# THE WELL INSTALLATION & GEOLOGIC INVESTIGATION FOR THE ISOLATED WETLANDS RESEARCH PROGRAM - PHASE 2

# by Kevin P. Rohrer, P.G.



# South Florida Water Management District Water Use Regulation Department

3301 Gun Club Road • West Palm Beach, Florida 33406 • www.sfwmd.gov

# The Well Installation & Geologic Investigation for the Isolated Wetlands Research Program -Phase 2

January 2000

By Kevin P. Rohrer, P.G. South Florida Water Management District Water Use Regulation Department Criteria and Rule Making Division 3301 Gun Club Road West Palm Beach, FL 33306 (561) 686-8800 www.sfwmd.gov krohrer@sfwmd.gov



# CONTENTS

3

	st of Figures	
Ex Ac	ecutive Summary	. 1 . 2
<b>1.0</b> 1.1		
1.1	Background Purpose and Scope	
2.0	Drilling Methods	
2.1	General	
2.2	Hollow Stem Auger Method.	
2.3	Tripod Method	. 6
2.4	Rotary Mud Method	. 7
3.0	Well Construction And Sampling Methods	8
3.1	General	
3.2	Penetration Rates and Split Spoon Sampling	
3.3	Classification of Soils and Grain Size Distribution	
3.4	Core Analysis	13
4.0	Flint Pen Strand Study Area	14
4.1	Site Description	14
4.2	Well Construction	15
4.3	Geology	15
4.4	Classification of Soils and Grain Size Distribution	15
4.5	Core Analysis	20
5.0	Stairstep Project Study Area	23
5.1	Site Description	
5.2	Well Construction	
5.3	Geology	23
5.4	Classification of Soils and Grain Size Distribution	26
5.5	Core Analysis	35
6.0	Hogan Island Farms Study Area	36
6.1	Site Description	36
6.2	Well Construction	36
6.3	Geology	36
6.4	Classification of Soils and Grain Size Distribution.	
6.5	Core Analysis	55

# CONTENTS

7.0	Citrus Project Study Area	
7.1	Site Description	
7.2	Well Construction	
7.3	Geology Stop	
7.4	Classification of Soils and Grain Size Distribution	
7.5	Core Analysis	
8.0	Conclusions	
9.0	Recommendations	
10.0	References	
Арр	endices	
App	endix A - Flint Pen Strand Field Notes	A-1
App	endix B - Stairstep Project Field Notes	B-1
	endix C - Hogan Island Farms Field Notes.	
	endix D - Citrus Project Field Notes	

đ

# LIST OF FIGURES

Figure 1:	Location of Isolated Wetlands Study Areas	4
Figure 2:	The typical construction design of a Wetland Monitoring Well	8
	for the Isolated WetlandProject - Phase 2	
Figure 3:	Location of Wetland Monitoring Wells and Geologic Cross Section A-A' at Flint PenStrand Study Area, Lee County	14
Figure 4:	Boring Logs for FP9	16
Figure 5:	Boring Logs for FP10	17
Figure 6:	Boring Logs for FP11	18
Figure 7:	Geologic cross section A-A' at Flint-Pen Strand Study Area, Lee County	20
Figure 8:	Selected Soil Survey Map of Lee County at the Flint Pen Strand Study Area	
Figure 9:	Location of Monitoring Wells on Stairstep Project Study, Lee County, Showing Cross Section A-A'	24
Figure 10:	Geologic Cross-Section A-A' at Stair Step Study Area, Lee County	
	Boring Logs for ST1	
	Boring Logs for ST2	
Figure 13:	Boring Logs for ST3	29
Figure 14:	Boring Logs for ST4	30
Figure 15:	Boring Logs for ST5	
Figure 16:	Selected Soil Survey Map of Lee County at the Stair Step Project Study Area	34
Figure 17:	Location of Monitoring Wells on Hogan Island Farms, Collier County,	37
Figure 18:	Boring Logs for HF1	
	Boring Logs for HF2	
Figure 20:	Boring Logs for HF3	41
Figure 21:	Boring Logs for HF4	42
	Boring Logs for HF5	
Figure 23:	Boring Logs for HF6	46
	Boring Logs for HF7	
Figure 25:	Boring Logs for HF8	50
Figure 26:	Geologic Cross Section A-A' at Hogan Island Farms Study Area, Collier County	
Figure 27:	Selected Soil Survey Map of Collier County at the Hogan Island Farms Study Area.	54
Figure 28:	Location of Monitoring Wells on Citrus Project Study Area,	
E' 00	Lee County, Showing Cross-Section A-A' and A'-B	- ^
	Boring Logs for WF1 Boring Logs for WF2	
	Boring Logs for WF3	
-	Boring Logs for WF4	
-	Boring Logs for WF5	
•	Boring Logs for WF6	
-	Boring Logs for WF8	
0	Boring Logs for WF9	
	Boring Logs for WF10	
•	Geologic Cross-Section A-A' at Citrus Project Study Area, Lee County	
	Geologic Cross-Section A'-B at Citrus Project Study Area, Lee County	
	Selected Soil Survey Map of Lee County at the Citrus Project Study Area	
8 101	service service in a por see county at the entrast reject biddy ried	75

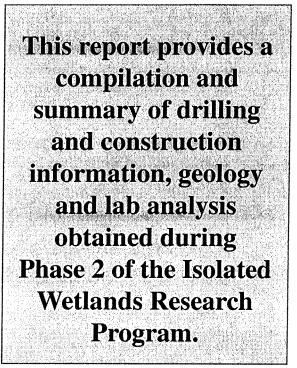
# **LIST OF TABLES**

Table 1:	Well Construction Specifications for Isolated Wetland Monitoring Wells	10
Table 2:	Hydrologic Properties of Selected Soils	12
Table 3:	Values of Hydraulic Conductivity for Selected Intervals	22
Table 4:	Values of Hydraulic Conductivity for selected Intervals	35
Table 5:	Range of Coefficient of Curvature (Cc) and Uniformity Coefficient (Cu) for Hogan Island Farms Study Area	55
Table 6:	Environmental Setting and Dominate Wetland Plants	
Table 7:	Range for Coefficient of Curvature (Cc) and Uniformity Coefficient for Citrus Project Study Area	75
Table 8:	Values of Hydraulic Conductivity for selected Intervals	75

## **EXECUTIVE SUMMARY**

The Isolated Wetlands Research Program was initiated in 1996 at the request of the Regulation and Planning Departments of the South Florida Water Management District. The objectives of this program were to develop a better understanding of the hydrology and ecology of isolated wetlands and provide guidance on the development of wetland protection criteria for water use permitting. The information collected as part of Phase 2 will assist in the interpretation of wetland hydrology and the geologic characterization of different wetland settings in South Florida.

This report provides a compilation and summary of drilling and construction information, geology, and lab analysis obtained during Phase 2 of the Isolated Wetlands Research Program. Twenty six wetland monitor wells in four study areas were installed as part of Phase 2. The four study areas include the Flint Pen Strand, Stairstep Project, Hogan Island Farms and Citrus Project.



Nine "local" wells, approximately 60 feet deep, and 17 shallow wells approximately 20 feet deep were drilled to obtain information on geology and to establish the infrastructure for long-term hydrological monitoring of isolated wetlands. Water level data collected from these wells will assist in determining local ground water gradients in the surficial aquifer system and to evaluate ground water influences on wetland water levels.

Hollow stem auger, tripod and mud rotary drilling methods were used to construct the wetland monitor wells to accommodate the site-specific field conditions and minimize environmental impacts. During the drilling of each well, unconsolidated lithologic samples were collected using a split-spoon sampler. Selected split-spoon samples were analyzed for particle size distribution (sieve analysis) on 371 samples to determine subsurface conditions that control ground water movement. Sieve analyses were plotted with respect to percent by weight for each sample. Using an NX core barrel, consolidated samples of limestone were also collected and analyzed in the laboratory for vertical and horizontal hydraulic conductivity. In addition, boring logs for each well provides lithologic descriptions of samples, and document standard penetration tests conducted on the entire depth of each well.

Site specific soil maps for each study area show soil types found in the study areas and are discussed as they relate to the water table and soil charactistics. Using the lithologic samples collected during drilling, geologic cross sections were drawn for each of the four study areas.

### ACKNOWLEDGEMENT

The author would like to acknowledge Christopher King, Janet Wise and Diane Bello-Smith, for creating and revising the graphics for this report. This project has benefited from the cooperation and contribution from the landowners and assistance from the property managers of each study area. This project also benefited from the cooperation of the well driller, Robert Miller with Precision drilling. Gratitude is expressed to the project manager Douglas Shaw, for his leadership and report review. Additional thanks is extended to the report reviewers, Michael Bennett and Susan Bennett.

### **1.0 INTRODUCTION**

#### 1.1 Background

The Isolated Wetlands Research Program was initiated in 1996 at the request of the Regulation and Planning Departments of the South Florida Water Management District (SFWMD). The objectives of this Program were to develop a better understanding of the hydrology and ecology of isolated wetlands in South Florida and provide guidance on the development of wetland protection criteria for water use permitting. Staff from the Resource Assessment Division of the SFWMD were charged with establishing a network of long term monitoring sites in isolated wetlands. The scope of the study is to address the following:

•The natural seasonal and annual hydrologic variability of isolated wetlands

- •The influence of ground water withdrawals on the frequency, timing, and magnitude of keyhydrologic parameters
- •The links between changes in hydrology and adverse changes in wetlands functions

Drilling for this project was divided into two Phases. In Phase 1, 20 wetland monitor wells were installed and instrumented in municipal wellfields and unimpacted reference areas in Lee, Martin, Osceola and Polk counties (Engineered Environmental Solutions Inc., 1997). This phase was completed in the spring of 1997.

In Phase 2, 26 wetland monitor wells were installed, which included 17 shallow wells (approximately 20 feet deep) and nine "local" wells (approximately 60 feet deep). The work was completed in June 1998. This report provides a compilation and summary of the drilling and construction information, geology and lab analysis obtained during phase 2 of the Isolated Wetlands Research Program.

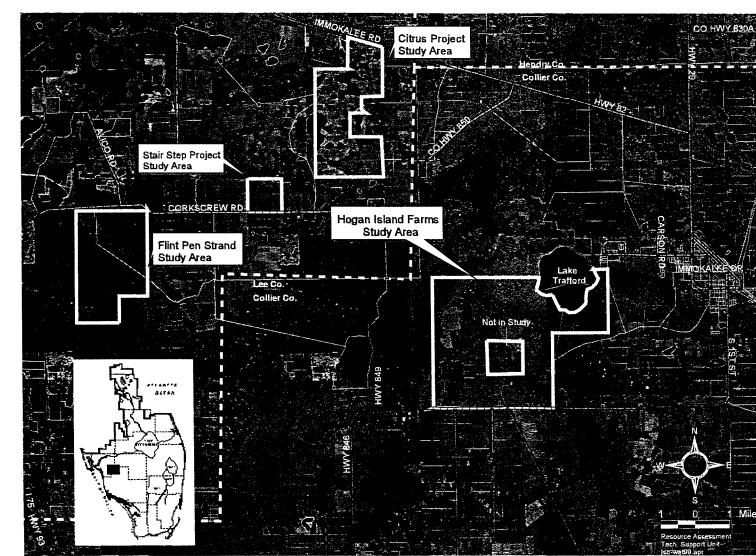
#### 1.2 Purpose and Scope

The purpose of the monitor wells is to establish the infrastructure for long-term hydrological monitoring of the isolated wetlands. Groundwater level measurements will determine local groundwater gradients of the surficial aquifer system that affect and impact the isolated wetland. Long-term monitoring will help to determine seasonal water level variations and detecting potential impacts to isolated wetlands from groundwater pumping. The information collected from the four study areas will assist in the interpretation of wetland hydrology and the geologic characterization of different wetland settings in South Florida.

During the installation of 26 surficial monitoring wells, geologic data was collected and then analyzed to interpret the geologic controls that impact the distribution and movement of the ground water. In addition to describing geology, standard penetration tests were conducted on the entire depth of each well, and grain size was plotted with respect to percent by weight was analyzed to interpret uniformity coefficients and density.

**Figure 1** shows the location of the four study areas for Phase 2. The three study areas in Lee County are Flint Pen Strand, Stairstep Project, and Citrus Project; the one study area in Collier County is Hogan Island Farms. Wells drilled in the Flint Pen Strand were intended to supplement seven wetland wells installed as part of Phase 1.

Phase 2 wells in this study area consist of one "local" well installed to the approximate depth of the production zone of the nearby Lee County Utilities Corkscrew Wellfield and two additional





wells installed in hydric flatwoods type wetlands that had not previously been monitored in this area. The Citrus Project and Hogan Island Farms sites were selected as representative of wetlands in lower west coast agricultural settings. Sites in the Citrus Project are located in and adjacent to wetlands in a large surface water management reservoir that is potentially influenced by ground-water pumping for irrigation of citrus groves. Sites in Hogan Island Farms are located in and adjacent to wetlands potentially influenced by groundwater pumping for irrigation of seasonal small vegetable crops. These wetlands are located in unfarmed flatwoods areas adjacent to irrigated fields. Groundwater pumping at both the Citrus Project and Hogan Island Farms is from the surficial (water table) aquifer. Wells installed at the Stairstep Project are intended as reference sites for wetlands on the Citrus Project. Some of these wells are also intended to provide water table information needed to support District land management and restoration activities being conducted on the southern portion of the Stairstep property.

### 2.0 DRILLING METHODS

#### 2.1 General

Three different drilling methods were used to construct the 26 wetland monitor wells. Methods were selected to accommodate site-specific field subsurface conditions and minimize environmental impacts. The different methods include; the hollow stem auger method, the tripod method and the mud rotary method. During the drilling of each well, unconsolidated samples were collected using a split spoon sampler. Consolidated formation samples were collected by coring to obtain an undisturbed sample. All samples were described and marked for analysis. A detailed description of each drilling method used in Phase 2 is provided below.

#### 2.2 Hollow Stem Auger Method

The majority of the wells (21) were drilled using a 6-5/8 inch inside diameter (I.D) hollow stem auger. This was the preferred method for drilling the shallow 20-foot and 60-foot wells because it was the fastest drilling. To obtain undisturbed samples with the hollow stem auger, the two foot split spoon sampler is attached to a 1-inch drill pipe and placed inside the hollow stem auger and driven into the ground using a slide hammer. After the sample is collected, the hollow stem auger is advanced. The hollow stem auger offers additional advantages in split spoon sampling because the augers do not have to be removed to advance the hole, the rate of penetration is quicker than the other methods, and reliable samples can be collected below the drill bit. After penetrating the length of the split spoon (2 feet), the hollow stem is advanced. Any additional cuttings in the hollow stem is than washed with water to remove the cuttings and to prevent cross contamination of samples from non targeted depths. After completing the borehole, a 2-inch PVC (polyvinylchloride) well casing was lowered down the center of the hollow stem and silica sand was poured around the casing. The hollow stem augers were then pulled out in sections while maintaining the level of sand until the sand was two feet above the 2-foot screen. Bentonite pellets are then poured on top of the sand to provide a 2-foot seal between the sand and cement grout. To complete the well, cement grout is poured down the center of the hollow stem auger and five foot section of augers are than removed while maintaining the level of cement to land surface.

In order to use the hollow stem auger method the drill rig required convenient access and to have dry ground to support the weight of the drill rig. Each site also had to be free of obstructions and trees. If these site conditions could not be met, the tripod method was employed.

#### 2.3 Tripod Method

The tripod method was used to drill three wells HF3, WF1 and WF2. These wells are located in areas with difficult access or when standing water prevented using a hollow stem auger drill rig. This is a labor intensive and time-consuming method requiring all equipment to be hand carried to the site. This method is similar to the method used by a cable tool drill rig where the operator uses a slide hammer to drive the split spoon sampler and steel surface casing in the ground to collect the sample. After removing the sample, a 4-inch diameter, 5-foot long steel casing was driven in the ground again, using the slide hammer. Cuttings are then washed out of the casing using water and the process is repeated until the desired depth is achieved. Two-inch PVC casing is lowered down into the 4-inch steel casing. Then silica sand is poured around the PVC screen. The steel casing is pulled out in sections while maintaining the level of sand, bentonite and cement grout.

#### 2.4 Rotary Mud Method

The mud rotary drilling method was used on seven of the 60-foot wells ("local wells") FP-11, HF5, HF6, WF8, WF10, ST4 and ST5. At these sites, the formation consisted of consolidated limestone that was too hard to advance the borehole using the hollow stem auger method. On several occasions, circulation was either lost or the hole would not remain open due to sand lenses located in the limestone. Rotary drilling requires using bentonite mud that is re-circulated from a mud pan through the hollow drill pipe. The bentonite mud assists to lift the drill cuttings from the bottom of the hole. The drill fluid builds a mud cake around the walls of the borehole to keep unconsolidated sediments from collapsing around the drill bit and to keep the hole open to install well casing.

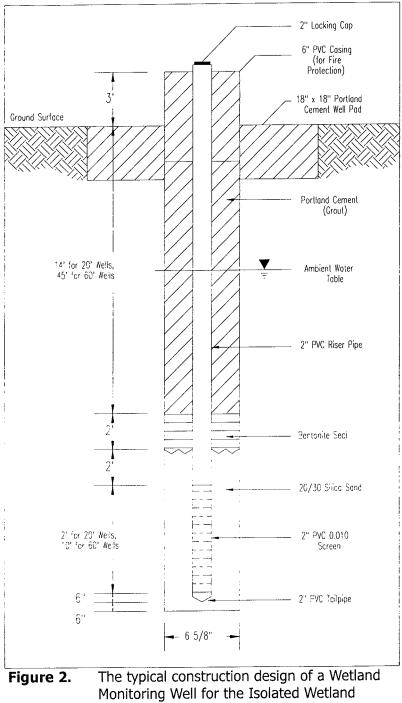
A core barrel was attached to the drill pipe to advance the borehole and collect the samples of the consolidated limestone. After collecting the core sample, a larger diameter tri-cone bit was attached to the drill stem and used to ream the borehole to the required casing diameter. To obtain unconsolidated samples within the limestone (sand layer) the split spoon sampler was attached to the drill pipe and hammered in the sediments.

After the designated depth was obtained, the well casing was lowered in the borehole. Tremie pipe was then lowered in the annular space between the well casing and the borehole. Silica sand was poured down the tremie pipe into the annular space until the sand was two feet above the 10-foot screen. Bentonite pellets were then poured in the tremie pipe 2-feet above the sand. To complete the construction of the well, cement is poured through the tremie pipe from the bentonite pellets to land surface.

## 3.0 WELL CONSTRUCTION AND SAMPLING METHODS

#### 3.1 General

Phase 2 includes the design, construction and analysis of samples collected during the installation of the isolated wetland monitor well network. During well drilling, samples were collected, described, and tabulated for each well. Also docuthe percent mented were recovery, blow counts, drilling methods, photographs of the core and cuttings, well construction specifications and monitor well location maps. Both the 20foot and 60-foot deep wells were completed to the contractual agreed upon depth or the first occurrence of a competent semi-confining layer that could impede the downward movement of the water table. The 20foot wells are located in the interior or edge of a wetland and are used to measure ground water levels directly influencing the wetland. The 60-foot wells referred to as "local" wells are used to measure adjacent background water levels to determine the hydraulic gradients and water table influences in the production zone that directly influence water levels in the wetland. Drilling continued past the contractual 60-foot depth at several sites to determine thickness of the clay or Figure 2. limestone encountered during well construction. This information is helpful when determining



factors affecting ground water movement. Figure 2 shows the typical construction design of the 20 and 60-foot isolated wetland monitor wells.

Project - Phase 2

**Table 1** lists the construction specifications for each of the monitor wells. Each well was constructed of 2-inch diameter, schedule 40 PVC casing with 2-inch diameter 0.010-inch slotted PVC screens. The shallow monitoring wells had 2 feet of screen and the 60-foot wells used 10 feet of screen. All wells were constructed using tri-loc threaded connections. Each well screen was packed with 20/30 silica sand followed by two feet of bentonite clay. Portland cement completed the well to the surface. All wells were fully developed using either centrifugal pump or airlift method until all visible particulate matter had been removed from the water. Discharge water from the well was placed on upland areas to minimize impacts to the wetland.

## 3.2 Penetration Rates and Split Spoon Sampling

The standard procedure for split spoon sampling followed the criteria established in the ASTM D-1586. Penetration rates were timed and recorded for each six inch split spoon sample collected. Sediment density is obtained from penetration rates in which the number of blows per foot are recorded as a split spoon sampler is driven by a 140 lb hammer falling 30 inches (Driscoll, 1987). Rate of penetration was recorded on the lithologic drilling log located in the Appendices A, B, C and D. The penetration rates for each well was also included in the study site boring logs, which is located in the separate chapters for each study area. Estimates of hydraulic conductivity of surficial material can be estimated from graphs based on particle size, uniformity coefficients and density (Holtz, 1981). This investigation does not include estimates of hydraulic conductivity for the samples collected.

The spilt spoon sampler is one of the best methods to collect an undisturbed sample from a known depth (Driscoll, 1987). This method was used for all wells, regardless of drilling method. The split spoon sampler was driven 2-feet ahead of the drill bit for each well. When using the rotary mud method the split spoon was attached to the drill rod and hydraulically pressed into the unconsolidated formation. The sample was collected and removed from the borehole, the split spoon sampler was opened and the inner transparent plastic tube containing the sample was removed and the sample described.

Once recovered, the clear plastic liner containing the split-spoon sample was capped at both ends to prevent the loss of the sample. General lithology was described by inspecting the contents of the clear plastic tube or by inspecting samples in the bit of the split spoon sampler that was not inside the plastic tube. Four, six-inch sections was measured and marked on the two foot clear tube to indicate which portion of the sample would be analyzed for grain size. The selected sixinch interval was than recorded in the field notes. The field notes documenting the interval as well as the general lithologic description for each well is located in the designated chapter Appendices of this report.

Consolidated samples that could not be collected with the split spoon method were cored using a NX core barrel that was attached to the drill rod. Inspected core samples were placed in corrugated cardboard core boxes and photographed. They were measured to obtain the required six-inch sample to determine percent return and record for falling-head permeability analysis. The results of the permeability analysis are tabulated for each study area in chapters 4 through 7.

#### 3.3 Classification of Soils and Grain Size Distribution

Particle size analyses is useful in classifying soils for interpreting wetland hydrology. Knowing the distribution of grain size with depth helps to determine the subsurface conditions that con-

Table 1.	Well Construction Specifications for Isolated Wetland Monitoring Wells
----------	--

e 1

								sensierse Geboordense	Casing	Total		Approx. Height of measuring	
Map Number	Site Name	SFWMD Well ID	Latitude	Longitude	Easting (X)	Northing (Y)	S/TWP/RGE	Well Diameter (inches)	Depth feet (bls)	Depth feet (bis)	Screen Interval (feet)	Point from landsurface (feet)	Elevation of MP (feet) (NGVD)
1	Flint Pen Strand	FP9	264233	817219	419489	760224	33/46S/26/E	2	17	19	2	3.00	19.56
2	Flint Pen Strand	FP10	264332	817234	419424	763818	33/46S/26/E	2	14	16	2	3.00	19.19
3	Flint Pen Strand	FP11	264352	817161	421819	764546	33/46S/26/E	2	50	60	10	2.95	19.26
4	StairStep Project	ST1	264601	816322	449332	773461	20/46S/27E	2	18	20	2	2.80	31.27
5	StairStep Project	ST2	26445	816323	449295	775023	20/46S/27E	2	18	20	2	3.00	31.16
6	StairStep Project	ST3	264643	816384	447286	774989	20/46S/27E	2	18	20	2	3.00	31.04
7	StairStep Project	ST4	264648	816333	448977	775157	20/46S/27E	2	50	60	10	3.10	32.19
8	StairStep Project	ST5	264509	816434	445627	770106	20/46S/27E	2	50	60	10	3.20	30.32
9	Hogan Island Farms	HF1	263963	815268	483720	750094	09/47S/28E	2	19	21	2	2.44	21.92
10	Hogan Island Farms	HF2	263964	815255	484124	750152	09/47S/28E	2	18	20	2	2.94	21.86
11	Hogan Island Farms	HF3	263807	815295	482806	744433	21/47S/28E	2	15	17	2	3.24	25.28
12	Hogan Island Farms	HF4	263904	815260	483964	750501	09/47S/28E	2	18	20	2	3.00	23.41
13	Hogan Island Farms	HF5	263805	815278	483353	744352	21/47S/28E	2	62	72	10	2.75	25.89
14	Hogan Island Farms	HF6	263961	815266	483770	750039	09/47S/28E	2	65	75	10	3.29	24.05
15	Hogan Island Farms	HF7	263975	815266	483775	750526	09/47S/27E	2	18	20	2	3.20	24.64
16	Hogan Island Farms	HF8	263705	815325	484762	740707	21/47S/28E	2	70	80	10	2.60	26.39
17	Citrus Grove	WF1	265184	815806	466285	794548	35/45S/27E	2	16.5	18.5	2	3.34	32.26
18	Citrus Grove	WF2	265018	815900	463192	788550	02/46S/27E	2	17.5	19.5	2	4.00	33.29
19	Citrus Grove	WF3	264924	816128	455729	785154	10/46S/27E	2	18	20	2	2.69	30.35
20	Citrus Grove	WF4	264777	816115	456107	779802	15/46S/27E	2	20	22	2	3.15	30.83
21	Citrus Grove	WF5	264856	815978	445627	770106	10/46S/27E	2	18	20	2	2.55	31.72
22	Citrus Grove	WF6	264784	816050	458262	780059	15/46S/27E	2	17	19	2	3.35	31.40
23	Citrus Grove	WF7	264796	815982	460483	780468	15/46S/27E	2	18	20	2	2.60	31.79
24	Citrus Grove	WF8	265184	815804	466360	794556	35/45S/27E	2	35	45	10	2.80	33.16
25	Citrus Grove	WF9	265021	815899	463219	788663	02/46S/27E	2	35	45	10	2.90	32.87
26	Citrus Grove	WF10	264795	815982	460474	780464	15/46S27E	2	55	65	10	2.96	32.18

5

:

trol ground water movement. Particle size analysis was performed on a total of 371 soil samples during this Phase 2 investigation.

Specific split spoon samples were analyzed for particle size distribution by the contractor, Engineered Environmental Solutions Inc., (EESI). A procedure for determining particle size distribution is described in the American Society for Testing and Materials (ASTM, 1980). The sixinch intervals were sieved using the procedure outlined in the ASTM-422 standard. The set of sieves used to determine gain size distribution includes numbers (mesh opening) 10 (2.0mm), 20 (0.85mm), 30(0.60mm), 40(0.42mm), 50(0.30mm), 60(0.25mm), 80(0.18mm), 100(0.15mm), 140(0.0.106mm), 170(0.09mm), and 200(0.075mm). The fraction smaller than a 200 sieve was analyzed by the hydrometer method as described in the above ASTM standards. The procedure for particle size gradation included taking a portion of the sample interval and oven drying at temperatures below 110 degrees Fahrenheit (higher temperatures may destroy clay particles). The sample is than pre-sieved, weighed and recorded. The oven-dried samples are placed on the largest mesh-size sieve of a group of interlocking sieves. The sample is then placed into the sieve stack, and is vibrated to enable individual particles to fall through the progressively smaller mesh size sieves. The shaker operates for 15 minutes per sample. The material retained on each sieve is weighed and expressed as a percentage of the total sample. The percent difference between the initial weight and the recovered weight should be less than 3 percent.

The sieve data was then entered into the Geotechnical Integrator Software (gINT) version 3.2. The results were then output by gINT in the form of grain size distribution curves. The curve is plotted on a graph which is comprised of grain size in millimeters along the X-axis and percent finer by weight along the Y-axis. In addition to the curves, gINT will interpret the curve and automatically classify the soil according to American Society of Testing Materials (ASTM) and Unified Soil Classification System (USCS). In certain instances, samples contained large amounts of shell material and limestone. This resulted in a large portion of the sample being retained on the #10 sieve and thereby altering the gradation curve. The gINT program would not classify the soil classification be input manually and where this occurred, the soil classification is preceded with an asterisk.

The overall gradation of a soil may be determined from the shape of the plotted curve. As an example, a near-vertical curve indicates a poorly-graded sand where all particles are of the nearly the same size and fall within the sand size range. Conversely, the spread of particles sizes over a relatively large range of grain size suggests a well graded soil. This distinction between poorly graded and well graded soils may be expressed numerically by a uniformity coefficient defined by the ratio of the  $D_{60}$  sieve and the  $D_{10}$  the sieve (ASTM, 1980):

 $C_u = D_{60}/D_{10}$ 

Where Cu = uniformity coefficient

D<sub>60</sub>=grain diameter at 60 percent passing

D<sub>10</sub>=grain diameter at 10 percent passing

For gravel, a uniformity coefficient of less than 4 indicates poor gradation, and greater than 4 indicates a good gradation and is represented by a smooth and reasonably symmetrical curve. In sands, the value of the uniformity coefficient for poorly graded soils from well-graded soils is 6

and greater than 6 indicate good gradation. A well graded soil is typically poorly sorted and has low permeability. A soil sample in which more than 50 percent of the coarse fraction by weight is retained on the number 40 (0.42mm) sieve may be described as gravel. A sample with more than 50 percent of the material passing the number 40 sieve but more than 50 percent of the retained on the number 200 (0.075mm) sieve may be described as a sand. Fine-grained soils are indicated, if more than 50 percent of the sample passes through the number 200 sieve size (Watson, 1993).

Another numerical parameter used to confirm conclusions based on the uniformity coefficient results, is the coefficient of curvature:

$$C_c = D_{30}^2 / (D_{10} D_{60})$$

#### **Equation 1**

Where:  $C_c$  =coefficient of curvature

 $D_{30}$  =grain diameter at 30 percent passing.

The coefficient of curvature should be between 1 and 3 for well graded sands. In general, the uniformity coefficient and coefficient of curvature are useful in determining the gradation of marginal soils, where it may be difficult to directly interpret the curve.

The sands with silt size fines may be considered a semi-confining layer that impedes the infiltration of ground water from the water table. The classification of this sand after particle size analyses indicates the sand is poorly graded with silty sand mixture (USCS classification). Fine grained soils, such as silt and fined grained sand, tend to have permeabilities that are lower then those of coarse grained, well graded soils. **Table 2** shows an abbreviated list of general hydrologic properties for soils that were characterized in this investigation.

USCS Symbol	Relative Permeability	K= ft /day	Drainage	
SP	High	>28.35	Good	
SW	Medium to High	> 2.835	Good	
SM	Medium to Low	2.835 - 0.0028	Fair to poor	
SC	Low	0.0028 - 0.0003	Very Poor	
ML	Low	0.2835 - 0.0028	Poor	

 Table 2.
 Hydrologic Properties of Selected Soils

Modified from I.Watson and A. Burnett 1993

S= sand W= well graded C= inorganic clay M= inorganic silt L = low liquid level /plasticity P= poorly graded

#### 3.4 Core Analysis

Coring was performed on selected consolidated formations using procedures described in ASTM standard, 2113-83. A NX core barrel was used to obtain samples of limestone too hard for the split spoon sampler to penetrate. These samples were collected and the depth interval recorded on the core sample. The core samples were than analyzed for vertical and horizontal permeability. Samples six inches in length that appeared to be representative of the formation or appeared to be atypical were selected for analyses to compare values that affect vertical ground water movement.

A total of eighteen rock core samples were collected during the construction of monitoring wells in Phase 2. Vertical permeability was calculated using a steady state air cross-flow method to determine air permeability. The testing was performed by Core Laboratories in Midland, Texas. The sample is placed in a rubber hassler sleeve under a pressure up to 400 psi to simulate the pressure at the depth of sample during testing. Upstream and downstream pressures are taken using mercury and water manometer gauges. Flow rates are measured across ceramic plates located between the sample.

The equation to convert permeability to hydraulic conductivity (ft /day) is (Core Laboratories, 1998):

K= (V L) / (A T P) where: K= Hydraulic conductivity (ft/day) V= Incremental produced volume (ft<sup>3</sup>) L= Length (ft) P= Differential pressure (ft of H<sub>2</sub>O) A= Cross-sectional area (ft<sup>2</sup>)

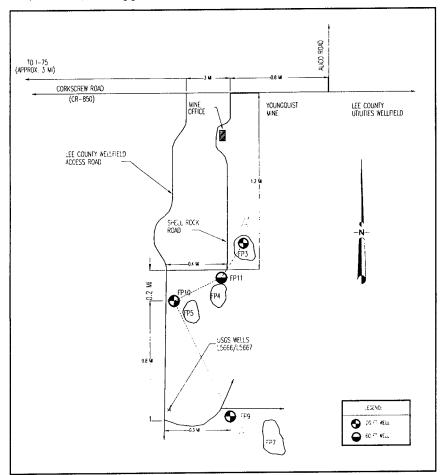
T = Incremental time (sec)

**Equation 2** 

## 4.0 FLINT PEN STRAND STUDY AREA

#### 4.1 Site Description

The Flint Pen Strand study area is located in south central Lee County in the vicinity of Lee County Utilities Corkscrew Well Field. The wetland monitoring sites are located just south of Corkscrew Road (CR-850) and approximately 3 miles east of Interstate 75 as shown in **Figure 3**.



**Figure 3.** Location of Wetland Monitoring Wells and Geologic Cross Section A-A' at Flint Pen Strand Study Area, Lee County

This site is likely impacted in several ways, including lowering of water levels in the water table from the nearby wellfield. In addition, many land use changes occurred near the well construction sites during Phase 2. Currently, in a section of the Flint Pen Strand study area there is ongoing mining activity for road building aggregate and processing for cement production. Road building and altering the landscape for future residential development was also occurring at the time wells was being constructed.

Monitor wells installed in Phase 1 were located in cypress dome swamp surrounded by pine or hydric flatwoods. In Phase 2, the monitoring wells are located in hydric flatwoods and wet prairie settings. Three monitor wells are constructed at the Flint Pen Site as part of Phase 2.

#### 4.2 Well Construction

Wells drilled at this site are designated with the letters FP. **Table 1** shows well construction specifications for the wells drilled at the Flint Pen study area. Monitoring wells FP9 and FP10, located in the hydric flatwoods and wet prairie settings were drilled 19 feet and 16 feet bls respectively. An additional 60-foot monitoring well (FP11), was installed to monitor water levels in the approximate zone that Lee County Utility is pumping ground water for water supply. This well is located near study wetland FP4 and along the edge of flat-pinewood margin.

The hollow stem auger method was used to construct wells FP9 and FP10. Well FP11 was first drilled using the hollow stem auger until limestone was encountered at approximately 23 feet bls. Difficulty washing the cuttings out of the borehole as well as drilling through the limestone using the auger bit necessitated changing to the mud rotary drilling method. The NX core barrel replaced the split-spoon sampler, and a four-foot sample was collected. After removing core samples, a tri-cone bit was installed and the core bore hole was reamed using the rotary method. This procedure was repeated until the well was completed. Wells FP9 and FP10 were completed in sand with a 2-foot screen. Well FP11 is completed with a 10-screen in limestone containing shell.

The bore logs for wells FP9, FP10, and FP11 are shown in Figures 4, 5 and 6. Penetration rates (blows/foot) were relativity consistent for wells FP9 and FP10. Where the first limestone was encountered approximately 16-feet bls (1 ft NGVD) the penetration resistances increase 80 percent to 76 (blows/foot). Penetration rates decreased after passing through the limestone layer.

#### 4.3 Geology

The geologic cross-section A - A' (Figure 7) is based on cuttings descriptions from wells drilled at the Flint Pen study area. Also included in this cross-section is FP3 installed during Phase I. Soil and geologic samples collected at this site indicate two feet of organic material overlies sand and shell mixture which grades into a fine sand and silt. Top of the limestone ranges from 16 feet to 24 feet bls (1 to -7 feet NGVD). In the 60 foot well (FP11) the top of the limestone is located at -7 feet NGVD. A three-foot thick lens of fine grained sand was encountered between 35 to 38 feet bls (-18 to -21 feet NGVD). Also observed was a five foot void between 45 to 50 feet bls (-28 to -33 feet NGVD). General descriptions of well cuttings, sieve analysis intervals and blow counts are provided in **Appendix A**.

#### 4.4 Classification of Soils and Grain Size Distribution

**Figure 8** shows the soil survey map for the Flint Pen Study area. The US Department of Agriculture Natural Resource Conservation Service (NRCS) has classified the soils at FP9 and FP10 as Pineda fine sand. This sand has characteristics of loamy, siliceous, hyperthermic Arenic Glossaqualfs. Pineda fine sand has an argillic horizon at a depth of approximately 49-70 inches bls. At site FP11 the soil is classified as Felda Series, is described as a deep, poorly drained, moderately permeable soil found in sloughs or depressions (USDA, 1990). The silty sand layer is also associated with increased blow counts indicating a more condensed and packed formation.

The surficial sands collected at the Flint Pen study area were analyzed for grain size distribution. The classification of sands after gradation analysis indicates that the sands are poorly graded silty sand and is designated by the USCS classification code as a SP soil suggesting a relative high Well Installation and Geologic Investigation for the Isolated Wetlands Research Program - Phase 2

Vest P	alm B 86-88	nent [ ub Road each, Flo 300 / Fax	rida 33	406			
PROJEC 1163/I DRILLING	FP-9 T NO.// solate G CON		DRILLER	LOCATION ing Program - Phase II Flint Pen Stra	nd, Lee Coun	ty, Florida	
GEOLOG Kevin I DRILLING Drill Rig WELL IN YES (X)	IST/OF Rohrei G EQUI g/Holl STALLI NC	FICE r/South F PMENT/ME ow Stem ED? CAS O C Sch	Horida V THOD A Auger SING MAT A.40 PV	Vater Management District           SIZE/TYPE OF BIT           4.5" Hollow Stem Auger           ./DIA.           SCREEN:           C/2"           TYPE Slotted	Splin PVC LE	NGTH 2' DIA.	START/FINISH DATE 5/8/98-5/8/98 2" SLOT SIZE .01
ELEVAT IFT. ABC REMARK	DVE M.		UND SUR	FACE TOP OF WELL CASING TOP & 17'/1	BOTTOM SCREEN		5/8/98
	Recovery Number	Penetration Resistance Blows/6" N-Value	Unified Classification		Log	Penetra Resista (Blows/I	nce pi
- Dep	Racover SS SS	3346 7 7467 10	PT SP	Sand 2	Notes		55 75 100 0 5
- 5	\$3 \$4	6467 10 4335 6	- sm-sc	Sand, yellow/red w/ shell fragments 6 Sand, organic fine silty sand, gray clay	<u>5.0</u>	•	
-10	S5	3345 7 4437 7			LQ.		
- 15	S7	1 1 1 2 2 3 4 6 6 10	-	Fine silty sand w/ some organic streaks			OX384
	59 510	4 4 8 30 12 8 25 refus		Limestone 18	<u></u> 		
-20 - -	511 512 513			Limestone, light gray, very hard, shell	<u>).7</u> 2.0		
-25	\$15 \$16			surcosic, shell grading to more shell	5.0		

Figure 4. Boring Logs for FP9

<u> </u>									·····
South Manag					E3				
Manag 3301 Gun West Palm	Club F	Road	rida 3'	3406	E				
561) 686	-8800	/ Fax	687-	6442					
BORING/WE				BORING LC	)G			•	
FP- PROJECT N	O./NAME		<u>t</u>	LOCATIO					
DRILLING C	ONTRAC	TOR/D	RILLER		an Strand	I, Lee Count	y, Florida		
Precision GEOLOGIST	Drilling	/Robe	ert Mil	ler					
Kevin Rol	UPMEN	uth FI	orida HOD	Water Management District SIZE/TYPE OF BIT		SAMP	LING METHOD	START/FIN	
Drill Rig/H	SA			4.5" Hollow Stem Auger	,		Spoon	5/7/98-5	
res 🛛	NO 🗆	Sch.	40 P	VC/2" TYPESlotted	MAT. PV		GTH 2' DIA.		SIZE .010
ELEVATION		GROU	ND SUI	RFACE TOP OF WELL CASING	TOP & BO	TTOM SCREEN	-	DATE 5/7/98	
REMARKS:									
Samp	le Su		tion	LOG OF TEST BO	RING		Penetra	tion	
Depth (ft) Type & Recovery	Number Penetratik Resistanc	Blows/6° N-Value	Unified Classification	·····	· · · · · · · · · · · · · · · · · · ·		Resista	nce	Graphic Litho Log Well
			D D D D D D D D D D D D D D D D D D D	FIELD DESCRIPTION		Log Notes	(Blows/F 01535	oot) 55 75 100	Vell Crap
		3	PI	Organic material w/ sand and wood			Ţ		
	2 4 4		SP.PT		2.0		<b>\</b>		
Ň	1	3		Sand, organic mixture	[				
. <sub>5</sub>	3 76				1		7		# K
	4 4 4	5.6	OL		6.0				
	9		ΨL	Fine silty sand, organic					
<b>s</b>	5 4 4		ML		8.0		•		
			•	Clayey sand	10.0				
<sup>s</sup>	6 22 5		SP	Fine sugar sand			Ĭ		
	7 63	34		the sage send			•		
X	6								Ĥ
15	8 4 4 4		sc		14.0		•		7
				Clayey sand	16.0				
			-	Limestone, surcousic infilling, shell \fragments	م.71				
- 51	d			Limestone w/ bivalves and coral					
20	1	{	ŀ	Limestone, light gray w/ coral, shell	19.0				
20				Limestone w/ shell fragments					
┞╀┼╸	+				23.0				<u></u>
Fine Sa	nd		Me Me	dium Sand	<u> [3]</u> [3]	Cement Grout	Silt/CI	ay w/ shell	<u></u>
 ित्रे Organic	Material		 ]]] Lim	nestone Clayey Sand	ليضيغ	Fine sand w/ sheli	Shiffing Shiffing	Backfill	
1221									

Figure 5.Boring Logs for FP10

ORI	NG/WELL		Γ	BORING L	DG				
	ECT NO./	NAME		LOCAT Ing Program - Phase II Flint P		an Count	. Florida		
RILL	ING CON	TRACTOR/	DRILLER		ren Stranu, L	ee county	, rionua		
EOL	OGIST/O								
		PMENT/ME		Vater Management District		SAMP	LING METHOD	START/FIN	ISH DATE
	Rig/Mu	d Rotary ED? CAS	ING MA	4.5" Hollow Stem Auge	er	Split	Spoon	5/6/98-5	5/11/98
S		D 🗆 Scł	1.40 P	C/2" TYPESlotted	MAT. PVC		GTH 10' DIA.	<u>2" SLOT</u> DATE	SIZE .010
Т. A	BOVE M				50'/60'			5/6/98	
:MA	RKS:								
	Sample	5.8	tion	LOG OF TEST 8	ORING		Penetra		
Depth (ft)	Type & Recovery Number	Penetration Resistance Blows/6 <sup>-</sup> N·Value	Unified Classification				Resista (Blows/		Graphic Litho Log Well
ň.	<u>⊢</u> 2 2	3456	PT	FIELD DESCRIPTION	0.5	Log Notes	0 15 35	55 75 100	V Litho
	X	9	F (	Organic Sand			<u> </u>		
	52	7787 15	SP	Fine sand yellow, organic			Ţ		
	53	5455	-		4.0		•		
5	X.	9		Sand, yellow/red, w/ shell fragmen	ts 6,0				C (X)
	S4	4466 10		Sand, gray to white			T		
	55	5557 10	-				•		
10	∧ ∕ 56	4468	-				•		
	X	10							
	S7	4456 9		Sand, white, sugar texture					
	58	3355					•		
15	S9	8	4				•		
	X	8			18.0				
	510	4755 12	1	Sand w/ shell fragments					
20	511	67120		Sana wy shon magnitika			•, _		
	ĂO	19	_	Sand, shell w/ some limestone	22.0				
	Б12	19 36 40 - 76	•	Fine grained sand white					
25 <sup>°</sup>	513		-1		24.0				
2.5				Limestone, light gray, very hard w/ shell fragments				•	

**Figure 6.** Boring Logs for FP11 (page 1 of 2)

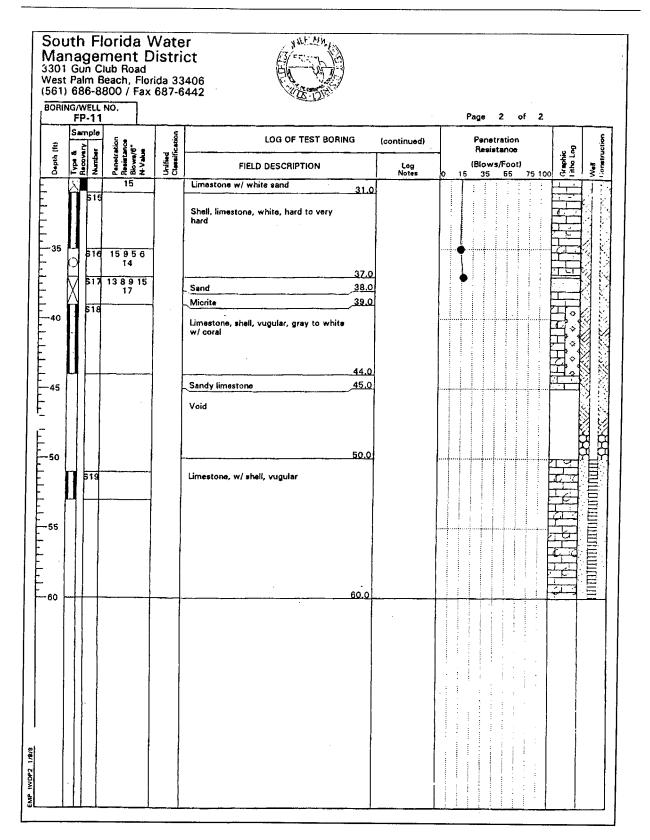


Figure 6. Boring Logs for FP11 (page 2 of 2)

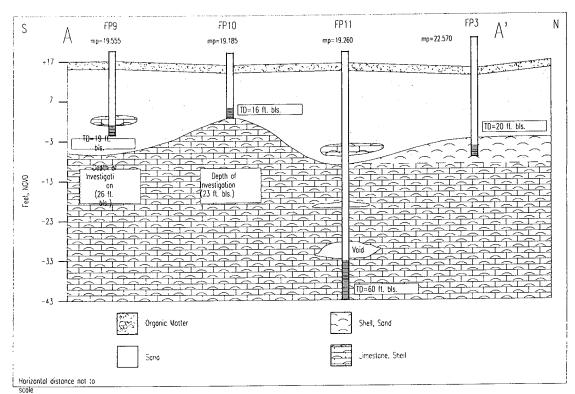


Figure 7. Geologic cross section A-A' at Flint-Pen Strand Study Area, Lee County

permeability. However, values of coefficient of curvature (Cc) ranged from 0.95 to 1.11 for FP9 and 0.93 to 1.14 for FP10 indicating well-graded sands. This discrepancy may be because of the USCS countywide scale and not site specific environmental factors. Samples taken from FP11 had a larger range of Cc numbers (0.23 to 1.12) primarily due to limestone and shell that was collected at this site. The uniformity coefficient (Cu) ranged from 1.6 to 4.4 for FP9, 1.5 to 1.8 for FP10 and 1.7 to 15.1 for FP11. The gradation curves plotted from grain size distributions data is provided in **Appendix A**.

