
	6.000	87.51	40	× ×						
	8.000	87.67	40							
1643	9.000		0							
1645	11.000	72.91	0							
1646	12.000	5.18	0							
1647	13.000	1.30	0					•		
	13.250	0.44	0							
	13.670	-0.26	0			r				
	17.000	-0.26	0							
1652	18.000		0							
1653	19.000		50							·
	20.000		50	16,000						
	21.000		43	16,000		-				
	23.000		43	16,000						
1712	38.000		50							
1724	50.000	90.00	50							
1725	51.000		0							
1730	56.000	0.00	0							
1825	111.000	-0.29	0							
1834	120.000		0							
1835	121.000		54							
	121.001	23.97	54		0.001	23.97				
	121.003	6.00	54		0.003	6.00				

					Specific-Ca	pacity Test		Recov	ery Test	
Time	Cumulative	Water	Pump	Specific	Elapsed	Drawdown	Elapsed	Residual	Time since	t/ť
	Time since	Level	Rate	Conductance	Time,	from Static	Time,	Drawdown	Pump	
	Beginning of	Change	(gpm)	(µS/cm)	Pumping	Level	Recovery	(ft)	Started	
	Pumping	(ft)*			(min)	(ft)	[r]		[1]	
	(min)						(min)		(min)	
	121.007	4.43	54		0.007	4.43				
	121.010	1.74	54		0.010	1.74				
	121.013	1.08	54		0.013	1.08				
	121.017	3.08	54		0.017	3.08				
	121.020	2.57	54		0.020	2.57				
	121.023	1.85	54		0.023	1.85				
	121.027	4.22	54		0.027	4.22		_		
	121.030	4.59	54		0.030	4.59				
	121.033	3.91	54		0.033	3.91				
	121.050	5.34	54		0.050	5.34				
	121.067	8.50	54		0.067	8.50				
	121.083	8.59	54		0.083	8.59				
	121.100	9.69	54		0.100	9.69				
	121.117	10.94	54		0.117	10.94				
	121.133	12.30	54		0.133	12.30				
	121.150	12.98	54		0.150	12.98				
	121.167	14.32	54		0.167	14.32				
	121.183	15.12	54		0.183	15.12				
	121.200	16.22	54		0.200	16.22				
	121.217	16.75	54	-	0.217	16.75				
	121.233	18.01	54		0.233	18.01				
	121.250	18.47	54		0.250	18.47				
	121.267	19.76	54		0.267	19.76				
	121.283	20.39	54		0.283	20.39				
	121.300	21.25	54		0.300	21.25				
	121.317	22.18	54		0.317	22.18				
	121.333	22.76	54		0.333	22.76				

Table D2---Continued

					Specific-Ca	pacity Test		Recove	ery Test	
Time	Cumulative	Water	Pump	Specific	Elapsed	Drawdown	Elapsed	Residual	Time since	t/ť
	Time since	Level	Rate	Conductance	Time,	from Static	Time,	Drawdown	Pump	
	Beginning of	Change	(gpm)	(µS/cm)	Pumping	Level	Recovery	(ft)	Started	
	Pumping	(ft)*			(min)	(ft)	[1]		[t]	
	(min)						(min)		(min)	
	121.417	27.54	54		0.417	27.54			ř	
	121.500	31.59	54		0.500	31.59				
	121.583	34.82	54		0.583	34.82				
	121.667	38.39	54		0.667	38.39	·			
	121.750	41.22	54		0.750	41.22				
	121.833	43.78	54		0.833	43.78				
	121.917	46.89	54		0.917	46.89				
	122.000	49.39	54		1.000	49.39				
	122.083	52.55	54		1.083	52.55				
	122.167	55.38	54		1.167	55.38				
	122.250	57.61	54		1.250	57.61				
	122.333	59.72	54		1.333	59.72				
	122.417	61.42	54		1.417	61.42				
	122.500	63.59	54		1.500	63.59				
	122.583	65.06	54		1.583	65.06				
	122.667	66.65	54		1.667	66.65				
	122.750	68.41	54		1.750	68.41				
	122.833	69.86	54		1.833	69.86				
	122.917	71.45	54		1.917	71.45				
	123.000	72.92	50		2.000	72.92				
	123.500	79.40	50		2.500	79.40				
	124.000	85.56	50		3.000	85.56				
	124.500	89.27	50		3.500	89.27				
	125.000	91.92	50		4.000	91.92				
	125.500	93.82	50		4.500	93.82				
	126.000	95.15	50		5.000	95.15				
	126.500	95.25	50		5.500	95.25				•

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					Specific-Ca	pacity Test		Recov	ery Test	
Time	Cumulative	Water	Pump	Specific	Elapsed	Drawdown	Elapsed	Residual	Time since	
	Time since	Level	Rate	Conductance	Time,	from Static	Time,	Drawdown	Pump	
	Beginning of	Change	(gpm)	(µS/cm)	Pumping	Level	Recovery	(ft)	Started	
	Pumping	(ft)*			(min)	(ft)	[1]		[t]	
	(min)						(min)		(min)	
1841	127.000	95.25	50	15,500	6.000	95.25				
	127.500	95.25	50		6.500	95.25				
	128.000	95.25	50		7.000	95.25				
	128.500	95.25	50		7.500	95.25				
	129.000	95.26	50	·	8.000	95.26				
	129.500	95.26	50		8.500	95.26				
	130.000	95.26	50		9.000	95.26				
	130.500	95.26	50		9.500	95.26				
1845	131.000	95.26	50	16,000	10.000	95.26				
	133.000	95.26	50		12.000	95.26	,		-	
	135.000	95.26	50	16,000	14.000	95.26				
	137.000	95.26	50		16.000	95.26				
	139.000	95.26	50		18.000	95.26				
	141.000	95.28	50		20.000	95.28				
	143.000	95.28	50		22.000	95.28			· .	
	145.000	95.28	50		24.000	95.28				
	147.000	95.28	50		26.000	95.28				
	149.000	95.26	50		28.000	95.26				· · ·
1905	151.000	95.26	50		30.000	95.26				
1911	157.000		50							
1912	158.000		0	16,100						
	158.001	91.11	0				0.001	91.11	157.001	157,001
1	158.003	90.93	0				0.003	90.93	157.003	47,577
	158.007	90.74	0				0.007	90.74	157.007	23,789
	158.010	90.53	0				0.010	90.53	157.010	15,860
	158.013	90.33	0				0.013	90.33	157.013	11,806
	158.017	90.12	0				0.017	90.12	157.017	9,459

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					Specific-Ce	pacity Test		Recov	ery Test	
Time	Cumulative	Water	Pump	Specific	Elapsed	Drawdown	Elapsed	Residual	Time since	t/t
	Time since	Level	Rate	Conductance	Time,	from Static	Time,	Drawdown	Pump	
	Beginning of	Change	(gpm)	(µS/cm)	Pumping	Level	Recovery	(ft)	Started	
	Pumping	(ft)*			(min)	(ft)	[1]		[1]	
	(min)						(min)		<u>(min)</u>	
	158.020	89.90	0				0.020	89.90	157.020	7,851
	158.023	89.68	0				0.023	89.68	157.023	6,739
	158.027	89.42	0				0.027	89.42	157.027	5,903
	158.030	89.18	0				0.030	89.18	157.030	5,234
	158.033	88.98	0				0.033	88.98	157.033	4,716
	158.050	88.02	0				0.050	88.02	157.050	3,141
	158.067	87.07	• 0				0.067	87.07	157.067	2,358
	158.083	86.11	0				0.083	86.11	157.083	1,886
	158.100	85.19	0				0.100	85.19	157.100	1,571
	158.117	84.06	0				0.117	84.06	157.117	1,347
	158.133	82.80	0				0.133	82.80	157.133	1,179
	158.150	81.70	0				0.150	81.70	157.150	1,048
	158.167	80.83	0				0.167	80.83	157.167	943
	158.183	79.98	0				0.183	79.98	157.183	858
	158.200	79.15	0				0.200	79.15	157.200	786
	158.217	78.30	0				0.217	78.30	157.217	726
	158.233	77.47	0				0.233	77.47	157.233	674
	158.250	76.65	0				0.250	76.65	157.250	629
	158.267	75.82	0			1	0.267	75.82	157.267	590
	158.283	74.98	0				0.283	74.98	157.283	555
	158.300	74.18	0				0.300	74.18	157.300	524
	158.317	73.37	0				0.317	73.37	157.317	497
	158.333	72.58	0				0.333	72.58	157.333	472
	158.417	68.66	0				0.417	68.66	157.417	378
	158.500	64.91	0				0.500	64.91	157.500	315
	158.583	61.28	0				0.583	61.28	157.583	270
	158.667	57.64	0				0.667	57.64	157.667	236

Hydrologic Data from a Lower Floridan Aquifer Well, Central Orange County, Florida

					Specific-Ca	pacity Test		Recov	ery Test	
Time	Cumulative	Water	Pump	Specific	Elapsed	Drawdown	Elapsed	Residual	Time since	1/ť
	Time since	Level	Rate	Conductance	Time,	from Static	Time,	Drawdown	Pump	
	Beginning of	Change	(gpm)	(µS/cm)	Pumping	Level	Recovery	(ft)	Started	
	Pumping	(ft)*			(min)	(ft)	[1]		[1]	
	(min)						(min)		(min)	
	158.750	53.71	0				0.750	53.71	157.750	210
	158.833	49.99	0				0.833	49.99	157.833	189
	158.917	46.78	0				0.917	46.78	157.917	172
	159.000	43.72	0				1.000	43.72	158.000	158
	159.083	40.78	0				1.083	40.78	158.083	146
	159.167	37.96	0				1.167	37.96	158.167	136
	159.250	35.26	0				1.250	35.26	158.250	127
	159.333	32.66	0				1.333	32.66	158.333	119
	159.417	30.20	0	а. 1			1.417	30.20	158.417	112
	159.500	27.81	0				1.500	27.81	158.500	106
	159.583	25.13	0				1.583	25.13	158.583	100
	159.667	22.51	0				1.667	22.51	158.667	95
	159.750	20.56	0				1.750	20.56	158.750	91
	159.833	18.72	0				1.833	18.72	158.833	87
	159.917	16.99	0				1.917	16.99	158.917	83
	160.000	15.34	0				2.000	15.34	159.000	80
	160.500	7.49	0				2.500	7.49	159.500	64
	161.000	2.70	0				3.000	2.70	160.000	53
	161.500	0.40	0				3.500	0.40	160.500	46
	162.000	-0.12	0				4.000	-0.12	161.000	40
	162.500	0.01	0				4.500	0.01	161.500	36
	163.000	-0.01	0				5.000	-0.01	162.000	32
	163.500	-0.06	0				5.500	-0.06	162.500	30
	164.000	-0.04	0				6.000	-0.04	163.000	27
	164.500	-0.06	0				6.500	-0.06	163.500	25
	165.000	-0.07	0				7.000	-0.07	164.000	23

Appendix D

St. Johns River Water Management District 77

					Specific-Ca	pacity Test		Recove	ery Test	
Time	Cumulative Time since Beginning of Pumping (min)	Water Level Change (ft)*	Pump Rate (gpm)	Specific Conductance (µS/cm)	Elapsed Time, Pumping (min)	Drawdown from Static Level (ft)	Elapsed Time, Recovery [Y] (min)	Residual Drawdown (ft)	Time since Pump Started [t] (min)	
	165.500	-0.07	0				7.500	-0.07	164.500	22
	166.000	-0.07	0				8.000	-0.07	165.000	21
	166.500	-0.07	0				8.500	-0.07	165.500	19
	167.000	-0.09	0				9.000	-0.09	166.000	18
	167.500	-0.09	0				9.500	-0.09	166.500	18
	168.000	-0.09	0				10.000	-0.09	167.000	17
	170.000	-0.09	0				12.000	-0.09	169.000	14
	172.000	-0.09	0				14.000	-0.09	171.000	12
	174.000	-0.07	0				16.000	-0.07	173.000	11
	176.000	-0.07	0				18.000	-0.07	175.000	10
	178.000	-0.07	0				20.000	-0.07	177.000	9
	180.000	-0.07	0				22.000	-0.07	179.000	8
	182.000	-0.06	0				24.000	-0.06	181.000	8
	184.000	-0.06	0				26.000	-0.06	183.000	7
	186.000	-0.04	0				28.000	-0.04	185.000	7
1942	188.000	-0.06	0				30.000	-0.06	187.000	6

*Water level relative to static water level at start of initial pumping.

St. Johns River Water Management District 78

					Specific C Tes	Capacity t 1		Recove	ry Test 1		Specific Tes	Capacity at 2		Recover	y Test 2		Pumpin Defl	g during ation
Time	Cumulative Time since Beginning of Pumping (min)	Water Level Change (ft)*	Pump Rate (gpm)	Specific Conductance (µS/cm)	Elapsed Time, Pumping (min)	Drawdown from Static Level (ft)	Elapsed Time, Recovery [t'] (min)	Residual Drawdown (ft)	Time since Pump Started [t] (min)	<u>vr</u>	Elapsed Time, Pumping (min)	Drawdown from Static Level (ft)	Elapsed Time, Recovery [t'] (min)	Residual Drawdown (ft)	Time since Pump Started [t] (min)	Ut'	Elapsed Time, Pumping (min)	Drawdown from Static Level (ft)
1100	0.000		80						.									
1102	2.000	35.71	80	_			-											
1103	3.000	49.80	80															
	4.000	50.50	80	8,500														
	5.000	48.59	80	9,000			-					L						
	6.000	47.89	80	9,000														
ľ	7.000	46.31	80	9,000								ļ	L					
	9.000	45.16	85	9,000														
	10.000	43.38	85	9,100														
1111	11.000		0															
1114	14.000	0.43	0									ļ						
1118	18.000		0					ļ										
1118	18.000	2.24	85	_	0.000	2.24												
	18.003	7.13	85		0.003	7.13							L					
	18.007	7.75	85		0.007	7.75								•				
	18.010	8.85	85		0.010	8.85												
	18.013	6.30	85		0.013	6.30				ļ								
	18.017	9.22	85		0.017	9.22		ļ					_					
	18.020	9.30	85		0.020	9.30												
	18.023	10.07	85		0.023	10.07				ļ								
	18.027	8.59	85		0.027	8.59												
·	18.030	10.97	85		0.030	10.97			ļ									
	18.033	11.86	85		0.033	11.86		ļ				ļ						
<u> </u>	18.050	13.19	85		0.050	13.19						ļ	ļ					
	18.067	13.19	85		0.067	13.19												
	18.083	16.33	85		0.083	16.33												
	18.100	17.79	85		0.100	17.79							_					
<u> </u>	18.117	19.25	85		0.117	19.25						ļ	L					
	18.133	20.20	85		0.133	20.20							L					
	18.150	20.76	85		0.150	20.76												
	18.167	21.80	85		0.167	21.80												
	18.183	23.31	85		0.183	23.31												
	18.200	24.58	85		0.200	24.58												
	18.217	25.26	85		0.217	25.26												
	18.233	26.06	85		0.233	26.06												

Table D3. Data collected during testing of packer interval 3 (2,016-2,086 ft bls), 8/26/96