The fine-grained soils, such as silts and fine-grained sand, tend to have lower permeabilities then those of coarse grained, well graded soils. Sands with more of a silt component may be considered a semi-confining layer that impedes the downward infiltration into the shallow water table. The smaller grain size results in a greater surface area and, in turn, a greater frictional resistance to the flow of ground water.

#### 4.5 Core Analysis

Wells FP9 and FP11 contained consolidated formations which were cored. The rock core samples were analyzed in the lab for hydraulic conductivity. **Table 3** lists the selected intervals that were analyzed in the Flint Pen Strand study area.

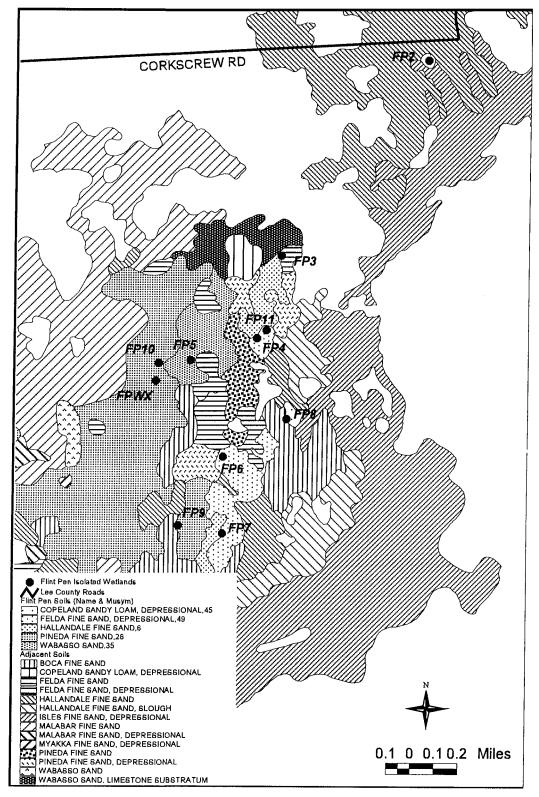


Figure 8. Selected Soil Survey Map of Lee County at the Flint Pen Strand Study Area

Sample Number	Site Name	Top Depth of core interval (ft-bls)	Bottom Depth of core interval (ft-bls)	Horizontal Hydraulic Conductivity (K <sub>h</sub> ) ft/day	Vertical Hydraulic Conductivity (K <sub>v</sub> ) ft/day	Description of core
8	FP9	22.5	23.0	0.0005	0.0098	Limestone
9	FP9	24.2	24.7	0.0004	0.0066	Limestone
10	FP9	25.5	26.0	0.0004	0.0066	Limestone
15	FP11	34.0	34.5	0.0005	0.0098	Limestone
16	FP11	40.3	40.8	0.0005	0.0098	Limestone
17	FP11	43.0	43.5	0.0003	0.0066	Limestone
18	FP11	57.0	57.3	0.0008	0.0131	Limestone

# Table 3.Values of Hydraulic Conductivity for Selected Intervals<br/>at Flint Pen Strand Study Area

## 5.0 STAIRSTEP PROJECT STUDY AREA

#### 5.1 Site Description

The Stairstep Project study area is part of a regional ecosystem of approximately 5,230 acres (including the Imperial Marsh) established as mitigation for impacts to wetlands associated with the Southwest Florida International Airport. The Stairstep Project is located in southeast Lee County off Corkscrew Road, approximately 4.7 miles east of its junction with Alico Road and 7.5 miles east of I-75 (**Figure 9**). Many of the cypress domes in and adjacent to pasture land were rim-ditched as part of past drainage efforts to convey excess surface water away from the edge of wetlands.

The study area consists of cypress dome swamps, wet prairie, and pasture. Five monitor wells were constructed at this site designated ST1 through ST5. Three shallow wells (ST1 through ST3), completed to a depth of 20 feet bls, are located in selected isolated cypress and marsh wetlands in the northern part of the property. These wetlands were selected as reference sites for wetlands of similar soil types and communities on the Citrus Project. Two "local" wells (ST4 and ST5), completed to a depth of 60 feet bls, are located in upland areas at the north-central and southwest edges of the property. Monitoring well ST4 is located in an uplands stand of pine trees adjacent to wetland ST2 that goes by the same name as the monitoring well found at this site. Well ST5 is located on the edge of a pasture in the southwest corner of the property along Corkscrew Road (SR850). These sites provide information on deeper ground water and on water table gradients between the wetlands and uplands. The monitoring wells are located in a large depression marsh associated with an offsite cypress dome that extends southward to this study site.

#### 5.2 Well Construction

**Table 1** shows well construction specifications for wells drilled at the Stairstep Project study area. Monitor wells ST1, ST2, and ST3 are completed to a total depth 20-foot bls (approximately 8.3 NGVD) with 2-foot screens completed in a fine-grained sand. These wells were constructed to monitor shallow water levels in isolated cypress dome wetlands. The hollow stem auger method was used to construct each of these wells. Using a slide hammer, the split-spoon sampler was driven ahead of the auger bit to obtain relatively undisturbed samples. After obtaining a 2-foot sample, the auger was advanced and washed out. This was repeated until achieving the desired depth.

Wells ST4 and ST5 are completed to a total depth of 60-foot bls (approximately 32 feet NGVD) wells that were completed with 10-foot screens within a limestone formation. Both of these wells were constructed using the mud rotary method. Split-spoon samples were collected in the unconsolidated sediments as described in section 3.2 of this report. A core barrel was later attached to the drill rod and limestone samples were collected below 24 feet NGVD. After removing core samples, a tri-cone bit was used to ream the borehole to facilitate continuous coring and well installation. This procedure was repeated until the well was completed.

#### 5.3 Geology

**Figure 10** shows the geologic cross-section A - A' based on information obtained from wells drilled at the Stairstep Project study area. The cross-section illustrates the general alignment of

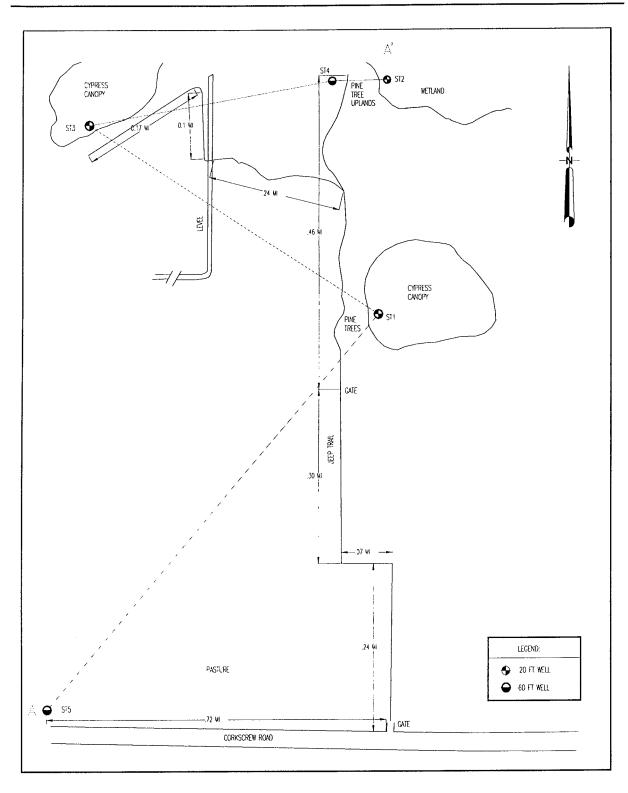
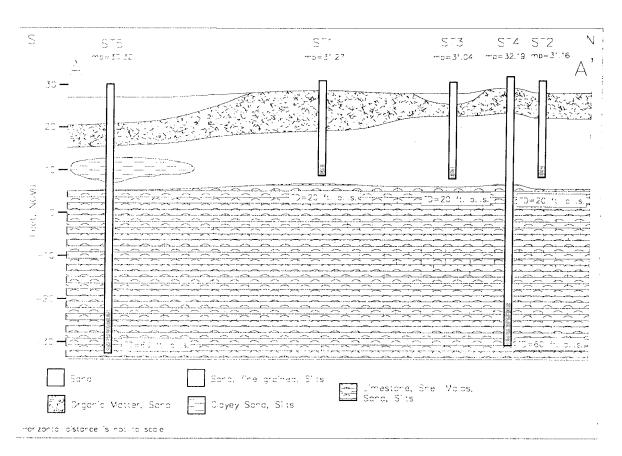


Figure 9.Location of Monitoring Wells on Stairstep Project Study,<br/>Lee County Showing Cross Section A-A'



Well Installation and Geologic Investigation for the Isolated Wetlands Research Program - Phase 2

Figure 10. Geologic Cross-Section A-A' at Stair Step Study Area, Lee County

wells and the relatively uniform geology found at each well site. Wells ST1, ST3, and ST2 were completed in fine-grained sand with alternating bands of organic matter. The thickness of this sand is approximately 23 feet as indicated by the cutting samples from wells ST5 and ST4. A very fine-grained sand deposit between 2 and 4 feet thick was observed in wells at ST1, ST2, and ST5 at a depth of 11 to15 feet bls (approximately 10 feet NGVD). These wells are most likely completed in the water table aquifer. Wells ST5 and ST4 indicate limestone occurring at 23 feet bls (approximately 5 NGVD). The thickness of the limestone is not known because none of the wells penetrated deeper then 60 feet bls. The limestone consists of shell fragments, sand and silts most likely correlated to confining beds of the lower Tamiami aquifer. Knapp et. Al. (1986) reported the thickness of the lower Tamiami to be 150 feet.

Bore logs for the five wells are shown in **Figures 11, 12, 13, 14** and **15**. Penetration resistance (blows/foot) was relativity consistent for the 20-foot wells from land surface to about 12 feet bls. At depths approximately 12 feet bls, where fine grained sand was encountered, the blow counts increased approximately 30 percent.

#### 5.4 Classification of Soils and Grain Size Distribution

**Figure 16** shows the soil survey map for the Stairstep study area. The majority of sands associated with the depression of the slough system are the Immokalee Sand where monitoring well ST5 is located. The Valkaria Fine Sand and Myakka Fine Sand, where ST2 and ST4 are located, is associated with the cypress dome and the upland pine flatwoods. Pompano Find Sand is associated with a pond cypress dome where ST3 is located. ST1 is located in a wetland depression that is associated with Felda Fine Sand.

The Immokalee Sand is associated with a nearly level, poorly drained soil found in historic flatwoods areas. Most of the time the water table is within 10 inches of the surface for 1 to 3 months and 10 to 40 inches below the surface for 2 to 6 months. The available water capacity is termed as medium in the subsoil and very low in the surface and subsurface layers (USDA, 1998). The Valkaria Fine Sand is associated with wet prairie sloughs. In most years the water table is within 10 inches of the surface for 1 to 3 months and 10 to 40 inches below surface for 6 months, and recedes to a depth of 40 inches for about three months. The Myakka Fine Sand is a deep, moderately permeable soil formed in thick beds of marine sands. Typically, the water table is within 10 inches of the surface from 1 to 3 months and 10 to 40 inches below the surface for 2 to 6 months. The Pompano fine sand is a deep, poorly drained soil that forms in thick beds of sandy soils that occurs in depressions, including most of the cypress domes on the site.

The surficial sand collected at the Stairstep Project site area was analyzed for grain size distribution. The classification of the sands after particle size analysis indicates that the sands are predominately, poorly graded sand with silty sand mixture and is designated by the USCS classification code as a SP soil. Coefficient of curvature values (Cc) ranged from 0.95 to 1.22 for ST1; 0.97 to 1.25 for ST2; 0.74 to 1.34 for ST3; 0.43 to 1.19 for ST4; and 0.37 to 1.19 for ST5. The value for coefficient of uniformity (Cu) for ST1 and ST2 ranged from 1.5 to 1.8, for ST3 the range is from 1.5 to 3.7, for ST4 from 1.5 to 28.2 and for ST5 values ranged from 1.4 to 14.5. The gradation curves plotted from grain size distribution data is located in **Appendix B**.

Precision Drilling/Robert N GEOLOGIST/OFFICE	rict 33406 -6442 BORING LOG rilling Program - Phase II Stairstep P R	oject, Lee County, Flori	da
DRILLING EQUIPMENT/METHOD	SIZE/TYPE OF BIT	SAMPLING ME	
WELL INSTALLED? CASING N	4.5" Hollow Stem Auger	Split Spoon	5/14/98-5/14/98
YES NO C Sch.40 ELEVATION OF: GROUND S	VC/2" TYPESlotted MA	. PVC LENGTH 2'	DIA. 2" SLOT SIZE .010
(FT. ABOVE M.S.L.)	JRFACE TOP OF WELL CASING TOP 18'	& BOTTOM SCREEN 20'	DATE 5/14/98
REMARKS:		=	0,1,100
Depth (ft) Type & Peretrain Number Allon Besistance Blows/6 Nufiled	LOG OF TEST BORING		Penetration Resistance Jlows/Foot) 35 55 75 100 0 36 55 75 100 0
Depth (ft) Type & Recovery Number Penetratic Resistanc N-Value N-Value	FIELD DESCRIPTION	Log (E Notes Q_15	Resistance 50 11 12 Blows/Foot) 6 9 11 12 35 55 75 100 0 11 × 0
S1 4456 PT 9 52 4557 SP-P	Organic, sand		<u>35 55 75 100 8.5 \$8</u>
53 2 2 3 2 5 5 54 2 1 2 3 3	Sand (50%), organic (50%) Organic (70%), sand (30%) brown		
$\begin{array}{c c} & S5 & 2 & 1 & 2 & 2 \\ \hline & & & & \\ \hline & & & & \\ \hline & & & & \\ \hline & & & &$	Sand, fine silty	2.0	
S7 4 4 6 8 10 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5		4.0	
S9 56811 14	Sand, fine grained, streaks of organic		2000 2000 2000 2000 2000 2000 2000 200
20	Sand, very fine, sugar	0.0	
	ledium Sand Bentonite Pellets Simestone ZZZZ Clayey Sand	Cement Grout	Sluff/Backfill

Figure 11. Boring Logs for ST1

Well Installation and Geologic Investigation for the Isolated Wetlands Research Program - Phase 2

Mar 3301 West (561) PROJE 1163 DRILL Preci GEOLO Kevin DRILL Drill WELL YES ELEVA	ABC Gun ( Palm 686-8 IG/WELL ST-2 CT NO SION COGIST/C NG CO SION D COGIST/C NG CO SION D COGIST/C NG CO SION D COGIST/C NG CO SION D COGIST/C NG CO SION C SION C S	2. /NAME ted Wetlar NTRACTOR/C rilling/Rob DFFICE er/South F JIPMENT/ME Illow Stem LED? CAS AO C SCH SCH CAS	Distric rida 33 687-6 687-6 Miller ORILLER ert Mille Iorida V THOD	Ct 406 442 BORING LOG LOCATION ling Program - Phase II Stairstep F er Water Management District SIZE/TYPE OF BIT 4.5" Hollow Stem Auger T./DIA. SCREEN: T/PESIotted M/ IFACE TOP OF WELL CASING TO	SAMPL Split S	ING METHOD Spoon STH 2' DIA.	START/FINI 5/14/98-5 2" SLOT S DATE 5/14/98	5/14/98
Depth (ft)	Type & Recovery Number	58.	Unified Classification	LOG OF TEST BORIN	Log	Penetra Resista (Blows/F	nce 'oot)	Graphic Litho Log Well Construction
		5 4 6 7         10         2       8 8 8 9         16         3       7 5 6 6         11         4       5 4 4 3         5       2 2 2 6         4       6 8 10 13         18       7 6 9 11         15       7 7 10 12         17       17	PT SP	2 inches of organic Fine grained sand Sand, light brown, some organic material Sand, silt, clay? Sand, silt Sand, fine grained Sand, silt Sand		•	55 75 100	
	Fine Sa	Material		edium Sand Bentonite Pellets mestone Clayey Sand	Fine sand w/ she		Clay w/ shell f/Backfill	-

Figure 12. Boring Logs for ST2

Ma 3301 West (561)	n <mark>ag</mark> I Gun t Palm	Clu Clu Be -88	1en ub Ro each, 00 /	t D bad Flori	Vate istri <sup>ida 33</sup> 687-6	ct 406		RODING	AN AN AN											
PROJ	ST ECT N	- <u>3</u> 0./N	AME					BORING	CATIO	N										
ORILL	ING C	ONT	RACT	OR/DF	ds Dril RILLER rt Millo		Program - I	Phase II Sta	airste	p Projec	t, Lee C	ount	<u>y, F</u>	loric	la					
GEOL	OGIST	/OFF	ICE				r Managan	nent Distric												
DRILL	ING E	QUIP	MENT	MET	HOD		SIZE/TYPE C	DF BIT				SAMPL Split			HOD			IISH DA		
	INST/				NG MAT 40 PV		•	SCREEN:		MAT. PV		LENG						SIZE .(		
	ATION		(		ND SUR			WELL CASING	3	TOP & BO			2111	-		DATE 5/14		<u> </u>		
REMA	RKS:																			
Ę,	Samp ∞ ≥	ole ĕ	ance	9.9	Unified Classification			LOG OF TES	ST BO	RING						stration stance /s/Foot) 55 75 100				
Depth (ft)	Type & Recovery	Number	Penetration Resistance		Unifie Classi		FIELC	DESCRIPTIC	N		Log Notes		D		lows 35	/Foot) 55	75 100	Graphic Litho Log	Well Constr	
 -		51	340			San	d, white													
-	$\mathbf{X}$	52	86 13		SP	San	l, tan to brov	vn												
5		53	546										•	)						
		54	444										•						₽	
-	Å.	55	544			Sand	l, tan						•							
- 	X		8			Sano	l, tan to crear	m, fine grained	d											
-		6	535 8	×4		Sand	l, cream to w	hite					Ī							
-		7	555 10			Sand	, light brown	, fine grained												
- 	∦ s	8	555 10					-					¢							
	// <b> </b> // s	9	643	5									¢							
	Å		7			Sand	, light brown	to dark brow	n	1									<u>a</u> E	
-	X		10			Sand	, dark brown	to light brow	n	20.0			-							
-20										20.0								<u></u>		
	Fine Si					dium S	<u>641</u>	Bentonite i	Pellets		Cement Gr	rout	-		] Silt/	Clay w	/ shell	_		
	Organi	c Ma	terial		Lim	estone	$\mathbb{Z}$	Clayey Sar	nd		Fine sand	w/ shell			Sluf	f/Backt	H			

Figure 13. Boring Logs for ST3

								. <u> </u>	
	th Fl								
Mar	nager	ner	nt D	istri	st Brown				
3301	Gun Cl Palm B	ub R	oad	40.22	106				
(561)	686-88	300	/ Fax	687-6	442				
	G/WELL		_						
BOHIN	ST-4	NU.			BORING LOG				
	CT NO./				LOCATION				
1163	I/Isolate		etland	<u>is Drill</u>	ing Program - Phase II Stairstep I	Project, Lee County	y, Florida		
Preci	sion Dri	illing			er				
	OGIST/OF			h					
	NG EQUI				Vater Management District	SAMPL	ING METHOD	START/FINISH	DATE
	Rig/Muc				4.5" Hollow Stem Auger	Split	Spoon	5/12/98-5/1	3/98
YES 1		ED?		NG MA1 40 PV		AT, PVC LEN	STH 10' DIA.	2" SLOT SIZ	= 010
	TION OF			ND SUR		P & BOTTOM SCREEN		DATE	
	BOVE M.	S.L.)			50	'/60'		5/13/98	
REMAI	HKS:								
[	Sample							<u> </u>	
3		c tio		atio	LOG OF TEST BORIN	G	Penetra Resista	tion	ctio
Depth (1	Type & Recovery Number	letra Listar	Blows/6 <sup>-</sup> N-Value	Unified Classification		Log	(Blows/I	oot)	Litho Log Welt Constructi
ð		Per	ng ź		FIELD DESCRIPTION			55 75 100 Ö	Con Kelt
Ł	∭ <sup>S1</sup>		4.4 7	PT			T		
F	$\Lambda$				Organic, sand, brown			- Hereiter	
F	<b>S</b> 2		44 9	SP			T	- E	
F			5		Sand, white, organic matter				
F	53		33	1			•		
5	X	4	6.						
-	<b>S</b> 4	34	55	.		6.0	•	<u> </u>	<u> </u>
	X		9		Sand, brown				
- ' 	S5	6 6	68						
-			2		Sand, tan fine grained				
- 10	/   	- 9 -	88				•••••		
-	V 30		88 5						
-									
-	<b>S</b> 7		99 6				Ī		
- 	$M \square$								
	V 88		46 8						
— 15 -	MTI		-			16.0	<u> </u>		
F	59		86	1	······································		7		
	X I	1	6		Sand, silty, tan				
-	510		52	ł			•		
	X	1	0		Sand, silty tan/gray				
-20	() 511	43	3 1 2	-					
F	X		6						
Ľ.			0.5	4		22.0			
Ļ.			25 4						
Ł	$\mathbb{N}$				Lime mud w/ pieces of limestone, _ micrite	24.0			
-	<b>Б</b> 13	17 18	8 11 8		······			P	
Î	Fine San	d	[::	M	edium Sand A Bentonite Pellets	Cement Grout	Silt.	Clay w/ shell	
	,		منعا چسم ا	نه <del>د</del>					
	Organic I	viateria	" 년		nestone Clayey Sand	Fine sand w/ sh	Sur Sur	f/Backfill	

**Figure 14.** Boring Logs for ST4 (continued on Page 31)

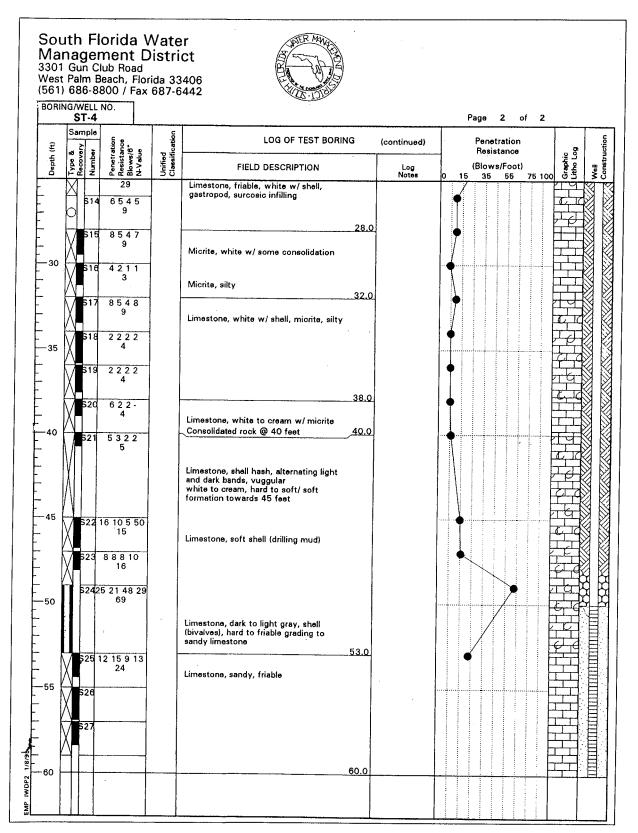


Figure 14. Boring Logs for ST4 (continued from Page 30)

Sout	h Flo	orida	Wate	r ARR MANA			
Mana	agen	nent l	Distri	ot Brown B			
3301 G	iun Clu	ub Road	orida 33	106			
			x 687-6				
BORING	/WELL N	io.		BORING LOG			
	ST-5						<u> </u>
PROJEC 1163/I			nds Drill	IDCATION	Project, Lee	County, Florida	
DRILLIN	G CONT	RACTOR	DRILLER				
GEOLOG			pert Mille	ər			
		/South MENT/M		Nater Management District		SAMPLING METHOD	START/FINISH DATE
		Rotary		4.5" Hollow Stem Auger		Split Spoon	5/15/98-5/19/98
WELL IN	STALLE	D? CA	SING MAT	T./DIA. SCREEN:			. 2" SLOT SIZE .010
YES 🛛			DUND SUR		AT. PVC		DATE
(FT. ABC		S.L.)			0'/60'		5/19/98
REMARK	(5:						
s	ample		5	LOG OF TEST BORI		Danot	ration .5
£ a	, <u>}</u> ;	Penetration Resistance Blows/6" N-Value	Unified Classification				ration tance s/Foot) 55 75 100
Depth (ft) Type &	Recovery Number	enetr esist dows -Vat	Inifie Lassi	FIELD DESCRIPTION	La		tance 00 57 s/Foot) 00 55 75 100 05 10 80
	/ S1	3446					
		8		Sand, white			
F K	/ \$2	7464			2.0	•	
		10		Sand, tan, silts	4.0		
F f	<b>S</b> 3	4222			4,0	•	
		4		Sand, tan to dark brown, organic			
F	<b>5</b> 4	3345	SP-PT			•	
		7		Sand to organic material, white to dark			
F	55	3233		brown		•	
		5		Sand to sandy organic material, light brown	10,0		
-10 F	<b>5</b> 6	4445				T T	
FV		8		Sand, tan to light brown	12.0		
FK	<b>S</b> 7	4478				7	
FV				Sand, white, clayey sand @ 14 feet			
F.K	<b>S</b> 8	2223	sc			Ţ	
-15 X				Clayey sand, white to cream, very fine grained	16.0		
FK	<b>S</b> 9	3248	SP			Ţ	
ΕV		v		Sand, white, very fine			
EN	510	7632					
					20.0		
E 20 D	<b>б</b> 11	6 Refusa	at	Limey sand w/ gastropods and	21.0		
66/8	512			sphilapod			₽₩
71				Limestone, coral, shell molds, vuggular			
λL							
\$ <u></u>	5 613						
ľ	Fine Sand	Ι.	M III N	ledium Sand Bentonite Pellets	Cemer	t Grout	ilt/Clay w/ shell
	Organic N	Aaterial		mestone Clayey Sand	Fine sa	and w/ shell	luff/Backfill

Figure 15. Boring Logs for ST5 (continued on Page 33)

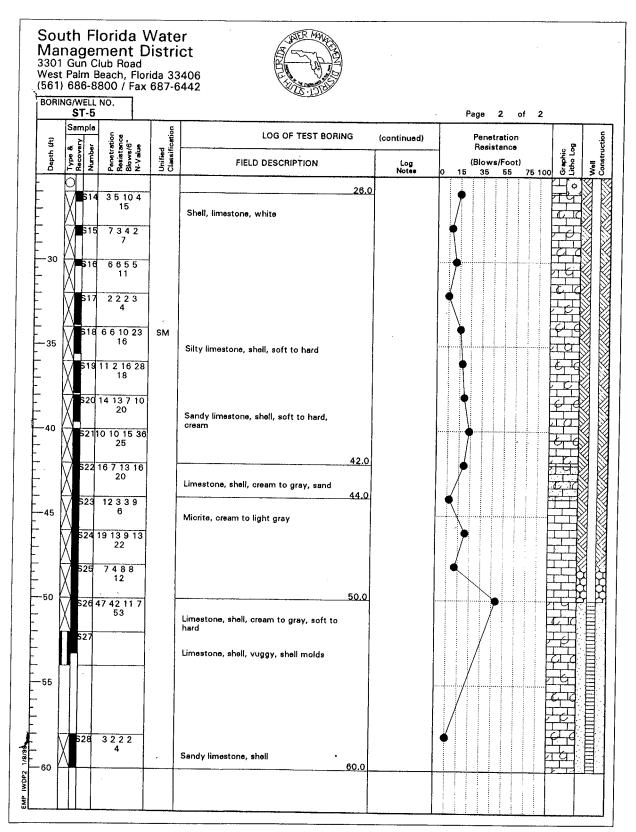


Figure 15. Boring Logs for ST5 (continued from Page 32)

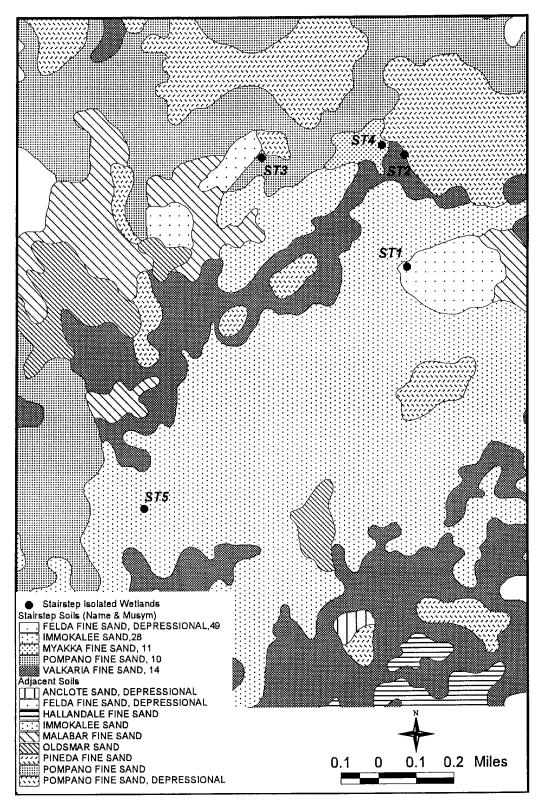


Figure 16. Selected Soil Survey map of Lee County at the Stair Step Project Study Area

# 5.5 Core Analysis

Wells ST4 and ST5 contained consolidated sediments that were cored and analyzed in the lab for hydraulic conductivity. **Table 4** lists the selected intervals that were analyzed.

Table 4.	Values of Hydraulic Conductivity for selected Intervals
	at Stairstep Project Study Area

Sample Number	Site Name	Top Depth of core interval (ft-bls)	Bottom Depth of core interval (ft-bls)	Horizontal Hydraulic Conductivity (K <sub>h</sub> ) ft/day	Vertical Hydraulic Conductivity (K <sub>v</sub> ) ft/day	Description of core
2	ST4	42.6	43.0	16.6316	313.877	Limestone
3	ST4	52.5	53.0	0.0003	0.0066	Limestone
4	ST5	21.0	21.5	0.0004	0.0066	Limestone
5	ST5	52.2	52.7	20.671	390.101	Limestone

# 6.0 HOGAN ISLAND FARMS STUDY AREA

## 6.1 Site Description

**Figure 17** shows the location of the monitoring sites located on Hogan Island Farms in Collier County. This site is characterized by isolated wetlands surrounded by small vegetable farming operations, pasture, rangeland, and hardwood hammocks. Wells drilled at this site are designated with the letters HF. Eight wells (HF1 through HF8) were drilled at this site to characterize the geology and to interpret ground water movement and wetland hydrology. Wells HF1, HF2, and HF4 are located on the edge of isolated wetlands. Well HF3 is located on the edge of an isolated wetland that was most likely once a part of a slough system. Altering the landscape to build an access road and crop fields may have isolated this wetland. Well HF7 is located in a hardwood hammock. Wells HF5 (73 feet) HF6 (75 feet) and HF8 (80 feet) were drilled as back ground "local" wells. These wells were drilled to provide information on the water table gradients between the isolated wetlands and the uploads. The remainder of the wells HF1, HF2, HF3, HF4 and HF7 (approximately 20-foot) were constructed on the edge of wetlands to determine geologic controls that may influence the water levels in the wetlands and to indicate direction of ground water movement.

### 6.2 Well Construction

**Table 1** shows well construction specifications for wells drilled at the Hogan Island Farms study area. Wells HF1, HF2, HF4 and HF7 were drilled approximately 20 feet bls using the hollow stem auger method. Well HF3 was drilled to 17 feet using the tripod method because of the sensitivity of the wetland and difficulty accessing the site with a mobile drilling rig. Each of these wells is completed with 2-foot screens.

The deeper wells HF5 (-46.11 feet NGVD), and HF6 (-50.95 feet NGVD) were initially drilled using the hollow stem auger method until limestone was encountered at approximately 20 feet bls. Difficulty washing the cuttings out of the borehole as well as difficulty drilling through the limestone using the auger bit nessitated changing to the mud rotary drilling method. The NX core barrel replaced the split-spoon sampler for formation samples. Well HF8 (-56 feet NGVD) was drilled using the mud rotary method through out its entire depth. The NX core barrel was used after getting to the consolidated limestone approximately 20 feet bls. Each of these wells is completed with 10-foot screens. Boring logs for wells HF1 through HF8 are shown in **Figure 18** through **25**. Penetration rates (blows per foot) were relatively consistent for each well for unconsolidated soils while high rates reflected consolidated composition, such as limestone, shell and fine sand.

### 6.3 Geology

Well cuttings and split-spoon samples were examined to determine the general lithologic units from eight monitoring wells drilled on the Hogan Island Farms study area. Figure 26 shows the geologic cross-section A - A' of eight wells. In most of the wells one to two feet of organic matter was observed from land surface except in well HF8, where organic matter was observed underlying approximately 5 foot of sand. Split spoon samples from wells HF5 and HF3, indicate approximately 8 feet of organic and sand mixture before undifferentiated sand was observed. Following the organic matter is a sequence of undifferentiated sands that ranged 6 to 19 feet thick and

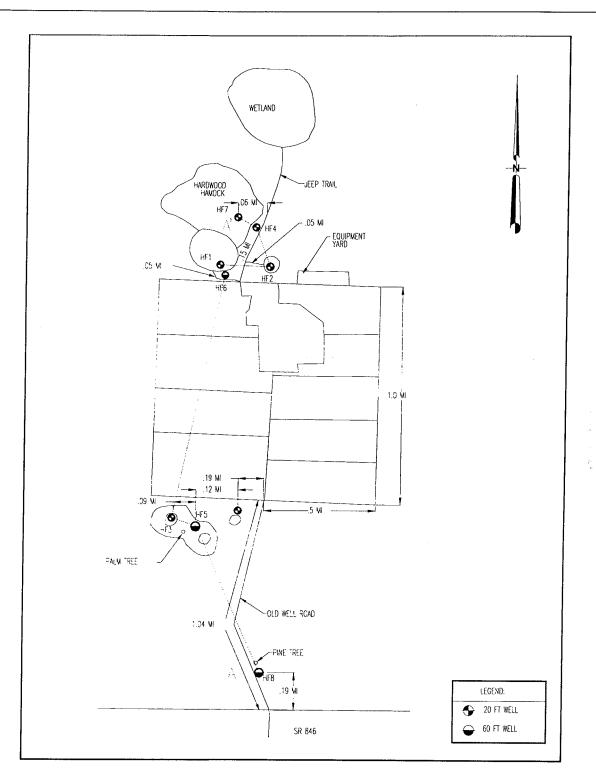


Figure 17. Location of Monitoring Wells on Hogan Island Farms, Collier County, Showing Cross Section A-A'

extended down between 13 feet to approximately -7 feet NGVD. Underlying the undifferentiated sands is sandy limestone, sand and shell mixture. The top of the sandy limestone ranges from 10 feet NGVD to approximately -16 NGVD and averages approximately 20-feet thick. Split spoon samples from monitoring well HF5, located between HF8 and HF6, indicated the shallow limestone layer is absent and is replaced by a thicker sequence of sand (34 feet thick). The absence of limestone in HF5 suggests a sedimentary facies change occurred. This may be either a result of a clastic depositional environment that was formed during the deposition of carbonate limestone, or a fluvial environment that eroded the limestone and sand was deposited in its place. In well HF3, located adjacent to HF5, limestone was observed at approximately 10 feet NGVD. Twenty foot wells, HF2, HF4 and HF7 also did not penetrate in the limestone suggesting the formation is dipping to the north in the study area.

Underlying the limestone is a horizon of variable clay, sand and silt approximately 30 feet thick. Samples collected from monitoring well HF6 located approximately 1.8 miles north of site HF8 is the same lithologic sequence but the depths are shifted approximately six feet shallower. The lowest unit penetrated by the monitor wells is another sequence of sandy limestone, limestone and phosphate. The top of this unit ranges in depth from -36 feet NGVD to -46 feet NGVD.

# 6.4 Classification of Soils and Grain Size Distribution

**Figure 27** shows the soil survey map on the Hogan Island Farms study area. The majority of soils occurs at this site are associated with the Oldsmar Fine Sand (wells HF5, HF8). Sands collected from wells installed on wetland edges (HF1 and HF3) are most likely from the Chobee series unit associated with depressional wetlands. Boca fine sand is associated with the upland fringe of wetlands where wells HF2, HF4, HF6, and HF7 are located.

Oldsmar fine sand is a nearly level, poorly drained soil found in flatwoods. Typically, the surface layer is dark grayish brown fine sand about 4 inches thick. The subsurface layer is fine sand to a depth of about 35 inches. The upper part of the subsurface layer is light gray, and the lower part is light brownish gray. The subsoil extends to a depth of about 60 inches. The permeability of this soil is typically slow. Under natural conditions, the seasonal high water table is between 6 to 18 inches for 1 to 6 months. During the remainder of the months the water table is below a depth of 18 inches, and recedes to a depth of more than 40 inches during extended dry periods (USDA, 1998).

The Chobee series consists of level, very poorly drained soils located mostly in swamps and marshes. These soils formed in thick beds of loamy marine sediments. The surface layer of these soils are black fine-loamy, siliceous, and are about 6 inches thick. The subsurface layer is also black fine sandy loam to a depth of about 13 inches. The subsoil is mottled sandy clay loam to a depth of about 45 inches. The upper part of the subsoil is dark gray, and the lower part is gray. The permeability of the Chobee soil is moderate. Under natural conditions, these soils are ponded for 6 months or more during most years. During other months, the water table is within a depth of 12 inches, and it recedes to a depth of 12 to 40 inches during extended dry periods. (USDA, 1998).

The Boca fine sand is a nearly level, poorly drained soil located in flatwoods. The surface layer is very dark gray fine sand about 4 inches thick. The subsurface layer is fine sand to a depth of about 26 inches. The upper part of the subsurface layer is light gray, and the lower part is brown. The subsoil is grayish brown fine sandy loam to a depth of about 30 inches. The permeability of this soil is moderate. The seasonal high water table is at a depth of 6 to 18 inches for 1 to

<b>Mar</b> 3301 Vest 561)	Gur Gur Palr 686	<b>jer</b> n Cl n B 5-88	nei Iub F each 800	nt D Road h, Flor	Nate Distri rida 33 687-6	ct 406						
BORIN	NG/WI		NO.	7		BORING LOG						
PROJE	ECT N	10./			de Dril							
DRILL	ING C	CON	TRAC	TOR/D	RILLER	ling Program - Phase II Hogan Island	i rari	ns, Collier C	ounty, Fi	orida		
Preci GEOLO				/Robe	ert Mill	er						
Kevir	n Ro	hre	r/Sou	uth Fl	orida V	Nater Management District		CANOLI	NG METHO	CTADT/CU		<u>.</u>
Drill	Rig/H	lol	ow S	Stem	Auger	4.5" Hollow Stem Auger		Sameli Split S			NISH DATE -5/21/98	
VELL /ES	INST.				NG MAT	T./DIA. SCREEN:	PVC	I ENG	TH 2' DIA	. 2" SLOT	SIZE 010	, _
LEVA	ATION	OF	:		IND SUR	FACE TOP OF WELL CASING TOP &	BOTT	OM SCREEN		DATE	JIZE .010	<u></u>
	BOVE	****	5.L.)			19'/2	1		<u> </u>	5/21/98		
	1				<del></del>	· · · · · · · · · · · · · · · · · · ·						_
Ð	Sam		io So e		Unified Classification	LOG OF TEST BORING				ration		
Depth (ft)	Type & Recovery	Number	Penetration Resistance	Blows/6 <sup>-</sup> N-Value	ified	FIELD DESCRIPTION		Log		tance s/Foot)	Graphic Litho Log Well	
<u>å</u> .		2 51		82 22	5 ਹੈ PT			Notes 0	● <u>15 35</u>	55 75 100		
	X			4		Organic matter						·
		<b>S</b> 2	53	34	SP-PT		2.0		•			1
	X			6		50% organic matter, 50% sand						1
	$\langle \rangle$	<b>S</b> 3		56	SP	2	4.0		•			Ž
•5	X		:	9		Sand tan to white, w/ organic matter				•		
	$\overline{\mathbf{N}}$	<b>S</b> 4		56 0	sм		6.0		•		$\square \square \blacksquare$	
	ŴП			•		Silty sand, very fine, gray to white, organic matter	B.0					
	M	S5		66 9	] [				₹			
10	Μ					Sandy limestone, shell, gray to white, hard, organic matter <u>10</u>	2.0					
	M	50		189 9		Shell, limestone, sand						
	$\left( \cdot \right)$	<b>S</b> 7	73	36					<b>√</b>			
	IX II			6Ŭ								
		<b>S</b> 8	55	56	SP		1.0		è			
15	XII		1	0		Sand w/ shell					C A	
		59				Shell, limestone, silts	5.0				यम्	
Ì		510	refu	ısal								Н
	Ш										HH E	1111
20	M	511		76 4		Cond Succession 1. 11. 11.			•			
	$\square$					Sand, limestone, shell, white					यम् -	
	Fine S	Sand			Me	dium Sand		ement Grout	F-G- Sik	t/Clay w/ shell		
لنظم				اننا			- KA					
32	Organ	nic M	ateriai	Ľ	Lim	nastone Clayey Sand	F	ine sand w/ shell	STORE SIL	iff/Backfill		

Figure 18. Boring Logs for HF1

Man 3301 West ( 561) PROJE 1163 DRILLI Precis GEOLO	Ager Gun CI Palm B 686-88 G/WELL I HF-2 CT NO./I /Isolate NG CON sion Dri OGIST/OF	NAME d Wetlan IRACTOR/D lling/Robo FICE	Distric rida 33 687-6 6 687-6 6 6 7 6 7 6 7 6 7 6 7 6 7 7 6 7 7 7 7	Ct 406 442 BORING LOG Ing Program - Phase II Hogan Island Fa	arms, Collie	r County, Flo	rida	
DRILLI	NG EQUI	r/South F PMENT/ME	lorida V THOD	Vater Management District SIZE/TYPE OF BIT	1	PLING METHOD		
	Rig/HSA		ING MAT	4.5" Hollow Stem Auger	Spli	t Spoon	5/22/98	-5/22/98
YES D		🛛 🗆 Sch	.40 PV	C/2" TYPESIotted MAT. PV	C LE		2" SLOT	SIZE .010
	TION OF		JND SUH	FACE TOP OF WELL CASING TOP & BC	TTOM SCREEK		5/22/98	
REMAR	RKS:							
1 1	Sample	Penetration Resistance Blows/6" N-Value	Unified Classification	LOG OF TEST BORING		Penetr Resist		Graphic Graphic Vell
Depth (ft)	Type & Recovery Number	<sup>5</sup> enetr Resist Blows V-Valu	Jnifie	FIELD DESCRIPTION	Log Notes	(Blows	/Foot) 55 75 10	Graphic Litho Log Well
-	\$1 51 52	5442 8 5556	SP-PT	Sand, organic matter, off white, fine grained				
	\$3	10 5567		Sand, organic matter mix light gray, fine grained		•		¥ ₩ ¥
	S4	10 6 6 6 12	-	Sand, organic matter, light gray fine grained Sand, organic matter, off white, fine		•		
	\$5	4334	_	grained Sand, w/ some organic matter, light gray fine grained				
-  	\$6 \$7	2 2 2 3 4 2 2 2 2 2 4	SP	Sand, organic matter, light brown to gray 12.0				
- - - 	∧ 	1222		Sand, light brown		•		555
-	$\square$		-	16.0	1			
	X 59	2104		void 17.0		•		
	510	1 0 2 2 2	sc	Sand, 50% organic matter 50% 18.0 Sand to sandy clay 20.0		•		
20								
	Fine San	d [		edium Sand D Bentonite Pellets	Cement Grout	si	t/Clay w/ shel	<b>_ I</b>
	Organic I	La Material		mestone	Fine sand w/	sheli Si	uff/Backfill	

Figure 19. Boring Logs for HF2

Sample         Control           Sample         Source           Sample         Sample           Sample	LOG OF TEST BORING FIELD DESCRIPTION Sand, some organic matter Sand (40%), organic matter (60%)	Log (Blows/F Notes 0 15 35 f	nce <u>6</u> 5
16 S2 11 6 6 5 12 S3 4 4 4 4 8 S4 3 2 2 3 4 S5 5 6 5 7 SC	Sand, some organic matter		
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Organio (60%), Sand (40%), brown to light brown 6.0 Sand, white to light gray, some organic matter 8.0 Sand to sandy clay, silty, gray 10.0 Sand, fine grained, white, shell fragments, micritic 12.0 Sandy clay, limestone, gray, friable, shell fragments 14.0 Limestone, friable, gray shell fragments micritic Limestone, friable gray 20.0		

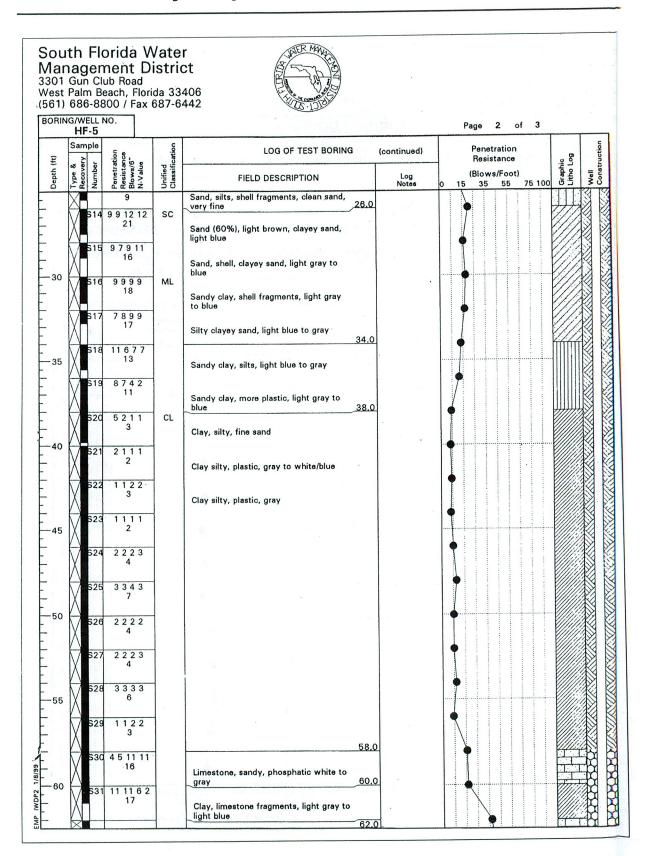
Figure 20. Boring Logs for HF3

South Fl Manager 3301 Gun Cl West Palm B	nent l lub Road each, Flo	Distrie orida 33	2t 406			<u>.</u>
(561) 686-8 BORING/WELL HF-4 PROJECT NO./			BORING LOG			
1163/Isolate DRILLING CON Precision Dr GEOLOGIST/OF	TRACTOR/ illing/Rot	DRILLER	ing Program - Phase II Hogan Islani r	I Farms, Collier	County, Florida	
Kevin Rohre DRILLING EQUI Drill Rig/HSA WELL INSTALL	PMENT/MI	Florida V ETHOD SING MAT	Vater Management District SIZE/TYPE OF BIT 4.5" Hollow Stem Auger /DIA. ISCREEN:			ART/FINISH DATE 21/98-5/21/98
	D GRO	h.40 PV	C/2" TYPESlotted MAT	BOTTOM SCREEN	<u>57H 2' DIA. 2"</u> DAT <b>5/2</b>	<u>SLOT SIZE .010</u> E <b>1/98</b>
Depth (ft) Type & Recovery Number	Penetration Resistance Blows/6" N-Value	Unified Classification	LOG OF TEST BORING		Penetration Resistance (Blows/Foot	truct Log
Depth (1 Type & Recover	4 4 6 4 10	PT	FIELD DESCRIPTION	Log Notes		75 100 5 5 5
- S2	4456 9 5566	SP	Sand, tan to light gray and light brown	2.0		¥
5 5 5 5 54	11 4445 8		Sand, light gray, very fine grained	6.0		
55	4344 7		Sand, very fine, light gray	8.0		
-10 S6	3355 8 7775					
- 15	14 3335 6	_				
59	5355 8			8.0		RAKK AMARK
- 20	2222 4	SM	Sand, silty, gray to blue	20.0		
Fine San	d		edium Sand 🛛 🏹 Bentonite Pellets 🕅	Cement Grout	Silt/Clay	w/ shoil
Organic	Material		nestone	Fine sand w/ sh	ell 100000 Sluff/Ba	ckfill

Figure 21. Boring Logs for HF4

South Florida M Management E 3301 Gun Club Road West Palm Beach, Flo 561) 686-8800 / Fax BORING/WELL NO. HF-5 PROJECT NO./NAME 1163/Isolated Wetlan DRILLING CONTRACTOR/D	Districa rida 3340 687-644	06	Farms, Collier (	County, Florid	da
DRILLING EQUIPMENT/ME <sup>-</sup> Drill Rig/Mud Rotary WELL INSTALLED? CAS YES X NO C Sch	lorida Wa	/2" TYPESiotted MAT.	Split S PVC LENC BOTTOM SCREEN	Spoon <u>STH 10' DIA. 2</u> D	START/FINISH DATE 6/8/98-6/9/98 2 <sup>.</sup> SLOT SIZE .010 ATE /9/98
Depth (ft) Types & Recovery Recovery Number Restatance Blows(6 Blows(6 Nv attee	0 Unified Classification	LOG OF TEST BORING	Log Notes (	Penetrati Resistan (Blows/Fc ) 15 35 5	ee the book (too
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	SP-PT SP-PT S SP SP SP Si SM Si Si Si Si Si Si Si Si Si Si Si Si Si	Organic matter (10%), sand (90%),       2         Sand (50%), organic matter (50%)       2         Organic matter (80%), sand (20%),       3         ine and silty light brown       3         Sand (60%), organic matter (40%),       3         ine and silty light brown       3         Sand (70%), organic matter (30%),       10         and (70%), organic matter (30%),       10         and (70%), organic matter (30%),       10         and light, dark brown to light brown,       10         and light gray to yellow, fine grained       10         and, light brown, fine grained       10         and, light brown, fine grained       18,1         and, silts, very fine grained       18,1	0		y w/ shell

Figure 22. Boring Logs for HF5 (page 1 of 3)



**Figure 22.** Boring Logs for HF5 (page 2 of 3)

44

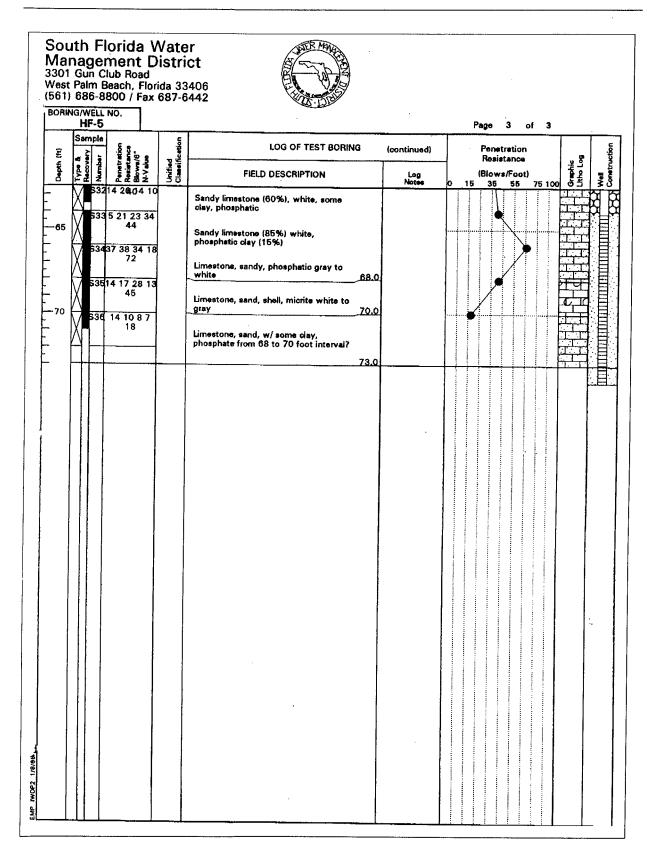


Figure 22. Boring Logs for HF5 (page 3 of 3)

South Florida Wat Management Dist 3301 Gun Club Road West Palm Beach, Florida (561) 686-8800 / Fax 687 BORING/WELL NO. <u>HF-6</u> PROJECT NO./NAME	rict	ma Calliar County Florida
DRILLING CONTRACTOR/DRILLE <u>Precision Drilling/Robert M</u> GEOLOGIST/OFFICE	R iiller a Water Management District SIZE/TYPE OF BIT 4.5" Hollow Stem Auger MAT./DIA. SCREEN: PVC/2" TYPESlotted MAT. PVC	SAMPLING METHOD START/FINISH DATE Split Spoon 5/30/98-5/30/98
Depth (tt) Type & Recovery Number Penetration Resistance NV value Vuhifad	LOG OF TEST BORING	Log (Blows/Foot)
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Organic matter, sand dark to tan    2.0	Notes 0 15 35 55 75 100 0 5 3 3 0
500 Fine Sand Fine Sand	Sand, white, fine 16.0 Sandy limestone, shell, gray course to fine, bivalves (18 ft) Limestone, calcite, white, shell, bivalves Medium Sand	Cement Grout

**Figure 23.** Boring Logs for HF6 (page 1 of 3)

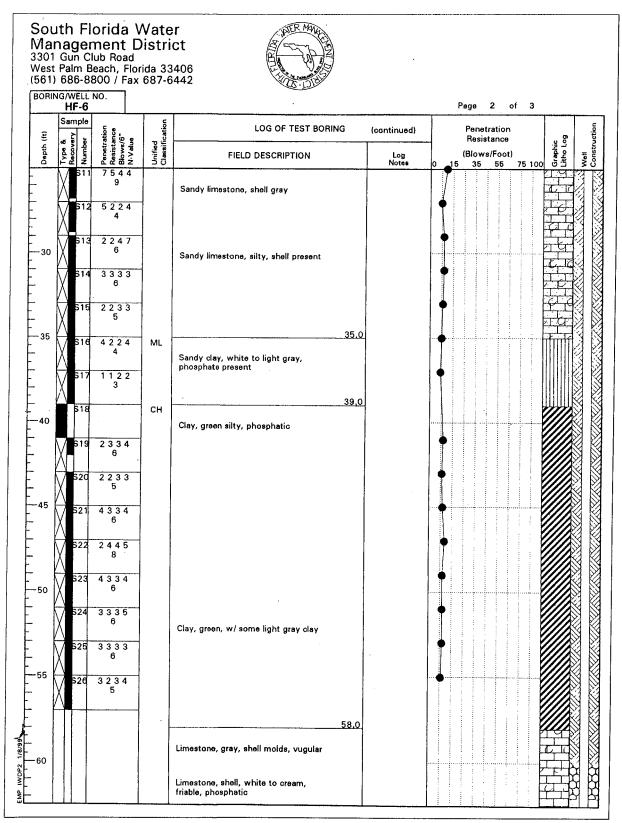


Figure 23. Boring Logs for HF6 (page 2 of 3)

South Florida Water Management District 3301 Gun Club Road West Palm Beach, Florida 33406 (561) 686-8800 / Fax 687-6442 BORING/WELL NO. HF-6 Page 3 з of Unified Classification Sample Penetration LOG OF TEST BORING (continued) Penatration Resistance Blows/6" N-V able Depth (ft) Type & Recovery Number Resistance Graphic Litho Log (Blows/Foot) ₩ S K FIELD DESCRIPTION Log Notes 75 100 35 55 Ч 65 70 75.0 لۍ ÷ 75 <u>.</u> WOP2 1/8/95 d.

**Figure 23.** Boring Logs for HF6 (page 3 of 3)

Mai 3301 Vest 561) BORII PROJ 116: DRILL Prec GEOL Kevi	nage I Gun t Palm ) 686- NG/WEI HF- VECT NG 3/Isola LING CC ision I OGIST/	Club Beac 8800 LL NO 7 7 NAM ated V DNTRA Drilling OFFICE rer/Sc	nt E Road h, Floo / Fax Vetlan CTOR/D g/Robe	ert Mill Iorida	Ct 3406 3442 ling Pro er Water N	gram - P	BORING I	TION		er County,		a TART/FIN		
Drill	Rig/H	SA		-	4.		w Stem Aug	jer	,	lit Spoon		/22/98		
WELL YES	INSTA	NO		ING MA			SCREEN: TYPESlotted		<b>•</b> •	ENOTU O	DIA 07	0.07	0.75	
ELEVA	ATION	OF:	GROU	IND SUF		TOP OF V	ELL CASING	TOP & BOT	TOM SCRE	ENGTH 2' EN	DIA. 2" DA		SIZE .	010
	ABOVE	M.S.L.)				<u> </u>	······	18'/20'			5/2	22/98		
Depth (ft)	Type & Recovery	anetration	resistance Blows/6" N-Vatue	Unified Classification		FIELD	LOG OF TEST	BORING	Log	R	enetratio esistanco lows/Fog	9	Graphic Litho Log	Well
		1         3           2         4.4           3         9.1           3         9.1           5         4.4           6         4           6         4           6         4           6         4           7         4.6           8         4.2           9         4.7           2         2           4.1         18	3 6 6         9         8 10         12         0 7 6         17         15 5         9         1 4 5         1 7 9         1 3         3         1 8 22         15 18         13	SP-PT	Drown Organic cream Sand, y Sand, b grained Sand, fi Sand, so	ellow fine ç	y to white, find white	w to 4.0	Notēs	0 15	35 66	76 100		
	Fine Sar Organic			لنغا	dium Sand		Bentonite Pelk		Coment Grout	<u> </u>	Silt/Clay Sluff/Bac			<u></u>

Figure 24. Boring Logs for HF7

DRILLING CO	Club Road Beach, Flor 3800 / Fax L NO. 3	ida 334 687-64 <b>ds Drill</b> RILLER	406 442 BORING LOG ing Program - Phase II Hogan Island Fa	rms, Collier Co	ounty, Florida	
GEOLOGIST/G Kevin Rohr DRILLING EQ Drill Rig/M WELL INSTAL	DFFICE er/South FI UIPMENT/MET UIPMENT/MET UIPMENT/MET UIPMENT/MET UIPMENT/MET UIPMENT UIPMENT UIPMENT UIPMENT UIPMENT UIPMENT UIPMENT UIPMENT/MET	orida V	Vater Management District           SIZE/TYPE OF BIT           4.5" Hollow Stem Auger           './DIA.           C/2"           TYPESlotted	Split S		INISH DATE 6/10/98 T SIZE .010
REMARKS: Sample (1) (1) (1) (1) (1) (1) (1) (1) (1) (1)	58.	Unified Classification	LOG OF TEST BORING	Log Notes 0	Penetration Resistance (Blows/Foot) 15 35 55 75 10	00 Graphic Litho Log Wall Construction
	1       3 3 7 7         10       10         2       10 10 10 10         2       20         3       8 9 10 10         19       19         4       3 4 6 8         10       10         5       6 6 9 9         15       6         6       6 6 8 8         14       14         7       6 6 6 6         12       10         8       5 5 5 6         10       10	SP	Fill material, white sand 4.0 Sand, organic matter (85%) Sand (60%) organic matter (40%), light brown 8.0 Sand light brown to tan Sand light gray to brown silty			
Y - Fine S	4 10 2 1 1 2 2 11 4 4 12 12 16 12 11 17 35 4 52 13 18 60 60		18.0 Sand (90%), Limestone, shell (10%) 20.0 Sand (10%) limestone, shell, silts, white to cream Limestone, shell, sand, white ledium Sand		SituClay w/ shu	

**Figure 25.** Boring Logs for HF8 (page 1 of 3)

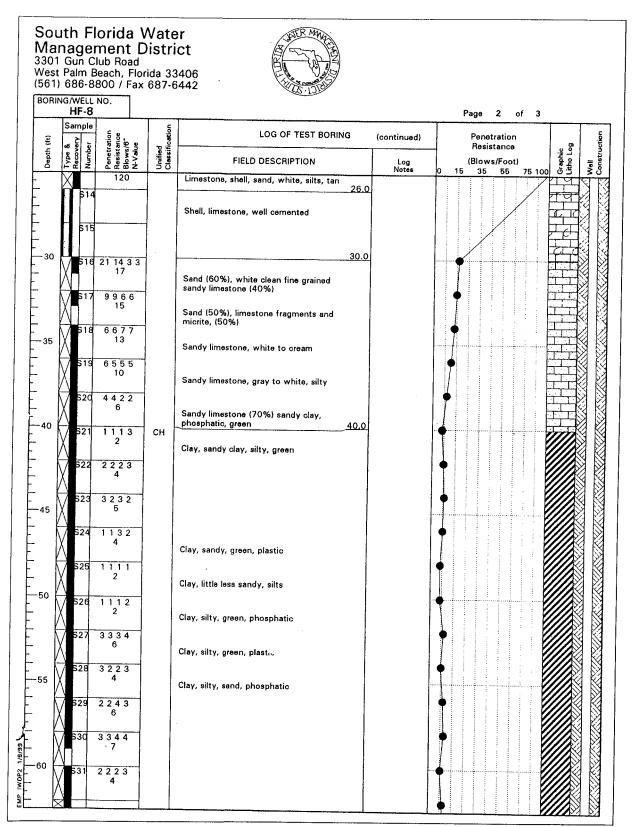


Figure 25. Boring Logs for HF8 (page 2 of 3)

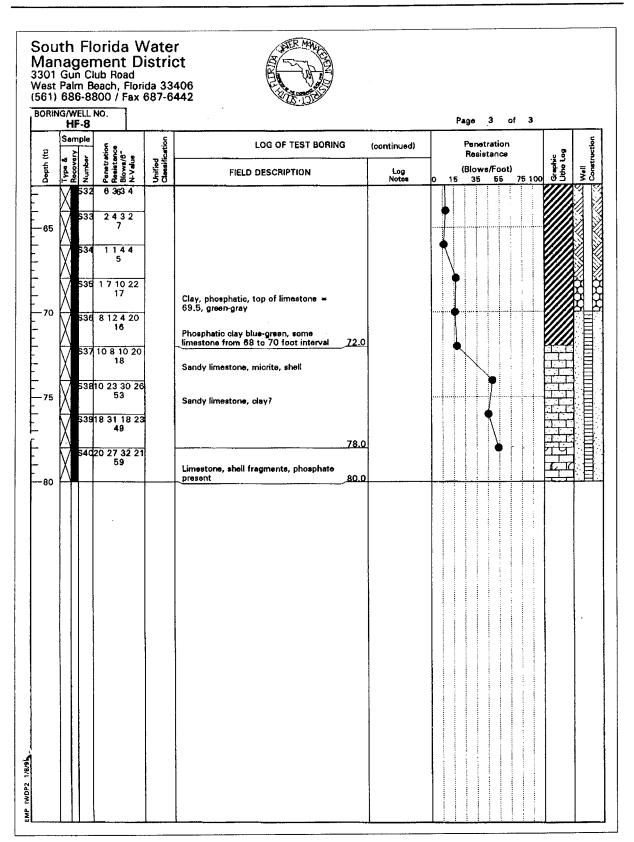


Figure 25. Boring Logs for HF8 (page 3 of 3)

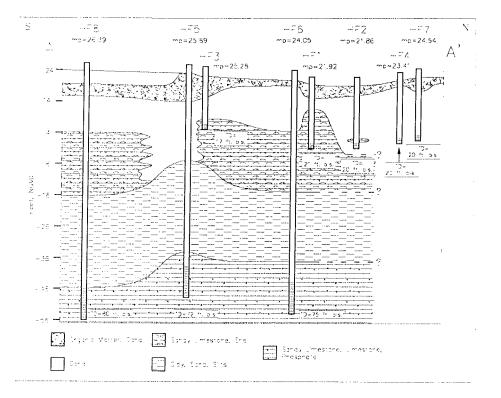
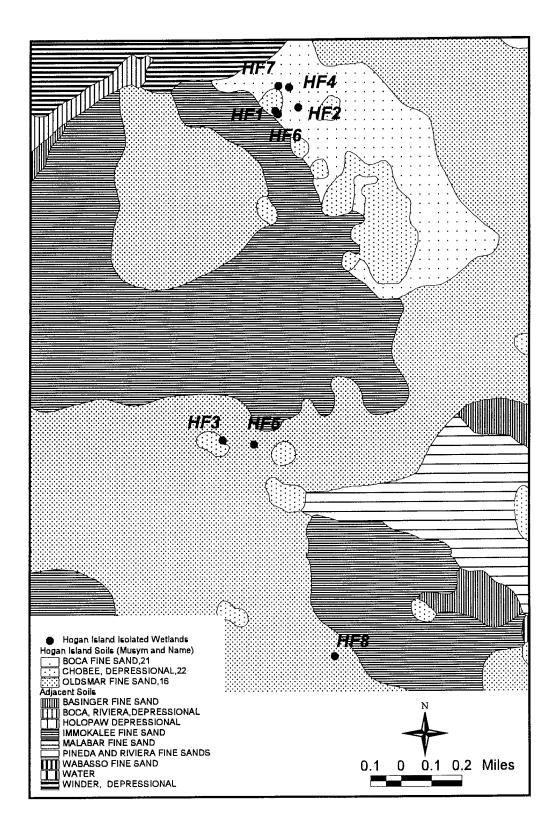


Figure 26. Geologic Cross Section A-A' at Hogan Island Farms Study Area, Collier County





6 months. During the other months, the water table is below a depth of 18 inches, and can be as great as 40 inches during extended dry periods.

The surficial sands collected at Hogan Island Farms study area were analyzed for grain size distribution. The classification of sands after gradation analysis indicates wells HF1, HF3, and HF5 are predominately poorly graded sand with silt with a classification of SP-SM. Wells HF2, HF4, HF6, HF7 and HF8 are poorly graded sand and are classified as SP soils. Values for the coefficient of curvature (Cc) and the uniformity coefficient (Cu) are shown in **Table 5**.

Well Name		of Curvature c)	Uniformity Coefficient (Cu)			
	Minimum	Maximum	Minimum	Maximum		
HF1	0.16	1.09	1.7	17.4		
HF2	0.98	1.16	1.7	2.5		
HF3	0.36	1.22	1.8	19.4		
HF4	0.93	1.25	1.4	2.4		
HF5	0.39	1.48	1.7	16.5		
HF6	0.50	1.10	1.4	16.5		
HF7	0.45	1.11	1.6	10.9		
HF8	0.54	1.83	1.5	13.2		

# Table 5.Range of Coefficient of Curvature (Cc) and<br/>Uniformity Coefficient (Cu) for Hogan Island Farms

## 6.5 Core Analysis

All samples collected at this site were collected using the split spoon sampler. The sandy limestone at this site was not sufficiently consolidated to effectively use a core barrel. Therefore, no core analysis was performed at this site.

# 7.0 CITRUS PROJECT STUDY AREA

## 7.1 Site Description

The Citrus Project study area is located in central Lee County off Immokalee Road (SR82), approximately 1.4 miles east of Bell Road near Lehigh Acres and 15.5 miles southeast of I-75 (**Figure 28**). **Figure 28** also shows the geologic cross-sections A-A' and A'-B'. The Citrus Project study area is characterized by citrus groves and diked wetlands reservoirs that are part of the water management system. The wetland reservoirs are interconnected with canals that regulate water levels at many of the wetland sites.

Ten wells designated by WF1 through WF10 were drilled at this site. Wells WF8, WF9, and WF10 are considered "local" wells and are drilled to depths of 45 feet, 45 feet and 65-feet deep respectively. These monitor wells were installed to determine the regional extent of the water table influences on the wetlands. The remaining wells (WF1 through WF7) were drilled shallow to an average depth of 20 feet bls. These wells were constructed adjacent to wetlands to measure ground water levels directly influencing the surface water levels in the wetlands. **Table 6** provides a summary of the environmental setting and dominant wetland plant types for each wetland monitoring well site.

Well Name	Wetland Number	Environmental Setting and Dominant Wetland Plants		
WF1 2		Grassy marsh with saw grass ( <i>Cladium jamaicense</i> ), Alligator Flag ( <i>Thalia geniculata</i> L.)		
WF2 4 Grassy marsh with Torpedo grass (Panicum repe				
WF3 10		Pond with pond cypress ( <i>Taxodium ascendans</i> ), Spike rush ( <i>Eleocharis cellulosa Torr</i> )		
WF4	WF4 10 Marsh with Spike rush ( <i>Eleocharis cellulosa Torr</i> )			
WF5	8	Cypress head (Taxodium distichum)		
WF6	11	Cypress head (Taxodium distichum)		
WF7	12	Pine flatwoods near edge of wet prairie		
WF8	2	Upland adjacent to WF1 (no dominant vegetation type)		
WF9	WF9 4 Upland adjacent to WF2 (no dominant vegetation typ			
WF10 12 Pine flatwoods near edge of wet prairie				

Table 6. Environmental Setting and Dominate Wetland Plants

## 7.2 Well Construction

Wells WF8 and WF10 ("local") were drilled using the mud rotary method. They were completed to 45 feet bls (-12 feet NGVD) and 65 feet bls (-33 feet NGVD) respectively. WF8 was originally drilled to 85 feet bls and back filled with cement and completed to -35 feet NGVD. Well WF9, also considered a "local" well, was drilled using the hollow stem auger method and drilled to 45 bls (-12 feet NGVD). These wells are completed with a 10 feet screen in a combination of sand, shell and silt.

**Table 1** provides well construction specifications for wells drilled at the Citrus Project study area. Monitor wells WF1 through WF7 are completed to an average depth of 20 feet bls (approxi-

mately 10 feet NGVD) with 2-foot screens at the bottom of the well. With the exception of monitor well WF4, these wells are completed in fine sands. Monitor well WF4 is completed in a combination of sand, shell and silts. Each of these wells was drilled using the hollow stem auger method.

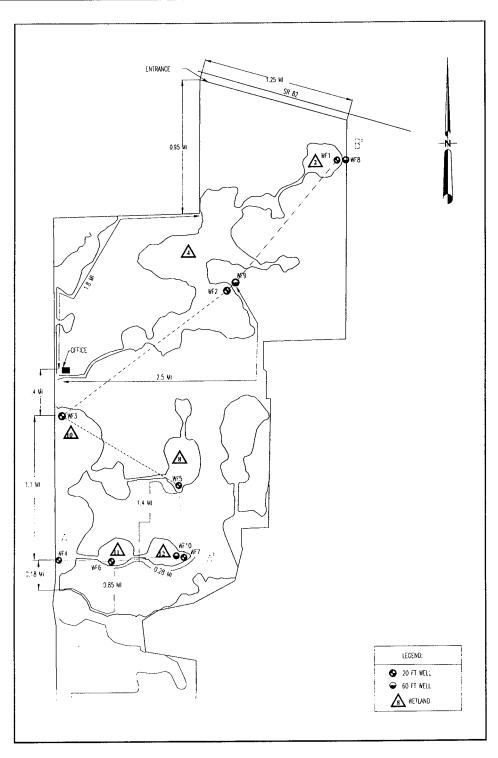
Boring logs for wells WF1 through WF10 are shown in Figures **29** through **37**. Penetration rates (blows/foot) were relativity consistent for wells WF1 through WF7. These wells were completed in sand except WF4. Well WF4 was completed in shell that contained sand, resulting in a 72 percent resistance (blows/foot) increase when this strata was encountered at approximately 17 feet bls (13 feet NGVD). In well WF8, where limestone was encountered at 33 feet bls the penetration rates increased 41 percent from 20 to 34 blow counts. In well WF9 penetration rates increased from 20 to 60 blows/foot when a layer of shell was encountered at approximately 16 feet bls (16.87 feet NGVD) and, again at 42 feet bls, where it increased 75 percent from 18 to 71 blows/foot. Well WF10 showed two occurrences where penetration rates increased due to the presence of shell and limestone. The first was at 20 feet bls (12.18 NGVD) and the second was at 42 feet bls (-9.82 NGVD). These increases were 69 and 92 percent respectfully.

## 7.3 Geology

**Figures 38** and **39** show the geologic cross-sections A – A' and A'-B. These cross-sections are based on cuttings descriptions of split-spoon samples collected during installation of wells drilled at the Citrus Project study area. Soil and geologic samples collected at this site indicate approximately a 25-foot layer of sand overlaying sand, shell and silt. A layer of organic matter several feet thick was present in wells WF5, WF3, WF2, and WF1 at a depth of 29 to 25 feet NGVD. Also observed at wells WF8 and WF6 is a lens of organic matter that is buried beneath several feet of sand at approximately 25 feet NGVD. At well WF4, a 2-foot layer of sandy clay was encountered at approximately 15 feet NGVD underlain by 5-feet of sand and 2-foot layer of shell at a depth of approximately 10 feet NGVD. Underlying the layer of sand and shell approximately 30 feet bls (-2 feet NGVD) is a layer of limestone (approximately 25 feet thick). This layer contains silts and shell fragments including sand. At well WF10 a 10-foot layer of lime mud was observed starting at approximately 33 feet bls (-5 NGVD). Below the layer of limestone is an another layer of limestone that grades more to a semi-consolidated limestone which contains shell and more fine-grained sand. A distinction was made due to the percentage increase of fine-grained sand observed in the cuttings.

## 7.4 Classification of Soils and Grain Size Distribution

**Figure 40** shows the soil survey map for the Citrus Project study area. In general, soils that occur at each wetland site are characteristic of the setting of the wetland. Soils collected from wells WF4 and WF7 are classified as Felda Fine Sand and are typically found in poorly drained depressions. Typically, the surface layer is fine sand about 4-inches thick and the subsurface layers extend to a depth approximately 3 feet. Under natural conditions, the soil is ponded for about 3 to 6 months or more. The water table is within a depth of 10 to 40 inches for the remaining 4 to 6 months. The permeability of Felda Fine Sand is rapid in the surface and subsurface layers and moderate or moderately rapid in the subsoil (USDA, 1984).