Table D3—Continued

					Specific (Tes	Capacity it 1		Recover	ry Test 1		Specific Tes	Capacity at 2		Recover	y Test 2		Pumpin Defla	g during ation
Time	Cumulative Time since Beginning of Pumping (min)	Water Level Change (ft)*	Pump Rate (gpm)	Specific Conductance (µS/cm)	Elapsed Time, Pumping (min)	Drawdown from Static Level (ft)	Elapsed Time, Recovery [t'] (min)	Residual Drawdown (ft)	Time since Pump Started [t] (min)	t/ť	Elapsed Time, Pumping (min)	Drawdown from Static Level (ft)	Elapsed Time, Recovery [t'] (min)	Residual Drawdown (ft)	Time since Pump Started [t]	UT	Elapsed Time, Pumping (min)	Drawdown from Static Level (ft)
	10.050	06 70	OF		0.050	06 70		an contractor	and an an and the second second second						(UUU)			
	18 267	20.70	<u> </u>		0.250	20.70							· · · · · · · · · · · · · · · · · · ·					
	18 283	28.53	85		0.283	28.53					+							
	18.300	29.50	85		0.300	29.50												
	18.317	30.16	85		0.317	30.16												
	18.333	30.82	85		0.333	30.82												
	18.417	33.95	85		0.417	33.95												
	18.500	36.66	85		0.500	36.66												
	18.583	39.83	85		0.583	39.83												
	18.667	42.13	85		0.667	42.13												
	18.750	43.73	85		0.750	43.73												
	18.833	45.27	85		0.833	45.27												
	18.917	46.40	85		0.917	46.40										<u> </u>		
	19.000	47.57	85		1.000	47.57												
	19.083	40.54	80		1.083	48.54					<u> </u>		ł					
	19.107	<u>49.3</u> 7	00 95		1.107	49.37							l					
	19.200	50.085	85		1.200	50.00	,											
	19.555	51 23	85		1.555	51.03												
	19.500	51 75	85		1.500	51 75												
	19.583	52.31	85		1.583	52.31			·									
	19.667	52.55	85		1.667	52.55												
	19.750	52.82	85		1.750	52.82					1		1			1		
	19.833	53.24	85		1.833	53.24												
	19.917	53.42	85		1.917	53.42												
	20.000	53.42	85	9,500	2.000	53.42												
	20.500	54.00	85		2.500	54.00												
	21.000	53.82	85		3.000	53.82												
	21.500	53.12	85		3.500	53.12				ļ								
	22.000	52.11	85	9,200	4.000	52.11												
	22.500	51.54	85		4.500	51.54						.					<u> </u>	
ļ	23.000	50.40	85		5.000	50.40						ļ						
	23.500	48.82	85		<u>5.5</u> 00	48.82						ļ		L				
	24.000	46.86	85		6.000	46.86										ļ		
	24.500	44.64	85		6.500	44.64												

					Specific (Tes	Capacity st 1		Recove	ery Test 1		Specific Tes	Capacity st 2		Recover	ry Test 2		Pumpin Defl	g during ation
Time	Cumulative	Water	Pump	Specific	Elapsed	Drawdown	Elapsed	Residual	Time since	t/ť	Elapsed	Drawdown	Elapsed	Residual	Time	t/ť	Elapsed	Drawdown
	Time since	Level	Rate	Conductance	Time,	from Static	Time,	Drawdowr	n Pump -		Time,	from Static	Time,	Drawdown	since		Time,	from Static
	Beginning	Change	(gpm)	(µS/cm)	Pumping	Level	Recovery	(ft)	Started		Pumping	Level	Recovery	(ft)	Pump		Pumping	Level
	of Pumping	(ft)* .			(min)	(Ħ)	[ť]		[1]		(min)	(t)	[[ť]		Started		(min)	(ft)
	(min)						(min)		(min)				(min)		[[] (min)			
		A4 70		0.000	7 000	44 70		Distant and a second se		0.0000000000000000000000000000000000000				The state of the s				
	25.000	41.73	85	9,600	7.000	41.73		<u>_</u>				+						<u></u>
	25.500	39.12	00 05		7.500	39.12						<u> </u>						
	20.000	36.90	00		8.000	37.41			1	<u> </u>								
 	20.500	30.00	05	0.000	0.000	30.00	· •••		<u> </u>			 					· · · · · · · · · · · · · · · · · · ·	
	27.000	35.91	00 85	9,900	9.000	35.72				<u> </u>		<u> </u>					<u> </u>	
	27.500	35 38	85		9.000	35.38												
	30,000	32 91	73	8 900	12,000	32 91						<u> </u>	- <u> </u>	· · · · · ·				
	32,000	32.66	73	10,000	14 000	32.66								· · ·				
	34 000	30.76	73	10,000	16 000	30.76					-				· · · · · · · · · · · · · · · · · · ·			
	36.000	29.61	80	10.000	18.000	29.61			1		1						1	
	38.000	29.27	80		20.000	29.27	<u></u>											
	40.000	28.53	80	10.000	22.000	28.53												
	42.000	28.31	80		24.000	28.31					1							
	44.000	27.87	80		26.000	27.87				[
	46.000	27.82	80		28.000	27.82										1		-
	48.000	28.78	80		30.000	28.78												
	50.000	29.85	80	10,000	32.000	29.85												
	52.000	30.98	80		34.000	30.98												
	54.000	30.56	80		36.000	30.56												
	56.000	30.49	80		38.000	30.49											+	
	58.000	30.20	80		40.000	30.20												
	60.000	30.75	86	10,000	42.000	30.75											<u> </u>	
	62.000	30.81	86		44.000	30.81		ļ	ļ	ļ					ļ		<u> </u>	
	64.000	30.70	86		46.000	30.70			<u> </u>				ļ		ļ			
	66.000	30.45	86		48.000	30.45			L			<u> </u>	ļ		ļ			
	68.000	30.89	86	10,000	50.000	30.89	·	ļ				 		ļ		ļ		
	70.000	30.75	86		52.000	30.75			<u> </u>			<u> </u>		ļ			<u> </u>	
	72.000	30.51	86		54.000	30.51			<u> </u>		_	<u> </u>			ļ			
	74.000	30.38	86		56.000	30.38			ļ			<u> </u>				<u> </u>	<u> </u>	
 	76.000	30.34	86		58.000	30.34		<u> </u>		ļ	ļ	<u> </u>			<u> </u>	<u> </u>	<u> </u>	
	78.000	30.20	86		60.000	30.20			<u> </u>	<u> </u>					<u> </u>		_	
	80.000	30.15	86	10,000	62.000	30.15			L			<u> </u>					-	
	82.000	30.07	86		64.000	30.07			<u> </u>	├────		<u> </u>					<u> </u>	
	84.000	29.74	86		66.000	29.74						1						

Table D3—Continued

					Specific (Tes	Capacity t 1		Recove	ry Test 1		Specific Te	Capacity st 2		Recover	y Test 2		Pumpin Defla	g during ation
Time	Cumulative Time since Beginning of Pumping (min)	Water Level Change (ft)*	Pump Rate (gpm)	Specific Conductance (µS/cm)	Elapsed Time, Pumping (min)	Drawdown from Static Level (ft)	Elapsed Time, Recovery [t] (min)	Residual Drawdown (ft)	Time since Pump Started [t] (min)	νľ	Elapsed Time, Pumping (min)	Drawdown from Static Level (ft)	Elapsed Time, Recovery [t ⁻] (min)	Residual Drawdown (ft)	Time since Pump Started [t] (min)	ťť	Elapsed Time, Pumping (min)	Drawdown from Static Level (ft)
COLOR DE LA COLOR	86,000	29 72	86	andre a arriter at the statement	000 83	29 72		The loss of special stars and the		ananan kultukan ang panganan t			and the second					A SHORE WE HAVE THE PARTY OF
1228	88.000	29.82	86		70.000	29.82						<u> </u>						
1230	90.000		86		, 0.000							+						
1231	91.000		0									<u> </u>						
1231	91.001	31.48	0				0.001	31.48	90.001	90,001	· · · · ·							
	91.003	29.44	0				0.003	29.44	90.003	27,274		T		••••				
	91.007	27.74	0				0.007	27.74	90.007	13,637					· ·			
	91.010	24.06	0				0.010	24.06	90.010	9,092								
	91.013	27.33	0				0.013	27.33	90.013	6,768								
	91.017	28.50	0				0.017	28.50	90.017	5,423								
	91.020	30.78	0				0.020	30.78	90.020	4,501								
	91.023	26.38	0				0.023	26.38	90.023	3,864								
	91.027	25.24	0				0.027	25.24	90.027	3,384								
	91.030	26.00	0				0.030	26.00	90.030	3,001								
	91.033	28.84	0				0.033	28.84	90.033	2,704								
	91.050	24.93	0				0.050	24.93	90.050	1,801								
	91.067	24.43	0				0.067	24.43	90.067	1,352								
	91.083	22.92	0				0.083	22.92	90.083	1,081								
	91.100	22.43	0				0.100	22.43	90.100	901								
	91.117	22.08	0				0.117	22.08	90.117	773								
	91.133	20.62	0				0.133	20.62	90.133	676								·····
	91.150	19.22	0				0.150	19.22	90.150	601								
	91.167	18.29	0				0.167	18.29	90.167	541								
	91.183	17.46	0				0.183	17.46	90.183	492		<u> </u>				ļ		
	91.200	16.60	0				0.200	16.60	90.200	451		<u> </u>	<u>.</u>	· · · · · · · · · · · · · · · · · · ·				
J	91.217	15.67	0				0.217	15.67	90.217	417								
	91.233	14.60	0				0.233	14.60	90.233	387		-						
	91.250	13.80	0				0.250	13.80	90.250	361		+						
	91.267	12.92	0				0.267	12.92	90.267	339		╉────┤			<u> </u>	•		
┣────	91.283	12.12	0				0.283	12.12	90.283	319		+			<u> </u>			
	91.300	11.36	0				0.300	11.36	90.300	301		+						
	91.317	10.47	0				0.317	10.47	90.317	285		╂~───┤						
	91.333	9.63					0.333	9.63	90.333	2/1								
	91.41/	5.54	0				0.417	5.54	90.417	21/					·····			
	91.500	2.98	0				0.500	2.98	90.500	181						I		

•

					Specific Te:	Capacity st 1		Recover	y Test 1		Specific Tes	Capacity st 2		Recover	y Test
Time	Cumulative Time since Beginning of Pumping (min)	Water Level Change (ft)*	Pump Rate (gpm)	Specific Conductance (µS/cm)	Elapsed Time, Pumping (min)	Drawdown from Static Level (ft)	Elapsed Time, Recovery [t [*]] (min)	Residual Drawdown (ft)	Time since Pump Started [t] (min)	К	Elapsed Time, Pumping (min)	Drawdown from Static Level (ft)	Elapsed Time, Recovery [t'] (min)	Residual Drawdown (ft)	Tin sin Pur Star [t (m
	91.583	1.05	0		Contract of the second s		0.583	1.05	90.583	155					
	91.667	-0.29	0				0.667	-0.29	90.667	136				-	
	91.750	-1.10	0				0.750	-1.10	90.750	121		-			<u> </u>
<u> </u>	91.833	-1.39	0				0.833	-1.39	90.833	109					
	91.917	-1.22	0				0.917	-1.22	90.917	99		+			<u> </u>
	92.000	-0.70	0		· · · · · ·		1.000	-0.70	91.000	91				<u></u>	
 	92.083	0.07	0				1.083	0.07	91 083	84				+	+
	92,167	0.95	0				1.167	0.95	91,167	78					1
	92.250	1.77	0				1.250	1.77	91.250	73					+
	92.333	2.42	0				1.333	2.42	91.333	69		· · · · · · · · · · · · · · · · · · ·			1
	92.417	2.79	0				1.417	2.79	91.417	65					
	92.500	2.90	0				1.500	2.90	91.500	61					
]	92.583	2.71	0				1.583	2.71	91.583	58					1
	92.667	2.32	0				1.667	2.32	91.667	55					
	92.750	1.79	0				1.750	1.79	91.750	52					
	92.833	1.21	0				1.833	1.21	91.833	50					
	92.917	0.69	0				1.917	0.69	91.917	48					
	93.000	0.28	0				2.000	0.28	92.000	46					
	93.500	1.17	_0				2.500	1.17	92.500	37					
	94.000	1.63	0				3.000	1.63	93.000	31					
	94.500	0.58	0				3.500	0.58	93.500	27					
	95.000	1.46	0				4.000	1.46	94.000	24					<u> </u>
	95.500	1.10	0				4.500	1.10	94.500	21				ļ	_
ļ	96.000	0.95	0				5.000	0.95	95.000	19				ļ	ļ
	96.500	1.32	0				5.500	1.32	95.500	17					_
	97.000	1.02	0				6.000	1.02	96.000	16					<u> </u>
	97.500	1.16	0				6.500	1.16	96.500	15					<u> </u>
	98.000	1.19	0				7.000	1.19	97.000	14				l	───
	98.500	1.06	0				7.500	1.06	97.500	13					
	99.000	1.19	0				8.000	1.19	98.000	12					╂────
	99.500	1.14	0				8.500	1.14	98.500	12					
	100.000	1.13	0				9.000	1.13	99.000	11					
	100.500	1.19	0				9.500	1.19	99.500	10					<u> </u>
1242	102.000	1.14	0				10.000	1.14	102.000						<u> </u>
<u> 1543 </u>	103.000	1.19	0				12.000	1.19	102.000	9				L	<u> </u>

2		Pumpino Defla	g during ation
ie :e ip :ed 1)	w	Elapsed Time, Pumping (min)	Drawdown from Static Level (ft)
<u>_</u>			

Table D3—Continued

					Specific Te	Capacity st 1		Recove	ry Test 1		Specific (Tes	Capacity t 2		Recover	y Test 2		Pumpin Defla	g during ation
Time	Cumulative Time since Beginning of Pumping (min)	Water Level Change (ft)*	Pump Rate (gpm)	Specific Conductance (µS/cm)	Elapsed Time, Pumping (min)	Drawdown from Static Level (ft)	Elapsed Time, Recovery [t ⁻] (min)	Residual Drawdown (ft)	Time since Pump Started [t] (min)	Vť	Elapsed Time, Pumping (min)	Drawdown from Static Level (ft)	Elapsed Time, Recovery [t'] (min)	Residual Drawdown (ft)	Time since Pump Started [t] (min)	Ŭ.	Elapsed Time, Pumping (min)	Drawdown from Static Level (ft)
1321	141 000		0							CHARGE THE AC						alarra da		
1322	142.000	0.00	46															
	142.001	29.71	46								0.001	29.71		1				
	142.003	6.16	46								0.003	6.16						
	142.007	0.91	46	~							0.007	0.91						
	142.010	-2.31	46								0.010	-2.31			-			
	142.013	-3.11	46								0.013	-3.11						
	142.017	2.18	46								0.017	2.18						
	142.020	1.77	46			· · · · · · · · · · · · · · · · · · ·					0.020	1.77		1				
-	142.023	1.57	46								0.023	1.57						
	142.027	-3.20	46								0.027	-3.20		1				
	142.030	2.75	46								0.030	2.75						
 	142.033	4.05	46								0.033	4.05						
	142.050	3.56	46								0.050	3.56						
	142.067	2.98	46								0.067	2.98		1				
	142.083	4.13	46								0.083	4.13						
	142.100	6.14	46								0.100	6.14						
	142.117	6.69	46								0.117	6.69						
	142.133	7.12	46								0.133	7.12						
	142.150	7.79	46								0.150	7.79						
	142.167	7.21	46								0.167	7.21						
	142.183	9.30	46								0.183	9.30						
	142.200	9.87	46								0.200	9.87						
	142.217	10.45	46								0.217	10.45						
	142.233	10.76	46								0.233	10.76						
	142.250	10.67	46								0.250	10.67						
	142.267	10.84	46								0.267	10.84						
	142.283	11.49	46								0.283	11.49						
	142.300	11.61	46								0.300	11.61						
	142.317	12.02	46								0.317	12.02						
	142.333	11.90	46								0.333	11.90						
	142.417	13.00	46								0.417	13.00						
	142.500	13.47	46								0.500	13.47						
	142.583	13.58	46								0.583	13.58			_			
	142.667	13.91	46								0.667	13.91						