**Figure 28.** Location of Monitoring Wells on Citrus Project Study Area, Lee County, Showing Cross-Section A-A' and A'-B

Precision Drilling/Robert Mi GEOLOGIST/OFFICE	ict 3406 6442 BORING LOG BORING LOG BORING LOG LOCATION Citrus Project Iler Water Management District SIZE/TYPE OF BIT r 4.5" HSA IT./DIA. SCREEN: TYPESIotted MAT. F RFACE TOP OF WELL CASING TOP & B	SAMPLING METHOD START/FINISH DAT Split Spoon 6/30/98-6/30/9 VC LENGTH 2' DIA. 2" SLOT SIZE .01 OTTOM SCREEN DATE	8
(FT. ABOVE M.S.L.) REMARKS:	16.5/1	8.5 6/30/98	
Depth (ft) Type & Type	LOG OF TEST BORING FIELD DESCRIPTION	Penetration Resistance Log (Blows/Foot) Notes 0 15 35 55 75 100 5 1	Well Construction
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Sand (90%), organic matter (10%) Sand (95%), organic matter (5%) Sand, gray, fine grained Sand, gray to light gray fine grained Sand, white to clear, fine grained Sand, light gray, fine grained 16.0 Sand, light gray to gray, limestone, friable, cream (18.5 ft) Sand, sandy limestone, cream to white, soft to hard 20.0	Notés         0         15         36         55         75         100         8         3           P         0 <td< td=""><td></td></td<>	
	dium Sand Bentonite Pellets S	Fine sand w/ shell	

Figure 29. Boring Logs for WF1

Man 3301 West   (561)	<b>ag</b> Gun Palm 686	en Clu Be -88	orida M nent Di ub Road each, Flori 100 / Fax (	istric <sub>da</sub> 334	st 406 442					
BORING	WF	-2			BORING LO					
1163	/Isol	ate	d Wetland	is Drilli	ng Program - Phase II Citrus F	roject, Le	e County, F	lorida		
	sion	Dril	lling/Robe		r					
Kevin	Roł	rer		orida V	Vater Management District		SAMP	LING METHOD	START/FIL	NISH DATE
Drill R	lig/H	lolle	w Stem	Auger	4.5" HSA			Spoon		-6/23/98
VELL I	_			NG MAT 40 PV		MAT. PVC	LEN	GTH 2' DIA	. 2" SLOT	SIZE .010
ELEVA	TION		GROUI	ND SUR	FACE TOP OF WELL CASING	TOP & BOTT 17.5/19.5	TOM SCREEN		DATE 6/23/98	
REMAR		111.0	5.6./		· · · · · · · · · · · · · · · · · · ·	17.0/10/				
ŀ	Samı z		ation 16°	Unified Classification	LOG OF TEST BO	RING		Peneti Resist		0 Graphic Litho Log Well
Depth	Type & Recovery	Number	Panetration Resistance Blows/6" N-Value	Unified Classif	FIELD DESCRIPTION		Log Notes	(Blows) 0 15 35	/Foot) 55 75 10	O Graphic Litho Log Well
-		S1	7 15 11 8 26	SP	Sand (85%), organic matter (15%)			,		
-		\$2	6332 6	SP-PT	Sand (50%) organic matter (50%)	<u> </u>				
-5	X	S3	55910 14	SP	Sand, light brown to tan, fine					
-	X	S4 S5	15 12 15 15 27 6 10 9 15	-	Sand, tan, fine grained					
-10	X	<b>S</b> 6	19 8 10 10 10 20					<b>A</b>		
	Á	S7	10 18 8 9 26		Sand, tan-gray, fine grained			•		
-15	$\left  \right\rangle$	<b>S</b> 8	11 23 7 8 30		Sand, fine gray	17.0				EFE
-	X	S91	0 8 2 refuse 10	3	Sand, fine, white, sandy limestone, 18,5 ft limestone contact					
						19.5				
	Fine	San	d [	<u> </u> ; ; ; ; м	edium Sand 🙀 🏹 Bentonite Pellet	• X X	Cement Grout	s	lt/Clay w/ sha	 M
	] Orga	nic l	نيا   Material	•—••• [ Li	mestone		Fine sand w/ s	holl	luff/Backfill	

Figure 30. Boring Logs for WF2

Ma 330 Wes (561 BORI BORI PRO. 116 DRIL	Anage 1 Gun ( at Palm I 1) 686-8 ING/WELL WF-3 JECT NO. 33/Isolat LING CON	/NAME ed Wetlar	Distr orida 3 < 687-	ict 3406 6442 BORING LOG Iling Program - Phase II Citrus Pro	oject, Lee Co	unty, Florida		
GEOL Kevi	LOGIST/O in Rohre		lorida	ler Water Management District	·····	****		
Drill	Rig/Hol	low Stem	Auge	4.5" HSA		SAMPLING METHO Split Spoon		NISH DATE -6/23/98
YES	X N	Sch	ING MA	C/2" TYPE Slotted M/	AT. PVC	LENGTH 2' D	A 2" 61.0T	
	ATION OF	: GROU	JND SU	RFACE TOP OF WELL CASING TOP	& BOTTOM SO	CREEN	A. 2" SLOT DATE	SIZE .010
	ABOVE M ARKS:	.S.L.)		18/	/20		6/23/98	
					<u> </u>			
Depth (ft)	Ype & Type & Number Number	Penetration Resistance Blows/6* N-Value	Unified Classification	LOG OF TEST BORING	3		etration stance	Graphic Litho Log Well
Depi	Type & Recover Number	Pene Resi Blow N-V2	Class	FIELD DESCRIPTION	Log Note	(Blow 6 0 15 35	/s/Foot) 55 75 100	Graphic Litho Log Well
	S1	2689 14	SP	Sand (95%), organic matter (5%)			55 75 100	
-	.52	5552 10		Sand gray, fine grained		•		
5	S3	7777 14				•	•	
•	S4	4576 12	sc	Clayey sand, organic matter	6.0	1		¥
-10	S5	2333 6		Clayey sand (50%), gray, shell sand mix (50%)	10.0	•		
	S6	2234 5	SP	Sand (50%), shell fragment mix (50%)	10.0			с ()
	S7	5566 11		Sand, shell mix, fine grained white				, C (
- 15	S8	6867 14						
	S9	9978 16						
-20	510	10666		Sand, shell, white, limestone?	20.0			
	Fine Sand	<u></u>		dium Sand Bentonite Pellets	Cement G	out	t/Clay w/ shell	
	Organic Ma	sterial	L Lim	estone Clayey Sand	Fine sand	w/ shell	lff/Backfill	

Figure 31. Boring Logs for WF3

DRILLING CONTRACTOR/DF Precision Drilling/Robe	istrict da 3340 687-644 <u>Is Drilling</u> AILLER	06	ect, L <del>ee</del> Cou	unty, Fiorida	
DRILLING EQUIPMENT/MET Drill Rig/Hollow Stem / WELL INSTALLED? CASIF YES X NO C Sch.	HOD	2" TYPESIotted MA	T. PVC & BOTTOM S 22		START/FINISH DATE 6/23/98-6/23/98 2" SLOT SIZE .010 DATE 6/23/98
Depth (t1) Type & Number Number Penetration Blows/6" N.Value N.Value	Unified Classification	LOG OF TEST BORING FIELD DESCRIPTION	Lo <sub>1</sub> Note		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	SP S SC C SP S SP S SP S	Sand (60%), shell (40%), tan to cream Sand (50%), shell (50%), mixture, light	 6.0 14.0 18.0		
Fine Sand       State       Organic Material	Mediu	um Sand Bentonite Pellets	Cement	<u> </u>	t/Clay w/ shell

Figure 32. Boring Logs for WF4

Mar 3301 West (561) BORIN PROJI 1163 DRILL Preci GEOLO Kevin	Gun C Palm E 686-8 GWELL WF-5 ECT NO. <u>3/Isolat</u> ING CON <u>sion D</u> OGIST/O n Rohrd	/NAME ed Wetlan ITRACTOR/D rilling/Robe FFICE	)istri rida 33 687-6 <b>ds Dril</b> RILLER <b>ert Mill</b> lorida \	ct 406 442 BORING LOG Ing Program - Phase II Citrus Projec			NISH DATE
Drill	Rig/Ho	low Stem			Split S	Spoon 6/26/98	3-6/26/98
YES	INSTALI		NG MA			TH 2' DIA. 2"SLO	T SIZE .010
ELEV/	TION O	F: GROU	IND SUF	FACE TOP OF WELL CASING TOP & BOT	TOM SCREEN	DATE	
(FT. A	BOVEM	.S.L.)		18/20		6/26/98	·
				· · · · · · · · · · · · · · · · · · ·			
Depth (ft)	Type & Samble Number	Penetration Resistance Blows/8" N-Value	Unified Classification	LOG OF TEST BORING		Penetration Resistance	00 Graphic Litho Log Well Construction
Dep	Type & Recover Number	Pere Blow	C at I	FIELD DESCRIPTION	Log Notes C	(Blows/Foot) 15 35 55 7510	0 Graphic Litho Log Well Construc
	\$1 \$2	3444 8 6798 16	SP.PT	Sand, organic matter, fine grained Sand (20%), organic matter (80%),			
	S3	6787 15 4568 11	SM	fine silty Sand (50%) dark gray, organic matter (50%) <u>6.0</u> Sand, dark brown to gray fine silts			
	S5	6777 14 5555 10	4 55	Sand, brown to light gray, fine grained			
-	S7	4 4 7 6 11 6 6 8 8	-	Sand, light brown to tan, fine grained			
	X   59	14 4444 8		18.0			LARAK D-D-D-D-D-D-D-D-D-D-D-D-D-D-D-D-D-D-D-
		3332 6		Sand, tan, limestone fragments located at 20 feet 20.0			
	Fine San	d 🔛	M	adium Sand	Cement Grout	Silt/Clay w/ shejl	<del>.</del>
	Organic	Material		nestone Clayey Sand	Fine sand w/ shell	I Stored Sluff/Backfill	

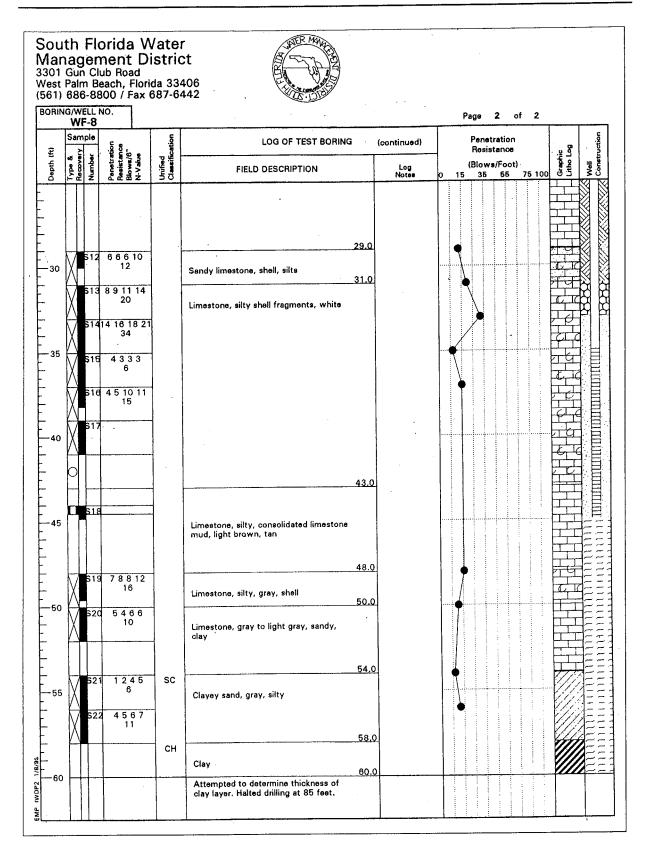
Figure 33. Boring Logs for WF5

Mar 3301 West (561) PROJE DRILL Preci GEOLO Kevir DRILL	Gun Cl Palm B 686-88 WF-6 CT NO./I S/Isolate Niso con DGIST/OF No Rohre NG EQUI	NAME ad Wetlan TRACTOR/E lling/Rob FICE	Distric rida 33 687-6 687-6 <b>nds Drill</b> ORILLER <b>ert Mill</b> THOD	ct 406 442 BORING LOG ing Program - Phase II LOCATION Citrus Projec	SAMPLING METHOD START/FINISH 0/ Split Spoon 6/16/98-6/16	
	INSTALL		ING MAT			
YES			1.40 PV		/C LENGTH 5' DIA. 2" SLOT SIZE . DTTOM SCREEN DATE	010
	BOVE M.		50H 30H	14/19	6/16/98	
REMA						
					·	
£	Type & Type & Number Number	Penetration Resistance Blows/6" N-Value	Unified Classification	LOG OF TEST BORING	Penetration Resistance Log (Blows/Foot) Notes 0 15 35 55 75 100 0	ruction
Depth (ft)	Type & Recover Number	V alt	assi	FIELD DESCRIPTION	Log (Blows/Foot) 통 율	Const
<u>ă</u>		<u> </u>	うび SP		Notes 0 15 35 55 75 100 0 5	S O
	S1	3458 9 4211	SP-PT	Sand (90%), fine grained, some organic matter		
	52	3	-	Sand (60%), fine grained, organic matter (40%)		
- 5	X 	4567		Sand, fine, silty (60%), organic matter (40%) 6,0		¥
-	\	11 5566 11	-	Sand, fine silty		
- 	∧ ▼ 56	7565		Sand, very fine silty		
-	/\ <b></b> S7	5655 11				THE.
- 15	S8	3324 5				
	\$9	6662 12	-	18.0		
-	510	55	SP	Sand (90%), limestone, shell, white <u>19.0</u> \10%}		
EMP 1 2 1/8/99						
äL	Fine San	۳ h		edium Sand Pr Pr Bentonite Pellets	Cernent Grout	
	Organic I			earum Sand	Fine sand w/ shell	

Figure 34. Boring Logs for WF6

Mai 3301 West (561) PROJ 116: DRILL PROJ DRILL PROJ DRILL DRILL DRILL DRILL DRILL DRILL VES	A Gun C Palm E 686-8 WG/WELL WF-8 ECT NO.1 3/Isolat ING CON ision Dr OGIST/O OGIST/O OGIST/O Rig/Mul INSTALL X NO	NAME ed Wetlan ITRACTOR/D illing/Robe FFICE IPMENT/MET IPMENT/MET d Rotary ED? CASI	Distri ida 33 687-6 87-6 <b>ds Dril</b> RiLLER RILLER <b>ort Mill</b> Orida V THOD NG MA .40 PV	Ct 406 442 BORING LOG Ing Program - Phase II Citrus Projec er Mater Management District SIZE/TYPE OF BIT 4.5" HSA T./DIA. SCREEN: T/PESlotted MAT. PVC	SAMI Split	PLING METHOD START/FINISH 1 Spoon 6/17/98-6/1 NGTH 10 DIA. 2" SLOT SIZE	8/98
	TION OF		ND SUF	FACE TOP OF WELL CASING TOP & BOT 35/45	TOM SCREEN	DATE 6/18/98	
REMA	RKS:					· · · · · · · · · · · · · · · · · · ·	
Depth (ft)	Zype & Type & Number	Penetration Resistance Blows/6" N-Value	Unified Classification	LOG OF TEST BORING	Log Notes	Penetration Resistance (Blows/Foot) 0 15 35 55 75 100 5	Litho Log Well Construction
10	S1 S2 S3 S4 S5 S6 S6 S7	2 2 4 3 6 4 3 6 6 9 6 4 5 5 9 4 3 3 5 6 3 4 5 6 9 7 7 7 7 14 5 5 5 7 10 4 4 refusal	SP SP SM	Sand, fill material from levee Sand, some organic matter, light brown 6.0 Sand, fine silty, gray 12.0 Sand, shell fragments, fine grained 14.0 Sand, silty, gray to light gray 16.0 Sand, gray, limestone, white, weathered, silty 18.0 Limestone, well cemented, micro-crystalline, shell fragments			
	Fine Sand	أننا			Cement Grout Fine sand w/ sh	Silt/Clay w/ shell	

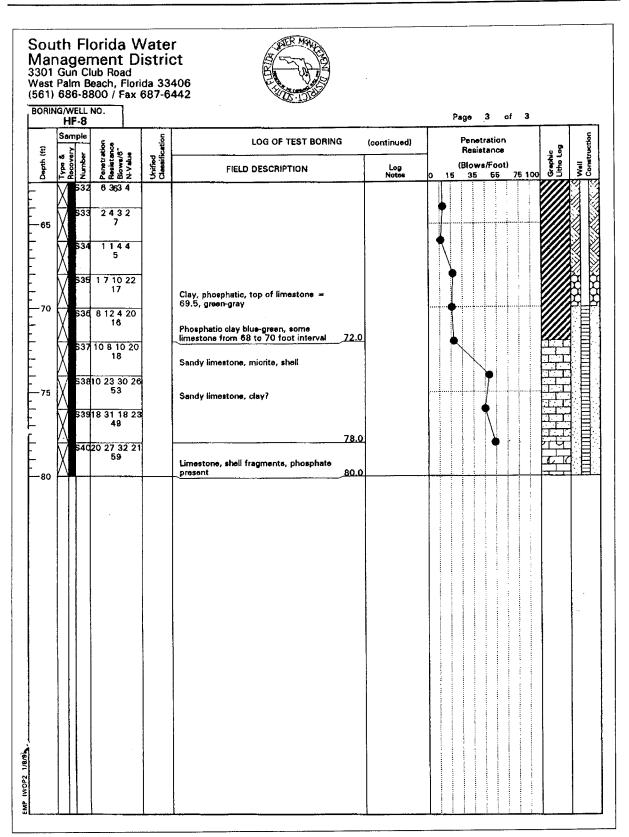
Figure 35. Boring Logs for WF8 (page 1 of 2)



**Figure 35.** Boring Logs for WF8 (page 2 of 2)

South Florida Wate Management Distri 3301 Gun Club Road West Palm Beach, Florida 33 (561) 686-8800 / Fax 687-6	ct 406	
BORING/WELL NO. WF-9 PROJECT NO./NAME 1163/Isolated Wetlands Dril	BORING LOG	t, Lee County, Florida
DRILLING CONTRACTOR/DRILLER Precision Drilling/Robert Mill GEOLOGIST/OFFICE	er	
Kevin Rohrer/South Florida V DRILLING EQUIPMENT/METHOD Drill Rig/Hollow Stem Auger	SIZE/TYPE OF BIT 4.5" HSA	SAMPLING METHOD START/FINISH DATE Split Spoon 6/18/98-6/19/98
WELL INSTALLED?     CASING MA       YES     NO     Sch.40 PV       ELEVATION OF:     GROUND SUF	FACE TOP OF WELL CASING TOP & BOT	TTOM SCREEN DATE
(FT. ABOVE M.S.L.) REMARKS:	35/45	6/19/98
Depth (It) Type & S Recovery Number ald we Penetration Resistance N Value V value Classification	LOG OF TEST BORING	Penetration         C <thc< th="">         C         <thc< th="">         C</thc<></thc<>
a 4.2 2 2 4.2 2 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	FIELD DESCRIPTION	Log (Blows/Foot) Notes 0 15 35 55 75 100 0 1 5 35 55 75 100 0 1 5 35 55 75 100 0 1 5 35 55 75 100 0 1 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5
S2 5588 13	Sand, yellow to light brown, fine grained	
9 5 54 5666 12	Sand, light brown to light gray, fine grained	
55 6 6 10 10 10 10 10 10 10 10 10 10 10		
57 4446 8	Sand, light gray to dark gray, fine grained 12.0 Sand, light gray, shell	
58 7 9 11 15 20	Sand (50%), shell fragments (50%)	
- 51030 33 refusa	Shell (60%), sand (40%), weathered limestone 19.0	
 	Limestone, bottom of interval is dolomitic, 20-22 ft is limestone, vugular with shell casts, tan to light brown	
512 11 2 2 2		
	adium Sand Article Bentonite Pellets Article Sand	Coment Grout

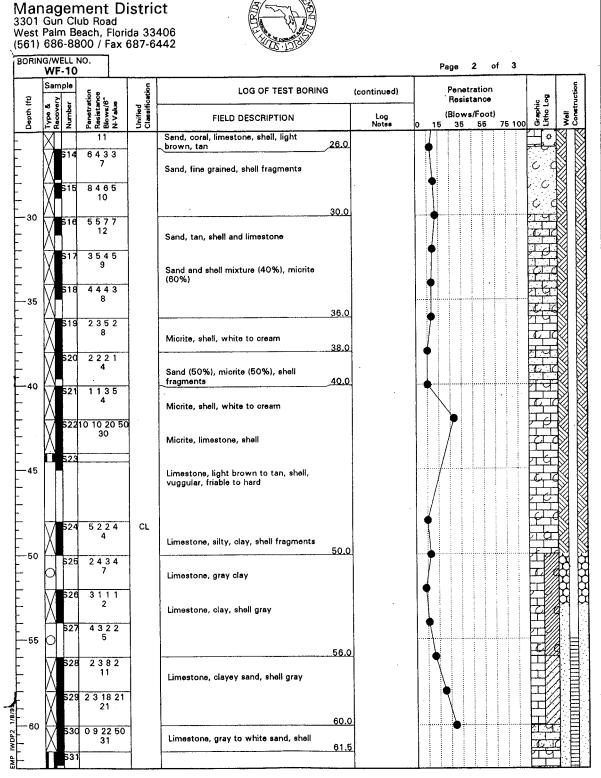
**Figure 36.** Boring Logs for WF9 (page 1 of 2)



**Figure 36.** Boring Logs for WF9 (page 2 of 2)

DRILLING CONTRACTOR/DF Precision Drilling/Robe GEOLOGIST/OFFICE Kevin Rohrer/South Flo DRILLING EQUIPMENT/MET Drill Rig/Mud Rotary WELL INSTALLED? CASIN	687-6	BORING LOG BORING LOG LOCATION LOCATION Cltrus Project, Cltrus Project, Cltrus Project, SIZE/TYPE OF BJT 4.5" HSA 1./DIA. SCREEN:	SAMP	LING METHOD ST	ART/FINISH DATE 25/98-6/25/98
	40 PV		C LEN	GTH 10' DIA. 2" DAT	
(FT. ABOVE M.S.L.) REMARKS:		55/65			5/98
Depth (ft) Type & Recovery Number Penetration Resistance N Value N Value	Unified Classification	LOG OF TEST BORING FIELD DESCRIPTION	Log	Penetration Resistance (Blows/Foot	aphic ho Log netruct
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	SM	Sand, white fine Sand, light brown, fine grained Sand, light brown to brown, fine grained, organic matter 8.0 Sand, dark brown to gray fine silts Sand, dark brown to gray, fine grained, silts Sand, brown to gray, fine grained, silts Sand, silts, brown to dark gray Sand, silts, brown to dark gray 19.3 Micrite, shell, white Sand, micrite, silty limestone mud	Notăs		

Figure 37. Boring Logs for WF10 (page 1 of 3)

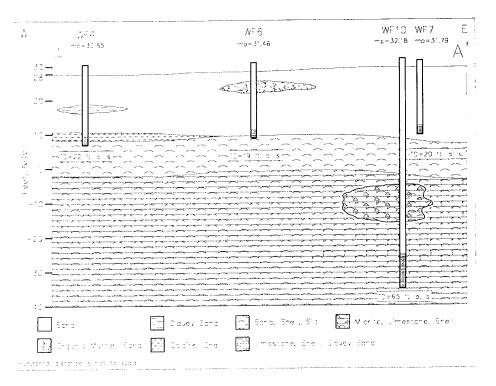


**Figure 37.** Boring Logs for WF10 (page 2 of 3)

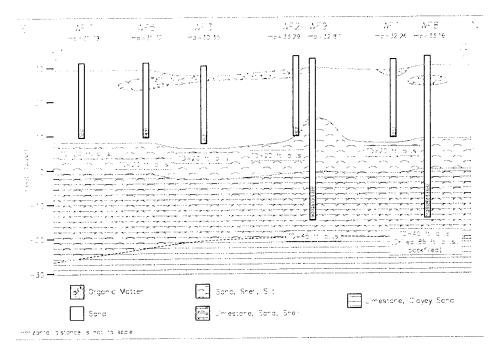
DRIN	W	VELL F-1C nple	NO.				······································	 	Page 3	of 3		
Depth (ft)	Type A		Penetration Resistance Blows/6" N-Value	Unified Classification			(continued)	-	Penetrati Resistan (Blows/Fo		Graphic Litho Log	Well Construction
å		Numbe	Penet Resist Blows N-V	30	FIELD DESCRIPTION		Log Notes	0 15			5 <u>5</u> 19	•
65					hard	35.0						
03												
												: 
												:
											ĺ	
											.	
												<b>`</b>
1												

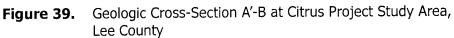
**Figure 37.** Boring Logs for WF10 (page 3 of 3)

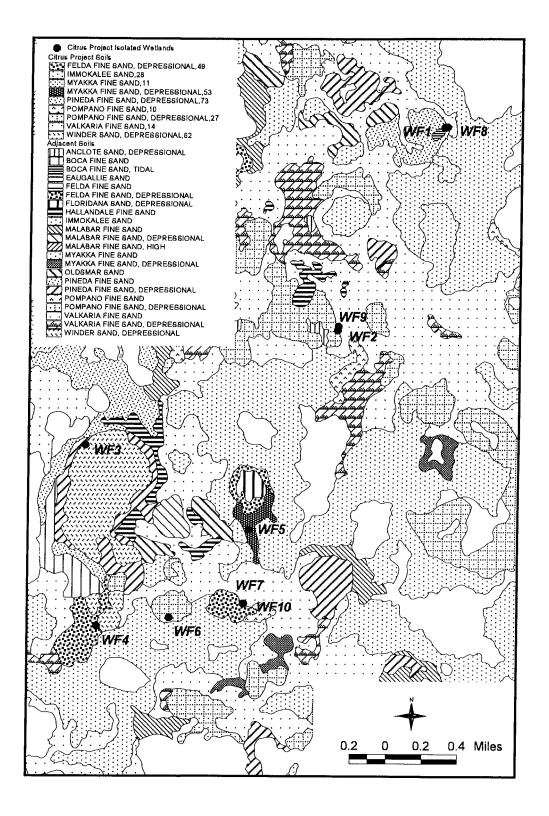
 $(1,1,1) \in \mathbb{R}^{n}$ 

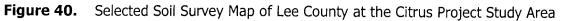


**Figure 38.** Geologic Cross-Section A-A' at Citrus Project Study Area, Lee County









73

Soils found at sites WF2 and WF6 are classified as Pompano Fine Sand. The surface layer is gray fine sand that is approximately 3-inches thick. The substratum is fine sand to a depth of 80 inches or more (USDA, 1984). Under most conditions, the water table is within 10 inches of the surface for about 3 months and up to 40 inches for more than five months. The available water capacity is low; however, the permeability is rapid (USDA, 1984).

At wells WF8 and WF9, Valkaria Fine Sand is the predominant surficial deposit at these locations. Typically, the surface layer is dark gray fine sand about 1-inch thick. The subsurface layer is about 4 inches of light gray sand. The sublayer is normally brown fine sand that extends to depths of 80 inches. Most of the time the water table is with 10 inches of the surface for about 6 months, and the soil is ponded for about 3 months. The water table is 10 to 40 inches below the surface most of the rest of the year. The available water capacity is very low and permeability is high (USDA, 1984).

At well WF3 the majority of the sand is classified as Winder Sand. This soil is found typically in depressions. The surface layer is dark gray sand about 3-inches thick. The subsoil extends to a depth of 29 inches. The upper 7 inches is gray sandy loam and the lower 6 inches is gray sand. The substratum extends to a depth of 80 inches or more. Under natural conditions, the water table is above the surface for 3 to 6 months. It is 10 to 40 inches below the surface during extended dry periods (USDA, 1984). The available water capacity is low in the surface and subsurface layers and medium in the subsoil. Permeability is rapid in the surface and subsurface layers and slow in the subsoil.

Soil at WF6 is classified as Myakka fine sand. The Myakka Fine Sand is a deep, moderately permeable soil formed in thick beds of marine sands. Typically, the water table is within 10 inches of the surface from 1 to 3 months and 10 to 40 inches below the surface for 3 to 6 months. Permeability is rapid in the surface and subsurface layers and moderate to moderately rapid in the subsoil (USDA, 1984).

Values for the coefficient of curvature (Cc) and the uniformity coefficient (Cu) are shown in **Table 7** for well WF1 through WF10. No analysis was performed at site WF7 since it is located immediately adjacent to deeper well WF10.

#### 7.5 Core Analysis

Wells WF4, WF8 and WF9 contained consolidated sediments that were cored and analyzed in the lab for hydraulic conductivity. **Table 8** lists the selected intervals that were analyzed and the results of this analysis.

Well Name		t of Curvature (Cc)	-	/ Coefficient Cu)
	Minimum	Maximum	Minimum	Maximum
WF1	0.94	1.18	1.5	4.3
WF2	0.85	1.14	1.7	2.3
WF3	0.46	1.25	1.7	5.7
WF4	0.18	1.16	1.16	17.4
WF5	0.87	1.13	1.7	1.9
WF6	0.33	1.17	1.6	12.9
WF7	No	analysis was	performed	at this site
WF8	0.69	1.15	1.6	15.4
WF9	0.33	1.08	1.6	20.0
WF10	0.63	1.16	1.6	12.9

# Table 7.Range for Coefficient of Curvature (Cc) and<br/>Uniformity Coefficient for Citrus Project Study Area

# Table 8.Values of Hydraulic Conductivity for selected Intervals at<br/>Citrus Project Study Area

Sample Number	Site Name	Top Depth of core interval (ft-bls)	Bottom Depth of core interval (ft-bls)	Horizontal Hydraulic Conductivity (K <sub>h</sub> ) ft/day	Vertical Hydraulic Conductivity (K <sub>v</sub> ) ft/day	Description of core
1	WF4	18.0	18.5	0.0046	0.0853	Limestone
6	WF8	21.5	22.1	0.0004	0.0066	Limestone
7	WF8	24.0	24.5	0.0002	0.0033	Limestone
11	WF9	21.0	21.5	0.0009	0.0164	Limestone

#### 8.0 CONCLUSIONS

This report provides a compilation and summary for the drilling and construction information collected during Phase 2 of the Isolated Wetlands Research Program. The 26 wetland monitor wells provide valuable geologic information to assist in the interpretation of wetland hydrology and the geologic characterization of different wetland settings. The monitor wells provide the infrastructure for the long-term hydrological monitoring for four isolated wetland study areas, which will help to determine seasonal water level variations and detection for potential impacts to isolated wetlands from adjacent ground water withdrawals.

Researchers will find this report useful when conducting investigations on the study wetlands and influences that ground water have on them. This report compiles hydrogeologic information collected for each of the study areas and addresses modeling data needs.

Unconsolidated samples collected during the drilling of the monitor wells were analyzed for grain size distribution (sieve analysis). Coefficient of curvature (Cc) values ranged from 0.23 to 1.14 at Flint Pen Strand study area. Stairstep study area the values ranged form 0.43 to 1.25. Hogan Island Farms ranged from 0.16 to 1.86, and at Citrus Project study area values for coefficient of curvature ranged from 0.18 to 1.25. The uniformity coefficient (Cu) ranged from 1.5 to 15.1 at Flint Pen Strand study area. At Stairstep the values for Cu ranged from 1.4 to 28.2. Hogan Island Farms Cu values ranged from 0.98 to 21.7and the Citrus Project study area Cu values ranged from 1.5 to 20.0.

Selective sections of the consolidated limestone were analyzed for vertical and horizontal hydraulic conductivity. Horizontal hydraulic conductivity values ranged from 0.002 to 20.671 and averaged 2.4875. Vertical hydraulic conductivity values ranged from 0.0033 to 390.101 with an average of 46.9443.

Rate of penetration was recorded for each of the wells. Geologic cross-sections were drawn for each of the study areas. Soil survey maps are presented to provide characterization of the soil in and adjacent to wetlands that may influence them.

### 9.0 RECOMMENDATIONS

Develop a maintenance program to ensure accurate water level measurements from wetland monitoring wells.

Install staff gauges near shallow (20-foot) wells to compare surface water elevations to ground water levels and provide back up for monitoring water level accuracy when surface water is at the same altitude as ground water.

Continue collecting monthly water level data to establish wetland base line conditions. Data recorders should be installed to provide more detailed water level data with greater temporal resolution. The ongoing water level monitoring will provide a long-term database to assist in the interpretation of hydrologic influences that impact the wetland in the study areas.

Calculate hydraulic conductivity from the sieve analysis data provided in this report. From the data provided, hydraulic conductivity can be calculated for 2-foot intervals for the entire depth of each monitor well. This would be helpful input data to a calibrated wetland model.

Develop a calibrated wetland model using MIKE SHE or similar model that can simulate interaction of surface and ground water for each of the study areas. The model should have the capability to estimate the vertical and horizontal movement of water. This model should also provide an evaluation of the controlling hydraulic conditions on other dependent variables.

Using data obtained during this investigation, develop wetland protection criteria for water use permitting.

#### REFERENCES

ASTM, 1980., American Society for Testing and Materials. Natural Building Stones; Soil and Rock. Annual Book of ASTM Standards, Part 19, Philadelphia, 634

ASAE, 1961., American Society of Agricultural Engineers., Measuring saturated Hydraulic Conductivity of Soils., Special Publication SP – SW-0262.

Core Laboratories, Inc., 2001 Commerce, Midland, Texas. Correspondence letter for vertical permeability analysis, December 1998.

Driscoll F.G., 1987. Groundwater and Wells. Second edition Johnson Division, St. Paul, Minnesota. 1089

Engineered Environmental Solutions, Inc., 1997. Isolated Wetlands Drilling Phase 1. Contract C-7665, South Florida Water Management District, West Palm Beach, Florida

Engineered Environmental Solutions, Inc., 1999. Isolated Wetlands Drilling Phase 2. Contract C-8665, South Florida Water Management District, West Palm Beach, Florida

SFWMD., 1996. Corkscrew Mitigation Bank. Technical Support Document. South Florida Water Management District, West Palm Beach, Florida

USDA., Soil Conservation Service (1998), Soil Survey of Collier County Area, Florida

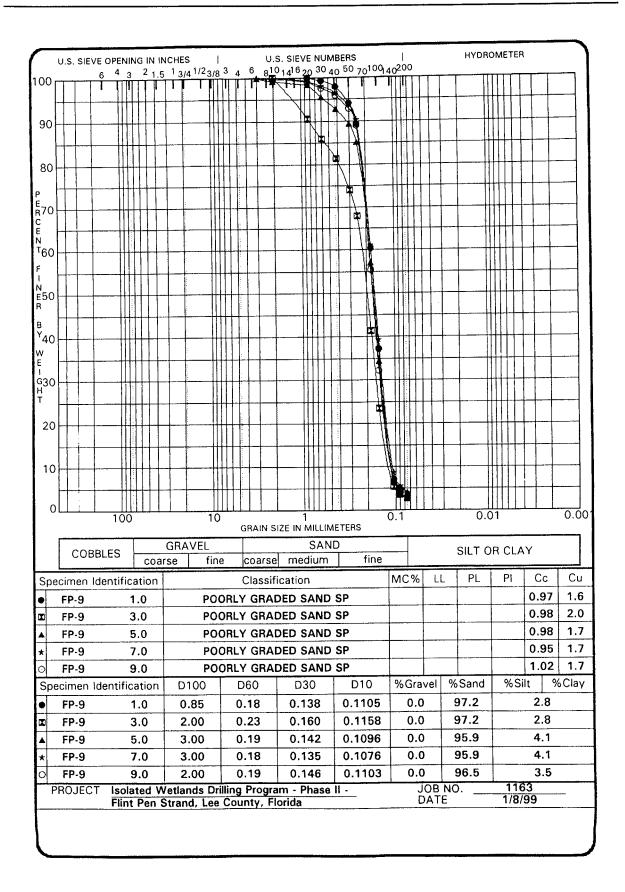
USDA., Soil Conservation Service (1984), Soil Survey of Lee County Area, Florida

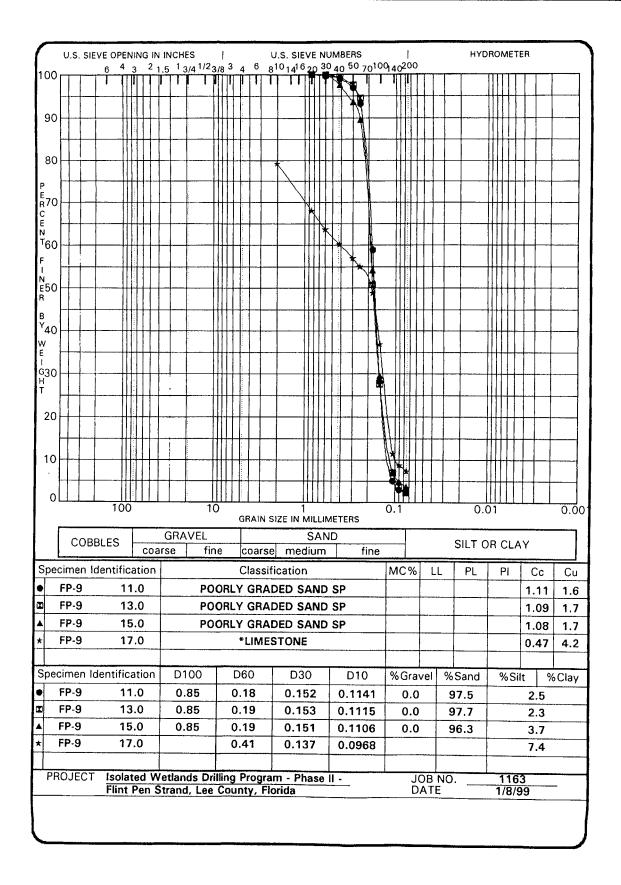
Watson and A. D. Burnett., 1993, Hydrology An Environmental Approach. Lewis Publishers, p. 61

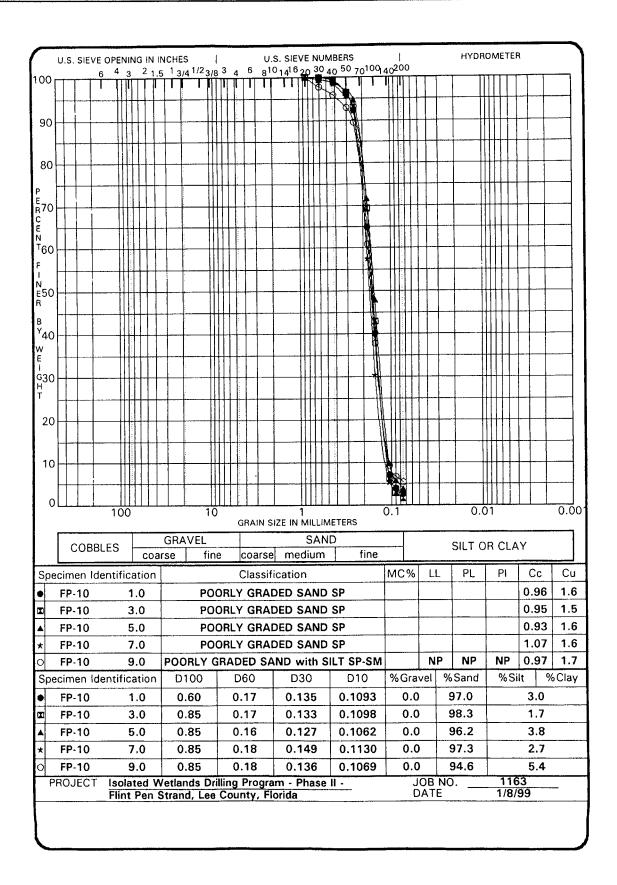
Holtz, R.D. and Kovacs W.D., 1981, An Introduction to Geotechnical Engineering. Prentice-Hall, Inc., Englewood Cliffs, N.J. p. 63.