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					Specific Tes	Capacity st 1		Recove	ry Test 1		Specific (Tes	Capacity t 2		Recover	y Test 2
Time	Cumulative Time since Beginning of Pumping	Water Level Change (ft)*	Pump Rate (gpm)	Specific Conductance (µS/cm)	Elapsed Time, Pumping (min)	Drawdown from Static Level (ft)	Elapsed Time, Recovery	Residual Drawdown (ft)	Time since Pump Started It1	t/t'	Elapsed Time, Pumping (min)	Drawdown from Static Level (ft)	Elapsed Time, Recovery	Residual Drawdown (ft)	Tim sinc Pum Startu
	(min)	38. 19			(0111-9) (111-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-	(19	(min)		(min)			N97	(min)		[t]
															(min
	142.750	13.92	46								0.750	13.92			
	142.833	14.14	46								0.833	14.14			
	142.917	14.40	46								0.917	14.40			
	143.000	14.05	46								1.000	14.05			
	143.083	14.43	46								1.083	14.43			
	143.167	14.57	46						-		1.167	14.57			
	143.250	14.55	46								1.250	14.55			
	143.333	14.57	46								1.333	14.57			
	143.417	14.77	46								1.417	14.77			
	143.500	14.29	46								1.500	14.29			
	143.583	14.35	46								1.583	14.35			
	143.667	14.80	46								1.667	14.80			
	143.750	14.69	46	· · · · · · · · · · · · · · · · · · ·							1.750	14.69			
	143.833	14.51	46								1.833	14.51		T	
	143.917	14.60	46								1.917	14.60			
	144.000	14.93	46							Ì	2.000	14.93			
	144.500	14.60	46								2.500	14.60			
	145.000	14.55	46	-							3.000	14.55			
	145.500	14.68	46			·					3.500	14.68			
	146.000	14.82	46	10.000					-		4.000	14.82			
	146.500	14.63	46			†			-		4.500	14.63			
	147.000	14.66	46								5.000	14.66			
1327	147.500	14.68	37						÷		5.500	14.68			
	148.000	14.41	37						-		6.000	14.41			
	148.500	14.60	37					1		-	6.500	14.60			
	149.000	14.25	37	10.000				1			7.000	14.25			
	149.500	14.58	37								7.500	14.58	,,		
	150.000	14.46	37		·····				-		8.000	14.46			
	150,500	14.57	37								8.500	14.57			
	151.000	14.51	37								9.000	14.51			
	151 500	14.38	37								9,500	14.38			
	152,000	14.24	37								10.000	14,24			
	154 000	14 47	37								12,000	14.47			
	156 000	14 40	37								14.000	14.40			
	158.000	14.30	37							<u> </u>	16.000	14.30			

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2	1 1 1	Pumpine Defla	g during ation
e e p ed	<i>ti</i> ř	Elapsed Time, Pumping (min)	Drawdown from Static Level (ft)

Table D3--Continued

					Specific Te:	Capacity st 1		Recove	ry Test 1		Specific (Tes	Capacity t 2		Recover	y Test 2		Pumpin Defla	g during ation
Time	Cumulative Time since Beginning of Pumping	Water Level Change	Pump Rate (gpm)	Specific Conductance (µS/cm)	Elapsed Time, Pumping (min)	Drawdown from Static Level (ft)	Elapsed Time, Recovery	Residual Drawdown (ft)	Time since Pump Started	vť	Elapsed Time, Pumping (min)	Drawdown from Static Level (ft)	Elapsed Time, Recovery	Residual Drawdown (ft)	Time since Pump Started	Vr	Elapsed Time, Pumping (min)	Drawdown from Static Level (ft)
	(min)				, constant		(min)		(min)				(min)		[t] (min)			(9
	160.000	13.94	37								18.000	13.94						
	162.000	14.05	37								20.000	14.05						
	164.000	13.81	37								22.000	13.81						
	166.000	14.35	37	10,000	r						24.000	14.35						
P10.45	168.000	14.10	38								26.000	14.10						
	170.000	13.77	38								28.000	13.77						
	172.000	13.89	38								30.000	13.89						
	174.000	13.89	38	10,000							32.000	13.89						
	176.000	13.83	38								34.000	13.83						
-	178.000	13.89	38								36.000	13.89						
	180.000	13.99	38								38.000	13.99						
	182.000	14.40	38								40.000	14.40						
	184.000	13.89	38	_							42.000	13.89						
····	186.000	13.72	38								44.000	13.72						
	188.000	13.86	38	_							46.000	13.86						
· · · · · · · · · · · · · · · · · · ·	190.000	14.11	38			[48.000	14.11	·					
	192.000	13.77	38								50.000	13.77						
	194.000	14.00	38			[52.000	14.00				1		
· · ·	196.000	13.63	38	10.000							54.000	13.63						
	198.000	13.94	38								56,000	13.94	<u>.</u>					
	200.000	13.77	38							······	58.000	13.77						
	202.000	13.83	38					l			60.000	13.83	<u>-</u>					
	204.000	13.61	38								62.000	13.61						
	206.000	13.61	38								64.000	13.61						
	208.000	13.89	38								66.000	13.89						
	210.000	13.88	38			<u>†</u>		<u> </u>			68.000	13.88						
	212.000	14.02	38								70.000	14.02						
	214.000	13.75	38			<u> </u>					72.000	13.75						
 	216.000	13.81	38	10.000		t					74.000	13.81						
	218.000	13.74	38	,							76.000	13.74						
 	220.000	13.78	38			<u> </u>			[[78.000	13.78		[
	222.000	13.33	38						1		80.000	13.33						
	224,000	13.67	38					<u> </u>			82,000	13.67						
 	226.000	14.13	38			<u>†</u>					84.000	14.13						-
	228.000	13.70	38	10.000							86.000	13.70						

					Specific Te	Specific Capacity Test 1 Elapsed Drawdown El		Recove	ry Test 1		Specific C Tes	Capacity It 2		Recovery	/ Test 2		Pumpin Defla	g during ation
Time	Cumulative Time since Beginning of Pumping (min)	Water Level Change (ft)*	Pump Rate (gpm)	Specific Conductance (µS/cm)	Elapsed Time, Pumping (min)	Drawdown from Static Level (ft)	Elapsed Time, Recovery [t [*]] (min)	Residual Drawdown (ft)	Time since Pump Started [t] (min)	vr	Elapsed Time, Pumping (min)	Drawdown from Static Level (ft)	Elapsed Time, Recovery [t] (min)	Residual Drawdown (ft)	Time since Pump Started [t] (min)	vr	Elapsed Time, Pumping (min)	Drawdown from Static Level (ft)
	230.000	13.48	38								88.000	13.48						
	232.000	13.67	38								90.000	13.67						
	234.000	13.92	38								92.000	13.92						
	236.000	13.89	38								94.000	13.89						
	238.000	13.85	38								96.000	13.85						
·	240.000	13.75	38								98.000	13.75						
	242.000	13.85	38								100.000	13.85						
1512	252.000	13.30	38								110.000	13.30				····-		
1529	269.000		38															
1530	270.000	10.07	0		~									40.07	407.004	407.004	<u></u>	
1530	270.001	10.87	<u>U</u>										0.001	10.87	127.001	127,001		
<u> </u>	270.003	10.00											0.003	10.00	107.003	10 242		
	270.007	10.65	0						<u> </u>				0.007	19.02	127.007	19,243		
	270.010	14 57											0.010	14 57	127.010	9 550		
<u> </u>	270.017	13 77	0										0.017	13 77	127.017	7 652		
	270.020	14.91	0										0.020	14.91	127.020	6.351		-
	270.023	7.78	0										0.023	7.78	127.023	5.452		
	270.027	7.87	0										0.027	7.87	127.027	4,775		
	270.030	10.65	0										0.030	10.65	127.030	4,234		
	270.033	12.19	0										0.033	12.19	127.033	3,815		
	270.050	11.72	0										0.050	11.72	127.050	2,541		
	270.067	8.96	0										0.067	8.96	127.067	1,908		
	270.083	9.22	0										0.083	9.22	127.083	1,526		
	270.100	8.88	0										0.100	8.88	127.100	1,271		
	270.117	7.05	0										0.117	7.05	127.117	1,090		
	270.133	6.82	0										0.133	6.82	127.133	954		
	270.150	5.29	0										0.150	5.29	127.150	848		
L	270.167	5.47	0										0.167	5.47	127.167	763		
	270.183	4.18	0										0.183	4.18	127.183	694		
i	270.200	4.15	0										0.200	4.15	127.200	636		
	270.217	3.74	0										0.217	3.74	127.217	587		
	270.233	3.45	0					ļ					0.233	3.45	127.233	545		
<u> </u>	270.250	2.24	0										0.250	2.24	127.250	509		
	270.267	2.35	0										0.267	2.35	127.267	477		

Table D3—Continued

					Specific (Tes	Capacity t 1		Recove	ry Test 1		Specific (Tes	Capacity it 2		Recovery	Test 2		Pumping Defla) during Ition
Time	Cumulative Time since Beginning of Pumping (min)	Water Level Change (ft)*	Pump Rate (gpm)	Specific Conductance (µS/cm)	Elapsed Time; Pumping (min)	Drawdown from Static Level (ft)	Elapsed Time, Recovery [t [*]] (min)	Residual Drawdown (ft)	Time since Pump Started [t] (min)	Vř	Elapsed Time, Pumping (min)	Drawdown from Static Level (ft)	Elapsed Time, Recovery [t] (min)	Residual Drawdown (ft)	Time since Pump Started [t] (min)	UK.	Elapsed Time, Pumping (min)	Drawdown from Static Level (ft)
	270.283	1.60	0										0.283	1.60	127.283	449		
	270.300	1.38	0										0.300	1.38	127.300	424		
	270.317	1.14	0										0.317	1.14	127.317	402		
	270.333	0.75	0										0.333	0.75	127.333	382		
	270.417	-0.64	0										0.417	-0.64	127.417	306		
	270.500	-1.60	0										0.500	-1.60	127.500	255		
	270.583	-1.99	0										0.583	-1.99	127.583	219		
	270.667	-1.91	0										0.667	-1.91	127.667	191		
	270,750	-1.41	0					ł					0.750	-1.41	127.750	170		
	270 833	-0.64	0										0.833	-0.64	127 833	153		
	270.000	0.23	0					<u> </u>					0.917	0.23	127 917	, 140		
	270.517	1.08	0										1 000	1.08	128.000	128		
	271.000	1.00	0					<u> </u>					1.083	1.76	128 083	118		
	271.000	2 18	0										1,167	2.18	128 167	110		
	271,250	2.34	0										1.250	2.34	128,250	103		
	271.333	2.20	0				· · · · · · · · · · · · · · · · · · ·	1					1.333	2.20	128.333	96		
	271.417	1.85	0								-		1.417	1.85	128.417	91		
	271.500	1.33	0										1.500	1.33	128,500	86		
	271.583	0.75	0	<u> </u>									1.583	0.75	128.583	81		
	271.667	0.22	0	<u> </u>									1.667	0.22	128.667	77		
	271.750	-0.20	0										1.750	-0.20	128.750	74		
	271.833	-0.47	0										1.833	-0.47	128.833	70		
	271.917	-0.53	0					1					1.917	-0.53	128.917	67		
	272.000	-0.42											2.000	-0.42	129,000	65		
	272 500	1 39	0										2 500	1 39	129 500	52		
	273.000	0.34	0					<u> </u>					3 000	0.34	130,000	43		
	273,500	0.40	0					[3,500	0.40	130,500	37		
	274.000	0.95	0		······································								4.000	0.95	131.000	33		
	274.500	0.29	o										4.500	0.29	131.500	29		
	275.000	0.69	0						t				5.000	0.69	132.000	26		
	275.500	0.64	0					<u> </u>			·		5.500	0.64	132.500	24		
	276.000	0.45	0					<u> </u>					6.000	0.45	133.000	22		
	276.500	0.70	0	. <u> </u>							·		6.500	0.70	133.500	21		
	277.000	0.56	0										7.000	0.56	134.000	19		
	277.500	0.59	0										7.500	0.59	134.500	18		

					Specific Te:	Capacity st 1		Recove	y Test 1		Specific (Tes	Capacity It 2		Recovery	Test 2		Pumpin Defla	g during ation
Time	Cumulative	Water	Pump	Specific	Elapsed	Drawdown	Elapsed	Residual	Time since	t/t'	Elapsed	Drawdown	Elapsed	Residual	Time	t/ť	Elapsed	Drawdown
	Time since.	Level	Rate	Conductance	Time,	from Static	Time,	Drawdown	Pump		Time,	from Static	Time,	Drawdown	since		Time,	from Static
	Beginning	Change	(gpm)	(µS/cm)	Pumping	Level	Recovery	(ft)	Started		Pumping	Level	Recovery	(ft)	Pump		Pumping	Level
	of Pumping		記 派 /		(min)	(ft)	[ť]		[[t]		(min)	(ft)↓	[t]		Started		(min)	(ft)
	(min)		DAMS.				(min)		(min) 🔤		Sec. S.		(min)		[t]			
															(min)			
	278.000	0.64	0								····	h	8.000	0.64	135.000	1/		
	278.500	0.55	0										8.500	0.55	135.500	16		
	279.000	0.61	0							·····			9.000	0.61	136.000	15		
ļ	279.500	0.61	0										9.500	0.61	136.500	14		
ļ	280.000	0.59	0										10.000	0.59	137.000	14		
	282.000	0.64	0										12.000	0.64	139.000	12		
ļ	284.000	0.64	0	_							+	<u> </u>	14.000	0.64	141.000	10		
	286.000	0.64	0							···			16.000	0.64	143.000	9		
	288.000	0.66	0										18.000	0.66	145.000	8		
	290.000	0.66	0										20.000	0.66	147.000	/		
	292.000	0.67	0										22.000	0.67	149.000	/		
	294.000	0.67	0										24.000	0.67	151.000	6		
	296.000	0.69	0										26.000	0.69	153.000	6		
	298.000	0.70	0									h	28.000	0.70	155.000	6		
[300.000	0.70	0										30.000	0.70	157.000	5		
1001	302.000	0.70	0										32.000	0.70	159.000	5		
1604	304.000	0.72	0				- <u></u> .						34.000	0.72	161.000	5		
1612	312.000		0															
1613	313.000	0.75	84												··· •		0 001	0.75
1613	313.001	0.75	84														0.001	0.75
	313.003	23.39	84								···						0.003	23.39
	313.007	18.59	84							<u>-</u>		ļ					0.007	18.59
	313.010	0.04	84														0.010	<u> </u>
	313.013	3.23	84													-	0.013	3.23
	313.017	0.72	84														0.017	0.72
	313.020	5.01	84														0.020	5.01
	313.023	4.40	84														0.023	4.40
	313.027	4.81	84														0.027	4.81
	313.030	1.4/	84				······································										0.030	1.4/
	313.033	6.60	84	·						· · · · · · · · · · · · · · · · · · ·					<u> </u>		0.033	6.60
	313.050	8.19	84			╞──────┤											0.050	8.19
	313.067	9.52	84			┥───┤											0.067	9.52
	313.083	10.15	84			┟──────┤											0.083	10.15
	313.100	13.00	84														0.100	13.00
	313.117	15.32	84								l						<u> </u>	15.32

					Specific Te	Capacity st 1		Recove	ry Test 1		Specific (Tes	Capacity st 2		Recover	y Test 2		Pumping Defla	g during ation
Time	Cumulative Time since Beginning of Pumping (min)	Water Level Change (ft)*	Pump Rate (gpm)	Specific Conductance (µS/cm)	Elapsed Time, Pumping (min)	Drawdown from Static Level (ft)	Elapsed Time, Recovery [t [*]] (min)	Residual Drawdown (ft)	Time since Pump Started [t] (min)	vr	Elapsed Time, Pumping (min)	Drawdown from Static Level (ft)	Elapsed Time, Recovery [t'] (min)	Residual Drawdown (ft)	Time since Pump Started [t]	L/L	Elapsed Time, Pumping (min)	Drawdown from Static Level (ft)
							(im)		(C				(11111)		(min)			
	313.133	16.82	84														0.133	16.82
	313.150	18.12	84														0.150	18.12
	313.167	18.69	84														0.167	18.69
	313.183	<u>19.</u> 25	84														0.183	19.25
	313.200	<u>21.</u> 25	84								ļ						0.200	21.25
	313.217	22.32	84					ļ			ļ						0.217	22.32
	313.233	23.40	84														0.233	23.40
	313.250	<u>24.10</u>	84														0.250	24.10
L	313.267	<u>24.71</u>	84								<u> </u>						0.267	24.71
	313.283	25.79	84									-					0.283	25.79
	313.300	26.66	84														0.300	26.66
	313.317	27.60	84														0.317	27.60
	313.333	28.14	84									<u> </u>					0.333	28.14
	313.417	31.83	84					· · · ·									0.417	31.83
	313.500	34.69	84														0.500	34.69
	313.583	37.22	84														0.583	37.22
	313.667	40.29	84														0.667	40.29
	313.750	42.27	84														0.750	42.27
	313.833	43.86	84														0.833	43.86
	313.917	45.26	84														0.917	45.26
	314.000	46.29	84														1.000	46.29
	314.083	47.41	84					•				ļ					1.083	47.41
	314.167	48.59	84														1.167	48.59
	314.250	49.36	84														1.250	49.36
	314.333	50.15	84		· · · · ·												1.333	50.15
	314.417	<u>50.79</u>	84									· · · -					1.417	50.79
	314.500	51.28	84														1.500	51.28
	314.583	<u>51.83</u>	84								ļ						1.583	51.83
	314.667	52.49	84														1.667	52.49
	314.750	52.61	84														1.750	52.61
	314.833	53.07	84														1.833	53.07
	314.917	53.31	84			<u> </u>											1.917	53.31
	315.000	53.59	84	10,000		<u> </u>											2.000	53.59
	315.500	54.64	84								_	ļ					2.500	54.64
	316.000	55.25	84														3.000	55.25

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					Specific Te:	Capacity st 1		Recove	ry Test 1		Specific Tes	Capacity st/2		Recover	y Test 2		Pumpin Defia	g during ation
Time	Cumulative Time since Beginning of Pumping (min)	Water Level Change (ft)*	Pump Rate (gpm)	Specific Conductance (µS/cm)	Elapsed Time, Pumping (min)	Drawdown from Static Level (ft)	Elapsed Time, Recovery [t [*]] (min)	Residual Drawdown (ft)	Time since Pump Started [t] (min)	<u>vr</u>	Elapsed Time, Pumping (min)	Drawdown from Static Level (ft)	Elapsed Time, Recovery [t [*]] (min)	Residual Drawdown (ft)	Time since Pump Started [t] (min)	U.	Elapsed Time, Pumping (min)	Drawdown from Static Level (ft)
	316.500	55.57	84					<u></u>									3.500	55.57
	317.000	55.66	84												· · · · · · · · · · · · · · · · · ·		4.000	55.66
	317.500	55.57	84														4.500	55.57
	318.000	55.73	84														5.000	55.73
	318.500	55.87	84														5.500	55.87
	319.000	55.84	84														6.000	55.84
	319.500	55.84	84												-		6.500	55.84
	320.000	55.95	84														7.000	55.95
	320.500	56.02	84														7.500	56.02
	321.000	55.87	84														8.000	55.87
	321.500	55.57	84														8.500	55.57
	322.000	55.66	84														9.000	55.66
	322.500	55.77	84														9.500	55.77
	323.000	55.68	84														10.000	55.68
	325.000	54.91	84	10,100													12.000	54.91
	327.000	51.48	84														14.000	51.48
	329.000	47.00	84														16.000	47.00
	331.000	41.75	84														18.000	41.75
	333.000	36.63	84														20.000	36.63
	335.000	33.86	84														22.000	33.86
	337.000	31.25	84							_							24.000	31.25
	339.000	29.28	84														26.000	29.28
	341.000	27.95	84														28.000	27.95
	343.000	27.84	84														30.000	27.84
	345.000	27.90	84														32.000	27.90
	347.000	28.06	84														34.000	28.06
	349.000	28.76	84														36.000	28.76
	351.000	28.53	84														38.000	28.53
	353.000	28.39	84														40.000	28.39
	355.000	28.28	84														42.000	28.28
	357.000	28.32	84	_											,		44.000	28.32
	359.000	28.10	84	10,900													46.000	28.10
	361.000	28.34	84														48.000	28.34
	363.000	32.38	84														50.000	32.38
	365.000	33.42	84	10,800													52.000	33.42

Table D3—Continued

						Recove	ry Test 1		Specific Te	Capacity st 2		Recover	y Test 2		Pumping Defla	during Ition		
Time	Cumulative Time since Beginning of Pumping	Water Level Change (ft)*	Pump Rate (gpm)	Specific Conductance (µS/cm)	Elapsed Time, Pumping (min)	Drawdown from Static Level (ft)	Elapsed Time, Recovery [t ²]	Residual Drawdown (ft)	Time since Pump Started [t]	<u>vr</u>	Elapsed Time, Pumping (min)	Drawdown from Static Level (ft)	Elapsed Time, Recovery [t [*]]	Residual Drawdown (ft)	Time since Pump Started	UK .	Elapsed Time, Pumping (min)	Drawdown from Static Level (ft)
							(min)		(((((())))))				(min)		(min)			
	367.000	33.15	84						ľ								54.000	33.15
	369.000	33.20	84														56.000	33.20
	371.000	32.73	84														58.000	32.73
	373.000	32.62	84														60.000	32.62
	375.000	32.22	84	···	_												62.000	32.22
	377.000	32.52	84						ļ								64.000	32.52
	379.000	32.03	84														66.000	32.03
	381.000	31.69	84											-			68.000	31.69
	383.000	31.15	84														70.000	31.15
	385.000	30.78	84														72.000	30.78
	387.000	30.64	84								_						74.000	30.64
	389.000	30.56	84														76.000	30.56
	391.000	30.49	84														78.000	30.49
	393.000	30.13	84						·								80.000	30.13
	395.000	30.31	04	10 700							<u> </u>						84,000	30.31
	397.000	29.91	04	10,700													64.000	29.91
	399.000	30.32	04						<u> </u>									30.32
	401.000	20.40	04									<u>-</u>					00.000	30.40
	405.000	20.10	04							····-	<u> </u>				···· ·		90.000	30.10
J	405.000	20.12	04								<u> </u>				· · · ·		92.000	30.12
	407.000	20.20	84								<u> </u>						96,000	20.20
	411 000	30.12	84														98,000	30 12
	413,000	30.02	84						· · · ·	ł	· · · · · · · · · · · · · · · · · · ·						100,000	30.02
	423 000	30.27	84							······							110,000	30.27
	433 000	30 10	84														120 000	30.10
	443,000	30.05	84	10.500		· · · · · ·	···										130.000	30.05
	453,000	29.64	84						· · · · · ·	1							140.000	29.64
	463.000	29.47	84	10,200													150.000	29.47
	473.000	30.15	84														160.000	30.15
	483.000	30.04	84		i			······									170.000	30.04
	493.000	29.72	84														180.000	29.72
	503.000	29.85	84					<u> </u>									190.000	29.85
	513.000	29.44	84	10,100													200.000	29.44
	523.000	23.62	84														210.000	23.62

					Specific Tes	Capacity st 1		Recover	y Test∴1		Specific Te:	Capacity st 2		Recover	y Test 2		Pumpin Defl	g during ation
Time	Cumulative Time since Beginning of Pumping (min)	Water Level Change (ft)*	Pump Rate (gpm)	Specific Conductance (µS/cm)	Elapsed Time, Pumping (min)	Drawdown from Static Level (ft)	Elapsed Time, Recovery [t'] (min)	Residual Drawdown (ft)	Time since Pump Started [t] (min)	UT.	Elapsed Time, Pumping (min)	Drawdown from Static Level (ft)	Elapsed Time, Recovery [t] (min)	Residual Drawdown (ft)	Time since Pump Started [t] (min)	U .	Elapsed Time, Pumping (min)	Drawdown from Static Level (ft)
1951	529.000			2,600													220.000	17.85
1955	533.000	17.85	84															
2000	538.000			2,600														

*Water level relative to static water level at start of initial pumping.

Appendix D

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					Pumpin	g during		Recover	ry Test 1		Specific-Ca	pacity Test		Recover	ry Test 2	
Time of	Cumulative	Water	Pump	Specific	Elapsed	Drawdown	Elapsed	Residual	Time since	t/t/	Elapsed	Drawdown	Elapsed	Residual	Time since	t/ť
Day	Time since	Level	Rate	Conductance	Time,	from Static	. Time,	Drawdown	Pump		Time,	from Static	Time,	Drawdown	Pump	
	Beginning	Change	(gpm)	(µS/cm)	Pumping	Level	Recovery	(ft)	Started		Pumping	Level	Recovery	(ft)	Started	
	of Pumping	(ft)* -			(min)	(ft)	[ť]				(min)	(Ħ)	[ť]			
	(min)	4 00			0.000	4.00	(min)		<u>(niiii)</u>				<u>(min)</u>		((())())	
1155	0.000	-1.68	85		0.000	-1.68									``````````````````````````````````````	
	0.003	-1.68	85		0.003	-1.68						<u> </u>		<u> </u>		
	0.007	- 1.08	85		0.007	- 1.08		<u> </u>								
	0.010	- 1.08	85		0.010	-1.08										
┣────	0.013	- 1.08	05		0.013	-1.00										
	0.017	- 1.00	00		0.017	-1.00		<u> </u>								
	0.020	-1.00	00		0.020	-1.00										
	0.023	-1.00	05		0.023	-1.00		<u> </u>						<u> </u>		
<u> </u>	0.027	-1.00	85		0.027	-1.00										
	0.030	-1.66	85		0.030	-1.66										
	0.055	-1.68	85		0.050	-1.68		<u> </u>								
	0.050	-1.68	85		0.000	-1.68										<u> </u>
┣	0.007	-1.68	85		0.083	-1.68										
	0 100	1.00	85		0.100	1.00										
	0.117	1.16	85		0.117	1.16										
	0.133	6.66	85		0.133	6.66										
	0.150	8.12	85		0.150	8.12										
	0.167	10.26	85		0.167	10.26										
	0.183	12.34	85		0.183	12.34										
	0.200	11.13	85		0.200	11.13		<u> </u>								
∦	0.217	16.99	85		0.217	16.99										
	0.233	17.70	85 20		0.233	10.83										
 	0.230	19.02	85		0.230	19 02										
	0.283	18.55	85		0.283	18.55										
	0.300	21.80	85	i	0.300	21.80										
	0.317	22.33	85		0.317	22.33										
	0.333	23.04	85		0.333	23.04										
	0.417	26.97	85		0.417	26.97	-									
	0.500	30.26	85		0.500	30.26										
	0.583	32.66	85		0.583	32.66										
	0.667	35.01	85		0.667	35.01										
	0.750	3/.51	85 05		0.750	37.51										
	0.033	<u> </u>	00 85		0.033	30.92 	·					<u> </u>				
	0.500 0.583 0.667 0.750 0.833 0.917	30.26 32.66 35.01 37.51 38.92 40.49	85 85 85 85 85 85		0.500 0.583 0.667 0.750 0.833 0.917	30.26 32.66 35.01 37.51 38.92 40.49										

Table D4. Data collected during testing of packer interval 4 (1,945-2,015 ft bls), 8/27/96

			(The second		Pumping during			Recover	ry Test 1		Specific-Ca	pacity Test	Recovery Test 2				
	o 1.4		P	.	Infla	tion	C		1			<u>.</u>	Flamed	Desident	Time		
		water	Pump	Specific	Elapsed	brawdown from Statio	Elapsed	Drawdown	Pump	, vr	Elapseo	from Static	Elapseo	Drawdown	Time since		
	Beginning	Change		(uS/cm)	Pumping		Becovery	(ft)	Started		Pumping		Becovery	(ft)	Started		
T was	of Pumping	(ft)*	(95)	(µo/ciii)	(min)	(ff)	It1	19	[t]		(min)	(ft)	(t ²)		[t]		
	(min)	2.02			. 		(min)		(min)	/45	(, , , , , , , , , , , , , , , , , , ,		(min)		(min)		
	1.000	41.51	85		1.000	41.51		Colored for a grand start of the									
	1.083	42.38	85		1.083	42.38		<u> </u>									
	1.167	42.96	85		1.167	42.96			- <u>-</u> -		<u> </u>						
	1.250	43.76	85		1.250	43.76											
	1.333	44.45	85		1.333	44.45											
	1.417	44.64	85		1.417	44.64	<u> </u>										
	1.500	45.11	85		1.500	45.11											
	1.583	45.49	85		1.583	45.49											
	<u>1.6</u> 67	45.51	85		1.667	45.51		_									
	1.750	<u>45.</u> 81	85		1.750	45.81											
	1.833	45.95	85		1.833	45.95											
L	1.917	46.37	85		1.917	46.37											
	2.000	<u>45.96</u>	85		2.000	45.96								ļ			
	2.500	<u>46.14</u>	85		2.500	46.14											
	3.000	45,49	85		3.000	45.49					<u> </u>						
	3.500	44.96	85		3.500	44.96											
	4.000	44,44	85		4.000	44.44											
L	4.500	43.76	85		4.500	43.76						l		ļ			
┣────┥	5.000	43.51	85		5.000	43.51					l	<u> </u>					
L	5.500	42.85	85		5.500	42.85				····-							
	6.000	42.11	85		6.000	42.11	<u> </u>					<u> </u>					
	6.500	41.34	85		5.500	41.34						}		<u>}</u> }			
	7.000	40.52	05 05		7.000	40.52						h		} 			
	7.500	29.91	00		7.500	39.91						+		<u> </u>		- 11 ⁻ H 211-1	
	8.000	37.68	85		8 500	37.68						<u> </u>		<u> </u>			
┠	9,000	36.48	85		9,000	36.48											
	9 500	35.34	85		9 500	35.34						h					
├	10,000	34 17	85		10,000	34.17	·····					†					
	12.000	25.56	85		12,000	25.56						<u> </u>					
	14.000	15.70	85	<u>.</u>	14.000	15.70						t					
1211	16.000	14.57	85	747	16.000	14.57						1					
	18.000	14.29	85	748	18.000	14.29											
	20.000	16.23	85		20.000	16.23	<u></u>										
	22.000	16.25	85		22.000	16.25											
	24.000	15.40	85		24.000	15.40											