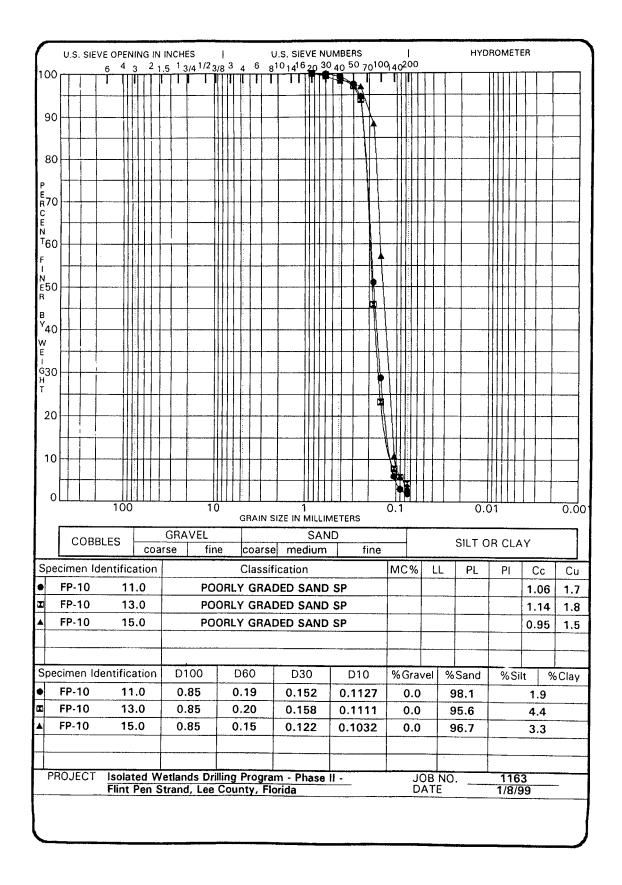
## **APPENDIX A**

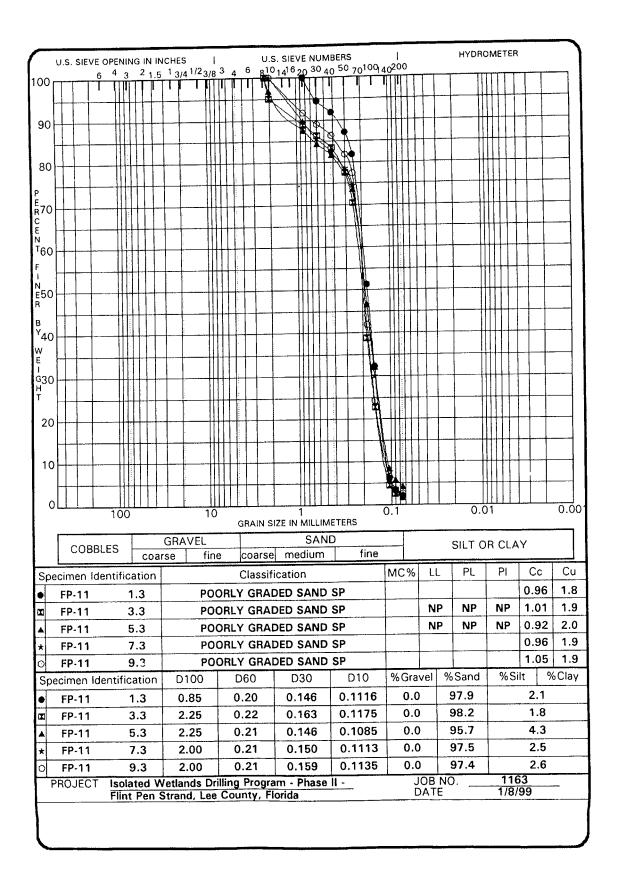
Flint Pen Strand Field Notes

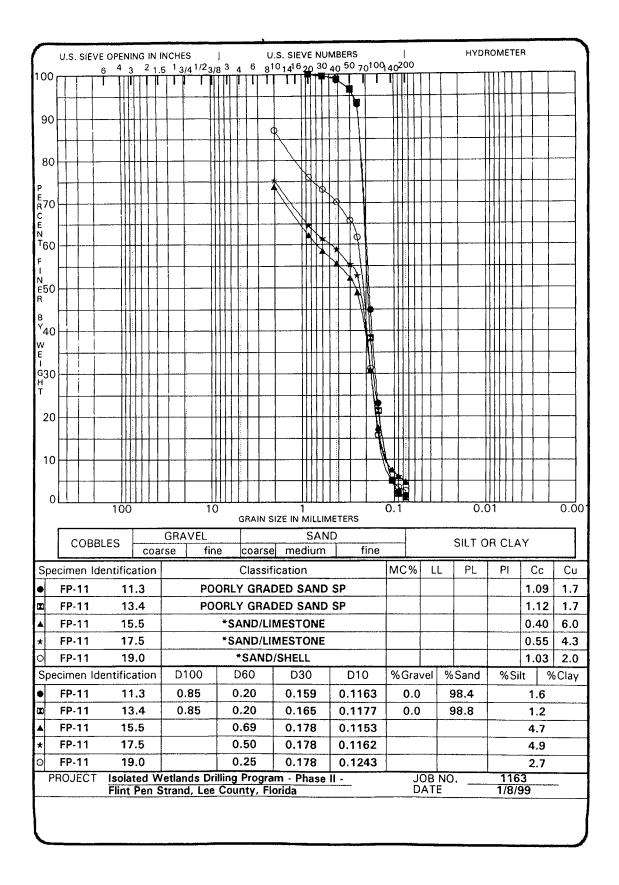


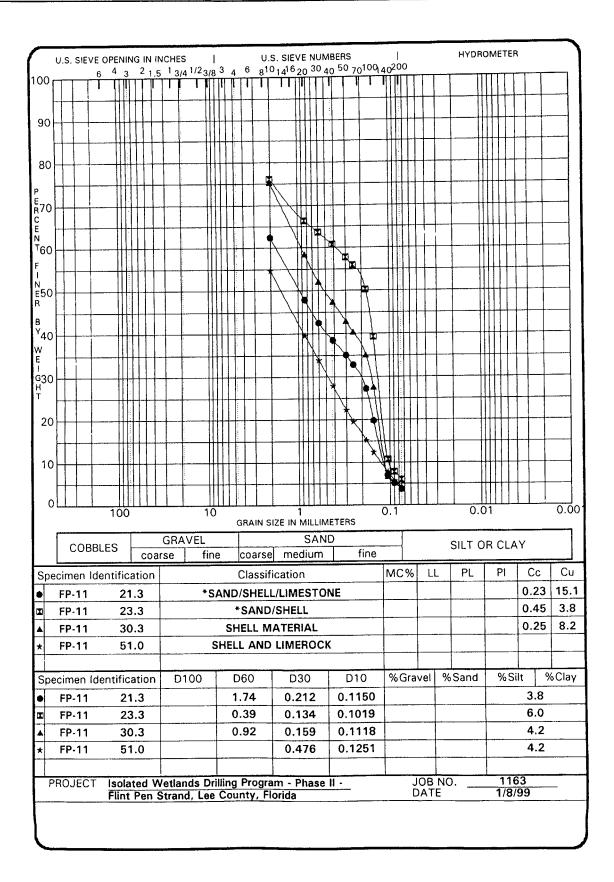








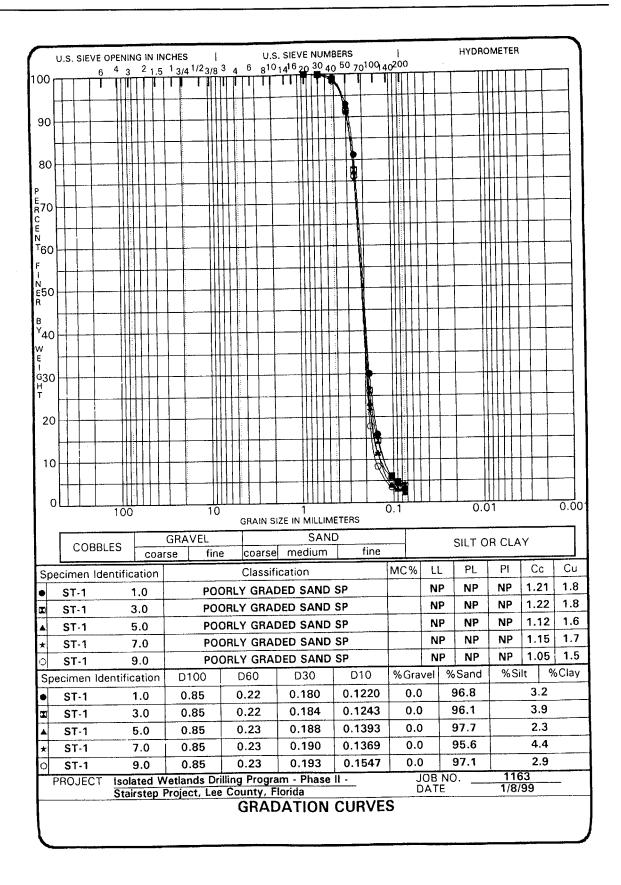


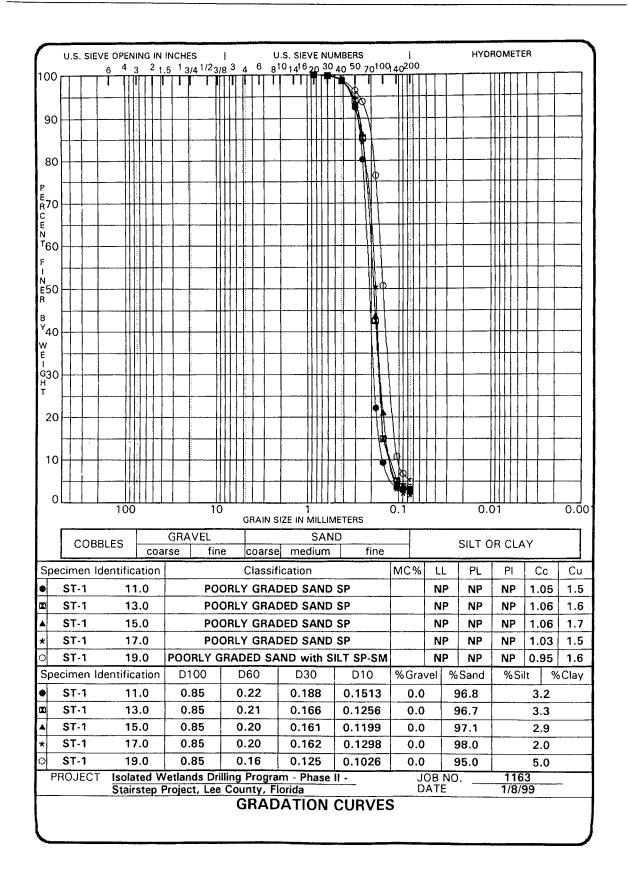


### **APPENDIX B**

**Stairstep Project Field Notes** 

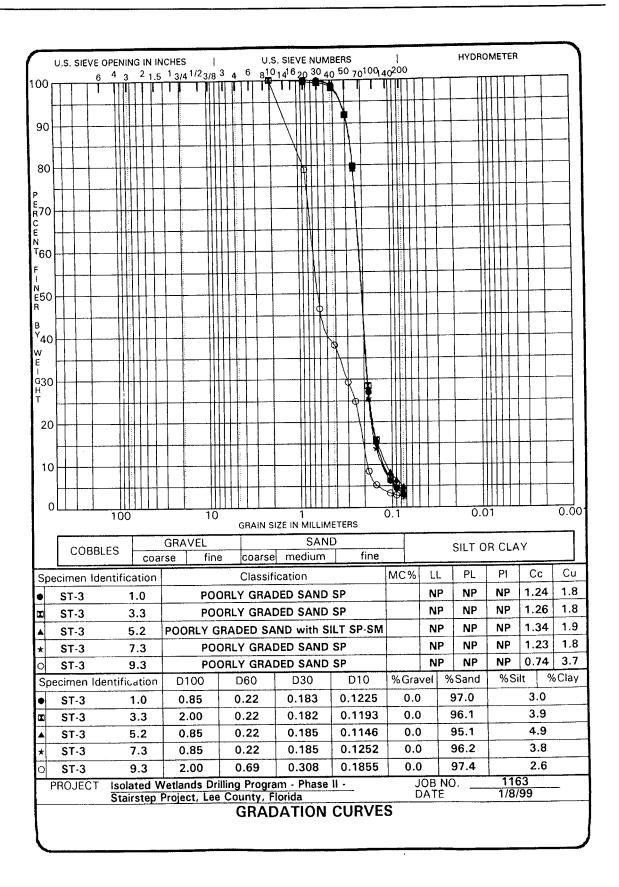


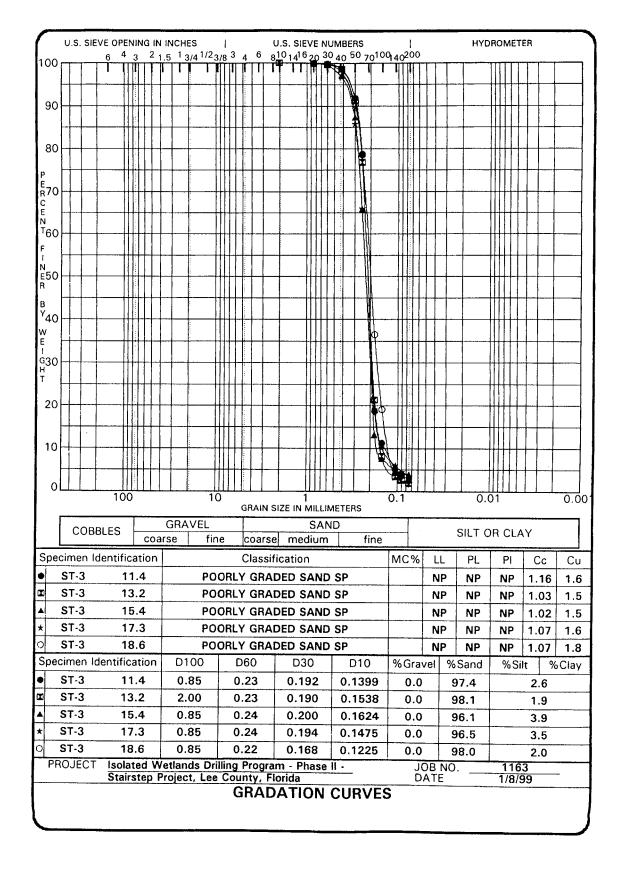


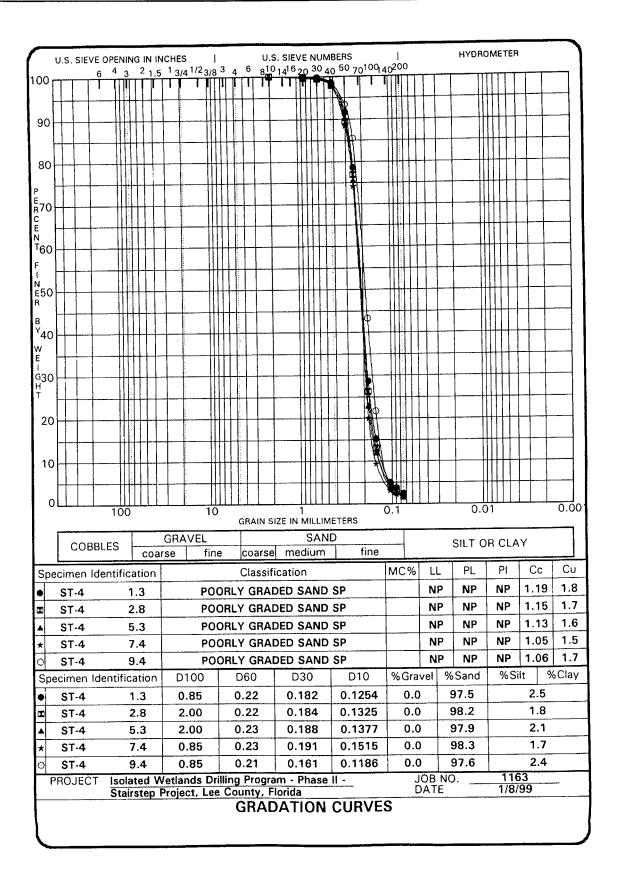


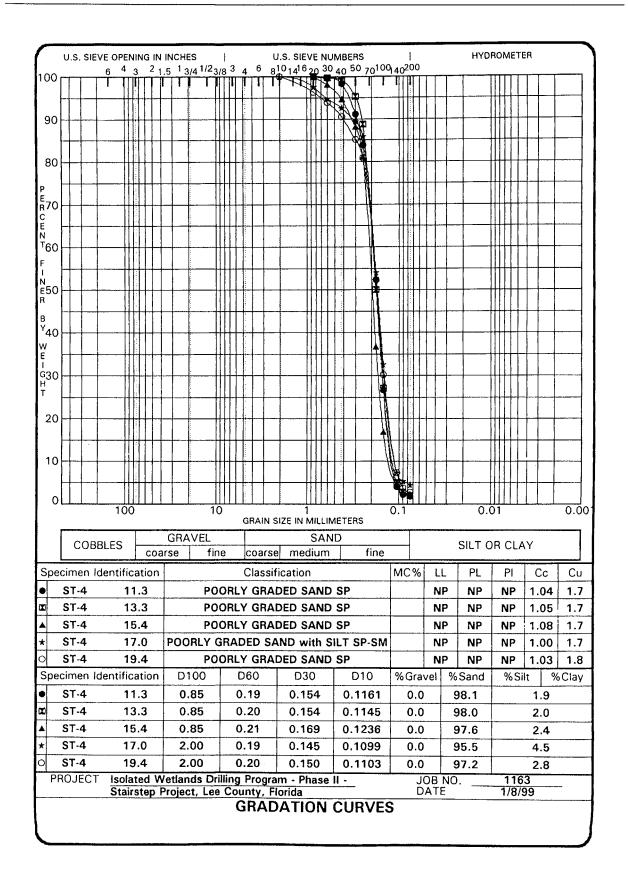
U	.s.	SI		OP	EN 1	IN	G I 2	IN	IN .5	СН 1	ES 20	5 4 1.	12 -		. 3		٨	6		ບ. ຄ1	.s 0	. s 12	518 11 6		сı О	NU 30	)   4	IBE	ER 50	s	20	10	94	10	 20	00						H١	D'	RC	)N	١E	TE	R						
0		r	Τ,		, П	3 	п		.5	Ť	3/	1	Ē	578 	Π	ΓÌ	4	Ť	T	۴	P	Ť	Ť	T	h	¥	ħ	Ĭ	Ţ	_	Ť	Т	Ť,	ΪŤ	T	Π	Τ	T			Γ			Π	Π		Τ	Γ	Τ					
			-			-	μ	_		_	-		_	4	+				+		┡			╢	╢	╉	P	Ą	H		╉			╫		╟	╉	╉	+		┢			H	H	t	+-	┢	╉				-	
																					L				Ц	1			ţ)	⊢	1			1		$\square$	+	4	_						H	╀	╆	╀	╋		-		-	
아		ſ				1																							Y	Ì						11																		
$\vdash$	-	┝	+-		╢	÷	H	-								t		┢	$^{+}$		t			Ħ	$\dagger$			1	1	T	1			T							Γ													
0	-		-				$\parallel$		_		ł				$\left  \right $	-		-	+		$\left  \right $			$\parallel$	┦	┝╋	╉	+	Ĵ	$\left  \right $	╉			╢		$\left  \right $		+	-		╀	-		╉	Ħ	t	╀	┢	+	-	1	-		
																Ļ			1-					4	4	Ц	╞	-	_	ļ	⊢			Щ		$\left  \right $	┢	+	_		-		_	₽	$\left  \right $	╀	╋	╀	+		+		-	
0																														ſ	'																							
0-	+	╞	+		Ħ		+				╞			Ħ	Ħ	t		t	╈		t			1	T	IT	1	1																			1							I
-	₋		_		╢		╀		-		+		-	₩	╂	+	+	+-	+		╉			╢	+	Н	╉	t	-		$\left  \right $			+	Ħ		╞┼	-†	-		╀			Ħ		t	t	t	1		1			
50 -					1									Ц	Ц				1		1				H	$\left  \right $	+	+	_		ļļ			+		-	H	-			╀			╢	+	+	╀	+	+		+		-	l
																ł																											_	11	$\downarrow$				$\downarrow$		4			
ļ	$^{+}$	t	+		₶	11	t	ſ						T	Π	T		Τ	T		T			T	Π	Π	T	I																										
50  -	+	+	+		+		╉	┝	$\vdash$	-				╫	$\parallel$	╉	+	+	╉		$^{+}$			╉	╟	$^{\dagger}$	$\uparrow$	-			t			+	$\dagger$	t	Ħ		-		t			Ħ	П	[†	T	T	T					
ļ	1.	-	_		#		+							$\parallel$	$\parallel$	+	-	+-	+	_	$\downarrow$			+	$\parallel$	Н	$\mathbb{H}$			╞				╀	╢	+	H	_			+			╢	+	H	+	+	+		+-			
10																									$\prod$		Ц			L	1				$\parallel$	1	Ц				+			$\parallel$	4	μ		$\downarrow$			+			ł
θľ	T	T			T		T				Ţ				Π			ſ																												$\ $								
ŀ	+	t	-+-		╢	ł	+	+	1	$\uparrow$	-			╢	+		$\dagger$	$\dagger$	+		$\dagger$			+	Ħ	Ħ				t	1			1	11	Ť	Π				T			T	T	Π	T	T	1		Γ	_		
30	-	+			$\parallel$	÷	+	+		+	-			╢	+	+		+	-		+			+	$\parallel$	+	$\left  \right $	+		$\vdash$	-	┞		+	$\parallel$	+	H		_	⊢	+			$\parallel$	+	H	╉	+	+		╀			۱
																								_	Ц						_	2				4	1				4			Ц	-	H	+	+	_		4.		-	ł
ſ	T	T															1																																					
20	+				╢		t	1	$\uparrow$	╞				Ħ	t	H		+	1		t			┥	tt	t	Π				•	ſŢ,					T							Π	T	Π								I
-	+		-			+		+	╞	+				+	+	H	╞	+	-		+			-	╢	╀	Н	-		┢	_	H	-	+	+	-	+		-	-	┽			+	+	H	+	-			+			1
10													_		ŀ		ļ				4				Ц	$\downarrow$				ļ		Ţ	Ŋ	_						-	_		_	4		Н	4	_			-			$\left\{ \right.$
'×																																	XII	V																			_	
Ì	+		+	-		Ì	Ħ	t	t	T					T	Π	1	T			1				Π	T				T			7	ξ,	Ć																			Ì
ΟL	1		_1	1		0		1	1	1				10	)	Ц	Ŀ	1		-	1			1	11	1						L		0.	. 1			l	L	J			Ö	.0	1							C	).(	อี
						Č									-		(	SR.	AI	N :	SI	ZE	E 11	11	MI	LL	IN	1E	ΓE	RS	5					_													_					г
ſ				BLES	2				(	GF	٩۶	V	EL													A		D													s	١L	т	0	R	C	Ľ	A.	Y					
				1	_			20	ar	se			1	fin	e	_		СС	ba	rs	e		m	e	diu	าม	n				f	in	е			1				_	-		_			-		- 1	_				=	7
pec	ni	ner	n Io	lent	ifi	Câ	ti	or	۱								(	CI.	as	si	fi	ca	ati	01	n									Ν	10	29	%		Ll			٢	L	_		Ρ	21			Сс	:		Cı	u
	รา	-2				1	.2						Ρ	0	0	RI	LY	′ (	GF	٩A		DE	D	S	A	N	D	S	Ρ										N	Ρ		N	Ρ			N	Ρ		1	.1	3	Ľ	1.	7
		2				3	.0						Ρ	0	0	RI	LY	' (	GF	۲A		DE	D	S	A	N	D	S	Ρ										N	Ρ		N	Ρ			N	Ρ		1	.2	2		1.3	8
		2				5	.0		1				P	0	0	R	LY	1	GF	٦A		)E	D	S	A	N	D	S	P		_								N	P	Ι	N	P			N	Ρ		1	.2	5		1.	٤
		-2					.4		-						-					٦A										-				T					N	Ρ	T	N	P			N	Ρ		0	.9	9	Γ	1.	Ę
		2					.4	-	╉							_			_	RA	_				_			_						t				1	N	P	1	N	P			N	Ρ		1	.0	4	ſ	1.	Ę
				len	rifi	_			$\frac{1}{2}$		D	10		ř	Ť	_	_	6			T		_	-	30		-	T			1(	5		9	%	G	ra	Ve	_		65	Sa		ī	-		68	_		Т	_	6 C	la	
1.									+						┢				3		+				8			+				 34	1	+-	-				-			в.			-					2.0	0			
		1.2					.2		-			8. 0			+			-			+			_	8			+			_	56	~ ~~	+		_		_	_			6.		-	$\vdash$					3.4	~~~			
		r-2	-			-	.0		-+			.8			╀				3		+				_			+						╀						_					-					4.				-
		r-2					.0		4			.8			╀				3		+				8	-		+		_		23		╀		_	0.0				_	5.			┢					2.				
		۲-2					.4					.8			1				25						20			-				64		+			).(					7.			┞						_			
		r-2					.4					.0		-		<del></del>			23						9			Ļ			5	14	4		_	0	).(		P			7.	9		1		11	6		2.	1			
PF	10	JE	ĊŤ	는 i c	50	la ir	te	d	W	et	la	nd ct	S		'iii A		g	P	ro tv	gr	FI	m	i -	۲ اء	'n	as	ie	11	-								0	)A	VT B	N' E	υ.				-	1	/8	3/9	<u>.</u> 99	)				
					o Ld		้อเ	e۲		10	1 <sub>c</sub>	ωι	, <b>L</b>		<u> </u>	-									C	)  \	J	6	<u>)</u>	JI	R	V	Ē	S																				-
																	•		.,	-11	~		•		~		-	~		-	•	-	· • •	~																				

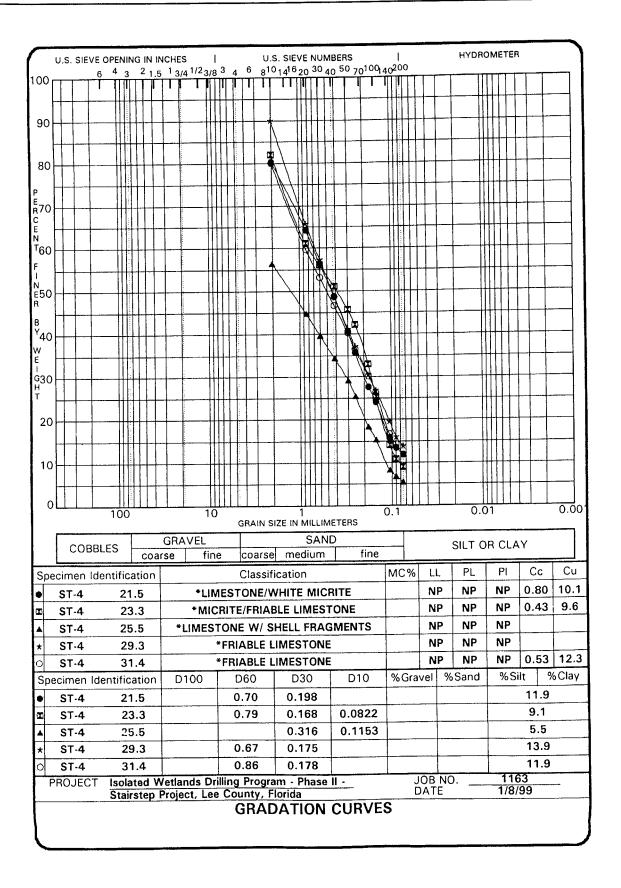
	U.S. 9		Е ОРЕ 6 4	NI 3					ES 3/4	1/2	3/	 8 3	3	1	6			5. S									01	ით	4(	,2'	00	}				Р	IYC	R	2M	IET	Er	١				
00			ŤΤ	ПĮ	Π	Π	Ň	Ť	I	Т	Ĭ	ĪП	Π	Π	Т	Ť	Ť	Ţ	7	ħ		Ţ	Ķ	Ĭ	T	Í	ľ-	T	T	Ī	$\prod$		Τ	T				Π	Π	Π				Γ		٦
						H			ŀ		╢	ft					╋		<u> </u>	Ì	H	Ĩ	2	Á	ſ		-		1				-					Ħ	IT	Π		-		T		
90	╽┼┼╌╆					$\vdash$			-		╢	$\parallel$	$\left  \cdot \right $	-			+			╟	$\left  \right $	Ŧ	÷)	Ļ		Ø			-+	+	Η	$\left  \cdot \right $	+		_			╢		Η	-			+		-
					ļ.				-		╢	Ц	$\parallel$				+			#	$\left  \right $	+		1		Ţ	-		+			$\left  \cdot \right $	+					#	╟	$\left  \right $	+	-				_
80																			_						¥.	7						Ц												1_		_
00									ŀ																N								Ì													
				IT.	Π	T					1	Ħ	11				T			I	T	T			Π	T	R					Π						Π		Π				Γ		٦
70	ѷ┠┼┼┼	-		II.	╟	$\vdash$			Ē		╢	Ħ			_		+			╫	┢╋	┢		┢	†	Ï	T	1	1		I		╈	-				Ħ	Ħ	П	1			t		٦
				╢	$\left  \right $	-	-		-		╢	╢	$\left  \cdot \right $				+			╫	╂╋	+-	$\frac{1}{2}$	-	╉	╢	Å	$\left  \right $	┥	H	$\parallel$	$\left  \right $	+	+				╢	╟	H	-	•		┢		-
60	┝┼╾┼								-		╢	╢	┼┥	-			+			╟	╢	╞		-	╋	$\frac{1}{1}$	╢	<u>ф</u>	+	$\left  \right $		$\left  \cdot \right $	+	+				╢	╟	┢┥	-			┢		-
											$\parallel$						$\downarrow$				Ш	1		-	╞	_1		1	_					_				#			_					_
1 50																																		_				1	1							
50											$\ $	$\ $																																		
l ,				ţĽ.	IT	П					1	Ħ	T		•		t			IT		T		l	T				1									$\parallel$		Π	1			Γ		-
40 ,	' <b> </b>			$\parallel$	╟	$\left  \right $			ŀ		╢	╢	┼┤				╈			╟	╢	╉	ł	┢	+		f	¶†	┥			$\parallel$	╉					╢	╟	Ħ	-	-		+		-
/	$\left  \right $			₩	╟	-			-		╢	╢	$\left  \right $	-			╉		••••	╟	╢	╀	┢	╞	+		$\ $	╢╢		$\parallel$		H	+	+				╢	╟	H	+	-		+		┥
30	) -	_							-		#	$\parallel$			-		4								+		Щ	ľ	$\left  \right $				4					#	Ц.		_			╞		_
									_														L				•																			
20																									1			11																		
20					Π				1			Π	Π		-		T		-	IT	Ħ	T		ſ	T			T	d			Π	T	1	_			T		Π				Γ		1
						Π			1		╢	$\parallel$	$ \uparrow$				$\dagger$				╟	╀		ŀ	t			μI					╈	╈				Ħ		$\left  \right $	-	+		┢		-
10	╵┟┼┼┼			╫	$\left  \right $	$\left  \cdot \right $					╫	╢	Η	-	_		+		_		$\left  \right $	┢		$\vdash$	╎			$\frac{1}{2}$	₩	ł	+		+	+	$\neg$			╢	+-	┝┥	+	-		┢		-
				#	$\left  \right $	Н	_		-	• • • •	#	╢	$\left  \right $				╀					+	-		╇		-		Y				+	+				#	-		-			_		-
0			10																	Щ			Ĺ						 D.	Îř 1							0.						, <b></b>		0.0	Ĭ
			10	,									(	GR	AI	N S	SIZ	εI	N	I MI	LL	.IN	1E	ТΕ	R	3			J.	1							<u>.</u>	<u> </u>							0.0	-
	c	DBBI	.ES	-					۱V								.T-					N	D			-	_								S	IL.	гс	)F		CL.	Α١	ŕ				
	<u> </u>						irs	e		1	ine	) 		-	-	rse		-	neo		un	n	1		_	Ť	n					T			-	_		T			T	_				7
pe T	cimer					n.	-									sit		•••••				_	_	_				-	M		%	2		.L	+	P		+	P		_		C	+	<u> </u>	
	ST-2			1			+																									+			+	N		╀	N		-+-		11		1.	
-	ST-2 ST-2			13 15												AS	•••••						-									+			+	N		+	N		+		02	-+-	1.	
	ST-2			17			┢										_											-				+			-	N	_	+	N		-+-		09		1.	-
-	ST-2			9			P	იი	DRI										•						¢.	ρ.	<u>c</u> ,	4				+			+	N		╀	N N		-		97 02		1. 1.	
<u> </u>	cimer					n	-		10		Ť		_	60	-				<u>7</u> 3	_	_	3	• •		-	10		41	%	50	ìre	 av	el	-	<u> </u> %S	ian		+	_	۳ 65		-		_	Cla	_
	ST-2			1.			$\vdash$		.8!		+		0				-		.1				$\vdash$			30					).(					6.0		+					.0			- 1
	ST-2			13		•••••	+-	•	.8!	-	+		0.	• ••			┢		.1			_			_	2		-+			).(			÷		3.0		+					.0 .0			-
	ST-2			5			1		.00		+		0.	_			┢		.1					_	_	-		-			).(			÷		5.0		+				••••	.0			
	ST-2	<u>)</u>		7			t		.00		+		0.				1		.1				<b></b>			05		-			).(			-		7.0		$\uparrow$			-		.0			
	ST-2	2	1	9.	0		T	2	.0(	)	1		0.	1	5		1	0	.1	1	7	-	<u> </u>			90		+		C	).(	0				5.5		$\uparrow$					.5			
P	ROJE	СТ	Iso	at	ed	V	) let	lar	nds	D	ril	lin	g	Pr	00	gra	m	•	P	ha	IS	e	11	-								JC	B	N	0.	-			1	1	63	-		_	_	-
			Sta	Irs	te	p I	rr	ojei	ct,	Le	ee									$\overline{\mathbf{n}}$	N		<u> </u>		10	>>	/Г					<i>ا</i> ر	١T	E					1/	8	9	9				
													U	n		۹L	-	1		J	IN		J	U	<b>٦</b>	• •		:3	,																	

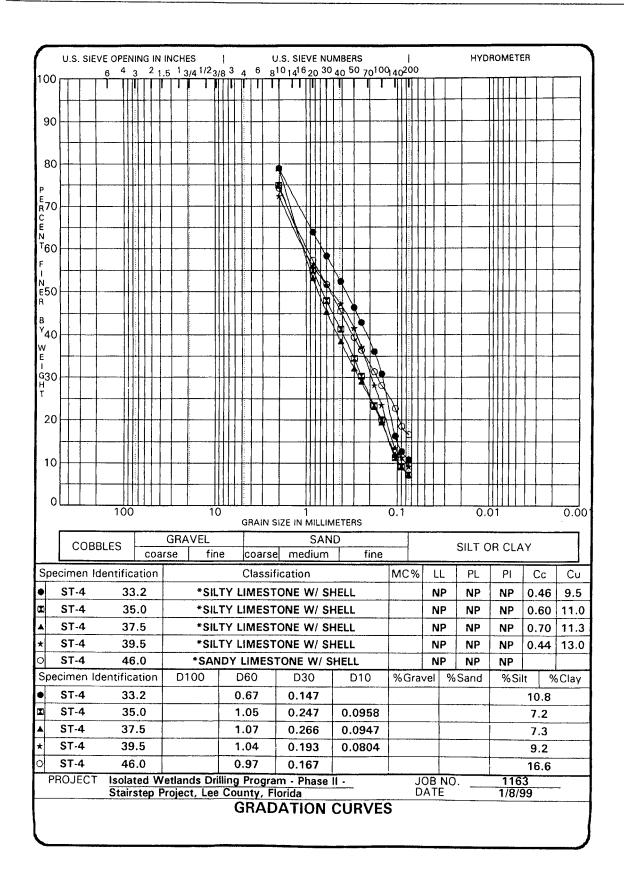


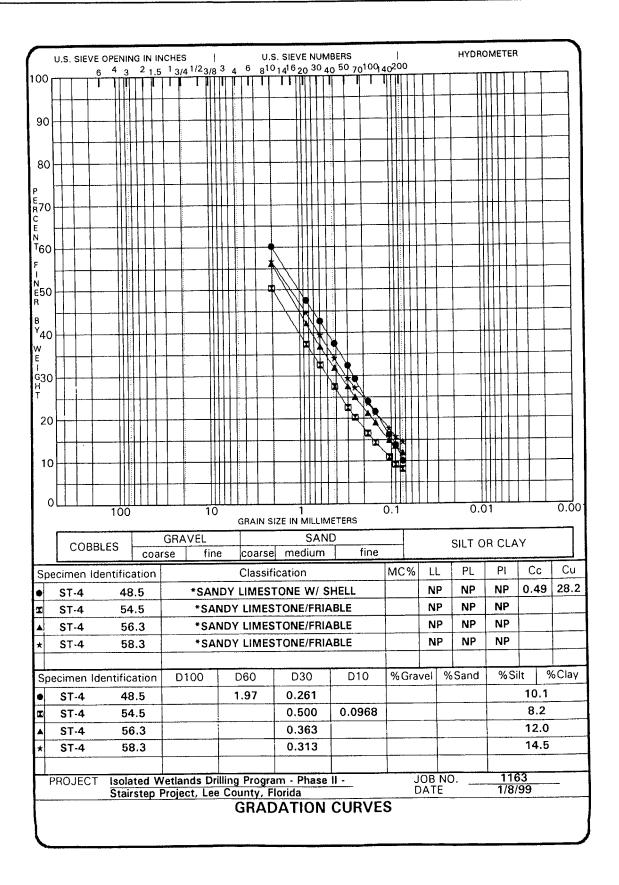










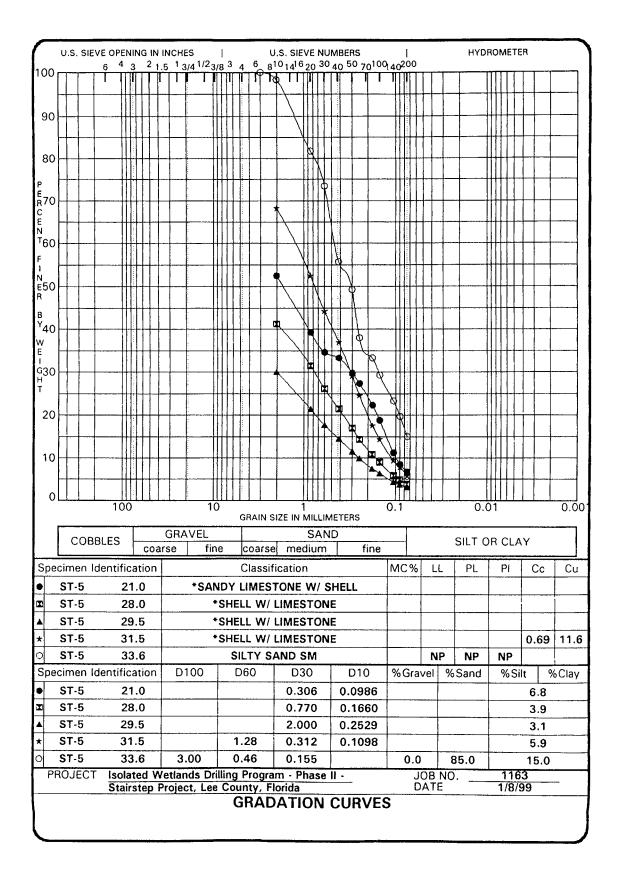


																		5100 1												
																												Ļ	_	
																						-	-				$ \uparrow $			
										+	<u> </u>	1			╢		<b> </b>	-		111	++	-+-			Щ		1 J.	1	1	
									$\parallel$	+-	+			Ш				11 11	- 11	11		1			11		+	+	+-	
							╢╢			1					++	+-	$\vdash$				+			-	┝┼┼	$\left  \right $	┝╌╄	+		
			$\left  \right $								-		$\rightarrow$		$\downarrow\downarrow$	+					+	-					$\square$	+	_+-	
			1 1				Ш															_			Ш					
													ĺ			-														
						•		Π							Π						T									
			$\uparrow$		+		┼┼	Η		+		$\uparrow$	-			1	$\square$					-		-#	Ì		H	-+	+	
		++	┼┼		-		+++	+			┼─	+	-+	H	╁┼	+					++	- -		-			H		-	$\neg$
	$\frac{11}{100}$									1				Ш				Ĺ	<u> [</u> 0.1	<b>F</b>			(	$\frac{1}{20}$	Ш	Ш				0.0
									G	RA	IN S	SIZE	INN	11.L	.IMI	ETER	RS													
OBBLE	S			· · · · ·	۱ <u>A</u>				_			1				)				-			SILT	OF	R (	CL	`A.			
				rse		ti	ine		-						n		ti	ine			<u> </u>						<del></del>		_	<u> </u>
				-															M	C %	+			-			_		· · ·	Cu
																					+			-+			-			1.7
				-				-	_												+						-+-			1.7
				10	01			-									58-	SM			- · ·		· · · · ·							1.7
																					1						-+-		-+-	1.7
				r	710									-		-	710	,	%	Gra	<u>.</u>			_						1.6 Clay
			_									ſ			+							+		-+-				.		
		~		+			+						·· ··		-+	·· · - ·						+		-+-						
5		~		<u> </u>			+					+			-†							+								
5							+	_				÷—			+							+		+						
- 5				L			+					+			-							+		-+						
CT I	sola	ted	W	/etla	anc	ds D	rill	in	g F	Pro	gra	âm -	PI		e l			1		J	OB	NC		I		11	63	3		
S	stair	ste	рF	Proj	ect	t, Le	ee (							<u> </u>		<u>.</u>	~	150	<u>.</u>		DAT	E			1	/8	/9	9		
	DBBLE Iden	DBBLES	1 Identification 1.0 3.0 5.0 7.0 9.0 1 Identification 1.0 3.0 5.0 7.0 9.0 7.0 9.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7	OBBLES         coal           1 Identification         1.0           3.0         5.0           7.0         9.0           1 Identification         1.0           3.0         5.0           7.0         9.0           1 Identification         1.0           3.0         5.0           7.0         9.0           7.0         9.0           7.0         9.0           CT Isolated W         1.0	GF           coarse           coarse           1.0           3.0           5.0           7.0           9.0           1 Identification           1.0           3.0           5.0           9.0           1 Identification           1.0           3.0           5.0           7.0           9.0           7.0           9.0           7.0           9.0           7.0           9.0           7.0           9.0           7.0           9.0           CT Isolated Weth	GRA           coarse           1 Identification           1.0           3.0           5.0           9.0           1 Identification           7.0           9.0           1 Identification           7.0           9.0           1 Identification           5.0           9.0           1.0           3.0           5.0           0.1           3.0           0.1           3.0           0.1           3.0           0.1           3.0           0.1           3.0           0.1           3.0           0.1           3.0           0.1           3.0           0.1           3.0           0.1           3.0           0.1           3.0           0.1           3.0           0.1           3.0           0.1           3.0           0.1           3.0           0.1	GRAVEL           coarse         f           coarse         f           1.0         P           3.0         P           5.0         POORLY           7.0         P           9.0         P           1.0         0.85           3.0         0.85           5.0         0.85           7.0         0.85           7.0         0.85           7.0         0.85           7.0         0.85           7.0         0.85           9.0         0.85           7.0         0.85           7.0         0.85           7.0         0.85           7.0         0.85	GRAVEL           coarse         fine           1.0         POO           3.0         POO           5.0         POORLY GI           7.0         POO           9.0         POO           1.0         0.85           3.0         0.85           5.0         0.85           9.0         0.85           7.0         0.85           7.0         0.85           7.0         0.85           7.0         0.85           9.0         0.85           7.0         0.85           7.0         0.85           7.0         0.85           7.0         0.85           7.0         0.85           7.0         0.85	GRAVEL           coarse         fine           1.0         POOR           3.0         POOR           5.0         POORLY GRA           7.0         POOR           9.0         POOR           1.0         0.85           3.0         0.85           5.0         0.85           9.0         0.85           7.0         0.85           7.0         0.85           7.0         0.85           7.0         0.85           9.0         0.85           7.0         0.85           7.0         0.85           7.0         0.85           7.0         0.85           7.0         0.85           7.0         0.85	GRAVEL       Coarse     fine       coarse     fine       1.0     POORLY       3.0     POORLY       3.0     POORLY       5.0     POORLY GRAD       7.0     POORLY       9.0     POORLY       1.0     0.85       0.0     0.85       0.0     0.85       0.0     0.85       0.0     0.85       0.0     0.85       0.0     0.85       0.0     0.85       0.0     0.85       0.0     0.85       0.0     0.85       0.0     0.85       0.0     0.85       0.0     0.85       0.0     0.85       0.0     0.85	GRAVEL       Coarse     fine     coarse       1.0     POORLY G       3.0     POORLY G       5.0     POORLY GRADED       7.0     POORLY G       9.0     POORLY G       1.0     0.85       0.85     0.22       3.0     0.85       0.85     0.22       7.0     0.85       0.85     0.21       7.0     0.85       0.85     0.19       CT     Isolated Wetlands Drilling Project, Lee County	GRAIN S       GRAVEL     Coarse     fine     coarse       1.0     POORLY GRA     3.0     POORLY GRA       3.0     POORLY GRA     5.0     POORLY GRADED SA       7.0     POORLY GRA     9.0     POORLY GRA       1.0     0.85     0.22       3.0     0.85     0.22       7.0     0.85     0.22       3.0     0.85     0.19       1.0     0.85     0.19       1.0     0.85     0.19	GRAIN SIZE       GRAVEL     Coarse     fine     coarse     r       1     coarse     fine     coarse     r       1     Identification     Classificat     r       3.0     POORLY GRADED     GRADED     SAND       5.0     POORLY GRADED SAND     SAND       7.0     POORLY GRADED     SAND       9.0     POORLY GRADED     GRADED       1.0     0.85     0.22     C       3.0     0.85     0.22     C       3.0     0.85     0.22     C       3.0     0.85     0.22     C       3.0     0.85     0.20     C       3.0     0.85     0.19     C       3.0     0.85     0.19     C	GRAIN SIZE IN N       BBLES     GRAVEL       coarse     fine     coarse     med       1     coarse     fine     coarse     med       1     1.0     POORLY GRADED SA       3.0     POORLY GRADED SA       5.0     POORLY GRADED SAND with       7.0     POORLY GRADED SAND with       9.0     POORLY GRADED SA       9.0     POORLY GRADED SA       1.0     0.85     0.22       0.1dentification     D100     D60       1.0     0.85     0.22     0.18       3.0     0.85     0.22     0.18       7.0     0.85     0.20     0.15       9.0     0.85     0.19     0.15       7.0     0.85     0.19     0.15       7.1     Isolated Wetlands Drilling Program - Ph     Stairstep Project, Lee County, Florida	GRAIN SIZE IN MILL       OBBLES     GRAVEL     SA       coarse     fine     coarse     mediur       1 Identification     Classification     Classification       1.0     POORLY GRADED SAN     3.0     POORLY GRADED SAN       3.0     POORLY GRADED SAN     SAN       5.0     POORLY GRADED SAN with       7.0     POORLY GRADED SAN       9.0     0.85     0.22       0.85     0.22     0.180       3.0     0.85     0.22     0.181       7.0     0.85     0.20     0.157       9.0     0.85     0.19     0.151       CT     Isolated Wetlands Drilling Program - Phas     Stairstep Project, Lee County, Florida	GRAIN SIZE IN MILLIMM       OBBLES     GRAVEL     SAND       coarse     fine     coarse     medium       1     Classification     Classification       1.0     POORLY GRADED SAND     3.0       3.0     POORLY GRADED SAND       5.0     POORLY GRADED SAND       5.0     POORLY GRADED SAND       7.0     POORLY GRADED SAND       9.0     0.85       0.22     0.180       3.0     0.85       0.85     0.22       0.181     7.0       7.0     0.85       0.20     0.157       9.0     0.85       0.19     0.151       CT     Isolated Wetlands Drilling Program - Phase II       Stairstep Project, Lee County, Florida	GRAIN SIZE IN MILLIMETER         OBBLES       GRAVEL       SAND         coarse       fine       coarse       medium         n Identification       Classification         1.0       POORLY GRADED SAND SP         3.0       POORLY GRADED SAND SP         5.0       POORLY GRADED SAND with SILT         7.0       POORLY GRADED SAND SP         9.0       POORLY GRADED SAND SP         9.0       POORLY GRADED SAND SP         1.0       0.85       0.22         0.16entification       D100       D60       D30         1.0       0.85       0.22       0.180       0.         3.0       0.85       0.22       0.181       0.         7.0       0.85       0.20       0.157       0.         9.0       0.85       0.19       0.151       0.         CT       Isolated Wetlands Drilling Program - Phase II - Stairstep Project, Lee County, Florida	GRAIN SIZE IN MILLIMETERS       OBBLES     GRAVEL     SAND       coarse     fine     coarse     medium     fine       in Identification     Classification     fine     fine     fine       1.0     POORLY GRADED SAND SP       3.0     POORLY GRADED SAND SP       5.0     POORLY GRADED SAND with SILT SP-       7.0     POORLY GRADED SAND SP       9.0     POORLY GRADED SAND SP       9.0     POORLY GRADED SAND SP       1.0     0.85     0.22       0.180     0.126       3.0     0.85     0.22       0.181     0.126       7.0     0.85     0.22       0.182     0.137       5.0     0.85     0.20       0.157     0.115       9.0     0.85     0.19       0.151     0.113       CT     Isolated Wetlands Drilling Program - Phase II -       Stairstep Project, Lee County, Florida	GRAIN SIZE IN MILLIMETERS       OBBLES     GRAVEL     SAND       coarse     fine     coarse     medium     fine       1.0     POORLY GRADED SAND SP       3.0     POORLY GRADED SAND SP       5.0     POORLY GRADED SAND SP       5.0     POORLY GRADED SAND SP       7.0     POORLY GRADED SAND SP       9.0     ORLY GRADED SAND SP       9.0     0.85     0.22       0.185     0.22     0.180       0.1261     3.0     0.85       0.20     0.157     0.1153       9.0     0.85     0.19     0.151       0.1360     Orling Program - Phase II - Stairstep Project, Lee County, Florida	GRAIN SIZE IN MILLIMETERS         OBBLES       GRAVEL       SAND         coarse       fine       coarse       medium       fine         Identification       Classification       Milling       Milling         1.0       POORLY GRADED SAND SP       Milling       Milling         3.0       POORLY GRADED SAND SP       Milling         3.0       POORLY GRADED SAND SP       Milling         3.0       POORLY GRADED SAND SP       Milling         7.0       POORLY GRADED SAND SP       Milling         9.0       POORLY GRADED SAND SP       Milling         1.0       0.85       0.22       0.180       0.1261         3.0       0.85       0.22       0.181       0.1283         7.0       0.85       0.22       0.181       0.1283         7.0       0.85       0.20       0.157       0.1153         9.0       0.85       0.19       0.151       0.1136	GRAIN SIZE IN MILLIMETERS         OBBLES       GRAVEL       SAND         coarse       fine       coarse       medium       fine         a Identification       Classification       MC%         1.0       POORLY GRADED SAND SP       MC%         3.0       POORLY GRADED SAND SP       MC%         5.0       POORLY GRADED SAND SP       MC%         7.0       POORLY GRADED SAND SP       MC%         9.0       POORLY GRADED SAND SP       MC%         1.0       0.085       0.22       0.180         0       0.85       0.22       0.180       0.1261         0       0.85       0.22       0.181       0.1283       0.0         5.0       0.85       0.20       0.157       0.1153       0.0         9.0       0.85       0.19       0.151       0.1136       0.0	GRAIN SIZE IN MILLIMETERS         OBBLES       GRAVEL       SAND         coarse       fine       coarse       medium       fine         n Identification       Classification       MC%       L         1.0       POORLY GRADED SAND SP       N         3.0       POORLY GRADED SAND SP       N         5.0       POORLY GRADED SAND with SILT SP-SM       N         7.0       POORLY GRADED SAND SP       N         9.0       POORLY GRADED SAND SP       N         1.0       0.85       0.22       0.180       0.1261       0.0         1.0       0.85       0.22       0.180       0.1261       0.0       0.0         1.0       0.85       0.22       0.181       0.1283       0.0         3.0       0.85       0.22       0.181       0.1283       0.0         5.0       0.85       0.20       0.157       0.1153       0.0         9.0       0.85       0.19       0.151       0.1136       0.0         7.1       Isolated Wetlands Drilling Program - Phase II - Stairstep Project, Lee County, Florida       JOB	GRAIN SIZE IN MILLIMETERS         OBBLES       GRAVEL       SAND         coarse       fine       coarse       medium       fine         n Identification       Classification       MC %       LL         1.0       POORLY GRADED SAND SP       NP         3.0       POORLY GRADED SAND SP       NP         5.0       POORLY GRADED SAND SP       NP         7.0       POORLY GRADED SAND SP       NP         9.0       POORLY GRADED SAND SP       NP         9.0       POORLY GRADED SAND SP       NP         1.0       0.85       0.22       0.180       0.1261       0.0         1.0       0.85       0.22       0.182       0.1310       0.0       0         3.0       0.85       0.22       0.181       0.1283       0.0       0         1.0       0.85       0.22       0.181       0.1283       0.0       0         3.0       0.85       0.22       0.181       0.1283       0.0       0         3.0       0.85       0.20       0.157       0.1136       0.0       0         7.0       0.85       0.19       0.151       0.1136       0.0       0	GRAIN SIZE IN MILLIMETERS         OBBLES       GRAVEL       SAND       SILT         coarse       fine       coarse       medium       fine       SILT         a Identification       Classification       MC%       LL       PL         1.0       POORLY GRADED SAND SP       NP       NP       NF         3.0       POORLY GRADED SAND SP       NP       NP       NF         5.0       POORLY GRADED SAND with SILT SP-SM       NP       NF         7.0       POORLY GRADED SAND SP       NP       NF         9.0       POORLY GRADED SAND SP       NP       NF         n Identification       D100       D60       D30       D10       %Gravel       %Sand         1.0       0.85       0.22       0.180       0.1261       0.0       97.2         3.0       0.85       0.22       0.181       0.1283       0.0       95.3         7.0       0.85       0.22       0.181       0.1283       0.0       95.3         7.0       0.85       0.20       0.157       0.1153       0.0       95.9         9.0       0.85       0.19       0.151       0.1136       0.0       96.2	GRAIN SIZE IN MILLIMETERS         OBBLES       GRAVEL       SAND       SILT O         coarse       fine       coarse       medium       fine       SILT O         a Identification       Classification       MC%       LL       PL         1.0       POORLY GRADED SAND SP       NP       NP         3.0       POORLY GRADED SAND SP       NP       NP         3.0       POORLY GRADED SAND SP       NP       NP         7.0       POORLY GRADED SAND SP       NP       NP         9.0       POORLY GRADED SAND SP       NP       NP         9.0       POORLY GRADED SAND SP       NP       NP         1.0       0.85       0.22       0.180       0.1261       0.0       97.2         3.0       0.85       0.22       0.182       0.1310       0.0       97.9         9.0       0.85       0.22       0.181       0.1283       0.0       95.3         7.0       0.85       0.20       0.157       0.1153       0.0       95.9         9.0       0.85       0.19       0.151       0.1136       0.0       96.2         CT       Isolated Wetlands Drilling Program - Phase II - Stairstep Project, Lee	GRAIN SIZE IN MILLIMETERS         OBBLES       GRAVEL       SAND       SILT OR         1000000000000000000000000000000000000	GRAIN SIZE IN MILLIMETERS         OBBLES       GRAVEL       SAND       SILT OR CL         1000000000000000000000000000000000000	GRAIN SIZE IN MILLIMETERS         OBBLES       GRAVEL       SAND         coarse       fine       coarse       medium       fine         1       Coarse       fine       coarse       medium       fine         1       0       POORLY GRADED SAND SP       MC%       LL       PL       PI         1.0       POORLY GRADED SAND SP       NP       NP       NP       NP         3.0       POORLY GRADED SAND SP       NP       NP       NP       NP         3.0       POORLY GRADED SAND SP       NP       NP       NP       NP         7.0       POORLY GRADED SAND SP       NP       NP       NP       NP         9.0       POORLY GRADED SAND SP       NP       NP       NP       NP         1.0       0.85       0.22       0.180       0.1261       0.0       97.2         3.0       0.85       0.22       0.181       0.1283       0.0       95.3         3.0       0.85       0.22       0.181       0.1163       0.0       95.9         9.0       0.85       0.19       0.151       0.1136       0.0       96.2         CT       Isolated Wetlands Drilling Program -	GRAIN SIZE IN MILLIMETERS           OBBLES         GRAVEL         SAND         SILT OR CLAY           1000000000000000000000000000000000000	GRAIN SIZE IN MILLIMETERS           OBBLES         GRAVEL         SAND         SILT OR CLAY           0 Identification         Classification         MC%         LL         PL         PI         Cc           1.0         POORLY GRADED SAND SP         MP         NP         NP         NP         1.18           3.0         POORLY GRADED SAND SP         NP         NP         NP         NP         1.16           5.0         POORLY GRADED SAND SP         NP         NP         NP         1.19           7.0         POORLY GRADED SAND SP         NP         NP         NP         1.19           9.0         POORLY GRADED SAND SP         NP         NP         NP         1.10           9.0         POORLY GRADED SAND SP         NP         NP         NP         1.10           9.0         POORLY GRADED SAND SP         NP         NP         NP         1.07           1.10         D60         D30         D10         %Gravel         %Sand         %Silt         %           1.0         0.85         0.22         0.182         0.1310         0.0         97.2         2.8           3.0         0.85         0.22         0.181

ι	J.S.	SIE	/E 0			٩G	IN 2	I IN 1.5		HE	S A 1	12	•		3		f	3	ປ 。1	.s 0	. 5	51E 1 6		E I	NU 30	JM	BE	R: 50	s ) -	70	10	) 01	4(	ا 20		)					ł	łY	DF	10	×.	IE T	TE	R					_	
0 -	TTT		6	4	3 111	т Т	2 1 [	1.5	г	3/	4	T	3/4		, IL	1	n	Ţ	Ť	Ē	Ť	T	T	П	Ŧ	1	Ň	Ţ	. '	Ĭ	-	Ľ	Ť	ÍT	Γ	Γ	Γ	Γ	Γ					T	T				Τ		Γ			
				_]			L	ļ.					╢	11	$\downarrow$			┿		-			╢	H	+	Ļ	P		à	+			+	╢	+	╀	┝	┝	+-				+	╢	H	t	┢	┢	╀		t		-	
																							Ш	Ц		_		ľ	ĥ	¥				ļļ			-	+	-	_	_	_	_	$\left  \right $		╞	┞	+-	╉		-			
아																													I	N									L				_			1		Ļ	_		-			
t	$\left  \cdot \right $	-		-†			t	T					11	Ħ	t		T		_	T			Π	Ţ	Π		-	T																										
0				-+	╟	╟	╉	┝	┢				╢	H	$^{+}$	+	t	+		╀			$\parallel$	ť	H	+		1	-	t	ľ					t	t	1	T							Τ	T	Ī	T					
-							+		_					Н	+	ł	+	+		╀			╢	+	$\left  \right $	╉		-	_	₩	Ħ		-	Η		╀	╈	╉	╈		-		-	╟	Ħ	$^{+}$	t	ϯ	1		+			
0-											_													Ļ		_		_		4	Ħ					+	+-	+	+		ļ.				$\left  \right $	╇	╀	+	╉		+		-	
						Π		T																						ł	I																		_		_			
ł						$\left  \right $	╞	$\dagger$	t				1	t			T			T					Π		-	1																			l							
50	╉					₽	╀	╀	┽		-		+	+	+	-	╈	+		╉			+		H		+		-	-	X	ф		Ħ		╈	t	╈	t		T		~	Ħ	Π		T	T						1
ļ						$\left  \right $	╞		-		-				H	+	+	-		+			+	╟	$\left  \right $	-	+	4	-	_		╢		╟		+	+	┽	+		+			╫	+	-	╉	╉	┥		┼╴			
															Ц					╧				$\prod$				_	_		ļ	11				4	4	-	╡		╞			╢	+		+	+			+-			┥
50	T																														N																							
ŀ	-	$\vdash$		-	Ħ		╈	+	+				1	t	H		†			1			1	Ħ	T				l		Γ			II																				ł
10		-					╉	┿	+		-		+	╟	H	+	┥	-		╉			╉	Ħ	+		-				┢	Ŵ.	$\left  \right $	Ħ			1	1	t		T			Ħ		Ħ	1	T						
			-		1	4	4	╞	+				+	-		_	-	_	-	+					+				$\left  \right $		╞	÷	+-	╢	-	H	+	+	╉		┢			╫	+	$\left  \right $	┥	+	-		╈			┥
30				1							ŀ														L							1	-			Ц	_	_	_					$\parallel$	+		-	-	_		+			-
30																																H																_						
	+	+	<u>†</u>		H		+	+	-+		ſ		+	╢	t	-	1	_		+				tt	t	Η			t		T	1	I	T				T			T	-		Π	Π	Π								
20	+-	-			+	:	+	┽	+		-		+	╟	+		+			+				$\parallel$	+-	+			┢		+		╢	H		H		+		•	╀				łt		+	-			+			
						:		_	_				_	ļļ						_				$\downarrow$		-			╞		╞		ł		-	H	4	-+	_		╉			+	╟	H	+	-		_		-		-
									ļ																																				$\parallel$			_		_				_
10	_							Í	T					Π																				Þ																				
		+	+-			-	╞┼	╈	╉		+-		-	Ħ	t	H	-	-	F	1		•	-	T	Ħ	t	-		╀		t			Y		Ħ		1			T	_			Π				_		Τ			
0		1		1(	Ш	·		1			:		1	$\frac{11}{2}$			•		L			-		Ц	L	1.	L.,		1.		1		C	Ц ), '	1	1		-1-					0	.0	)1						1	(	0.	0
														0			GF	ł٨	IN	SI	ZE	: 1	Nİ	M	LL	.IN	16	٢E	R	s																								
	6	-01	BBL	=		Γ			G	R/	٩V	Έl	_												SA		D														s	IL.	r	ο	R	С	Ľ	A	Y					
		-00	DL	_3			С	ba	rse	e			fir	ne			c	08	irs	e		m	e	di	ur	n			_	1	fir	ne	_	_		_					-		_	_	_					_		-		_
Spe	cim	en	Ide	nti	fic	at	io	n									С	la	ss	ifi	Ca	ati	o	n				_						M	С	%	6	1	L			Ρ	L	_		P	1	_		C	2		C	ί
	ST	-5			1	1.(	С					F	۶C	0	R	Ľ	1	G	RA	۱C	26	D	S	iΑ	N	D	S	Ρ										ľ	NF	)		N	Ρ	_		N	Ρ		0	.9	6	+	1.	-
	ST	.5			1:	3.0	D			-		F	۶C	0	R	Ľ	r	G	RÆ	۱C	DE	D	S	SA	١N	D	S	Ρ										١	NF	<u> </u>	L	N	P			Ν	Ρ		0	.9	9		1	.6
	sт	-5			1!	5.0	D					F	20	C	R	Ľ	Y	G	R/	1	DE	D	S	ŞΑ	N	D	S	Ρ										1	NF	>		N	Ρ			N	Ρ		0	.9	95		1	. [
+	ST					7.0						1	РС	C	R	Ľ	Y	G	R/	١C	DE	D	S	ŞΑ	N	D	S	P										I	NF	>		N	Ρ			N	Ρ		0	.9	96		1	. 5
	ST	-5			1	9.0	0					1	PC	)C	R	Ľ	Y	G	R/	٩Ľ	DE	D	Ś	SA	N	D	S	P			_							I	NF	2	ľ	N	Ρ			N	_	_		9.9	)3	i L_	1	.4
_		_	lde	nti				n	-	D	)1(	00	1	Ţ		C	)6	60					D:	30	)				D	1	0			%	60	30	a	ve	Ī	%	55	a	١d	1		9	6	Si	t		9	60	Cla	a
ŗ_	ST					1.0				0	).8	35		Ť		0		20				0	.1	4	5		1	0	.1	11	1	1	1		(	0.	.0		1	1	96	5.4	1							3.	6			_
	ST			. –		3.			-			35		1				18				-		4			Ť			-		8	1		_	0.			↑	-	97	7,0	3	-	Γ		_			2.	4			
	ST				_	5.			-			35		t				17						-	2		$\uparrow$	_				91	-+			0.			1	!	98	3.:	3	_	t					1.	7			
-	ST			_		7.			┢╴			35	_	╉				17	_	-				_	4	-	t	_	_	_	_	)5			-	0			+			3.4			1-					1.	6			
,	ST					9.			$\vdash$	_		35		+				15		-	-	_	_		3		+	_			_	11	+			0			+			7.4			$\uparrow$					3.				_
	RO.		:T	10				V	Ve					 ril	lir					ra	l Im						11				_					-	J	O	3	N				_	1	,	11	6	3					
				S	ai	rs	te	p	Pro	oje	ec	t,	Le	e	С	0	ur	nty	Į,	FI	lo	ric	la														Ď	A	T							1	/8	3/	99	)				
																			A						۱	VI.	(	1	T	R	١	/Ē	: <	2																				

.

٥



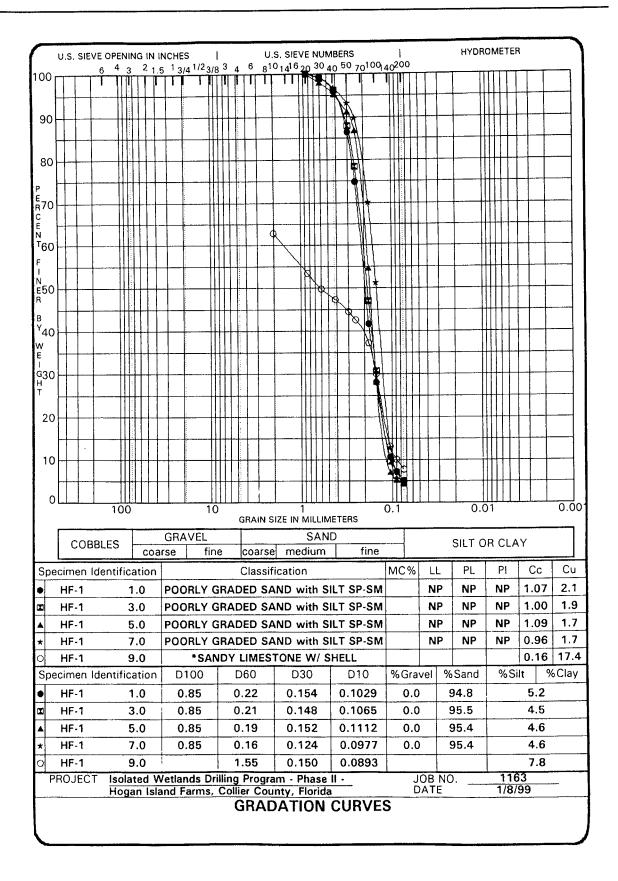
This page intentionally left blank.

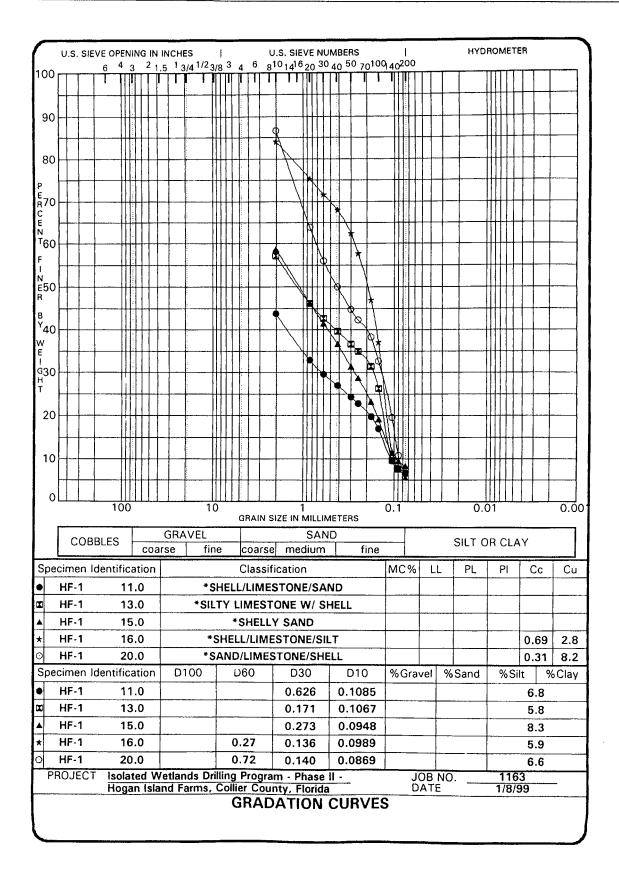
.

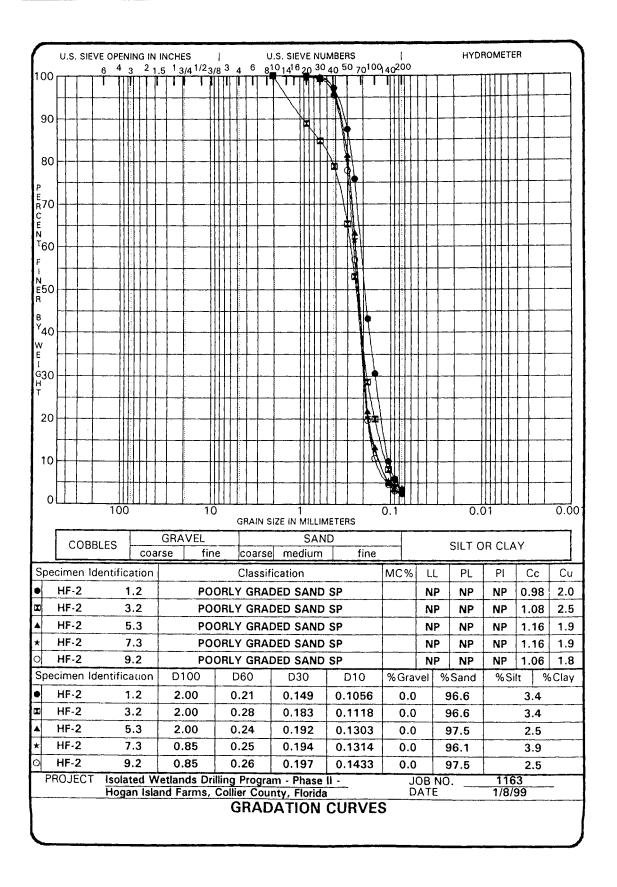
## **APPENDIX C**

.

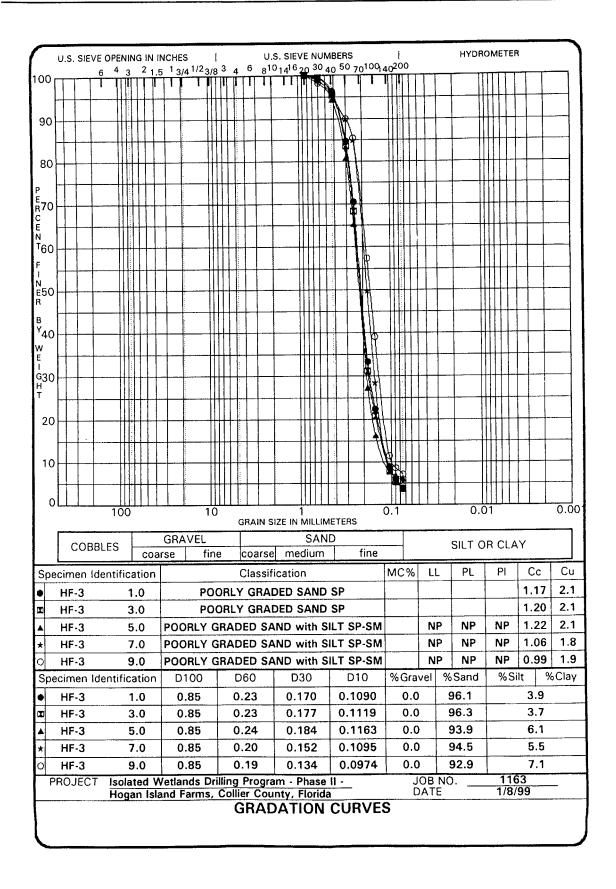
Hogan Island Farms Field Notes

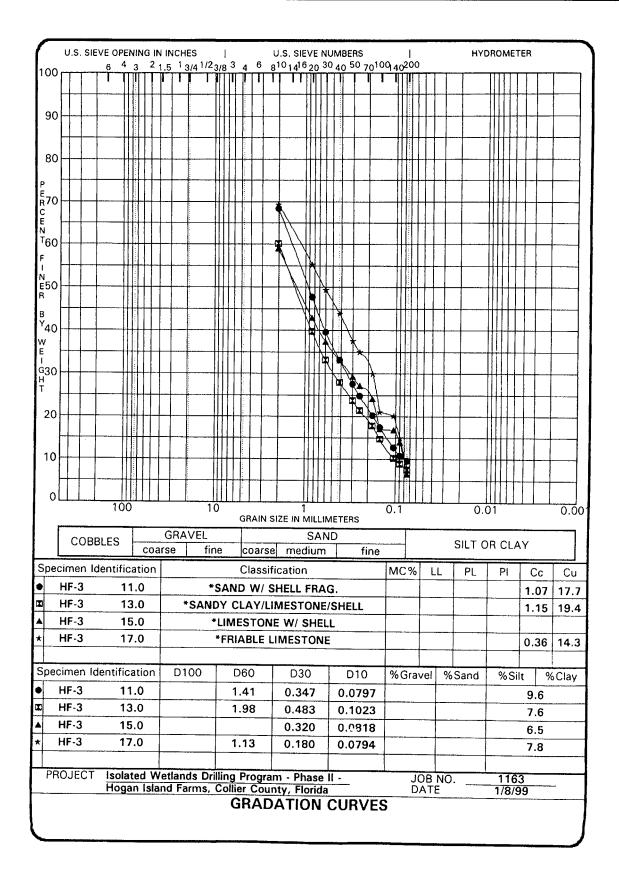


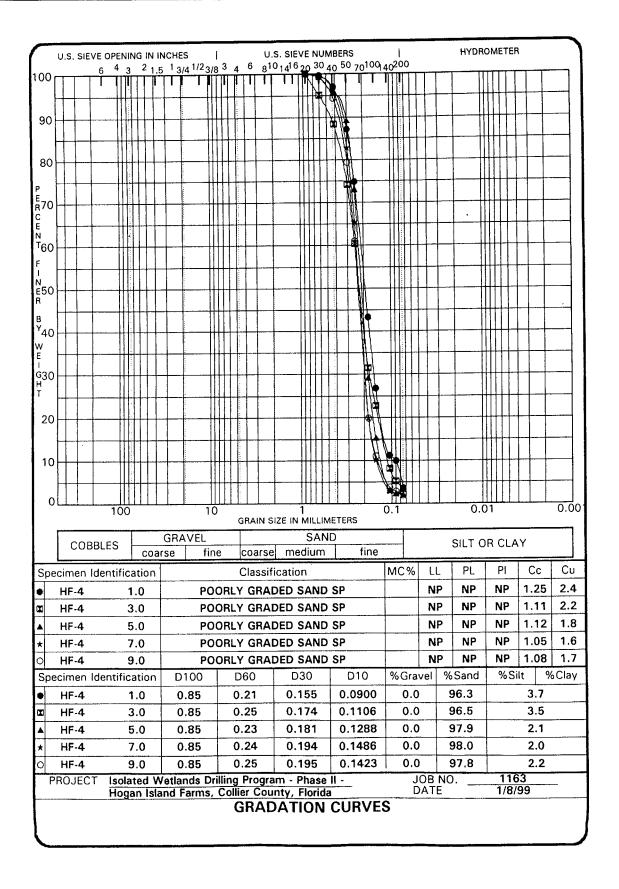




	HF-2 HF-2	11.3 13.3	-+	.85 .85		.25 .25		197 193		0.145 0.128		0.0 0.0		98.2		1.8	
Spe	cimen I	dentification	D	100		60		30		D10		%Gra	vel	%Sand	%5		6Clay
>	HF-2	19.3					ADED						NP		NP	1.03	1.7
-	HF-2	15.3 17.4					ADED						NP NP	NP NP	NP NP	1.12	1.8 1.8
	HF-2 HF-2	13.3					ADED						NP	NP	NP	1.16	1.9
	HF-2	11.3					ADED						NP	NP	NP	1.05	1.8
Spe	cimen I	dentificatior	1			Class	sificati	on				MC%	LL	PL	PI	Cc	Cu
	СОВ	BLES co	GR/ arse	AVEL fin	e	coar	se m	SA ediun	ND n	fi	ne			SILT	DR CL	AY	
		·····				GRAIN	SIZE IN			TERS			<u>.                                    </u>		<u> </u>		
С		100		10				Щ.				0.1		0.			0.0
					╫╢								$\left  \right $		╢╫		
10	┝┝╌┝										Ĩ,						
		┟──╸┼┼┟┝┝┝┟	$\left  \right $				_			-	╢		$\left  \right $			+ -	
20													+	_			
			+	H									+				
30	)		$\left  \right $								H		┥┥╸┥				
/											+	_					
40	) 										<b>ф</b>						
							_										
50	)		<u>   </u>										$\left  \right $		┼┼┼┼╌		
							_			<b>.</b>			┥┼┥				
60	) <u> -</u>		+										+++				
								-									
70	,																
															╫╢╄╋		
80	,		<u> </u>												╢╢┼		
													4				
90							_			$\mathbb{N}$					╎╎┼┼		
									ĻŊ								



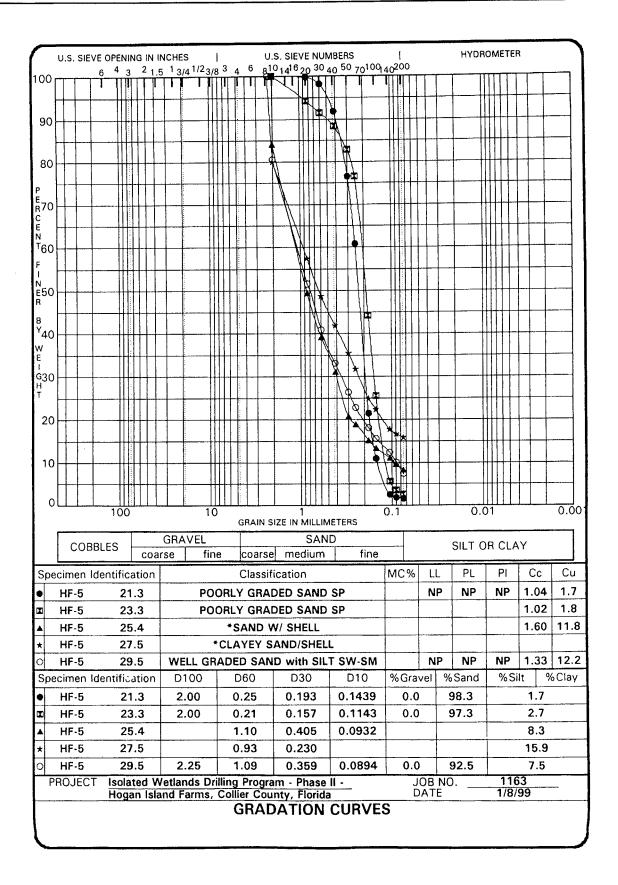


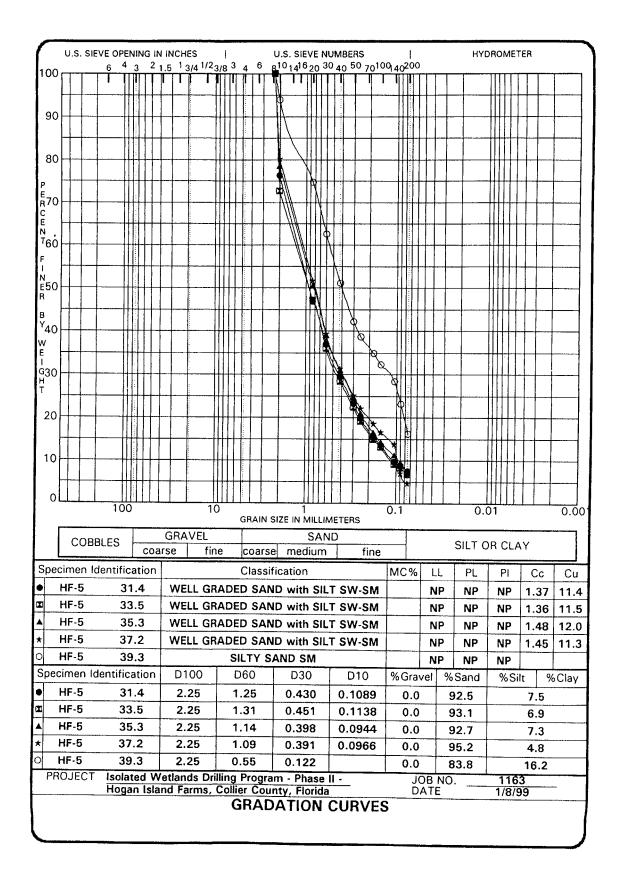


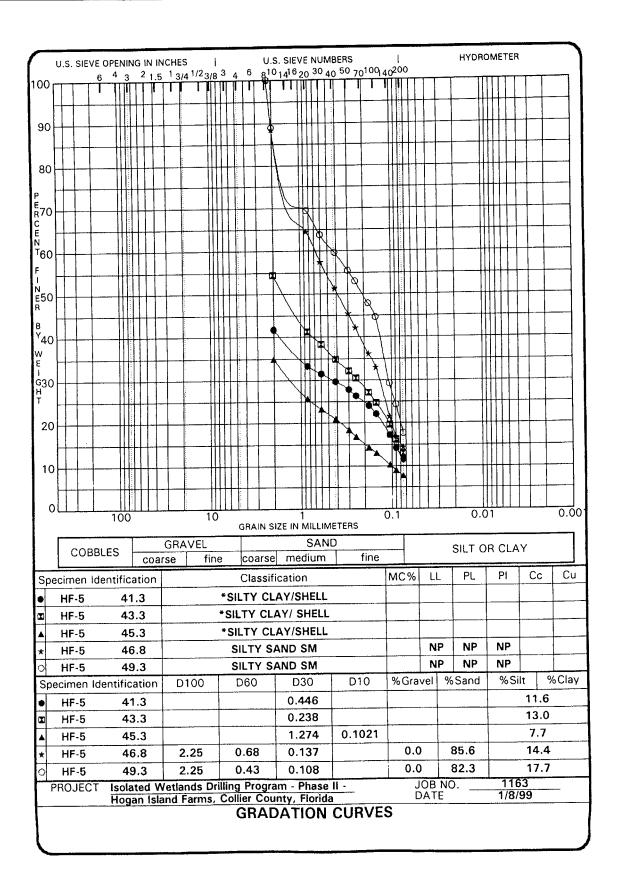
	U.S.	SIE	/E OPI 6 4	EN 				ICH 1			2,,	1	3	4	(	6		I.S.									<u>م</u> 10	00	40	 20	0					ΗY	'DP	0	ME	TE	R				
<sup>00</sup> [			ŤΤ	Π	Î	Ť	1	Ť	I		Ĵ	ĥ	Ī	Ť	Т	P	Ť		Ţ	Ц	Į	Ť	Ŕ	K	Ţ	ή	'n	L.	ΪĬ	Ţ	Т	Г	Γ		Τ		Τ		Π	Γ	Γ	Γ			
ŀ	+			+	$\left  \right $	╉			+		+	+	╟	ł	╈	╉		┢─		+	Ħ	0	ĥ	A					-+		+	-			+		-+		╞	ŀ	╞	┢╴	+		
90		-				+			-		-		H	+	+-	+		$\vdash$		-		$\parallel$		A	B	K					+	-	╞		╉	·			_	╞─	┝	-	╉		
-	+-			4		-								-	1	$\downarrow$		L		+		4	Ļ		Ł	H	þ				-		-				_	4-		-		-	-		_
80															1			L			Ш			Ľ	Ĭ	$\parallel$						L			-		$\downarrow$						-		
_ [					Π	T																	Γ		R		T																		
70						╈			T		+				t	+		1		T	It			-	T	Ì			1		1		T		T		1	T	T				T		
ŀ	+			H	+	╈	-		+		-				+	╉		$\vdash$				+		┢┈	╈	t			+		╈	┢─			+		-		-		-		+		┤
60	+			$\left  \right $	++	+-			+		-+		╟	╉	╀	┽		$\vdash$			H	+		┝		╢	H	╞─	╢		+	ŀ	H		+		+	+	╋	$\square$			+		+
-		_		4	$\left  \right $	+-			-		-				-	+		ļ		-	4	+			-				+	-	+	-					_	4					+		_
50		_				_			_																		1	<b> </b>			1												_		
40		T		$\ $	Π	Γ										T		Γ		T					Γ			ſ			T							ſ							]
40					Ħ	1			t				Π		T	1									T					T	T	ľ			1			T					T		
ŀ		+				+			t			H	╟╋	-	+-	+		+		-			$\uparrow$	-	+		Ħ	+	╢		+	$\vdash$			+		╢	$\parallel$	+-	Η	-	-	+		-1
30						┿			+			+	$\left  \right $	-	+	+		-		+	$\left  \right $	+			+	-			╢	+	╉	┝			+			╢	+	-			+		-
ŀ	+				$\parallel$	-			-		-				-	+		Ļ		+					╞	_	$\downarrow$	-	-#		+						-	4	_		_		-		_
20	$\downarrow$				$\parallel$															_					<b>_</b>		1	ļļ			_								_						
10																																													
10												T	T		t	T	*****			T	Π	T			T			11	Ĩ	T					T		1						T		1
-		-+		Ħ	Ħ	t			ŀ				1		1	╞						+			t	1		Y		t	-	-			T		╢	$\dagger$					1		1
٥L			10	0	11	_			ŀ.		10	)	1	ŀ	1	-		l		1	.11	1	·		1			0	), 1	<u> </u>	1					0	.0	1	Ш					0.	۲ 00
F													_	G	RA		I S	IZE	IN					TEI	RŞ					- <u>r</u>								_							
	C	) 86	LES								in			+								<u>N</u>	D			£:,				-					SIL	T.	٥f	7	CL	A,	Y				
	imo	n Id	entif	ior			ars	e	<u> </u>			-		+			se	ca	me					_	-	10	ne	· .			2			1	_		Ť			T			T		
·		· · · ·			.0	50	-				~	<u></u>	21								~~~		c	<b>n</b>				1	VI	C 9	/0					י <u>ר</u>	+			+		C	+		u
	1F-4				.0		┢																			• •		+			-		NP NP			IP IP	+		IP ID	+		30.	+	1	
	HF-4				.0		+																-					+-			+		NP	-		IP IP	+		IP IP	+		.05 .04	-+	1	
	 HF-4				.0		-				-	-		-	_			DEI						-				+			-	-	NP			IP	+		IP			02	+	1	
	IF-4				.0		+									_		DEI	_		_							+			-+		NP	-		IP	╉		IP	-		93		1	
pec	ime	n Id	entif	-			T	D	10				-	26	-	_	T		D	_	_				D1	0		1	%	Gr	av				Sa			-	%S					Cla	_
ŀ	HF-4	Ļ		11	.0		1	0	.8	5		•	C	).;	23	}		(	0.1	17	8		,	0.	1:	29	0	1		0.	.0		+-	9	7.	3	╈					.7			
H	1F-4	 	1	13	.0		1	0	.8	5			C	).1	19	)	1	_	0.1							13	_			0.			╈		8.		+					.7			
٢	IF-4	<u> </u>	1	15	.0			0	.8	5			C	).1	18	}		(	0.1	14	6		ł	0.	1'	12	4	T		0	.0		1		7.		1					.9			
	1F-4		1	17	.0				.8					).1				(	0.1	15	0			0.	11	13	8			0.	0		1	9	8.	1					1	.9			
	IF-4				.0				.0					).1			Ι		0.1						1(	06	3	Ι			.0		Ι		7.	3						.7			
PR	JJE	СТ	Iso Ho	at	ed	۷ دا	/el		1d ar	s [ m	Dri		<u>ווי</u>	P	ro r	) G	rai	n	- F	h	as	e	1	-	-						JC	DE	3 N TE	0				1	11) /8,	63 /0	3				
				90		310			u		·/	50					D							11	D	V		C				_							10	J	J				