Table D4—Continued

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					Pumpin	g during		Recove	ry Test 1		Specific-Ca	pacity Test	Recovery Test 2			
Time of Dav	Cumulative Time since	Water Level	Pump Rate	Specific Conductance	Elapsed Time,	Drawdown from Static	Elapsed Time,	Residual Drawdown	Time since Pump	t/t′	Elapsed Time,	Drawdown from Static	Elapsed Time,	Residual Drawdown	Time since Pump	t/t′
	Beginning	Change	(gpm)	(µS/cm)	Pumping	Level	Recovery	(ft)	Started		Pumping	Level	Recovery	(ft)	Started	
	of Pumping	(ft)*			(min)	(ft)	[ť]		[t]		(min)	(ft)	[ť]		[t]	
	(min)						<u>(min)</u>		(min)				(min)		(min)	
	26.000	16.82	85		26.000	16.82										
	28.000	19.03	85		28.000	19.03										
	30.000	18.69	85		30.000	18.69										
	32.000	17.96	85		32.000	17.96				ļ						
	34.000	17.52	85		34.000	17.52										
	36.000	18.84	85		36.000	18.84										
	38.000	21.61	85		38.000	21.61								· · · · · · · · · · · · · · · · · · ·		
[40.000	20.92	85		40.000	20.92								l		<u> </u>
	42.000	21.52	85		42.000	21.52										
	44.000	21.39	85		44.000	21.39								l		
	46.000	21.27	85	· ····	46.000	21.27										
	48.000	21.12	85		48.000	21.12										
	50.000	20.92	85		50.000	20.92										
	52.000	20.92	80 85		52.000	20.92		<u> </u>								
	54.000	20.63	00	· · · · · · · · · · · · · · · · · · ·	54.000	20.63			· · · · · ·						· · ·	
	58.000	20.59	00 85		58,000	20.59										
	60,000	20.30	85	<u> </u>	60,000	20.00										
	62,000	19 98	85		62,000	19.98										
	64 000	19.80	85	· · · · · · · · · · · · · · · · · · ·	64 000	19.80										
	66.000	19.90	85		66.000	19.90										
	68.000	19.60	85		68.000	19.60								ł		
	70.000	19.24	85	752	70.000	19.24								İ		
	72.000	19.24	85		72.000	19.24								1		
	74.000	19.19	85		74.000	19.19										
	76.000	19.21	101	· · · · · · · · · · · · · · · · · · ·	76.000	19.21										
	78.000	18.86	101		78.000	18.86										
	80.000	18.73	101		80.000	18.73										
	82.000	18.69	101		82.000	18.69										
	84.000	18.84	101		84.000	18.84										
	86.000	17.84	101	751	86.000	17.84										
,	88.000	18.86	101		88.000	18.86										
	90.000	18.88	101		90.000	18.88										
	92.000	18.34	101		92.000	18.34										
	94.000	17.85	101		94.000	17.85										
	96.000	18.12	93		96.000	18.12									-	

					Pumpin	g during		Recover	y Test 1		Specific-Ca	pacity Test	Recovery Test 2			
Time of Day	Cumulative Time since Beginning of Pumping (min)	Water Level Change (ft)*	Pump Rate (gpm)	Specific Conductance (µS/cm)	Elapsed Time, Pumping (min)	Drawdown from Static Level (ft)	Elapsed Time, Recovery [t'] (min)	Residual Drawdown (ft)	Time since Pump Started [t] (min)	W	Elapsed Time, Pumping (min)	Drawdown from Static Level (ft)	Elapsed Time, Recovery [t'] (min)	Residual Drawdown (ft)	Time since Pump Started [t] (min)	ťť
	98.000	17.70	93		98.000	17.70										
1335	100.000	17.92	93		100.000	17.92		_								
1340	105.000		101	751				L								
1351	116.000		101					_								
1352	117.000		0													
1352	117.001	16.67	0				0.001	16.67	116.001	116,001						
L	117.003	16.74	0				0.003	16.74	116.003	35,153						
	117.007	14.00	0				0.007	14.00	116.007	17,577						
<u> </u>	117.010	19.77	0				0.010	19.77	116.010	11,718						
 	117.013	17.16	0				0.013	17.16	116.013	8,723						
	117.017	14.79	0				0.017	14.79	116.017	6,989						
	117.020	14.00	0				0.020	14.00	116.020	5,801						
	117.023	15.62	0				0.023	15.62	116.023	4,980						
L	117.027	17.43	0				0.027	17.43	116.027	4,362						
	117.030	16.01	0				0.030	16.01	116.030	3,868						
L	117.033	16.83	0				0.033	16.83	116.033	3,484						
<u> </u>	117.050	12.43	0				0.050	12.43	116.050	2,321						
	117.067	12.10	0				0.067	12.10	116.067	1,743						
L	117.083	12.30	0				0.083	12.30	116.083	1,394						
L	117.100	12.04	0				0.100	12.04	116.100	1,161						
	117.117	9.99	0				0.117	9.99	116.117	996						
	117.133	9.18	0				0.133	9.18	116.133	871						
_	117.150	7.79	0		ļ		0.150	7.79	116.150	//4						
	117.167	6.91	0				0.167	6.91	116.167	697						
	117.183	6.4/	0				0.183	6.47	116.183	634						
	117.200	4.32	0				0.200	4.32	116.200	581						
ļ	117.217	3.93	0				0.217	3.93	116.217	537						
	117.233	2.95	0				0.233	2.95	116.233	498						
	117.250	2.35	0				0.250	2.35	116.250	465						
 	117.267	1.98	0	·			0.267	1.98	116.267	436						
	117.283	0.84	- 0				0.283	0.84	116.283	410						
 		0.50	0				0.300	0.50	116.300	388						
L	117.317	-0.17	0				0.317	-0.17	116.317	367						
L	117.333	-0.66	0				0.333	-0.66	116.333	349						
	117.417	-3.06	0				0.417	-3.06	116.417	279						
	117.500	-4.87	0				0.500	-4.87	116.500	233						

Table D4—Continued

					Pumpin	g during		Recover	y Test 1		Specific-Ca	pacity Test	Recovery Test 2			
Time of	Cumulative	Water	Pump	Specific	Elapsed	Drawdown	Elapsed	Residual	Time since	t/ť	Elapsed	Drawdown	Elapsed	Residual	Time since	t/ť
Day	Time since	Level	Rate	Conductance	Time,	from Static	Time,	Drawdown	Pump		Time,	from Static	Time,	Drawdown	Pump	
	Beginning	Change	(gpm)	(µS/cm)	Pumping	Level	Recovery	(ft)	Started		Pumping	Level	Recovery	(ft)	Started	
	of Pumping	(ft)*			(min)	(ft)	[t]		, (t)		(min)	(ft)	[* [ť]		[t]	
	(min)						(min).		(min)				<u>(min)</u>		(min)	
	117.583	-6.03	0				0.583	-6.03	116.583	200						ļ
	117.667	-6.57	0		ļ		0.667	-6.57	116.667	175					· · · · · · · · · · · · · · · · · · ·	
	117.750	-6.53	0				0.750	-6.53	116.750	156						ļ
	117.833	-5.98	0				0.833	-5.98	116.833	140						ļ
	117.917	-5.09	0				0.917	-5.09	116.917	128						ļ
	118.000	-4.02	0				1.000	-4.02	117.000	117				 		
	118.083	-3.00	0				1.083	-3.00	117.083	108	<u> </u>					
	<u>118.1</u> 67	-2.20	0				1.167	-2.20	117.167	100						ļ
	118.250	-1.72	0				1.250	-1.72	117.250	94						
	118.333	-1.60	0				1.333	-1.60	117.333	88	<u>,</u>					
	118.417	-1.80	0				1.417	-1.80	117.417	83						L
	118.500	-2.27	0				1.500	-2.27	117.500	78						<u> </u>
	118.583	-2.90	0				1.583	-2.90	117.583	74						
	118.667	-3.61	0				1.667	-3.61	117.667	71						
	118.750	-4.22	0				1.750	-4.22	117.750	67						
	118.833	-4.70	0				1.833	-4.70	117.833	64						
	118.917	-4.93	0				1.917	-4.93	117.917	62						
	119.000	-4.92	0				2.000	-4.92	118.000	59	_					
	119.500	-2.62	0				2.500	-2.62	118.500	47						
	120.000	-3.85	0				3.000	-3.85	119.000	40						
	120.500	-3.82	0				3.500	-3.82	119.500	34						
	121.000	-3.04	0				4.000	-3.04	120.000	30						
	121.500	-4.02	0				4.500	-4.02	120.500	27	_					
	122.000	-3.33	0				5.000	-3.33	121.000	24						
	122.500	-3.53	0				5.500	-3.53	121.500	22						
	123.000	-3.74	0				6.000	-3.74	122.000	20						
	123.500	-3.33	0				6.500	-3.33	122.500	19	-					
	124.000	-3.69	0				7.000	-3.69	123.000	18						
	124.500	-3.52	0				7.500	-3.52	123.500	16						
	125.000	-3.47	0				8.000	-3.47	124.000	16						
	125.500	-3.63	0				8.500	-3.63	124.500	15						
	126.000	-3.45	0				9.000	-3.45	125.000	14						
	126.500	-3.55	0				9.500	-3.55	125.500	_13						
	127.000	-3.55	0				10.000	-3.55	126.000	13						
Table D4—Continued

Inflation			
Time of DayCumulative Time sinceWater LevelPump Rate (gpm)Specific ConductanceElapsed Time, PumpingDrawdown From Static Recov (min)Elaps From Static (µS/cm)Time of Beginning of Pumping (min)Water Level (t)*Pump (gpm)Specific Conductance (µS/cm)Elapsed Time, Pumping (min)Drawdown Elaps Time, (min)Elaps From Static (Form Static (t)*	d Residual Time since t/t' Drawdown Pump ery (ft) Started [t] (min)	Elapsed Time, Pumping (min) Elapsed from Static Level (ft)	Elapsed Time, RecoveryResidual DrawdownTime since Pumpt/t'Recovery [t'](ft)Started[t'][t][t](min)(min)
129.000 -3.52 0 12	000 -3.52 128.000 1	1	
1406 131.000 -3.49 0 14	000 -3.49 130.000	9	
1425 150.000 0			
1425 150.001 -3.44 103		0.001 -3.44	
150.003 -1.39 103		0.003 -1.39	
		0.007 18.81	
		0.010 4.32	
150.013 -0.39 103		0.013 -0.39	
150.017 -9.90 103		0.017 -9.90	
150.020 0.22 103		0.020 0.22	
150.023 -0.29 103		0.023 -0.29	
150.027 0.28 103		0.027 0.28	
150.030 -1.24 103		0.030 -1.24	
150.033 3.30 103		0.033 3.30	
150.050 4.29 103		0.050 4.29	
150.067 5.64 103		0.067 5.64	
150.083 3.97 103		0.083 3.97	
150.100 8.86 103		0.100 8.86	
150.117 10.20 103		0.117 10.20	
150.133 11.85 103		0.133 11.85	
150.150 11.09 103		0.150 11.09	
150.167 14.07 103		0.167 14.07	
150.183 14.95 103		0.183 14.95	
150.200 16.38 103		0.200 16.38	
150.217 16.69 103		0.217 16.69	
		0.233 17.60	
		0.250 18.59	
		0.267 19.63	
		0.283 20.13	
			
		0.333 22.22	
		0.583 20 47	
	···· ···· ·····	0.667 30.95	

Table D4—Continued

					Pumpin	g during	ing Recovery Test 1					pacity Test		Recover	y Test 2	
											F 1 1		ei -	<u> </u>		and the second second
		water	Pump	Specific	Elapsed	Drawdown	Elapsed	Residual		U. U.	Elapsed	Drawdown from Stotio	Elapsed	Residual	Dump	, vr
Day	I Ime since	Chapter	Hale		Lime,	Irom Static	nime,		Fump		Pumping	nom Static	Pocovoru		Fump	jin.
	of Rumping		(gpin)	(µS/ciii)	(min)	Level (#)	recovery	1 19			(min)	(ff)	Inecovery [+/]	- uv	Started	
	(min)					- 19	(min)		(min)		(iiiii)	(0)	(min)		(min)	
	150 750	32 57	103		Sandi Posto Dilla (M			and an			0 750	32 57			Contraction (10, 047)	
	150.730	33.39	103							İ	0.833	33 39				
	150 917	34 38	103						··		0.917	34.38		<u> </u>	· · · · · · · · · · · · · · · · · · ·	
	151.000	35.40	103					F		· · · · ·	1.000	35.40				
<u>}</u>	151.083	36.31	103				······································				1.083	36.31				
[151.167	36.96	103	2				<u>***</u>			1.167	36.96				
	151.250	37.38	103								1.250	37.38				
	151.333	37.54	103								1.333	37.54				
	151.417	37.98	103				· · · · · · · · · · · · · · · · · · ·				1.417	37.98				
	151.500	38.20	103		[1.500	38.20				
	151.583	38.20	103		·						1.583	38.20				
	151.667	38.09	103								1.667	38.09				
	151.750	38.43	103								1.750	38.43				
	151.833	38.53	103								1.833	38.53				
	151.917	38.51	103								1.917	38.51				
1427	152.000	38.72	103	899							2.000	38.72				
	152.500	38.83	103								2.500	38.83				
	153.000	38.64	103								3.000	38.64				
	153.500	38.67	103								3.500	38.67				
	154.000	38.23	103								4.000	38.23				
	154.500	38.02	103								4.500	38.02				
	155.000	37.66	103	760							5.000	37.66				
	155.500	37.33	103								5.500	37.33				
	156.000	37.32	103								6.000	37.32				
	156.500	36.89	103								6.500	36.89				
_	157.000	36.75	103								7.000	36.75				
	157.500	36.53	103								7.500	<u>36.53</u>				
	158.000	36.20	<u> 103</u>								8.000	36.20				
_	158.500	35.65	103								8.500	35.65				
	159.000	35.26	103								9.000	35.26				
	159.500	35.12	103								9.500	35.12				
	160.000	34.96	103								10.000	34.96		L		
	162.000	33.13	103								12.000	33.13				
	164.000	31.28	103					L			14.000	31.28		L		
	166.000	30.92	103								16.000	30.92		L		
	168.000	30.35	103		L						18.000	30.35		L		