U	.s. s	IEVI	E OPE		NG	11 6	1	NC	не	s				``				U.	s.	SI	£\	/E	NU 20	JN	181	ERS	S		იი		~2	 00	)					ΗY	DR	0	ME	ΤE	R					
0 —			6 4	3	, TT	2	1.5	5	13	/4	1/2	3/	8 (	3	4	6 - T	<b>r</b> -	81' 14		4		20	. 30 10	54 FT	0	50 T	7	<u>י</u> ו	T	14	02 11	Ē	, TT	Т	T	-	Γ	-	Т	Π	Π	Т	Г	Γ	Т			1
Ĭ			'				ľ		1		1	Ĩ				1		<u> </u>						1							4		Ц	_			-		-		$\parallel$	╞		╀	-+			ł
					Π	1	1	1				Π		T												$\phi$																						
>ի	┝┼┙			++	╂╂	+	╀	╉		-		ť	$^{\dagger\dagger}$	t	-		t	-		-		Ħ	Ħ	T	ľ	M							Π															
+		4			$\parallel$	+		+		_		+	+	╀	-	╞	╞		_	_		H	+	+		₩	_	┢		_		-	Η				1-	_~~	1	Ħ	Ħ	╧	t	T				1
0				Ш			1					_		+		L					_	Ц	+		-	1	]_	-			#		⊢		_		┾		-+	╫	H	+	+	╀				
Ĭ								Ì							1									Ц	-			1											_	╢				-				-
				Π		Τ																																										
0-	++	+				╟╢	+	┥		ſ		+				t	╋		t			T	T			1	P	T			IT						Τ											
$\vdash$	┼╌┼	+				$\left  \right $	+	╉		-		┥	╟	+	t	┢	╉		$\left  \right $		_	+		$\left  \right $		-	ł	$\dagger$			╢		┢				t		1	Ħ	T		T	T				
아	<u>.</u>	_		Щ	-	Ц	+	-		-		4		μ	+	+	+		╞		_	H		┢╸╽	+	-	1	+			⋕	╢	╀	╞	-		╀		-	₩		H	+	+				
		1																	L					Ц							Ш		+	L			╇			#	╀	$\left  \right $	+	+				-
	$\prod$	_		$\Pi$	ſ	Π	T	T							11111																									$\parallel$	1			1		<u> </u>		
0	$\dagger$	+			1	Ħ	1	+		ſ		1	11	Ħ		1-	T		Τ			T	T					T			$\prod$																	
┝	╆╍┤	+		H		$\left  \right $	+	-+		-		$\neg$	╫	H	-	╉	╉		╎			╫	╟	┦				ł			╢	Ħ	╈	1	t		+				T	Ħ						٦
.0	+			#		$\downarrow$	4	4		+		_	╢		+	╀	+		╀			╢	╟	+	H		-	╉			╢	$\left\  \right\ $	╉	╀	┢	+	╉			╟╢	+	H	╉	╉		+		-
													$\parallel$		_				1			ļļ	╢		:			┛					-	+	-	-					+	$\left  \right $	-	-+		+		-
																																				_								_		-		4
10	+ +			$^{\dagger\dagger}$		T							Π	Π		T			T			Π	Π									1.00																
ł	++	-		╫		+	$\left  \cdot \right $			-		-		Η	-	╉	+		+			╫	$^{\dagger\dagger}$	╎	÷		-	ť	56	2	╢			t	1	T	-†			Ħ	Ħ			-				
20				$\parallel$	╟	+-				-				$\parallel$	-	+	-		+			╢	╀╋	╇		_	$\vdash$	+	B	1			+	+	+-	+	╉			₩	╟	$\mathbf{H}$	-	-+		+		1
																			1			$\parallel$	44			-			Ţ	(l)	Ш			-	+	_	┦		_	H	$\parallel$	+	-	-		+		-
																							11						β	$\langle [$	Į,										Ц					ļ.,		
10				1	Î	t	Π							T					T			Π	Π	T			ļ				8	X												1				
ł	+			╫		╉	$\left  \right $	-								+	-		t			╢	$\dagger$	+-		$\vdash$	1-				ſ	ľ	Ħ	1	$\uparrow$	T				Π	IT					Τ		
ol				11	Ĥ							-1	Ш О			1	_		1			<u>Ш</u> 1	11	1			1			(	).	1 1		1	1	1			0.	0	1						0	.0
			'	0	,								Č		(	GR	AI	N :	SIZ	ZE	IN	N	۱LI	LIN	٨E	TE	RS	;									_											_
	C.	ΩBI	BLES	:				(	SR	A	VE	L	_			_			_				S/		ID							_					S	IL.	r (	OF	۲ (	сι	A	Y				
						С	0	ars	e			fi	ne	:				rs	-				iu	m			_	tı	ne	-	_		-	1			T	_	_	Т			-	_	-		-	
pec	cime	en l	dent	ifi	ca	tic	n	L							_	_		si													M	IC	%	2	L		+	P		+		PI			00 20			
	HF-	5			1.	5	_											RA				_	_					• ••		_	<u> </u>			+	N		+	N		+		NP	-†		.2			2.2
	HF-	5			3.	4		+		_	RL		_		_	_	_	_												-				$\downarrow$		P	-	N		+		NP			.4			2.8
	HF-	5			5	.3					RL				_						_													-		IP	+	N		+		NP				8		2.2
	HF-	5			7.	.2			-		RL																_		_					_		IP	+	N		-		NP	-		.3			2.:
	HF-	5			9	.3		F		_	RL		G	R/		_	-			VC	-			1 5	SIL.	_	-			M	_					IP		N	-	+	_	NP		-	.2		<u> </u>	1.5
pe	sime	en l	dent	tifi	ca	itio	on		. (	21	00	)			C	)6	0		1			3					D	_			<sup>9</sup>			_	el			Sar		-		%	Si	-			5C	ıa
	HF-	5			1	.5					85				_		24	_					77		-	_			93	-	-		0.			.		6.'		$\downarrow$					3.9			
	HF-	5			3	.4					00						24		1			_	71		1				65				0.			-		1.1							8.2			
	HF-	5			5	.3			_		85				~		25		$\downarrow$			_	86		1	_		-	03	_	-		0.			$\vdash$		5.:							4.1			
1	HF-					.2					85		_				24				_	_	82						27					0				5.		-					5.0			
	HF-					.3					8						23						89					24	45	5			_	0	_			5.	3			4	16		4.	/		
PF	SOJ	EC	Г <u>İ</u>	sol	at	ec	1 1	Ne	etl	ar F	nds arr	: [ ne	)ri	lir Cr	1 <b>9</b>	P	ro · · ·	igi Co	rai Ur	m htv	· /	PI FI	na Ior	se rid	:     a	- 1	-							D.	DB A T	E E	U.					1/	10 8/:	99 99	)			
			r	10	Jd	11	15	di	iu	<u>r</u>	art	. 13														CI	JÌ	R١	VI	ES	S			-														
																					_	-	-																									

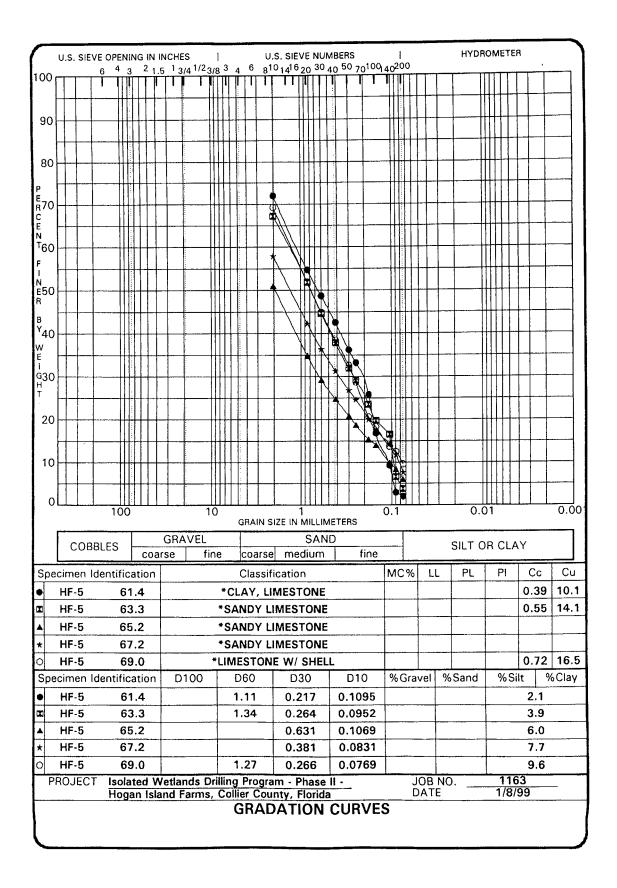
	U.S	. SIE	VE OI 6		NIN 3					ES 3/4	1/2	 ع/۶	 3 3	٨		6		I.S.								010	042	10	 201	0				н	YD	RC	M	ETI	ER				
<sup>00</sup> [			Ť	Ţ	Ů	Π	Π	ŕΪ	Т	1	Т		Π	П	T	Π	Ť	h	Ú	Ť.			Ĩ	T	Ť	ň		Ĩ	Π	Π	Π	Т				Π	T	Τ	T	T	T		٦
				╫			-			-		H	+	┢╢	╉	┥		╞╴		ŦF		Ń	Š.	+						╋		-+-						T	+	T		-	
90	+					H						H	╉		+	╉				╢	$\left  \right $	H	Ä	$\mathbf{T}$				╫		+		┥	•••		-	$\left  \right $			┢		+		
				╢	$\left  \right $	$\left  \right $						╢	╉	H	+	+		$\vdash$		╢		$\left  \right $	$\mathbb{A}$	H				╢		+	$\left  \right $						+	+	+-	+-	+		
80										-		Ц.			+	_		-		╢		$\left  \right $	+	Æ	_			#		4	$\mid$	$\downarrow$						+			+		
				4						ļ		Ш				4		L		╢				K	) 							_											_
70																								4																			
/0															Τ									Ĩ				Π		Π													
				T	Ħ	Π						Ħ	T		T					T	IT	Π			ŧ.	-		1		Π								Т	T				
60					Ħ	Π						Ħ	╈		╈	1		1				Ħ		┥		<u> </u>		Ħ		Ħ	H	$\uparrow$					$\dagger$	╈		T	╈		
Ì				╢	╟	H	-	-		-		╢		$\left  \right $	+	+		┝		╫	╟	H	+	-+	┨			╢		H	+	+	$\neg$			+	+	╈	+	-	╉		
50				$\parallel$		+	-			-			-		╀	+		╞		╢		H	-	+		-		╢	-	H		+	-		-		+	┿	+-	┢	+		
	+			#			_	_		ļ: 						_		L_		#	$\parallel$	μ		$\downarrow$	_			$\parallel$		$\parallel$		+				$\parallel$	$\parallel$	+	-	-			
40	_											Ш								$\parallel$		$\prod$		_				1		$\square$		_								-			
,										ŀ																l																	
							1									T		Γ		T		Π	1	T				T		Π						Π	Π	T	T				
30	+-	Í		Ħ	Ħ		1						1		Ť	╈				⋕			+	+				Ħ	Ħ		1	↑	-			Ħ	Ħ	1	t	1	╈	• ••	-
	+			╢	╢	H	+			-			+		╉	┽		-		╫	-	┢┼		╉				╢			╡	-			-	╢	╢	+	+		+		┥
20				╢		$\left  \cdot \right $		-		-		$\left  \right  \right $	+		+	╉				╢	-	$\left  + \right $	+	+				╢		H	+	+				╢	╢	+-	+	+	┿		-
-				1			4	_					4		╞	-				4				$\downarrow$		Ţ.						4			_	$\ $	$\downarrow$		_				
10	_			#			_	_																			Ì	Ц				_											
					:																																						
o					***								Π			T				Π	Π	Π					2	0.0		Π	Τ						Π	Τ					
			1	ÖC	)					<u></u>	1	0		6		. (A)		ZE	1.61	1					1		0	.1				_		(	0.0	)1			<u> </u>			0.	0
Г					Τ			G	R	VI				T	Π.Α	4.011					Al		_						Т														٦
	С	OB	BLES	,	-	c	ba	rse				ne			:0	ar	se	ſ	ne				Ĺ		fi	ne							S	ILT	0	R	С	LA	Y				
pec	ime	en la	lenti	fic	at	io	n							C	Cla	ISS	ifi	са	tio	n							IN	٨C	2%	6	L	L	Т	PL			ΡI			Cc		С	<u>≓</u>
1	HF-	5		11	1.:	3					PC	00	RI	.Y	G	R	AD	E	5 8	SA	NC	5 :	SP	,			1			╋	N	IP	T	NF	,		NF	,	1	.04	1	1.	7
	HF-	5		13	3.2	2					PC	0	RI	.Y	G	R	٩C	E	5 5	SA	N	) :	SP	ł			T				N	IP		NF	•		NF	-		.0	-+	1.	
I	HF.	5		18	5.4	1					PC	0	RI	.Y	G	R	٩C	DE	) 5	SA	NE	5 :	SP							1									1	.09	3	1.	8
ł	HF-	5		17							PC	0	RI	Y	G	R	AD	)EI	) 5	SA	NC	2	SP										T							.05		1.	
	HF-	_		19		-					PC	0	P۱	.Y	G	R/	٩D	)EC	-	-	NE	2										Ρ		NP			NP	>	1	.02	2	1.	7
			lenti	fic	at	io	n		D	100	)			De	50				D	30				D	10	)	0	60	Gr	av	el	9	6S	and	j		%	Sil	t		%	Cla	iy
	HF-			11						.85		$\downarrow$		0.:						99		_			49				0.					6.8				_	3	3.2			
	HF-		~~~~~	13						00		1		0.:			_			96					39	• •	+		0.					.6					4	1.4			
	HF-			15			_			.00		-		0.:			_		···· •	84		$\downarrow$			31		+-		0.					.6						3.4			
	HF-			17						00		1		0.2			+			90		+			43		_		0.					.9						2.1			
	1F-!	5 ECT	lso	19 19				°.+		85		1		0.2						88				.1	42	4			0.		10			.4						1.6			_
· // ·				) ga	an	u Is	la	nd		ias arn	ns,	C	ol	lie		20 Co	un	ity	, F	lo	s0 id	a	•	-					ì	DA	AL AL	N( E	J.	_			111 1/8	16 3/9	<u>3</u> 99			-	
																		A.					1	IC	21	E/E	C		_	• • • • •								-					

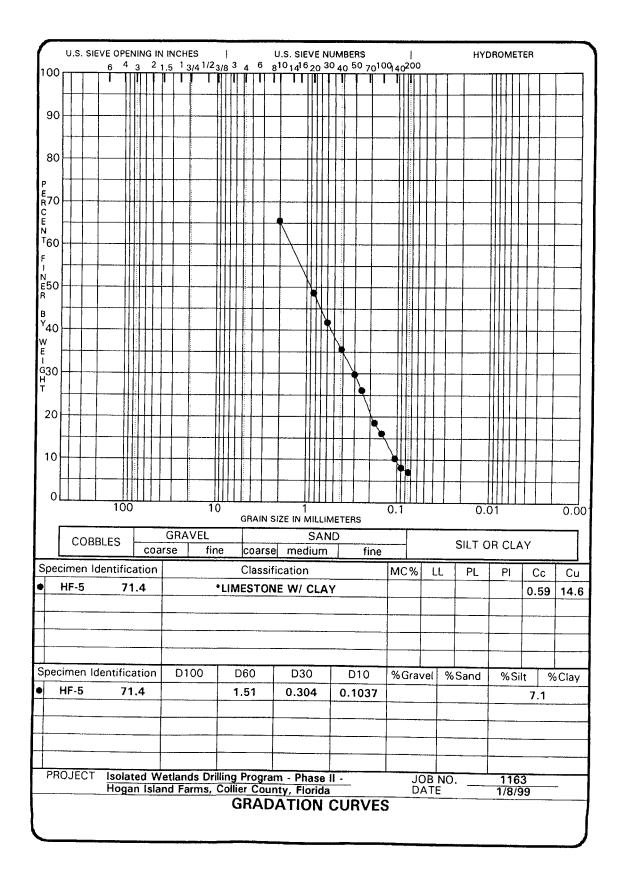


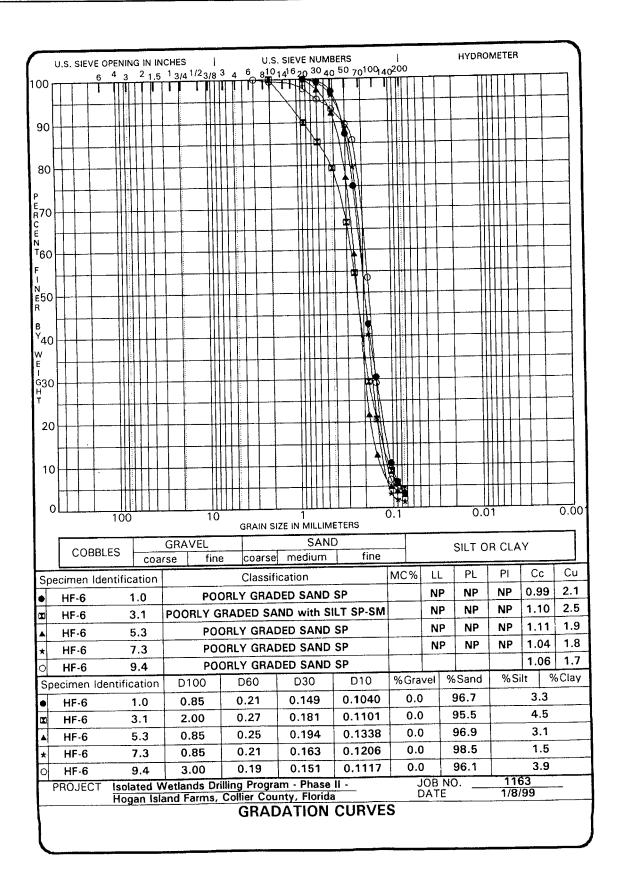


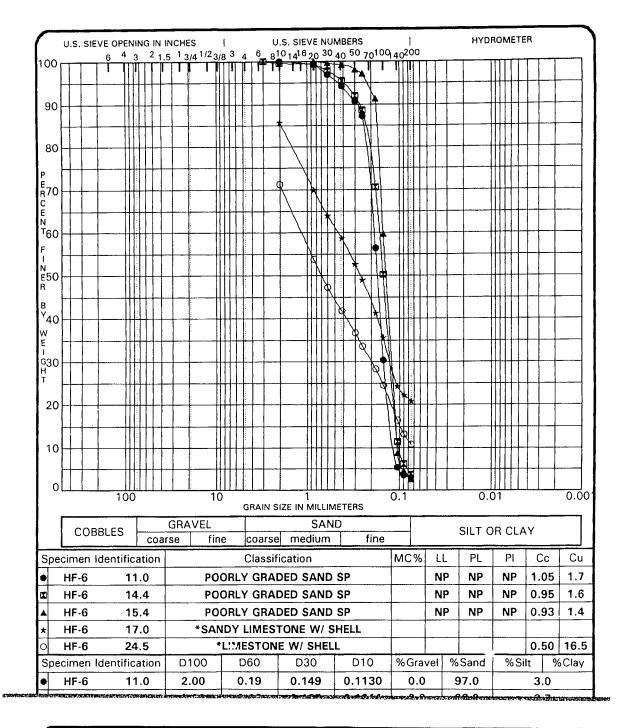


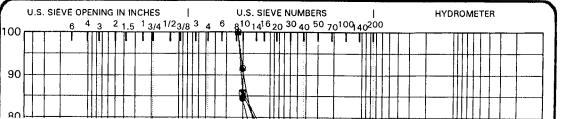
	J.S. S	IEVE OPE 6 4	NIN 3					122	 /g 3		6		1.S. 9 10 <sub>12</sub>						01 <sub>0</sub>	91 <i>4</i> 1	ا 200ر			HY	'DR	OM	ΞTE	R			
٥ſ	Π	TŤŢ	Ŭ	Π	ΪŢ	ΤŤ	<u> </u>	Γľ	Ĩ	ΓŤ	Π	Γĥ	ΤŤ	Π	ĨĬ	Π	Ť	Γ	ŤΤ	Ī	ÍM	TT	Τ		П	Π	Τ	Π			
+	┝╌┝╸	++			┢╌╄			┥	++		┼╌	$\square$	F		╫	+		<u> </u>	╈			+				╫				. ·	
아		-			┝╌┼╸	_			₩.		+-		<u>R</u>		114	+	-	-		-		┼┼				₩	+-	┝┤	$\rightarrow$		
								_			ļ	ļ'	Μ_		Щ			ļ					_			111	_				
													M																		
아									11				Ш	$\mathbf{N}$	Ш	П	-									Π					
ŀ				$\parallel$							+		$\uparrow\uparrow$	$\mathcal{M}$		╉			+			╶┼╌┼	-	-			$\uparrow$				
0	$\left  \right $				$\left  \cdot \right $			+	╟┼	$\left  \right $	+-	$\left  - \right $	$\downarrow$	d		$\mathbb{H}$		-	+			++			+	╋╋	+	$\left  \right $			
-				ļ.					Щ.		-		A		ΠŇ			-		_		+				+++	+	$\left  \cdot \right $	-+		i
₀┝					Щ						1_		Ц.					1.	ļ			$\downarrow \downarrow$	_			╎╎┼					
													$  \rangle$				A														1
					Π				T					$\left  \right $	$\prod$		N			1		$\prod$	Τ		T	$\prod$	Γ	Π	T		1
0 -			t		$ \uparrow$			-+	+		$\uparrow$		1	$\neg$						$\uparrow$			1	-		<b>†††</b>		+	-†		1
┢	┝╌┼╴			$\left  \right $	┟╺┟						┢			-f	Ыł	+	+	μ¢		-+		++	+	+	╢	╫┼	+	┝╌┼	-		
0		+			$\left  \right $	_			++				-		IN.	+	-	+		,		+		+	-	$\left  \right  \right $	+		+		
L												-	ļ			R				11						╢╢			_		
ᅡ			ŀ														<u>g</u>														
																		\$	ļţ		-										
_											1		1	-		$\uparrow$	-	R	1-1	1		11	+-	1							
아	╞╌┟╌				┞╌┼			-			+			-+	┟┟┼	+		† –	6	W			+			╫╋	+		-+		
-		·			$\left  \right $	_			╢		+					+		-	+&			┼┼			╢	$\left  \right  \right $	+	┝╌┼╴			
ᅌ									11-					-		$\square$		-		4		11			_						
oL											ļ						1														
-		10	5					10	)		8 4		IZE I	1	A11 1	16.6	ETE			0.	1			0	.0	1				0.0	0
Г		•••••	Т		G	RA	VE								SA					<u> </u>	Т										
	со	BBLES	$\vdash$	coa	arse			fin	e	c	oa	rse	n	ned			Ť	f	ine					SILT	OF	R CI	LA'	Y			
eci	men	Identifi	cati	ion						C	las	sif	icat	ion						M	С%	ΙL	L	ΡĻ	Т	PI	Т	С	с	Cu	
Н	F-5	5	1.2	2	1				;											+-		N	IP	NP	+	NP	,		<u> </u>		
Н	F-5	5	3.2	2	1				;	SIL	ΤY	SA	AND	) S	М							N	P	NP	+	NP	,				
Н	F-5	5	5.2	2	P	00	RL	YG	RA	DE	D	SA	ND	wi	th	SI	LT	SP-	SM			N	P	NP		NP	,	0.6	62	6.0	
Н	F-5	5	7.3	}					;	SIL	TΥ	SA	ANC	) S	М							N	P	NP		NP	,				
	F-5		9.2						*S	AN	D١	<u> </u>	ME	ST	ON	IE												0.9	97	15.4	ŧ
		Identifi			ļ		00			D6				D3(				D10	)	%	Gra	vel	%	Sand		%	Silt	t	%	Clay	
	F-5		1.2				25			0.5				.11						$\bot$	0.0		-	31.2				18	.8		
	F-5		3.2				25			0.5				.16		_				_	0.0			37.1				12			
	F-5		5.2		<b> </b>		25	+		0.4				.13						_	0.0			37.3				12			
	F-5		7.3			2.	25			0.4				.12				0.00		_	0.0	)	8	35.9				14			
	F-5		9.2		Vet	lan	de			1.4				.36 Ph				09	53	<u> </u>		ОB		_	1.	- 7 7	61	7.	1		
		Hog	an	Isla	and	Fa	us arm	IS,	Co	lier		our	nty,	Fl	orio	da		-			D	DAT	E E	•		1/8	163 3/9	9		-	
													A٦				211	R\		ς							••		•		-

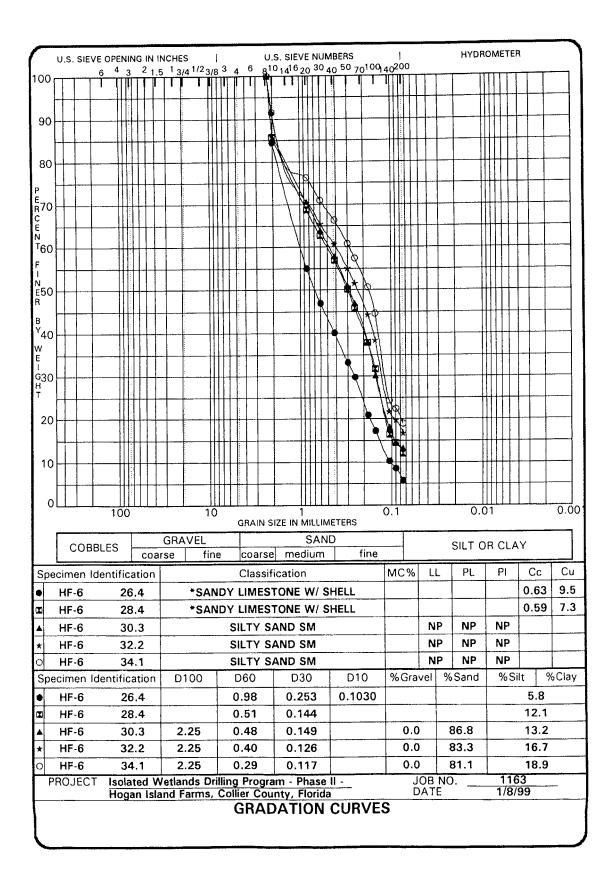






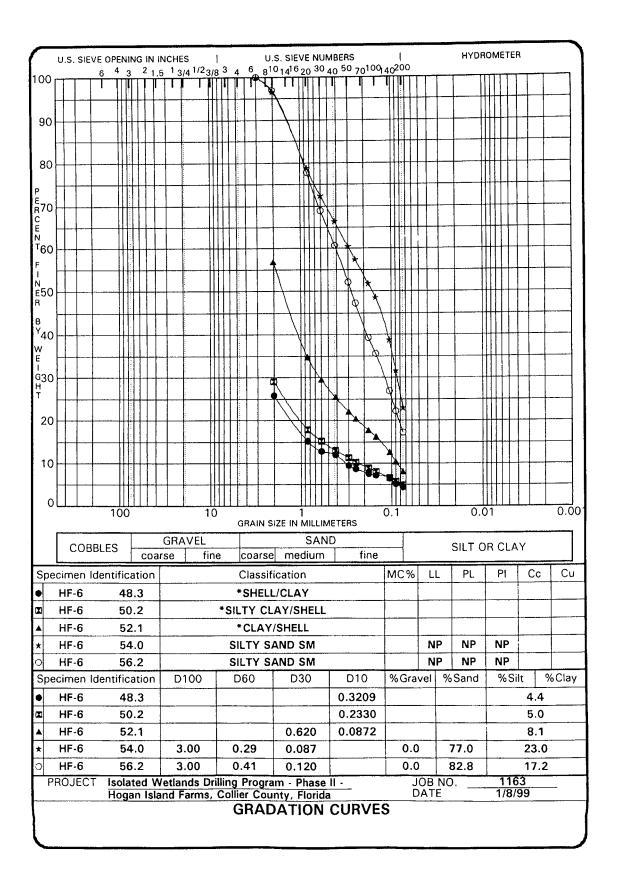




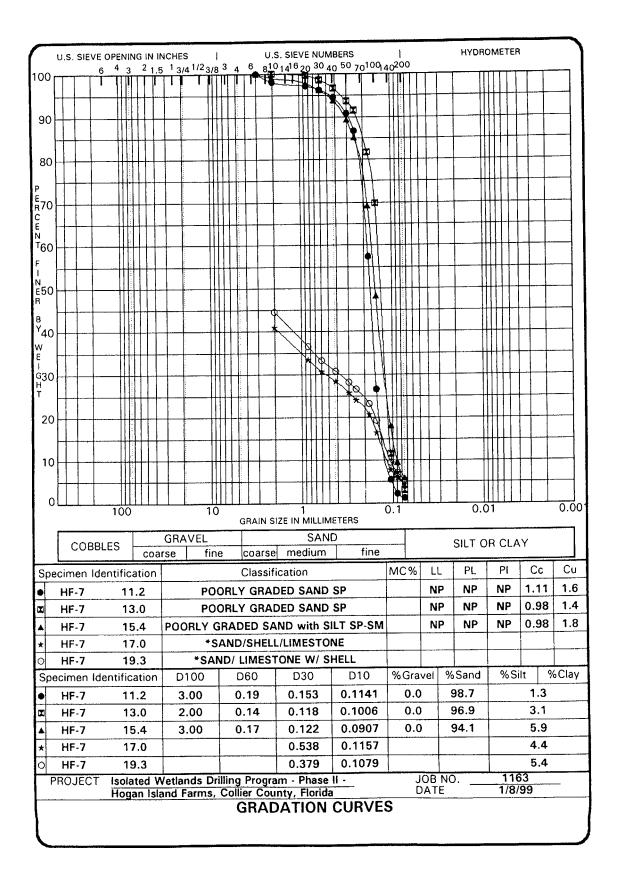


	U.S. SI	EVE OPE 6 4	ENI 3			INC .5			/2;	 א/{	3		1	6			. S 14 <sup>1</sup>							70	10	Գ⊿	102	1200	b					ΗY	DF	10	ME	TE	R			
00		ŢŤŢ	ŢŤ	Π	Tİ	ΓŢ	η̈́	í –	T	Ĩ	Π		Π	T		t	T	Π	Ť	Π	Ţ	ĺ	I	Ĩ	1	T	Ĩ		Г	Π	Τ		Γ			Π	Π			[	Τ	
				╟	$\left  \right $	-				╈	Η			-	-			╡		$\parallel$			<u> </u>	-			╢	-	┝	┢┥	┥				-	╂╊	Ħ	┢	┢─	-	$\uparrow$	
90				╟	+		_		_	+	H		+	-		1	┢	-	-	┝┼		-		╉			H		$\left  \right $	H	-		┝		-	╢	╟	╀	$\vdash$		╀	
			╢	╢						4	$\prod$		-			╢		+						+				-	-		-		-		+	₽		╀	-		+	
80				11	$\left  \right $				_					4		ľ,	ſ	X												$\square$			L		_	#	Ц	1			-	_
																$\square$	ł	$\mathbb{H}$					Ĺ								_											
70																		M	N																							
/0		1		Π	T					Ħ			1	1		T	T			Ŕ	Ì			Ť	_					Π					Ť.	IT	Ħ				T	
				┢╋╴						╁	Ħ	-	╈	+		╞	1		Ì	T	N			╈					Η	$\square$	+				+	H	╟	t			╞	
60				╟	H	+			-	╫	H		╉	+		╀		$\mathbb{H}$	+	Ŧ		f	À	+				+	$\left  \cdot \right $	$\left  \right $	-				-	╟	+	┢─	-		╀	
				┝┝	$\square$				_	$\parallel$	$\prod$	-	+	_		╞		X			Ì		1 \	Ţ				-							-	#	4	-			-	
50			Ц.	1	Ц					1	$\prod$		1	_		1			4			$\mathcal{T}$	2	Ļ	1		Щ		$\square$	Ц							Ц.				<u> </u>	
				Ш															N				À	Å	1																	
40					Π					Π	Π		T							Ŕ				V	$\prod$				Π						T	T		Π				
40				T.						$\parallel$	Ħ	╡	1	+		t			$\parallel$	Ť	М	,			۱ <del>۳</del>				Η	$\left  \right $	1		Ļ		$\parallel$	Ħ	╟				T	
		++		Η-	$\left  \right $					╫	$\left  \right $		╀	╉		$\mathbf{k}$	_	╢	$\parallel$	╀		A	$\vdash$	╋	H	$\mathbf{t}$	$\parallel$		Η	+	╉				+	+	+	Η	-		┞	
30	+	┼┦		+	$\left  \cdot \right $					╢	╢	_	╉	+		$\downarrow$	$\leftarrow$	╢	╢	+	╞╌┨	_	R Q	╀	+	H		-	μ	4	+				+	+	+	$\left  - \right $	-		┢	
						_	_			⋕		-	+	_		-		Å	$\ $	_				6	$\Box$	Щ	Ų.				_										L	
20										$\parallel$									N		:				þ		N															
																					X		r			Å	Þ								Π	Π						
.				Ţ						T	Π	T	1	1		ſ		1	Π	T		-1	*	*	*		R	Π	Π	1	╋				1		1				T	
10	+			$\uparrow$		+			-		┢╋		╀	╈	_			╢	$^{\dagger}$	╀		-		t		X	Į		H	╈	╈				1	Ħ	$\dagger$		$\neg$		-	
	++			+	$\left  \right $	+	-			╟	┢╋		+	+		-		╫	╫	╀	Ц	-		+			P				+	_			+	$\parallel$	+		-		-	
οl	<u> </u>	10	[]]] 0				Ľ		10	Ш		ľ	1					1	Ц							0.	1				1			0	Ц	1		_				0.0
r									_		_	G	R/		I S	IZE	IN	_				ER	s			<u> </u>									.0	ʻ						0.0
	СОВ	BLES	-				'A	VEI				-								N	D						_					S	IL.	T +	OF	२।	CL	٨	Y			
	imanı	dantifi				rse			fin	e				ar		=	me		ur	n		÷	1	in	e				T	_		T			Ť	_					<del></del>	
·	imen I													_		_	tic			-						N	IC	%	2	_L			P		-	_	91	-		c	_	Сι
	HF-6 HF-6		6. 8.		_	PO		4L )	<u>r (</u>	iK			_				<u>ע</u> D			S	LI	5	5P-	S	M				-		P	+	N		+		IP	+	0.	52	-	7.
	HF-6		2.		-				•																		-		╀		P	+	N	_			IP	+			+	
	HF-6		4.														D LA								_		~		╀	N	Ρ	┿	N	٢	+-	N	IP	+			+	
	HF-6		6.		-				<u> </u>							_	LA		_										╎			+-			+			+	0	0.2	+.	15
	imen I		_		n	[	01	00			_	De			T		-	30	-	7		D	10	)	_	%	56	ìra		el	0	/ %S	ar	hd	+	c	%S	_	_	_		15. Clav
	HF-6		6.					25		-		).(			+	. (	).1		-						-			).(				88		_	╉	-		_		.9		, a '
	HF-6		8.					25				).:			1		).1		-							-		).(			_	85			╈			_		.9	-	
ł	HF-6		2.					00				).:			+		0.1			+								).(				81			+					.6		
ŀ	HF-6	4	4.	0	1										1		1.3			-	C	).1	20	07	,		_						_		╀					0		
	HF-6		6.														).2			1															┢					.8		
PR	OJECT		ate	d	W	etla	ind F	is I	Dri	llir	١g	P	rc	g	ar	n	- P	ha	s	e İ	-	_						ļ	0	B	N	Ĵ.	-			1	1	63			_	
		Hog	an	1.15	sia	nđ	ra	rm	<b>S</b> ,	<u>c</u> c				A					ric	ta								Ľ	JA	TI	E					1	/8/	99	9			

ş



	υ	.s.	SIE	VE ( 6	סרנ 4							ES 3/4	1/2	231	l 8	3	۸	e	6					VE 20						70	10	۹,	10	ا 20	0					н	YD	нс	٩C	IET	Er	۱			
00	Π			Ť	٦	ΠÌ	ĺΠ	Ţ	ή	T	Ť	1	T	1	Î	T	Ţ		η	Ť	ľ	Ť	Π	Í	ĺ	Н	Ĵ	, 	ſ	Ť	Т		Π	Π	Π	Т	Т	T	T			Π	Π	Π	Τ	Τ			
	Η	-			-			╉	+	-+		-		╢	╢	+	-	╈	+		$\vdash$			╫	+	$\left  \right $		7	•	+			╢		╟╋	-	┢	+					╁┼		1	┥		$\vdash$	
90	$\parallel$	_						+	+	-				$\parallel$	$\parallel$			+	-						+		_	Å	À	+			$\parallel$		4		-	+	+				-	H	-+	-		-	
	Ц																							Ш				1		L			$\parallel$										Ш	Ц	_				
00																	-		1											V																			
80	Π					T		T	Ţ	T				1	Ħ	T		T	T		1		1	Ħ									Ħ	T	T	T	1	1				Π	IT	Π		T			
						Ħ		$\dagger$	t	╉		:		╫	$\parallel$	╋		╞	╈		ŀ		┥	Ħ	Ħ	Ħ			Ŷ	╢			Ħ			╈	┢	<u> </u>	1			H		Ħ	┥	+			
70	$\vdash$				-	H		╉	╉	+		-		╢	+	+		+-	╋		-		-	╢	+	H				H,	-		╢	+	+	+	╀	╞	╉			Н	╟	H	╉	-+		-	
	$\vdash$					$\parallel$	$\left  \right $	+	-	+		_		-	$\left  \right $	╇	-	-	+		-		-	ļļ			4	_		ļ	<u> </u>		╢	$\left  \right $	_	╞			+			Щ	μ.		+	$\downarrow$			
60	Ц		-				Ц												1		ß	<b>.</b>								M																_			
								Ì																						H									Ì										
	Π					Π	Π		T	T				1	11			T			Γ		T	ø						ľ	T		Ħ		T		T	1			_			H		1			
50	H							╈	t	╉		-		╢	Ħ	$\dagger$		╞	ϯ		╞		+	Ħ	N	N	ź			╢	H		╢	H	+	$\uparrow$		-	╈	****	-		+	H	╉	╈			****
	┝┤	$\neg$			+	$\parallel$	$\parallel$	+	╀	+				╢	$\parallel$	+	-	+	+		-		+	╟	$\parallel$	$\parallel$	4	Y	Ł				╢	$\ $	+	┞	$\vdash$		╀		_			$\parallel$	+	+			
40	$\left  \right $				_		$\parallel$		1	-				$\parallel$	₽	1		-	+		_		_	-	$\ $	$\prod$			Ø	ł			$\parallel$		1	Ļ	_	ļ	_			$\parallel$							
					_																									þ	8																		
20																Τ														T	I	[	Π		T	Γ						Π	T	Τ					
30						Ì	Π	1		1		:				t	ŀ	t	╀		-		1	Ħ	Ħ				-	1	\$	t			╋	+		-	1		-	Ħ			╈	+			
	$\left  + \right $		_			╢	╉	╉	+	+				╢	╫	╉		╈	+	-	-		┽		H	$\left  \right $	+	-		╀		+	╢		+-	+	$\vdash$		+		-	╢	+	+	+				
20	$\left  \right $	-+			+		$\left  \right $	+-	+	+				╢		+		-	+	_			-	-	$\prod$		-			╀	-{	₩-	#			-						$\parallel$	+	-	_	_	_		
			_					_	1							ļ			-	_											1	Ŵ										$\prod$			1				
10			·															Ì												l																			
· `														Π	Π	T		Γ	Γ					Π	Π					Ţ		2	Š					_	T			T		T	T	T			
	1	1			1		Ħ	T	t	╞				Ħ	Ħ	t		T	t				T		Ħ	┥		-		t			Ť		+	-	-	-	-		╡	$^{+}$	$\dagger$	-†-	$\dagger$	+			_
01			l		10	Ш. О	LL	1	1_			:	1		U	1	<u> </u>	1	1	. 1			1	1	Ш		1			1		Ō.	Щ 1		1	L		L			).(	<u>  </u> )1			1.	1			).C
r		*****															GF	٦A	IN	SI	ZE	IN	I N	111	LII	M	ΕT	ER	S																				
		СС	DB	3LE	s							VE					1									NE	)							Į					SI	LT	0	R	С	LA	١Y	,			
l			- 1				-		1	se		_	TI.	ne	;		-	-	ars		_	me		_	m		L		f	in	e	-				_		_			_	_			· · ·	_		1	
				den	titi			2n	-+-					_								tic					-					N	10	29	6		LL	_		PL			Ρ			С	С		Cu
		1					.0					RL			_								_		_					_		Ļ					NP	2		NP	_		NF	>		1.0	)7		2.1
	-	- 1					.0		-+-			RL								_	_	_	-					_		_		╞				-	NP			NP			NF		+	1.0			1.9
		1 1			-		0.0					RL			_								*	_	_		_	-			_	-			4		NP	-		NP	_		NF		+	1.0			1.7
		- 1					.0 .0	_	-	۲	10	RL *			· ···														_	S	M				-		NP	'		NP			NF		+		96 0	+	1.7
	_	_	_	len	_	-					<u>1</u>	00	5A	191		*****	6		<u>c</u> 2	1		D			1 2	3r T	12		-	-			. r	~		1-	1		~		,	_	07	<u> </u>	1	).1 T	6		7.4
	· ·	-1					.0	· · ·	+			85		╉						+		~~~~				╀	~	••••				Ľ	-		av	/e				anc	-		%	Si				o C	lay
		-1				3.					_	85		╉			.2	2		+-		).' ).'	_			╀			0:	****		-		0.					-	8	$\downarrow$					5.			
		-1				5.			+			85		╉			.2			+		). ).^	_			╉			00	_				0.			+		5.							4.			
		-1		•••••		7.			╉			85		+			.1			╀		). ). '				+			1 )9:			┝		0. 0.			+			4						4.			
		-1				<del>.</del> 9.			╈					╉			.5			╀		). ). '				╀			)89			┝	_		<u> </u>		+	9	<b>.</b>	4	+					4.0			
PR			ĊТ	ls	ol	ate	ed	٧	Ve	etla	an	ds	Ď	rill	in	g	P	ro	gr	an	n	- F	'n	as	ie	Ļ,			.03	-		Ι.,			10	)F	1	10					1	16		7.8	0		
				H	og	ar	11	sl	an	nd	Fa	rn	۱S,	C	0	llio	er	С	οι	IN	ty	, I	Flo	ori	da	a									D	Ă٦	ΓË		•			_	1/8	3/9	<u>.</u>	)		-	
																G	iF	۲A	۱/	)/	٩.	TΙ	C	) [	I.	C	:1	JF	۲۱	/	ES	3					-												