Table D4—Continued

					Pumpin	g during		Recover	y Test 1		Specific-Ca	pacity Test		Recover	y Test 2	
Time of	Cumulative	Water	Pump	Specific	Elapsed	Drawdown	Elapsed	Residual	Time since	t/t′	Elapsed	Drawdown	Elapsed	Residual	Time since	۲/۲
Day	l ime since	Level	Hate (apm)		l ime,	from Static	l Ime,	Drawdown	Pump		l ime,	from Static	lime,	Drawdown (#)	Pump	
	of Pumping	Change: (ft)*		(µS/cill)	(mín)	Level (ft)		(19			(min)			1 (1)		
	(min)	÷			(1111)	(17	(min)		(min)		1		(min)		(min)	
	170,000	30 18	103		2029-02088-079-08-07-486-04-4	and the second second second	(1) III.3 (2007)				20,000	30 18	Constant Constant Constant	2	NUMBER AT LET UT AUTOM	in personal of the second states
	172,000	29.35	103								22.000	29.35				
	174.000	29.33	103								24.000	29.33				
	176.000	28.81	103								26.000	28.81				
	178.000	29.42	103								28.000	29.42				
	180.000	29.03	103	749							30.000	29.03				
	182.000	28.72	103								32.000	28.72				
	184.000	28.80	103								34.000	28.80				
	186.000	28.61	103								36.000	28.61				
	188.000	28.12	103								38.000	28.12				
	190.000	28.26	103	751							40.000	28.26				
	192.000	28.06	103								42.000	28.06				
	194.000	27.84	103								44.000	27.84				
	196.000	27.77	103								46.000	27.77				
	198.000	27.57	103								48.000	27.57				
	200.000	27.35	103								50.000	27.35				
	202.000	26.97	103								52.000	26.97				
	204.000	26.97	103	750							54.000	26.97				
	206.000	26.86	103								56.000	26.86				
	208.000	26.83	103								58.000	26.83				
	210.000	26.67	103								60.000	26.67				
	212.000	26.58	103								62.000	26.58				
	214.000	26.50	103								64.000	26.50				
	216.000	26.30	103								66.000	26.30	·			
	218.000	26.55	103								68.000	26.55				
	220.000	26.41	103								70.000	26.41				
	222.000	26.23	103	746							72.000	26.23				
	224.000	26.12	103								74.000	26.12				
	226.000	25.95	103								76.000	25.95				
	228.000	25.76	103								78.000	25.76				
	230.000	25.75	103					ļ			80.000	25.75				
	232.000	25.53	103			-					82.000	25.53	-			
	234.000	25.48	103	748							84.000	25.48				
	236.000	25.27	103								86.000	25.27				
	238.000	25.60	103								88.000	25.60		ļ		
1	240.000	25.35	103								90.000	25.35				

Table D4—Continued

					Pumpin	g during		Recove	ry Test 1		Specific-Ca	pacity Test		Recover	y Test 2	
Time of	Cumulative	Water	Pump	Specific	Elapsed	Drawdown	Elapsed	Residual	Time since	t/ť	Elapsed	Drawdown from Static	Elapsed	Residual	Time since	t/t′
Day	Beginning	Change	(apm)	(uS/cm)	Pumpina	Level	Recoverv	(ft)	Started		Pumping	Level	Recoverv	(ft)	Started	
	of Pumping	(ft)*		v - 7.	(min)	(ft)	[ť]		[t]		(min)	(ft) (ft)	[ť]		[t]	
	(min)						(min)		(min)				(min)		(min)	
	242.000	25.27	103	<u> </u>							92.000	25.27				
	244.000	25.26	103								94.000	25.26				
	246.000	25.35	103	749							96.000	25.35				
	248.000	24.85	103								98.000	24.85				
1605	250.000	25.02	103					· .			100.000	25.02				
1637	282.000		103													
1638	283.000		0												· · · · · · · · · · · · · · · · · · ·	
1638	283.001	26.78	0										0.001	26.78	132.001	132,001
	283.003	26.71	0										0.003	26.71	132.003	40,001
	283.007	26.67	0										0.007	26.67	132.007	20,001
	283.010	26.69	0										0.010	26.69	132.010	13,334
	283.013	20.35	0										0.013	20.35	132.013	9,926
	283.017	14.49	0										0.017	14.49	132.017	7,953
	283.020	25.43	0										0.020	25.43	132.020	6,601
	283.023	<u>2</u> 4.80	0										0.023	24.80	132.023	5,666
	283.027	29.46	0										0.027	29.46	132.027	4,963
	283.030	25.31	0										0.030	25.31	132.030	4,401
	283.033	<u>23.34</u>	0										0.033	23.34	132.033	3,965
	283.050	23.25	0					<u></u>					0.050	23.25	132.050	2,641
	283.067	23.04	0								ļ		0.067	23.04	132.067	1,983
	283.083	20.83	0				·····						0.083	20.83	132.083	1,586
	283.100	19.11	0										0.100	<u>19.11</u>	132.100	1,321
	283.117	17.87	0								_		0.117	17.87	132.117	1,133
	283.133	17.04	0										0.133	17.04	132.133	991
	283.150	16.28	0										0.150	16.28	132.150	881
	283.167	14.46	0										0.167	<u>14.46</u>	132.167	793
	283.183	13.77	0	_									0.183	<u>13.77</u>	132.183	721
	283.200	12.81	0								<u></u>		0.200	12.81	132.200	661
	283.217	12.08	0										0.217	12.08	132.217	610
	283.233	10.75	0					<u> </u>					0.233	10.75	132.233	567
	283.250	9.73	0							L			0.250	9.73	132.250	529
	283.267	8.70	0										0.267	8.70	132.267	496
	283.283	7.87	0					L			ļ		0.283	7.87	132.283	467
	283.300	6.88	0							L	_		0.300	6.88	132.300	441
	283.317	5.54	0										0.317	5.54	132.317	418
	283.333	4.37	0			_				<u> </u>	L		0.333	4.37	132.333	397

Table D4—Continued

					Pumpin	g during		Recover	y Test 1		Specific-Ca	pacity Test		Recovery	/ Test 2	
Time of Day	Cumulative Time since	Water Level	Pump Rate	Specific Conductance	Elapsed Time,	Drawdown from Static	Elapsed Time,	Residual Drawdown	Time since Pump Started	vť	Elapsed Time, Pumping	Drawdown from Static Level	Elapsed Time, Recovery	Residual Drawdown (ft)	Time since Pump Started	١/٢
	Beginning of Pumping	Change (ft)*	(gpm)	(µS/cm)	Pumping (min)	(ft)	[t']	(1)	[t] (min)		(min)	(ft)	[ť] (min)		[t] (min)	
	(min)					T	<u> (1100)</u>	e or opposite part and an and the set			1		0.417	0.77	132.417	318
	283.417	0.77		/				+					0.500	-2.04	132.500	265
	283.500	-2.04			<u> </u>	┼────							0.583	-4.21	132.583	227
	283.583	-4.21		<u></u>		+							0.667	-5.72	132.667	199
	283.007	-5.72		<u></u>		+							0.750	-6.58	132.750	177
	283.750	-0.30		/		<u> </u>		+					0.833	-6.83	132.833	159
ļ	283.833	-0.03	+	<u>.</u>		┼────		+					0.917	-6.53	132.917	145
	203.917	-0.53		<u>/</u>		+		+					1.000	-5.81	133.000	133
	204.000	-1.70		<u></u>		+	<u> </u>	1	<u> </u>				1.083	-4.79	133.083	123
┣───	204.003	-4.79	+	<u>/</u>	<u>├</u> ────								1.167	-3.71	133.167	114
	204.107	-2.78		<u></u>									1.250) -2.78	133.250	10/
 	204.230	-2.10				<u> </u>							1.333	3 -2.10	133.333	100
<u> </u>	284,333	-1.80			e e	+		1					1.417	-1.80	133.417	94
┣────	284 500	-1.83			<u> </u>	+		1					1.500) -1.83	133.500	
┣────	284 583	-2.18											1.58	3 -2.18	133.583	84
┣────	284 667	-2 75			├───		<u> </u>						1.66	7 -2.75	133.667	
	284 750	-344											1.75	0 -3.44	133.750	70
	284 833	-4.11		<u></u>	<u> </u>								1.83	3 -4.11	133.833	70
┣────	284 917	-4.68		ol									1.91	/ -4.68	133.917	6
	285 000	-5.03	3 (0		1							2.00	-5.03	134.000	0/
	285,500	-3.26	3 (L			2.50		134.500	
	286.000	-3.50		0						L			3.00		135.000	
	286.500	-4.35	5 (0									3.50	0 -4.35	135.500	
	287.000	-3.12	2 (0					L	L			4.00	-3.12	136.000	3(
	287.500	-4.08	3 0	0						<u> </u>			4.50	0 -4.08	130.000	2
<u> </u>	288.000	-3.71	1	0									5.00	0 -3.71	137.000	21
 	288.500	-3.53	3	0						<u> </u>			5.50		137.000	2
 	289.000	-4.00		0					<u> </u>	_			0.00	-4.00	138 500	2
	289.500	-3.53	3	0						<u> </u>			7.00	0 -3.00		21
 	290.000	-3.80	2	0									7.00	0 -3.00	139 500	19
	290.500	-3.78	3	0						<u> </u>			1.50	<u>0 -3.70</u>	140 000	
	291.000	-3.63	3	0						<u> </u>			0.00	0 -3.03	140.000	1
├ ───	291.500	-3.83	3	0					<u> </u>	<u> </u>			0.50	-3.67	141 000	1
	292.000	-3.67	7	0									9.00	00.07	1	L

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Table D4—Continued

1

					Pumpir	ig during		Recove	y Test 1		Specific-Ca	pacity Test		Recover	y Test 2	
Time of Day	Cumulative Time since Beginning of Pumping (min)	Water Level Change (ft)*	Pump Rate (gpm)	Specific Conductance (µS/cm)	Elapsed Time, Pumping (min)	Drawdown from Static Level (ft)	Elapsed Time, Recovery [t [*]] (min)	Residual Drawdown (ft)	Time since Pump Started [t] (min)	vr	Elapsed Time, Pumping (min)	Drawdown from Static Level (ft)	Elapsed Time, Recovery [t'] (min)	Residual Drawdown (ft)	Time since Pump Started [t] (min)	×.
	292.500	-3.71	0										9.500	-3.71	141.500	15
	293.000	-3.75	0										10.000	-3.75	142.000	14
	295.000	-3.69	0										12.000	-3.69	144.000	12
	297.000	-3.69	0										14.000	-3.69	146.000	10
	299.000	-3.69	0										16.000	-3.69	148.000	9
	301.000	-3.67	0						_				18.000	-3.67	150.000	8
	303.000	-3.67	0										20.000	-3.67	152.000	8
	305.000	-3.66	0										22.000	-3.66	154.000	7
	307.000	-3.66	0										24.000	-3.66	156.000	7
	309.000	-3.66	0										26.000	-3.66	158.000	6
	311.000	-3.64	0										28.000	-3.64	160.000	6
	313.000	-3.64	0										30.000	-3.64	162.000	5
	315.000	-3.63	0										32.000	-3.63	164.000	5
	317.000	-3.58	0										34.000	-3.58	166.000	5
1714	319.000	-3.61	0										36.000	-3.61	168.000	5

*Water level relative to static water level at start of initial pumping.

					Step-Dr	awdown		Recove	ry Test 1		Step-Dra	awdown		Recover	y Test 2	
Time of Day	Cumulative Time since Beginning of Pumping	Water Level Change (ft)*	Pump Rate (gpm)	Specific Conductance (µS/cm)	Elapsed Time, Pumping (min)	Drawdown from Static Level (ft)	Elapsed Time, Recovery	Residual Drawdown (ft)	Time since Pump Started [t]	W	Elapsed Time, Pumping (min)	Drawdown from Static Level (ft)	Elapsed Time, Recovery	Residual Drawdown (ft)	Time since Pump Started [t]	UT .
	(min)						(min)		(min)				6.1		(min)	
1342	0.000		0													
1343	0.000		19													
1346	3.000		19	1,700												
1347	4.000		20	950												
1355	12.000	4.71	20	690												
1357	14.000	20.10	20	700												
1359	16.000		67	730												
1401	18.000		67	710												
1403	20.000		67	700												
1411	28.000		67													
1412	29.000		73													
1415	32.000		73	690												
1417	34.000		80	690												
1418	35.000		80	690												
1419	36.000		80	710						<u> </u>						
1420	37.000		80	690												
1427	44.000		80													
1428	45.000		75	690												
1429	46.000		75	690												
1430	47.000		75	700												
1431	48.000		70	690												
1433	50.000		70	690												
1435	52.000		70	690												
	58.000		70													
	59.000		67													
	66.000		6/	690												
1455	72.000		67													
1456	73.000		30	690												
	78.000		30	690												
1510	93.000		- 30				·		 							
151/	94.000					<u> </u>										
1524	102.000	25 00	0									<u> </u>				
1542	120.000	35.00	00	744												
1552	130.000		00 80	/ 14												
	100.000		00					L			<u> </u>					

Table D5. Data collected during testing of packer interval 5 (1,722-1,792 ft bls), 8/28/96

Table D5—Continued

					Step-Dr Te	awdown		Recove	ry Test 1		Step-Dr Tes	awdown st 2		Recove	ry Test
Time of Day	Cumulative Time since	Water Level	Pump Rate	Specific Conductance	Elapsed Time,	Drawdown from Static	Elapsed Time,	Residual Drawdown	Time since Pump	t/t	Elapsed Time,	Drawdown from Static	Elapsed Time,	Residual Drawdown	Time Pu
	Beginning of Pumping	Change (ft)*	(gpm)	(µS/cm)	Pumping (min)	Level (ft)	Recovery [t']	(ft)	Started [t]		Pumping (min)	Level (ft)	Recovery [t']	(ft)	Sta
	(min)						<u>(min)</u>		[<u> (uuu)</u>						
1555	132.000		80	· · · · · · · · · · · · · · · · · · ·		<u></u>									
1556	133.000		0								+				
1605	142.000							+							
1619	156.000	100.00								<u> </u>					<u> </u>
1620	157.000	103.00	80							 		1			
1641	179.000	0.00						-							
1641	178.000	2.23						-		<u> </u>					-
1042	179.000	35.13	6		0.001	35.13									
	179.003	16.38	6		0.001	16.38				<u> </u>					<u> </u>
	179.007	10.00	6		0.000	10.00		1			1				<u> </u>
	179.010	16.86	6		0.010	16.86		1							
	179.013	11.68	6		0.013	11.68									
	179.017	8.85	6		0.017	8.85		1							
	179.020	9.44	6		0.020	9.44		1					<u> </u>	1	
	179.023	9.38	6		0.023	9.38									
	179.027	7.38	6		0.027	7.38									
	179.030	6.96	6		0.030	6.96									
	179.033	11.13	6		0.033	11.13									
	179.050	12.38	6		0.050	12.38							<u> </u>		
	179.067	13.85	6		0.067	13.85									
	179.083	15.09	6		0.083	15.09		1				I			
	179.100	15.62	6		0.100	15.62		-							
	179.117	16.83	6		0.117	16.83									
	179.133	17.63	6		0.133	17.63									
	179.150	18.33	6		0.150	18.33		_							
	179.167	18.88	6		0.167	18.88									
	179.183	18.94	6		0.183	18.94									.
	179.200	20.18	6		0.200	20.18				······					
L	179.217	20.09			0.217	20.09									
	179.233	20.34	6		0.233	20.34		-			- <u> </u>				
	1/9.250	20.57			0.250	20.57									
	1/9.26/	20.45	6		0.267	20.45		i		<u> </u>					
	1/9.283	21.23	6		0.283	21.23									
	179.300	21.45	6		0.300	21.45									
	1/9.31/	21.36	6		0.31/	21.36		1							1

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Table D5—Continued

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Table D5—Continued

	44 1977 - 44				Step-Dr	awdown		Recove	ry Test 1		Step-Dra	awdown		Recove	ry Test 2	
Time of		Water	Pump	Specific	Elapsed	Drawdown	Elansed	Residual	Time since	t/t'	Elapsed	n ∠ Drawdown	Elapsed	Residual	Time since	t/t′
Day	Time since	Level	Rate	Conductance	Time,	from Static	Time,	Drawdown	Pump		Time,	from Static	Time,	Drawdown	Pump	
	Beginning	Change	(gpm)	(µS/cm)	Pumping	Level	Recovery	(ft)	Started		Pumping	Level	Recovery	(ft)	Started	
	of Pumping	(ft)*			(min)	(ft)	(ť)		[t]		(min)	(ft)	. [ť]		(t)	
	(min)				1.970 (1.44)		(min)		(min)					1 C	(min)	
	189.000	31.19	6	i	10.000	<u>31.19</u>										
	191.000	31.14	6	· · · · · · · · · · · · · · · · · · ·	12.000	31.14										
	193.000	31.45	6	719	14.000	31.45										
	195.000	31.80	6		16.000	31.80										
1700	197.000	31.03	6		18.000	31.03										
1702	199.000	32.05	34		20.000	32.05										
	201.000	77.63	34	721	22.000	77.63										
	203.000	97.81	34		24.000	97.81								-		
	205.000	80.19	34		26.000	80.19		<u> </u>								
1/10	207.000	68.81	7.5	127	28.000	68.81										
	209.000	60.00	7.5		30.000	60.00								4		
	211.000	55.00	7.5	710	32.000	55.00						<u> </u>	, , , =			
	213.000	52.05	7.5	/19	34.000	52.05						<u></u>				
	215.000	49.85	7.5		36.000	49.85										
	217.000	48.48	7.5		38.000	48.48										
	219.000	47.50	7.3		40.000	47.50		<u>}</u>				<u> </u>				
	221.000	40.00	7.5		42.000	40.00								-		, .
	223.000	44.05	7.5		44.000	44.05				· · · · · · · · · · · · · · · · · · ·				+		
	223.000	41.91	7.5	715	40.000	41.91		<u> </u>								
1732	229.000	44.89	12.5	/13	50,000	41.40										
1702	231 000	56.07	12.5		52 000	56.07										
	233,000	62.93	12.5	714	54 000	62.93										
1737	234.000		12.5	<u>, , , , , , , , , , , , , , , , , , , </u>	0000	02.00								1		
1738	235.000		0													
	235.001	60.69	0				0.001	60.69	155.001	155.001						
	235.003	65.13	0				0.003	65.13	155.003	46.971						
	235.007	66.81	0				0.007	66.81	155.007	23,486			_			·····
	235.010	68.16	0				0.010	68.16	155.010	15,658						
	235.013	66.29	0				0.013	66.29	155.013	11,655				1		
	235.017	65.98	0				0.017	65.98	155.017	9,338						
	235.020	67.60	0				0.020	67.60	155.020	7,751						
	235.023	66.98	0				0.023	66.98	155.023	6,653						
	235.027	67.36	0				0.027	67.36	155.027	5,828						
	235.030	67.58	0				0.030	67.58	155.030	5,168						
	235.033	67.69	0				0.033	67.69	155.033	4,656						





St. Johns River Water Management District 118



Figure D2. Orlando Utilities Commission Southeast test well: packer interval 2, specific-capacity test

Table D5—Continued

					Step-Dr	awdown		Recover	y Test 1		Step-Dra	awdown		Recover	y Test 2	
Time of	Cumulative	Water	Pump	Specific	Flansed	Drawdown	Elansed	Residual	Time since	t/t'	Elapsed	Drawdown	Elapsed	Residual	Time since	t/t/
Dav-	Time since	Level	Rate	Conductance	Time.	from Static	Time,	Drawdown	Pump		Time,	from Static	Time,	Drawdown	Pump	
	Beginning	Change	(gpm)	(µS/cm)	Pumping	Level	Recovery	(ft)	Started		Pumping	Level	Recovery	(ft)	Started	
	of Pumping	(ft)*			(min)	(ft)	[ť]		[t]		(min) 🛛	(ft)	[ť]	12234	[t]	
	(min)						(min)		(min)						(min)	
	235.050	66.23	0				0.050	66.23	155.050	3,101		[
	235.067	66.70	0				0.067	66.70	155.067	2,328						
	235.083	66.37	0				0.083	66.37	155.083	1,862						
	235.100	66.12	0				0.100	66.12	155.100	1,551						L
	235.117	65.69	0				0.117	65.69	155.117	1,330						
	235.133	65.46	00				0.133	65.46	155.133	1,164						
	235.150	65.02	0				0.150	65.02	155.150	1,034						
	235.167	64.69	0				0.167	64.69	155.167	931				ļ		
·	235.183	64.23	0				<u> </u>	64.23	155.183	847						
 	235.200	63.89	0				0.200	63.89	155.200	776				ļ		
	235.217	63.54	0				0.217	63.54	155.217	717			<u></u>	ļ		
<u> </u>	235.233	63.37	0				0.233	63.37	155.233	665						
	235.250	63.12	0				0.250	63.12	155.250	621				1		
	235.267	62.91	0				0.267	62.91	155.267	582						
	235.283	62.66	0			· · · · · ·	0.283	62.66	155.283	548				I I		
	235.300	62.42	0				0.300	62.42	155.300	518						
 	235.317	62.17	0		<u> </u>		0.317	62.17	155.317	491				<u>├</u>		
	235.333	61.95	0	······		· · · · · · · · · · · · · · · · · · ·	0.333	61.95	155.333	400				<u> </u>	···	N
	235.417	60.80	0				0.417	50.80	155.417	3/3						
	235.500	59.67	0				0.500	59.07	155.500	311				<u> </u>		
	235.583	58.57	0				0.563	57.50	155.563	207				┢─────┤		
	235.667	57.50	0				0.007	57.30	155.007	200		·		<u> </u>		
	235.750	55.40					0.750	55.43	155,730	197						
 	235.633	54 40					0.833	54.42	155.033	170	<u> </u>			<u>├───</u>		
┣───	235.917	52.45	0		<u></u>		1 000	53 45	156,000	170				╂────┼		
	236.000	52.40	0				1.000	52 49	156 083	144						
∦	236.003	51 56	0				1.000	51 56	156 167	134						
 	236.250	50.63					1 250	50.63	156 250	125						
┣───	236 333	49 74					1 333	49 74	156 333	117	· · · · · · · · · · · · · · · · · · ·			┼────┼		
	236 417	48.87			· _ · _ · _ · _ · _ · _ ·		1 417	48.87	156 417	110				┼───┤		
J	236 500	48.01					1.500	48.01	156.500	104						
├	236 583	47 17	0		<u> </u>		1.583	47.17	156.583	99						
	236 667	46.36					1.667	46.36	156.667	94		<u> </u>				
	236 750	45.55	0		<u> </u>		1.750	45.55	156.750	90		└──── ─				
	236.833	44.77					1.833	44.77	156.833	86			<u> </u>	<u>├───</u>		

Table D5—Continued

					Step-Dr	awdown	Recovery Test 1				Step-Dra	wdown	Recovery Test 2			
				ald a state of the second second second second second second second second second second second second second s		st 1					les	t2				
Time of	Cumulative	Water	Pump	Specific	Elapsed	Drawdown	Elapsed	Hesidual	I ime since	₩	Elapsed	Drawdown	Elapsed	Residual	lime since	l t/t
Day	I ime since	Level	Hate		l ime,	from Static	lime,		Pump		l ime, Dumping	from Static	lime,	Urawdown	Pump	
	Beginning	Change	(gpm)	(µS/cm)		Levei	Recovery	(1)	Starteo		Pumping	Level	Hecovery	00	Starteo	
5.00	of Pumping	(I I)			(min)	(1)			(min)		((100))	(1)	(L)		[l] (min)	
							<u>(min)</u>		(((((((<u> </u>	
	236.917	44.00	0				1.917	44.00	156.917	82						
	237.000	43.26	0				2.000	43.26	157.000	79			·			
	237.500	38.97	0				2.500	38.97	157.500	63			·			
	238.000	34.57	0				3.000	34.57	158.000	53						
	238.500	31.56	0				3.500	31.56	158.500	45						
	239.000	28.94	0				4.000	28.94	159.000	40						
L	239.500	26.63	0				4.500	26.63	159.500	35						
	240.000	24.61	0		Ĺ		5.000	24.61	160.000	32						
	240.500	22.84	0				5.500	22.84	160.500	29						
	241.000	21.30	0				6.000	21.30	161.000	27						
	241.500	19.95	0				6.500	19.95	161.500	25						
	242.000	18.77	0				7.000	18.77	162.000	23						
	242.500	17.74	0				7.500	17.74	162.500	22						
	243.000	16.83	0				8.000	16.83	163.000	20						
	243.500	16.03	0				8.500	16.03	163.500	19						
	244.000	15.34	0				9.000	15.34	164.000	18						
	244.500	14.73	0				9.500	14.73	164.500	17						
	245.000	14.19	0				10.000	14.19	165.000	<u> </u>						
1749	246.000	13.28	0				11.000	13.28	_166.000	15						
1752	249.000		0													
1753	250.000		80													
1754	251.000		0		_				-							
1806	263.000		0			_										
1807	264.000		80													
1808	265.000		0													
1853	310.000	4.00	0													
1854	311.000		1.5													
	311.001	3.53	1.5								0.001	3.53				
	311.003	16.93	1.5								0.003	16.93				
	311.007	12.76	1.5								0.007	12.76				
	311.010	4.11	1.5								0.010	4.11				
	311.013	19.43	1.5								0.013	19.43				
	311.017	15.40	1.5	· · · · · · · · · · · · · · · · · · ·							0.017	15.40				
	311.020	11.68	1.5								0.020	11.68				
	311.023	10.47	1.5								0.023	10.47				
	311.027	14.73	1.5								0.027	14.73				

Table D5—Continued

			(134) (134)		Step-Dr	awdown	Recovery Test 1				Step-Dra	wdown	Recovery Test 2			
Time	Currentiations	Watar	Duma	Casalia	Floppod	St] Droudown	Elancod	Dooiduol	Timo oinoo	•10	Elancod	Drowdown	Flopsod	Desidual	Timo olinoo	
			Rate	Conductance	Time	from Static	Time	Drawdown	Pump	N. Star	Time	from Static	Time	Drawdown	Pumn	VL
	Beginning	Change	(apm)	(uS/cm)	Pumping	Level	Becovery	(ft)	Started		Pumpina	Level	Recovery	(ft)	Started	
	of Pumping	(ft)*	192.11	(point)	(min)	(ft)	(ť]		[t]		(min)	(ft)	[ť]		[t]	
	(min)						(min)		(min)		The second second second second second second second second second second second second second second second s				(min)	
	311.030	14.29	1.5						<u> </u>		0.030	14.29				
	311.033	11.99	1.5								0.033	11.99				
	311.050	15.61	1.5								0.050	15.61				
	311.067	14.57	1.5								0.067	14.57				
	311.083	15.39	1.5								0.083	15.39				
	311.100	16.06	1.5								0.100	16.06				
	311.117	17.54	1.5			_					0.117	17.54				
	311.133	17.79	1.5								0.133	17.79				
	311.150	17.65	1.5								0.150	17.65				
	311.167	17.96	1.5								0.167	<u> </u>				
	311.183	17.71	1.5								0.183	17.71				
	311.200	18.26	1.5								0.200	18.26				
	311.217	17.68	1.5								0.217	17.68				
	311.233	17.67	1.5								0.233	<u>17.67</u>				
	311.250	17.65	1.5								0.250	17.65	·			
	311.267	18.25	1.5								0.267	18.25				
	311.283	17.04	1.5						د 		0.283	17.04				
	311.300	17.54	1.5								0.300	17.54				
	311.317	17.51	1.5								0.317	17.51				
ļ	311.333	<u>17.18</u>	1.5								0.333	<u> </u>				
	311.417	17.70	1.5								0.417	17.70				
L	311.500	16.99	1.5								0.500	16.99				
	311.583	17.46	1.5								0.583	17.46				
ļ	311.667	17.46	1.5								0.667	17.46				
l	311.750	17.38	1.5								0.750	17.38	<u> </u>			
L	311.833	16.58	1.5								0.833	16.58			· .	
ļ	311.917	16.69	1.5					ļ			0.917	16.69				
L	312.000	16.96	1 <i>.</i> 5	714	L		<u>.</u>				1.000	16.96				
ļ	312.083	16.66	1.5								1.083	16.66				
ļ	312.167	16.83	1.5								1.167	16.83				
L	312.250	16.31	1.5								1.250	16.31				
		16.50	1.5								1.333	16.50				
L	312.417	16.53	1.5				<u>.</u>				1.417	16.53				
·	312.500	16.50	1.5								1.500	16.50				
ļ	312.583	16.25	1.5								1.583	16.25				
	312.667	16.36	1.5								1.667	16.36				

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Table D5—Continued

					Step-Dr	awdown st 1		Recove	ry Test 1		Step-Dra	iwdown t 2	Recovery Test 2			
Time of Day	Cumulative Time since	Water Level	Pump Rate	Specific Conductance	Elapsed Time,	Drawdown from Static	Elapsed Time,	Residual Drawdown	Time since Pump	t/t′	Elapsed Time,	Drawdown from Static	Elapsed Time,	Residual Drawdown	Time since Pump	t/t'
	Beginning of Pumping	Change (ft)*	(gpm)	(µS/cm)	Pumping (min)	Level (ft)	Recovery [t']	(ft)	[t]		Pumping (min)	Level (ft)	Recovery [t']	(ft)	Started [t]	
							<u>(min)</u>		(11001)		4 750	10.00			<u> </u>	
	312.750	16.80	1.5					<u> </u>			1./50	16.80		<u> </u>		 _
J	312.833	16.25	1.5	ļ			ļ	<u> </u>			1.833	16.25		<u> </u>		ļ
	312.917	16.31	1.5		<u> </u>	<u> -</u>		ļ			1.91/	16.31		 		<u> </u>
	313.000	16.25	1.5		<u> </u>						2.000	16.25				<u> </u>
 	313.500	16.23	1.5		[<u> </u>	{{		2.500	16.23		{		
	314.000	16.14	1.5					<u> </u>			3.000	16.14				
	314.500	15.92	1.5	i 	l			<u> </u>			3.500	15.92				ļ
	315.000	15.83	1.5								4.000	15.83				L
	315.500	16.20	1.5		ļ		l	L			4.500	16.20				ļ
	316.000	15.95	1.5		ļ			L			5.000	15.95				L
	316.500	18.66	5								5.500	18.66				L
	317.000	20.26	5	707							6.000	20.26				
	317.500	21.23	5								6.500	21.23			······································	
	318.000	22.18	5					L			7.000	22.18				L
	318.500	22.63	5								7.500	22.63				
	319.000	23.18	5					[8.000	23.18				
	319.500	23.56	5								8.500	23.56				
	320.000	24.08	4								9.000	24.08				
	320.500	24.32	4								9.500	24.32				
	321.000	24.49	4	574							10.000	24.49				
	323.000	22.65	4							_	12.000	22.65				1
	325.000	19.88	4	· · · · · · · · · · · · · · · · · · ·							14.000	19.88				
	327.000	18.73	4	693							16.000	18.73	· · · · · · · · · · · · · · · · · · ·			
	329.000	51.59	17					T			18.000	51.59				
	331.000	68.10	17								20.000	68.10				
	333.000	76.38	17	670							22.000	76.38				
	335.000	81.45	17			[<u> </u>		<u></u>	24.000	81.45				
	337.000	84.40	17								26.000	84.40				
	339.000	86.35	14.5					<u>├</u> ────			28.000	86.35				
	341.000	87.48	14.5					†			30.000	87.48				
	343 000	88.68	14.5								32.000	88.68				
	345 000	89.07	14.5		<u> </u>			<u> </u>			34.000	89.07				
	347 000	89.78	14.5	506	<u> </u>			<u> </u>			36.000	89 78				
	349 000	90.10	14.5	000				<u> </u>			38,000	90 19				
	351 000	59.00	14.5					<u> </u>			40,000	90.63				
	353 000	00.00	1/ 5	<u> </u>				<u> </u>			42 000	00.00		└──── ┤		
	333.000	90.08	14.5		L	L	L	L			42.000	30.00		L		

Table D5—Continued

					Step-Drawdown Test 1			Recover	y Test 1		Step-Dra	wdown	Recovery Test 2			10
Time of	Cumulative	Water	Pump	Specific	Elapsed	Drawdown	Elapsed	Residual	Time since	t/ť	Elapsed	Drawdown	Elapsed	Residual	Time since	t/t′
Day	Time since	Level	Rate	Conductance	Time,	from Static	_Time,	Drawdown	Pump		Time,	from Static	Time,	Drawdown	Pump	
	Beginning	Change	(gpm)	(µS/cm)	Pumping	Level	Hecovery	(π)	Started		Pumping (min)	Level /ft)	Recovery	(π)	Started	
	(min)	· (1)			erm)		(min)		(min)		((1))	(1)	լել		(min)	
	355,000	01 20	1/ 5						Contraction of the second second second second second second second second second second second second second s		44 000	91.30		100. Balance 100.	(causy)	
┣	357,000	91.00	14.5	607							46.000	91.04				
	359,000	91.51	14.5				<u> </u>				48.000	91.51				<u></u>
	361.000	91.51	14.5					<u> </u>			50.000	91.51				
	363.000	92.03	14.5						· ·····		52.000	92.03				
	365.000	92.21	14.5								54.000	92.21				·
	367.000	92.06	14.5	616					- <u></u> . v		56.000	92.06				
	369.000	92.14	14.5								58.000	92.14				
	371.000	92.34	14.5								60.000	92.34				
	373.000	92.33	14.5								62.000	92.33				
	375.000	92.15	14.5								64.000	92.15				
2000	377.000	92.50	14.5	632				<u> </u>		<u>_</u>	66.000	92.50				
2009	386.000		14.5													
2010	387.000		0					<u> </u>								
	387.001	92.80	0										0.001	92.80	75.001	75,001
	387.003	92.84	0										0.003	92.84	75.003	22,728
	387.007	92.78	0										0.007	92.78	75.007	11,365
	387.010	92.67	0										0.010	92.67	75.010	7,577
	387.013	92.10	0					ļ			L		0.013	92.10	75.013	5,640
 	387.017	92.54	0										0.017	92.54	75.017	4,519
	387.020	91.99	0										0.020	91.99	75.020	3,751
	387.023	92.17	0										0.023	92.17	75.023	3,220
	387.027	92.12	0					ļ					0.027	92.12	75.027	2,821
	387.030	92.14	0										0.030	92.14	75.030	2,501
	387.033	91.93	0										0.033	91.93	/5.033	2,253
	387.050	91.60	0							<u> </u>			0.050	91.60	/5.050	1,501
	387.067	91.32	0										0.007	91.32	75.00/	1,12/
	387.083	91.00	0					<u> </u>					0.083	91.00	75.083	901
ļ	387.100	90.07	0		ļ			<u> </u>				·	0.100	90.07	75.100	/51
	307.117	90.39	0		L			<u> </u>					0.117	30.39	75.117	<u>644</u>
	307.133	90.08	0		<u> </u>		- <u></u>		· · ··· <u>-</u> · · ····				0.100	80.00	75.100	<u>504</u>
	297 167	09.79 09.79	0										0.130	80.19	75.150	
	397 102	80 16	0										0.107	80.16	75 192	401
	387 200	89.10	0					 					0.100	88.85	75 200	376
├ ────	387 217	88.57	0		<u> </u>								0.217	88.57	75.217	347

Table D5—Continued

					Step-Dr	awdown st 1	Recovery Test 1				Step-Dra	awdown				
Time of	Cumulative	Wator	Dump	Specific	Flancod	Drawdown	Flansed	Besidual	Time since	+/+/	Elansed	Drawdown	Elansed	Besidual	Time since	+/+/
Dav.			Bate	Conductance	Time	from Static	Time	Drawdown	Pump		Time	from Static	Time	Drawdown	Pumn	UL
Day	Beginning	Change	(apm)	(uS/cm)	Pumpina	Level	Recovery	(ft)	Started		Pumping	Level	Recoverv	(ft)	Started	
	of Pumping	(ft)*	1969	()	(min)	(ft)	[ť]		.[t]		(min)	(ft)	[ť] 🍝		[t]	
	(min)	S.C.		A			(min)		(min)						(min)	
	387.233	88.27	0										0.233	88.27	75.233	322
	387.250	87.97	0										0.250	87.97	75.250	<u> </u>
	387.267	87.67	0										0.267	87.67	75.267	282
	387.283	87.39	0										0.283	87.39	75.283	266
	387.300	87.09	0										0.300	87.09	<u>75</u> .300	251
	387.317	86.79	0										0.317	86.79	75.317	238
	387.333	86.51	0										0.333	86.51	75.333	226
	387.417	85.08	0										0.417	85.08	75.417	181
	387.500	83.68	0										0.500	83.68	75.500	151
	387.583	82.31	0										0.583	82.31	75.583	130
	387.667	80.97	0										0.667	80.97	75.667	113
	387.750	79.67	0										0.750	79.67	75.750	101
	387.833	78.40	0										0.833	78.40	75.833	91
	387.917	77.12	0										0.917	77.12	75.917	83
	388.000	75.90	0										1.000	75.90	76.000	76
[388.083	74.70	0										1.083	74.70	76.083	70
	388.167	73.52	0					[1.167	73.52	76.167	65
	388.250	72.36	0										1.250	72.36	76.250	61
	388.333	71.12	0										1.333	71.12	76.333	57
	388.417	70.00	0										1.417	70.00	76.417	54
	388.500	68.90	0										1.500	68.90	76.500	51
	388.583	67.83	0										1.583	67.83	76.583	48
	388.667	66.76	0										1.667	66.76	76.667	
	388.750	65.43	0					<u> </u>					1.750	65.43	76.750	44
	388.833	63.96	0										1.833	63.96	76.833	42
	388.917	62.86	0										1.917	62.86	76.917	40
	389.000	61.89	0										2.000	61.89	77.000	39
	389.500	56.39	0										2.500	56.39	77.500	31
	390.000	51.54	Ō										3.000	51.54	78.000	26
	390,500	47.27	0				·						3.500	47.27	78,500	22
	391.000	43.46	0										4.000	43.46	79.000	20
	391.500	39.99	0			[·	[4.500	39.99	79.500	18
	392.000	36.86	0		·						· · · · ·		5.000	36.86	80.000	16
	392.500	33.72	0										5.500	33.72	80.500	15
	393.000	31.56											6.000	31.56	81.000	14
	393.500	29.64	0										6.500	29.64	81.500	13

Table D5—Continued

					Step-Dr Te	awdown st 1	Recovery Test 1				Step-Dra Tes	awdown It 2	Recovery Test 2			
Time of Day	Cumulative Time since	Water Level	Pump Rate	Specific Conductance	Elapsed Time,	Drawdown from Static	Elapsed Time,	Residual Drawdown	Time since Pump	ťť.	Elapsed Time,	Drawdown from Static	Elapsed Time,	Residual Drawdown	Time since Pump	Vr
	of Pumping (min)	Change (ft)*	(gpm)	(µS/cm)	Pumping (min)	(ft)	[ť] (min)	(π)	[t] (min)		Pumping (min)	(ft)	flecovery [t']	(11)	[t] (min)	
	394.000	27.95	0	1			[7.000	27.95	82.000	12
	394.500	26.44	0										7.500	26.44	82.500	11
	395.000	25.12	0										8.000	25.12	83.000	10
	395.500	23.92	0				[8.500	23.92	83.500	10
	396.000	22.87	0										9.000	22.87	84.000	9
	396.500	21.94	0					1					9.500	21.94	84.500	9
	397.000	21.11	0										10.000	21.11	85.000	9
	399.000	18.47	0	1							-		12.000	18.47	87.000	7
	401.000	16.80	0				[14.000	16.80	89.000	6
	403.000	15.64	0	,									16.000	15.64	91.000	6
	405.000	14.76	0	1									18.000	14.76	93.000	5
	407.000	14.07	0				[20.000	14.07	95.000	5
	409.000	13.50	0				[22.000	13.50	97.000	4
	411.000	13.04	0				[24.000	13.04	99.000	4
	413.000	12.62	0										26.000	12.62	101.000	4
	415.000	12.26	0	1									28.000	12.26	103.000	4
	417.000	11.93	0	1			[30.000	11.93	105.000	4
	419.000	11.64	0										32.000	11.64	107.000	3
	421.000	11.38	0										34.000	11.38	109.000	3
	423.000	11.14	0										36.000	11.14	111.000	3
	425.000	10.89	0										38.000	10.89	113.000	3
	427.000	10.67	0										40.000	10.67	115.000	3
[]	429.000	10.48	0				ſ						42.000	10.48	117.000	3
[]	431.000	10.32	0										44.000	10.32	119.000	3
	433.000	10.15	0										46.000	10.15	121.000	3
	435.000	10.01	0										48.000	10.01	123.000	3
	437.000	9.87	0				[50.000	9.87	125.000	3
[439.000	9.73	0										52.000	9.73	127.000	2
	441.000	9.58	0										54.000	9.58	129.000	2
	443.000	9.46	0										56.000	9.46	131.000	2
	445.000	9.35	0				[58.000	9.35	133.000	2
	447.000	9.24	0										60.000	9.24	135.000	2
	449.000	9.13	0										62.000	9.13	137.000	2
	451.000	9.03	0										64.000	9.03	139.000	2
l 1	453.000	8.92	0				[66.000	8.92	141.000	2
	455.000	8.83	0										68.000	8.83	143.000	2

Table D5—Continued

					Step-Dr Te	awdown st 1	Recovery Test 1				Step-Dr Tes	awdown st 2	Recovery Test 2			
Time of Day	Cumulative Time since Beginning of Pumping (min)	Water Level Change (ft)*	Pump Rate (gpm)	Specific Conductance (µS/cm)	Elapsed Time, Pumping (min)	Drawdown from Static Level (ft)	Elapsed Time, Recovery [t'] (min)	Residual Drawdown (ft)	Time since Pump Started [t] (min)	vr	Elapsed Time, Pumping (min)	Drawdown from Static Level (ft)	Elapsed Time, Recovery [ť]	Residual Drawdown (ft)	Time since Pump Started [t] (min)	N
	457.000	8.74	0										70.000	8.74	145.000	2
	459.000	8.67	0										72.000	8.67	147.000	2
	461.000	8.58	0										74.000	8.58	149.000	2
	463.000	8.50	0										76.000	8.50	151.000	2
2128	465.000	8.42	0										78.000	8.42	153.000	2

1

*Water level relative to static water level at start of initial pumping.





Appendix D

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Figure D2. Orlando Utilities Commission Southeast test well: packer interval 2, specific-capacity test

Delta-s per log cycle = 92 ft Pump rate (Q) = 50 gpm Transmissivity = $(264 \times Q)/92$ ft = 143 gpd/ft Residual drawdown (ft) ťť

Figure D3. Orlando Utilities Commission Southeast test well: packer interval 2, recovery test

Appendix D











-5 Delta-s per log cycle = 30 ft Pump rate (Q) = 83 gpm Transmissivity = $(264 \times Q)/30$ ft = 730 gpd/ft Residual drawdown (ft) • П ťť

Figure D7. Orlando Utilities Commission Southeast test well: packer interval 3, recovery test 1

Appendix D





Figure D8. Orlando Utilities Commission Southeast test well: packer interval 3, recovery test 2



Figure D9. Water level changes and specific conductance during pumping and recovery tests: packer interval 4





Figure D10. Orlando Utilities Commission Southeast test well: packer interval 4, specific-capacity test

St. Johns River Water Management District 127



Figure D11. Orlando Utilities Commission Southeast test well: packer interval 4, recovery test 1

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Figure D12. Orlando Utilities Commission Southeast test well: packer interval 4, recovery test 2

Hydrologic Data from a Lower Floridan Aquifer Well, Central Orange County, Florida

80 Pumping rate (gpm) 60 40 20 0 Recovery test 1 step 1 Step-drawdown test 1 ∠ ο δ 8 8 8 8 8 000 Specific Conductance (μS/cm) Step-drawdown test 2 Change in water level relaive to static level at start of pumping (ft) Recovery test 2 Adjust pump rate during inflation 0 Adjust pump step 2 10 rate 20 Adjust pump rate 30 40 50 60 70 Vater level change 80 Specific conductance 90 100 110 O 180 240 300 Time (min) since beginning of pumping 60 120 360 420 480 0







Figure D14. Orlando Utilities Commission Southeast test well: packer interval 5, step-drawdown test 1

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St. Johns River Water Management District 131



Figure D15. Orlando Utilities Commission Southeast test well: packer interval 5, step-drawdown test 2





Figure D16. Orlando Utilities Commission Southeast test well: packer interval 5, recovery test 1


Figure D17. Orlando Utilities Commission Southeast test well: packer interval 5, recovery test 2

Appendix D

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