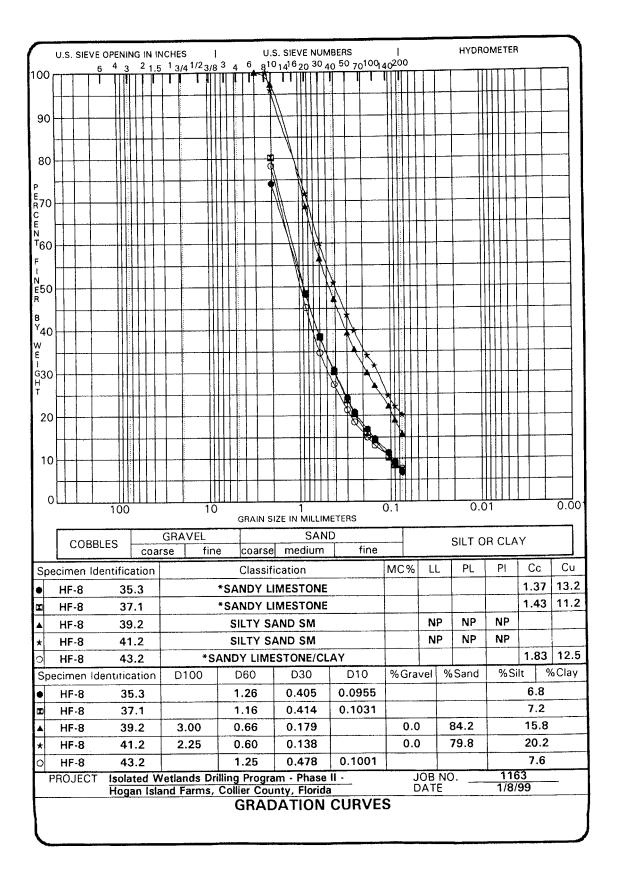
_	U.S. 9	SIEV			IN 3					s /4 1	12	3/8			1	6			5. 5 ) 1 d								<u>م</u> 1	00	۵r	 20	0					ΗY	DR	0	ME.	TE	R				
00		T	Ť	ŢŢ	ÎП	Π	I		Γ	14	Γ	Ī	Π	Π	İΠ	T	ГÎ	9	4	Į	Í		A.	Ĭ	T	ή		Γ	Ĩ	Í	Τ	Т			Т		Π	T	Τ				T		
		+		╀┼╉		+	╉	+				₩	┢	H		-	-	╀			Î	K	-  <u>'</u>	ľ	╈		┢		+			┢	-	-	╉		-#	┢	+				╀		-
90		+		┼┼┤			+	╉					+		-			+			╢	H	¥	1	H		$\vdash$		+		+	╞	-		╀		╢	+	+	$\vdash$	-		╀		-
	┝╌╿╌╿╴					-		-				Ш						1				1.	4	4	Ŧ				4			1	$\vdash$	_	╞		╢	$\parallel$	4		_				_
80																					$\prod$			V	1																				
00																																													
							T	1				Ш		Π		-		T		-	Ħ	Ħ	T		T	Γ			T			T													
70	$\left  + + \right $		•				+	+				Ħ	H	Ħ	T		-	╈			$\dagger \dagger$	$\mathbf{H}$	╉		7	4	╞		-		╈	1			╈		╢	Ħ	-				╈		
: 	┝┼┼┼		•		+	$\left  \right $	╀	╈				╢		$\left  \right $				╋		-	╫	╫	+		┨	Ŧ				-	+	╀			╀		╢	$\parallel$	+		+		+-		-
60		_		$\left  \right  \right $		-	+	+	_			$\parallel$	-	$\left  \right $				+			Н	╢	+	+	╢	+	<u> </u>				+	1			-		╢	$\ $			4		+		-
								_										1			Щ	Ц	1	-	1						$\downarrow$	L			1			Ļ			_				_
50																										φi																			
50				П								$\left\  \right\ $			Ī						I	IT		ſ					$\Pi$		Γ		$\left[ \right]$					$\ $		T	T				]
		+				T	$\uparrow$	$\dagger$					1		T			$\dagger$			Ħ	Ħ	ϯ	1	╈	t				$\parallel$	$\dagger$				$\dagger$		$\parallel$	Ħ	11	1			†		1
40	┝┼┼	+		╢		$\left  \right $	+	╀	-			$\parallel$	+	$\left  \right $				+			╢	╫	╀	-	╉	-{	$\ $		+	╢	╉	$\left  \right $		•	+		╢	╢	╫	+	-		+-		-
'	+ +	-+		╢		4	+-	+				$\ $	╇	$\left  \right $				╀			╢	$\parallel$	+	-	+	{	ł		╢		+	$\left  \right $			╀		╢	╢	$\parallel$	+	-		+		-
30	$\square$						-											1			$\parallel$	Ц	1		_		Ï		4		1	Ļ					$\parallel$			_					
																											8																		
~~																											U	ĺ	Π																
20							T	1				III	T					$\uparrow$			Ħ	Ħ	t	Γ	T	_	Ť	N.	1	Ħ	t				ľ				Ħ		1				1
		+				╈	1	╉					╉		+			+		1	╢	╟			╁		+	f	╢		╀	Η			┢		╢	╟	$\left  \right $	╉	┥		┢		
10		_			+	+	+	╋				$\left  \right $	+		+			╀╴		-	╢	H	+	-	╉	_	_\$		3		+				+		+	H	$\left\{ \right\}$	-	+		-		-
					$\left  \right $	+	-	+	_		_		+		+	-		-		_	╢		-		+			7			+		-		-	•			$\prod$	-+-			-		_
ol				Ű								Щ								1									1	ř															
			П	00							I	0		c	SR.	All	N S	IZI	E 1/	Г И И	ліг	LIA	ИE	TE	R	5		C	), 1							0.	.01							0.0	00
ĺ			LES				1	GF	ł٨	VE	L										S,	41	١D	1	-					Τ					~	т.	~ ~		 > 1		 /				٦
		/00				co	ar	se		_	fi	ne			СС	a	rse	2	m	ec	liu	m				fi	ne	)		1	-				511	.T (		( (		A 1	(				
pec	cimen	n Id	entif	ica	ati	or	1							(		as	sif	ica	ati	or	1								M	٥٥	6		LL		F	۲		F	יי		С	c		С	u
	HF-8			1	.0	)					PC	0	RI	_Y	<u> </u>	3R	A	DE	D	S		ID	S	P								1	NP		N	IP		N	P		1.	17		2.	1
	HF-8				.0		$\downarrow$				PC	00	RI	<u>-</u> Y	(	SR	A	DE	D	S	AN	ID	S	P								1	NP		N	IP		N	Ρ		1.	16		2.	3
	HF-8	-			.0												A		•		_				<b></b>	_			• • •			1	٧P		N	IP		Ν	P		1.:	25		2.	2
· · · · · ·	HF-8			_	.3					-						~~~	A	_		_		_						_					NP	+		IP		N				01	-	1.0	6
· · · · · ·	HF-8				1.1	_	+		~ 4		_	00			-		A	DE	-			١D	S		-			_					NP	_		IP		N		-		06	_	2.(	
			entif				1			00										)3	- · ·		-	_		10		+		Gr	~	/el	-			nd	_	%	6S		_		%(	Cla	y
	HF-8				.0					35		+-		0.		· · · · ·			0.				+			09		_		0.	_		$\downarrow$		6.8		+			_	3.				
	HF-8				0.0		+			35		┼		0.					0.				+			99				0.					5.8						4.				
	HF-8 HF-8				.0 .3		+	-		35 35	_	+-		0. 0.		_	_		0.						_	06		_		0.			+-		5.		-			_	4.				
	HF-8				.3 .1		+			35 )0		╀		0. 0.		_	-		0. 0.				+	_		51 37		+		$\frac{0}{0}$			╞		8.		+				1.			-	
	OJEC	CT	lso				Ne				Dr	l illi										e			. 1.	3/	2	1		0.			N		6.4	+		- 1	16		3.	6			
		- •	Ho	ga	n	Isl	an	d	Fa	rm	s,	С	ol	lie	1	Co	DUI	nty	Y,	FI	ori	da			-						D		ΈE	0.				1/	8/	<u>99</u>	)				
													(	G	R	A	D	Δ	T	Ĩ	٦Ā	J	Ĉ	Ē	IÂ	١Ū	F	S	_								-								

U	I.S.	SI		OP			G	IN	IN	CF 1	HE	5 4 1	12		3			6			s. D₁									<b>_</b> 1	00	141	<sub>0</sub> 2	 00	)					H	YD	RC	D∿	ΛE.	TE	R					
00		<b></b>		5	ŧ П	3 			. <u>5</u> T	Ť	3/	4 '	T	3/8 	Π	Π		Ť	Ē	Ŧ		4	Ŕ	Į,	Ţ	Π		T	ή	Γ	T	Ī	Ĭ	I	Π	٦			Т			Π	Π	Т	Π			Ţ			
-		╞				+	$\left  \right $	-	-		-				-	$\square$		-		+			╢	P	1		5	+		-			H		-				╉			╢	╢	╀	┢		-	+			
90								4	_		_									4					-		A	Ť,	2 2	-		_		:			-	-	╉			#	$\left  \right $	+-	-	-		+			
																		_						Ц			Ц	N	1	Ι,				-				-	1			╢		$\downarrow$				_			ļ
																											1	V		Ň												1			L			┛			
80-	Γ				Π									Π	T													Ì		Ņ									1												
		1	1			-		-						Ħ	Ħ	Ħ	:			1				T				ħ		1					Τ			ſ				Π			Γ						
70		+	+		╫		+	-	$\neg$		-			╢	H	+		-		┥			╢	+		┢		+	┞┤	Η			H		┢	$\vdash$	-		+			Ħ	Ħ	t			T	-†			1
	╞	-	-		╢		+-				-			╢	╟	+	_		-	+			+	+		╀	┝	╉	è-	┞	┞	_			╀	╞	╞	┢	+			╢	$\parallel$	+	+-	$\vdash$	+	╉			
60-			_		#		$\left  \right $			L	_			$\parallel$	╢	╞	-		<b> </b>	+				+		╀	-	+	+	-	┞	-			╀		-	-	+			╢	H	-	╀	┝	-	+			
					$\parallel$									1	$\prod$								_	ļ		-			4	1	Ļ				4.	-		<b> </b>	4			#		+		-	-	4			
50 -																												$\downarrow$	1	ļ	Â		ļĮ.			L		_				$\parallel$						_			
10-					Π	I	Γ							$\ $																ľ	ĺ																				
, †	t		+			Ħ	1			ł				Ħ	tt	T		1	T	1			T		Π	1		T		ſ			I						T			$\ $	Π	T	Γ			Ī			
40	+	+	╉		$\parallel$		╈	Η	-	┢	ł			Ħ	╢	╈		†	$\dagger$				T	H	Ħ	t	+	+		t			Ħ	t	1	t	T	1-	╡			$\parallel$	t	Ħ	t	ŀ	T				1
v	┝	┢	+		$\parallel$	╞┼	+	$\left  \cdot \right $		-	_	-		╢		╉			╀				+	╟	╢	+	+	+		╉	$\left  \right $		╫	H	+		┢	╈	+			$\parallel$	Ħ	┝┼╴	+	$\uparrow$	╀	+			1
30		-	-+		$\parallel$	$\left  \right $	-				_			╢	╢	+	-	-	-	_			-		┝	╉	+	+		╂	dia 1		╢		╀	-	╞	+	-+			╢	+	$\left  \right $	+-	-	┝				$\frac{1}{2}$
			_		4					-	_				$\prod$	-			-	_	_		-	-	$\parallel$	1		-		P			╢		-			-	_			╢	+		+	-	-	_			
20																														Ľ	Ц			[:]		L	-						_			-					
20																																																			
	-				1		Τ	Γ			-			Π	Π	T		Γ	Ι						Π		******				•	U	N				ļ														
10	+	-		-	Ħ		t			ſ				ļ	Ħ	t		T							Ħ	T				T		ſ	Ŋ	U	T		Γ								T	Γ	Τ				]
-	+		+		╢		╈							Ħ	Ħ	t	ŀ	T	┢	-				ŀt	Ħ	T		1		t		-4	Î	ġ	T	t	ſ	T				1		Ħ	T		T				1
0L	<u> </u>	<u> </u>	1.	1	00	) )	1			I				10	11	1	ľ		1				1		1.1		<u>.</u>			_		0	.1	n	1	J	4	1			0	.0	1	ш	1.	1	1		i	0.0	0 0
r						_											G	RA	IN	SI	ZE	11		_	_	-		ER	S																						٦
	C	0	BBI	_ES	5	-		0.2	) ars			VI		in	<u> </u>	_			ars	20	[	m				-	) T			fir	ne			-					S	IL	Т	0	R	¢	LA	١Y					
L Spec	im	<u></u>	Ide	onti	fiz	1		-	T		-		-		-	_		-	ss	_	<u> </u>		_	-			_					Tr	Ń	C (	%	Ē	L		T	P		T		PI		1	Ĉ	c	T	С	1 1
· · · · · · · · · · · · · · · · · · ·	HF-					.a 1.			┼				D	~	<u></u>	21	-	-		-	_		-				SP	,			-	ŀ				┢	N		+	N		+		NF		1		12	+	1.	
	ידר ארי	-				<u>1.</u> 3.	_		+					-			-		R/				••••									╉				╞	N		╀	N		+		NF		+		)4	+	1.	
	-IF				_	<u>5</u> .	·		+				-	-					R/	_												$\uparrow$	_		_	╞	N		$\dagger$	N				N		+		96		1.	
	-IF					7.			F	-0	00	RI	_							_							_		SP	.5	ŝM	t			-	t	N		+	N		-		N	~			03	+	1.	.8
· · ·	łF					9.			Ť	-			_				• • •		R/				-		• •		_					t		_		t	N	Ρ	+	N	Ρ			N	P	-	_	95		1.	.5
Spec		····	ld	ent			-	n	t		D	10	О			I	26	50				Ľ	)3	0				C	01	0		1	%	G	ra	ve	el	9	65	Sar	٦d			%	S	ilt		(	%(	Cla	iγ
	٦F	-8			1	1.	2				0	8	5			(	).:	24	ŀ			0.	1	87	1		C	).'	12	9	1			0	.0	)			9	3.!	ō						3.	5			_
n }	٩F	-8			1	3.	2				2	00	)			(	).:	20	)			0.	1	51	1	T	C	). '	11	1	2			0	).C	)			9	3.:	3	Ţ					1.	7			
L I	HF	-8			1	5.	4		ſ			8					_	16		_		0.					_		09	_	-				.0	_				5.1								2			
	٩F						3					00		_				16				0.			_	_	~~		80			1			).(				_	3.8								.2			
	HF		_				2					.0			_			16				0.							10	)5	4			0	).(			Ļ		7.4	4							6			_
PR	OJ	IEC	CT	is H		at	ed n I	V  el	Ve	etl vd	ar F	nd: ari	3 [ ne	Dri		ng	i F	r i	og Co	ra	m nt	-	PI F	na Ioi	se	e I Ia	<u> </u>	•									B		0.	-	-			1/	16	53 '99	9				
					~5	Jul		101			-			· /	-													Ū	R	V	Έ	S					-				_	-									
																		. •	. •	_	-	. •	-	-				-		Ĩ		_																			

•

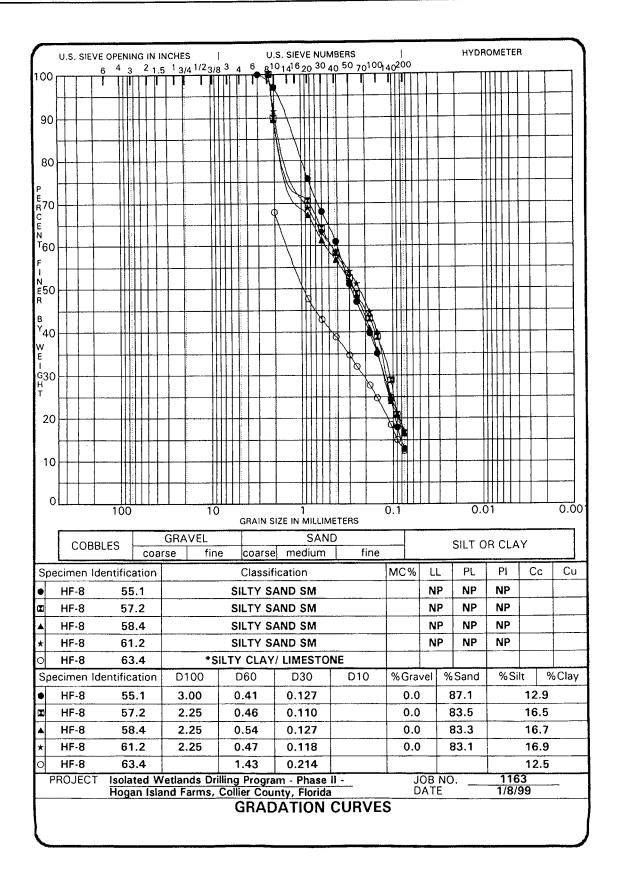
P	ROJE	こして	ISO	lat	ed	1 1	Ne	tla	Inc	ds	D	rill	lin	10	P	ro	יהכ	rar	n	- 1	Ph	12.	S P	1									in	۱P	N	$\cap$					11	61	5				
			1.									1										JU		1			)8	3.	כ						1								7	.8	\$		
L	HF-				0. 0.		+-		0.8	55		╀			).1 .5			+		0. 0.	_	_		+			)9	_				D.(	0		-	9	5.	4	$\downarrow$					ŀ.e			-
ļ	HF-				.0		+-	~~~~~	3.0			+			).1			-+-		0.		·		+			1	_				D.			L		5.		$\downarrow$					ŀ.€			
	HF-				.0		+		0.8			+		~	).2					0.							0				(	Э.	õ			9	5.	5					4	1.5	;		
	HF-				.0		$\perp$		0.8					_	).2				1	0.	15	54			0	.1	0	29	9		(	э.	0			9	4.	8	Ţ				5	5.2	2		
pe			denti	fica	iti	on	Ţ	C	01	00	)			ſ	D6	60		Ι		D	)3	0				D	)1(	0		%	60	Gra	av	el	Γ	%	Sa	nd	$\uparrow$	(	%5			T	-		
	HF۰	1			0.0		+				βA							_					_					_					┦			+			+			-+	_	.1			7.4
-	HF-				.0			PO		~~~~									-							_				-			+		NP NP	-	-	IP IP	+	-	IP IP	+		.0 .9			.7  .7
	HF-				1.0 1.0			PO PO		••						_						_								-					NP	+								.0			1.9
-	HF-				.0																_	· · ·						~~~~					-		NP	_		IP	-		<b>IP</b>	+		.0			2.1
ipe I			denti				+		 						*****			sifi												N	10	?%	6		_L			֊լ	Ţ		ΡI			Сс	;		Cu
			BLES			-	ar	se			fi	ne	3		c	20	ar	se		m	ec	_	_				1	fir	e			1					SII	_T	01	R	С١	_A	Y			<u>.</u>	
					_		_(	GR	A	VE	L				Ť							S										Γ					_							-			7
•			1	00							1	Ö			Ģ	8/	1	IS	175	: 11	1		L.		<u>.</u> т	50	ic.			0.	1	<u>.</u>	•					C	0.0	1	<u> </u>	4- <b>-</b> -	4		ملسبه	C	0.0
C	ьЦ				Π		Γ		T			Π	Π	T		T					1	T		Π	1	1		Ť			T		T				T			T		1		t			
													Π	T	T	T	T		Γ			Π	Π	Π	1			Ť		Z	Ť,	÷ •					T			T		T	1	1	1		_
10	,Ш_	ŀ																				I			ľ			T		1		ſ	Γ				T							Γ			
	۱ ا																													$\mathbb{N}$								_									
20	, ⊥			$\parallel \mid$				_							ŀ	$\downarrow$						$\parallel$																									
!	<u> </u>						$\downarrow$					$\parallel$			-	1			L			$\parallel$			4				1		Ц		Ļ														
30	┉					$\mid \downarrow$	$\downarrow$	+					$\parallel$	μ	-	+	_	·	L								 	1	•	<b> </b>							1				$\parallel$			1			
<b>/</b>		<b>_</b>		$\parallel$		μ	+	+	_				$\parallel$	$\parallel$	-	+			L		_	$\parallel$			-			R	1				-	Ļ							1	1					
, 4(	$\downarrow \downarrow$	+		╢			╀	+				$\parallel$	4	$\left  \right $	-		4				_	$\parallel$	$\downarrow$		-		Ø	Ą		1			+				-				$\prod$	-		-			
L 3						$\parallel$	+	+	-			$\parallel$		╟		-	4		-			$\parallel$			Ø	Y	-	-					+				+		_			-	-	╞	_		
50	> <u> </u>   <			+	+	╟╟	╀	+				╢	$\parallel$		-	+	-				-	T.	k	k				-			╟						-	•	-	$\ $	$\prod$	+		+			
	$\left  \right $	╞		$\parallel \mid$	+	╟	+	_	_			╢	+		-	+	+		-		$\geq$	H	+					ł			╟		+				+		+	$\parallel$	$\parallel$	╇	╀	+-			
6	ו∦י	+			+	╟	╉	╉	-			╢	+	╢		╉	+		P	7			╀	Η		_		╢	+		╟	╞	╀	┞			╀			╢	$\parallel$	╀	╀	+			
				╢		╟	+		-			$\parallel$	+	╟	+	+	-		+				╉	1				W	+				+	╞	-		+		-	╢	$\left  \right $	╋	+-	╀			
7(	י <b> </b>  -	+		+	+	╟		+	-	-		╢		╢		+	+		╞		_		╋	+		-	H	H	1				╀	┢		$\vdash$	+		-	╢	$\left  \right $	+	╉	╉	_		
) :		+		$\parallel$	ſĦ	╟	╉	+	+			$\parallel$	+	╢		╀	+		┢				+				1	H			╢	╢	╉	t		-	╈			╢	$\parallel$	$\dagger$	$\dagger$	╉			
80	가	+	<b> </b>			╞╂	+	╀	-			$\parallel$	+	╢	+	╉	+		+		_		+	┢	H			ţ			₩	╢	╉	┝		$\vdash$	+		+	╢	$^{\dagger \dagger}$	+	╉	╉			
				╫	Ħ	H	+	+	+			$\parallel$	+-	╞┼		╉	┥		$\uparrow$				+	$\dagger$		•		$\parallel$			╢		$\dagger$	+-	$\vdash$	<b>†</b>	╋			Ħ	$\dagger$	1	╋	$\dagger$			
90	忭	-			T	Ħ	+	+						Ħ		1	-†		1				t			Ĩ	ß				Ħ		t	+	1		1		+	Ħ	$\parallel$	$\dagger$	1	1			
~		1				Ħ	†	+						Ħ		+			T				t	t	1	Ż	k	+			Ħ	Ħ	t	t	1	1	1			Ħ	Ħ	Ť	T	T			
00	Ϋ́Π		Π	Ţ	Π	Π	Ť	5	ή	ŗ	T	T	Ī	Π	Ţ	T	η	Ť	Γ	T	Т	Ī	T		Ű		Γ	T	Т	1	Ţ	I					Τ			Π	Π	Τ	T				

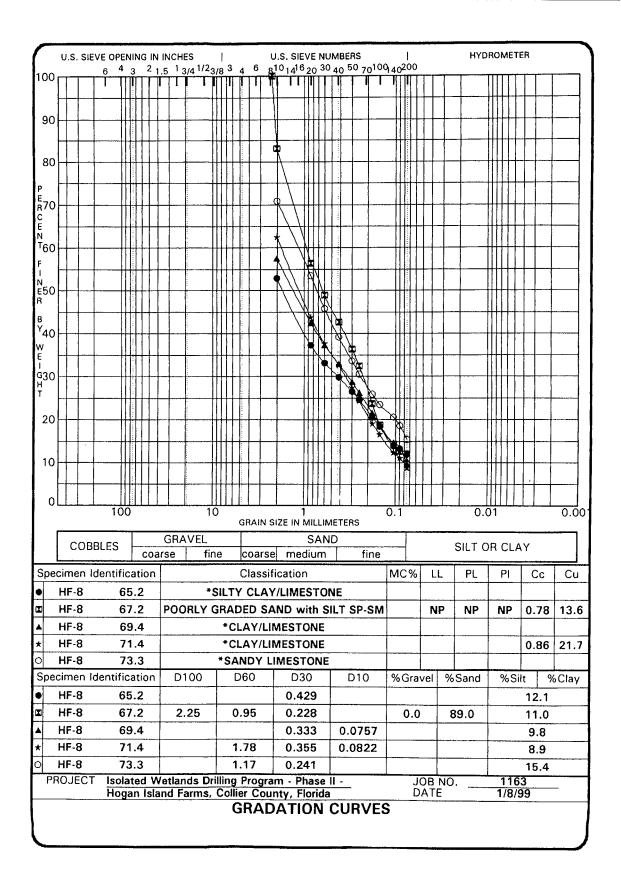
1

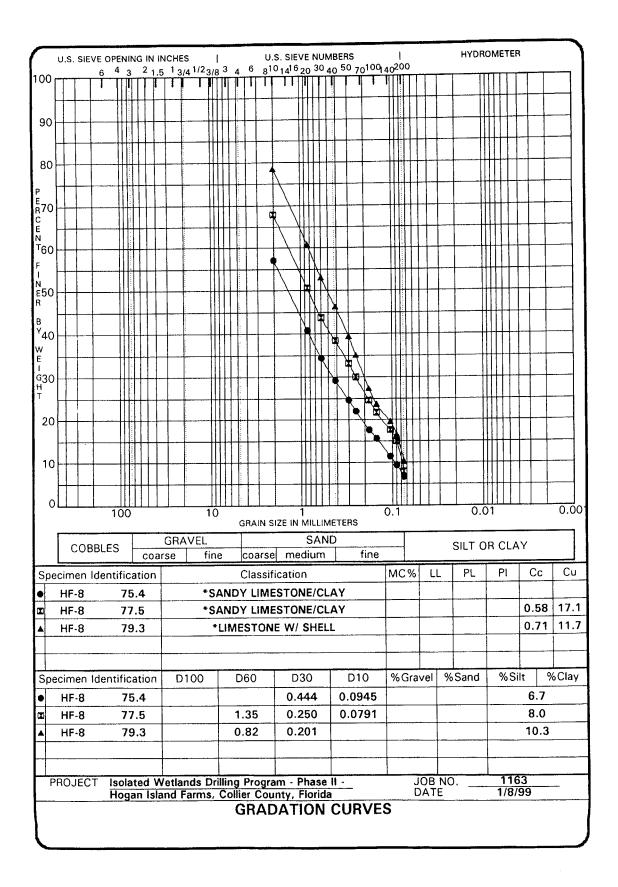


U.S. SIE	VE OPENING IN 6 4 3 2 1		  /8346	U.S. SIEVE N		0.4200		HYC	ROMET	ER	
	$\frac{6}{1}$ $\frac{4}{1}$ $\frac{3}{1}$ $\frac{2}{1}$										
90									╊╋╋╋ ┲╋╋╋		
				<b>*</b> \\					╎╎╎		
80											
р Е70							┝┼╍┾╸		╫╫┼	+	
70							$\left  \cdot \right $		╋╋╋	•{}}	
C E N				+ \ \					╫╫┼┼		
<sup>T</sup> 60									╫╫┼		
F 1 N										+	
E50							+ +				
B H		-		<u>+</u>					╫╫┼┼		—–
<sup>4</sup> 40											
					$\mathbb{N} \mathbb{V}^{\mathfrak{n}}$				╎╎╎┝╄┼		
330 										$\left  \right $	
										+++	
20				+							-
								+		<u> </u>	
10											
0											
· <u></u>	100	10		1 5IZE IN MILLIN		0.1		0.0	01		0.0
СОВЕ		GRAVEL		SAN	·			<u></u>			
	coa	rse fin		e medium	fine			SILT C		ι Υ 	
1	dentification			fication		MC%	LL	PL	PI	Cc	Cu
HF-8 HF-8	<u>45.2</u> 47.0		ANDY LIMI ADED SAN				NP	NP	NP	1.46 1.25	16.0 12.7
HF-8	49.2			AND SM			NP	NP	NP	1.25	12.7
HF-8	51.2			AND SM			NP	NP	NP		
HF-8 Specimen Id	53.2 lentification	D100	D60	D30	D10	%Grav	NP	NP Sand	NP %Si	+	Cla
HF-8	45.2		1.25	0.378	0.0781			334110	%Si	9.6	Clay
HF-8	47.0	2.25	0.89	0.279		0.0	1	87.8		12.2	
HF-8	49.2	2.26	0.60	0.174		0.0	1	33.6	·	16.4	
HF-8 HF-8	51.2 53.2	2.25 2.25	0.60	0.152		0.0		34.2		15.8	
PROJECT	Isolated W	etlands Dri	0.48 Iling Progra	0.130 m - Phase	-    -	0.0 JC		36.2	116	13.8 3	
	Hogan Isla	nd Farms,	Collier Cou	nty, Florida		D/	ATE		1/8/9	9	-
			UNAD	ATION	COUNCES	כ					

3

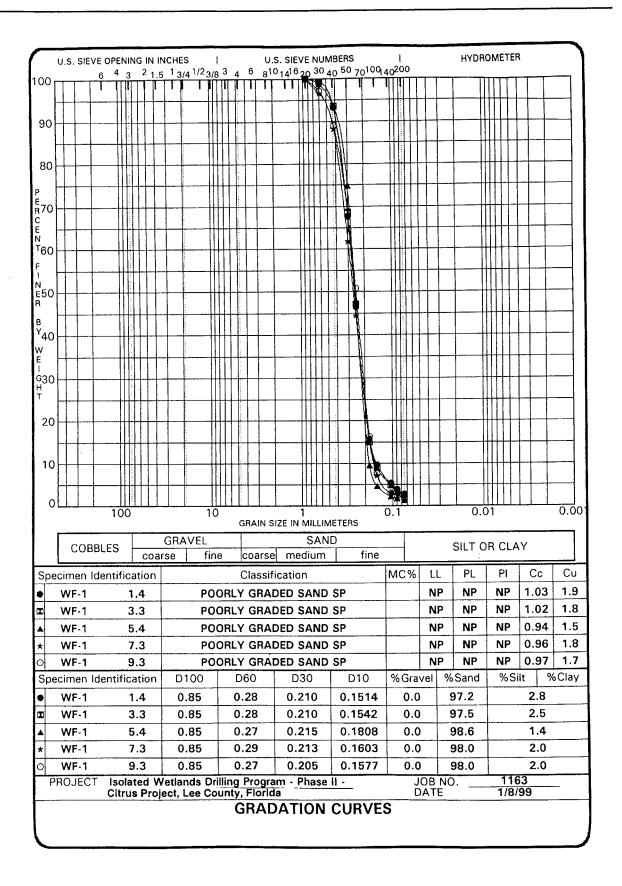


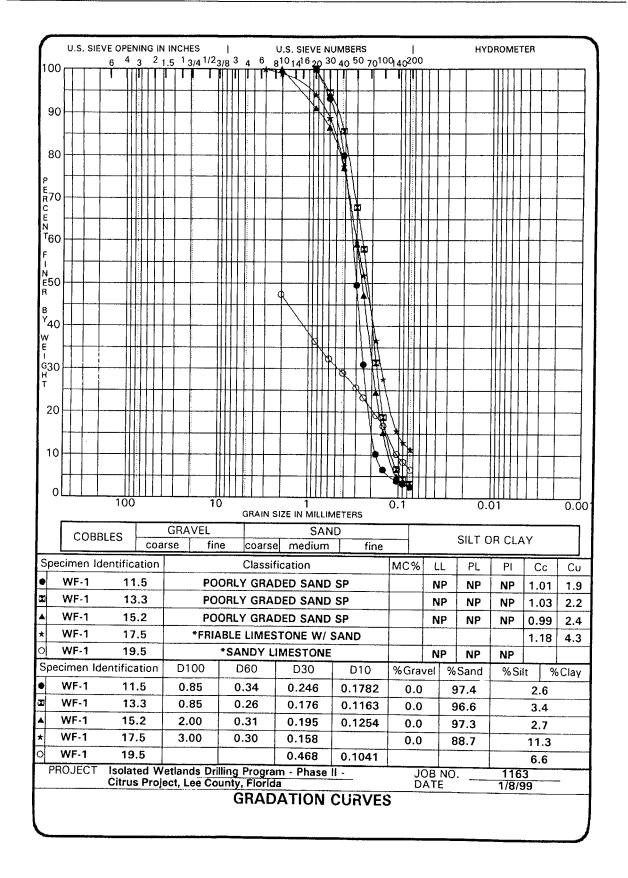


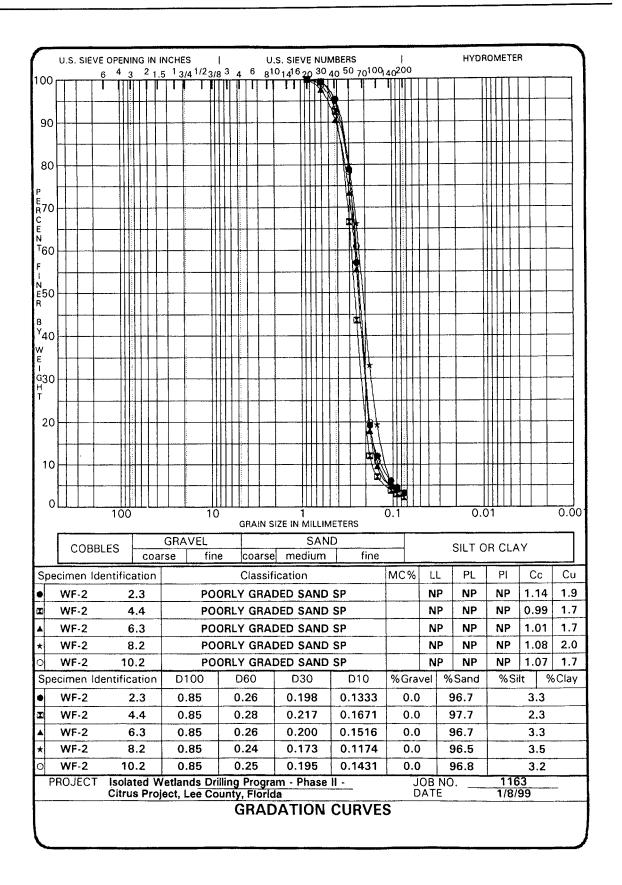


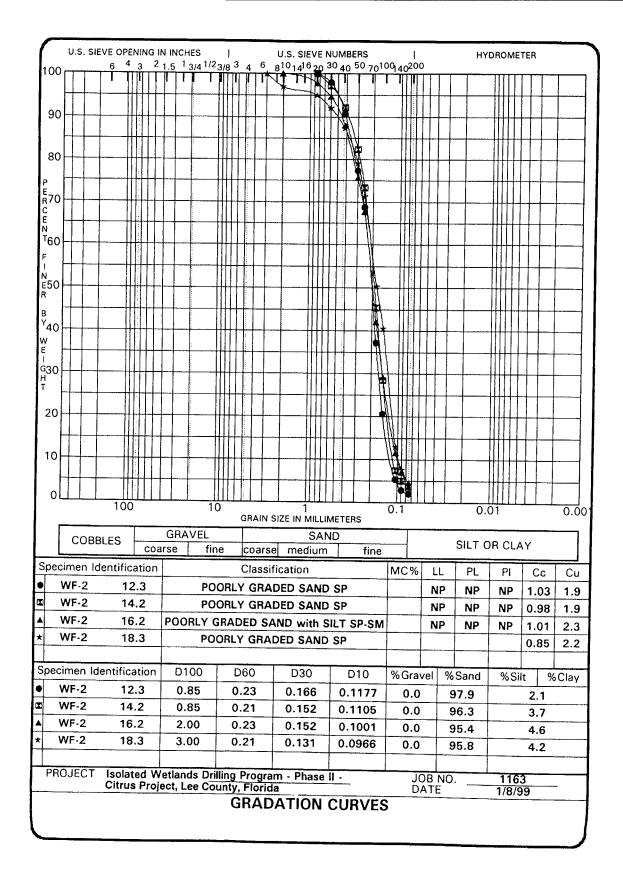
## **APPENDIX D**

## **Citrus Project Field Notes**

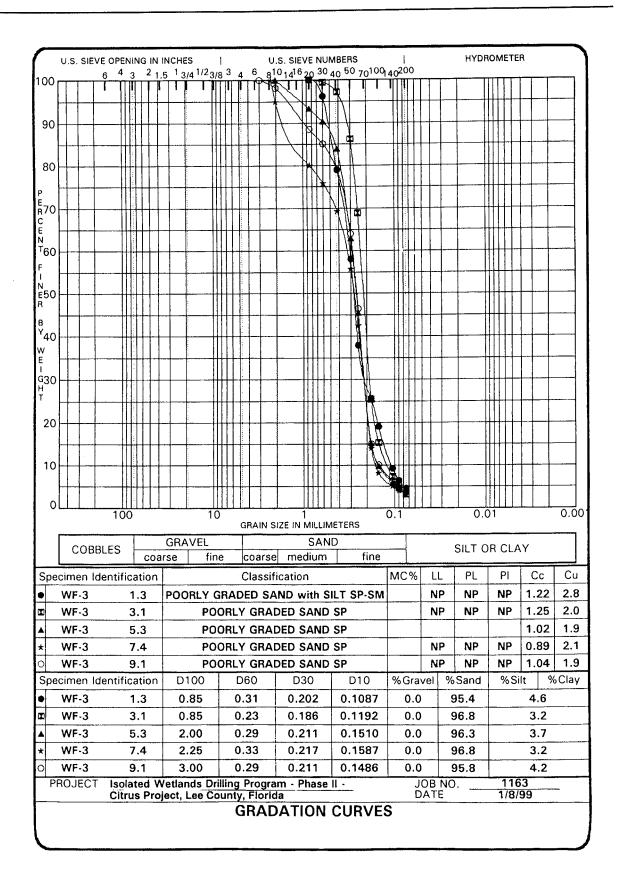




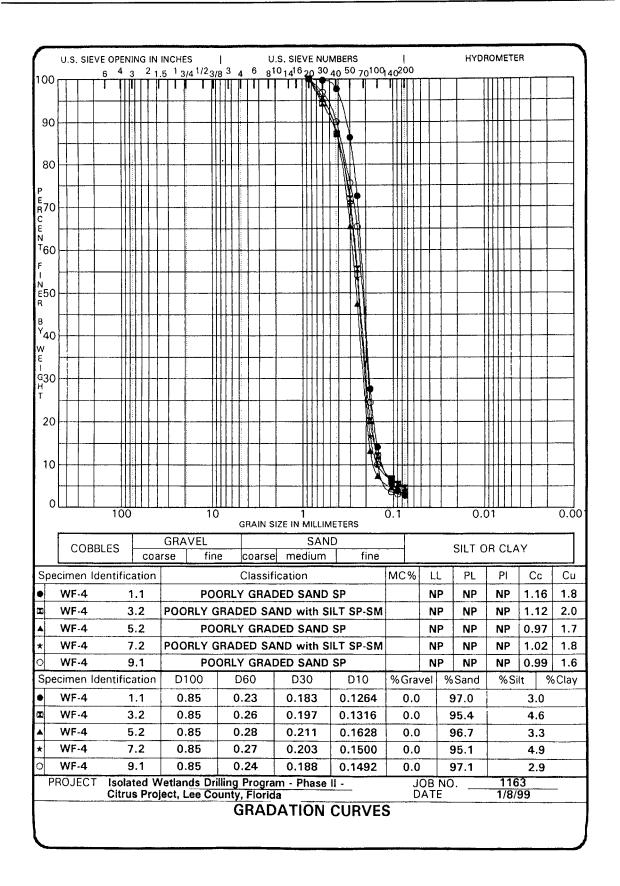




D-5



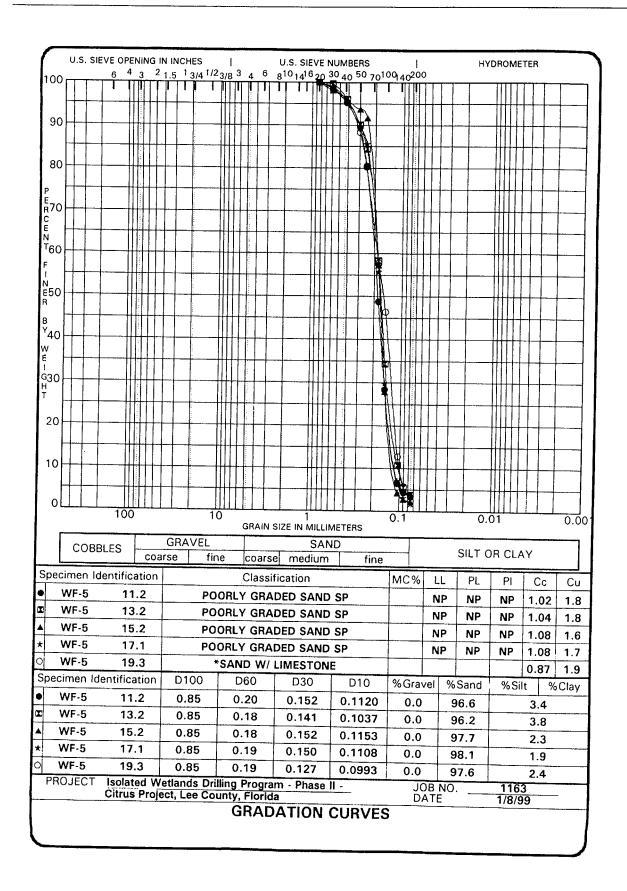
PF	(O)	ECT	lsc Cit	rus	teo s F	d /	Ne	tla ct,	nd Le	s i	Dri Co	ui	nty	1,	FI	or	id	a	<u>.</u> Т						-						J D	ÕĪ A	3 N TE	٩C	).			1	11 /8	63 /9	3			-	
	WF			19									(	0.1	72	2			0.	20	6		t	0			57						+			_					3	3.7			
	WF			17			+					-		o.:					0.	_			- <del>-</del>				2	+					+				+					3.4 3.9		<u> </u>	
~ -	WF			15			╀		-			┝		0.: 0.:			-	_	0. 0.		_		+		· · · · ·	42	25 37	+					+			-	+					3.1			
	WF WF	_		11 13			+					-		0.					0.				+				23				•		$\downarrow$				_					2.2			
			denti				1	C	10	00		-		D						30	•••••					10			%	G	ra	ve	!	%	S	and	T	(	%	Sil	t		%	CI	ay
	WF	-		19					*****	_		N	_				łE	٤L	, L			S	т		-																0	.4	- 1		.7
	WF			17	.0	)					_	_				_		_	., L	_	-		_		_							t			$\uparrow$		+					.8	-		8
	WF			15			+					<u></u>							SI									+				$\vdash$			+-		+					.0. .9	-		 1
	WF			13	• • • •		+												SI						• • • •		· ·	+				┝			+		+			-		.9 .0			7. 8.
pe	WF		denti	tic 11			1						*						ati SI									+	M	<u>C</u>	%	-	LL	-		PL	-		PI	_		Co			<u></u>
				-			ar	se			fir	he		-			se		m			m				f	ne	-		1		Ţ				LT				_A	Y				
		<u></u>	BLES	••••			-	GR	A١	/E	L			T			• 3		E 11		S			_		د 				Т							~								7
0	<u> </u>		1	00	<u></u>	L d-a	-		E.		1	0	Ц	 ~					<b>-</b>	1	۱.L.	ц.		<u>ل</u> ــــــــــــــــــــــــــــــــــــ			L	(	Щ. Э.	1		<u> </u>	1	1		C	0.0	1	L	L.,	۰	1	_	C	.0
~			•		il-		$\uparrow$	1	+			╫	$\parallel$		1	+		+		+	╟	╟	+	-	╎			-f.			H	$\dagger$	╀	┢	╉			H	╟	+	┢╸	+	+		
10	<u> </u>			$\parallel$		┝╂	╋	╞	+			╢	+		-	+	• • •			+	╢	╢	╉	+	╉		H				╢	╈	+	+	+			╟	╟╋	+	┢	+	+		
	╞┼╴	-   .			:	$\left  \right $	+-	+	-		_	╢			+			┢		+	$\parallel$	╢	╉		╉			P			╟	╉	+	┢	-		+	╟	╟┼	┢	-	+	╉		
20		+		$\dagger$		∏	+	+	_			$\parallel$		$\parallel$	┥			+		-	╟	╟	╉	+	╉		1		+		╎	+	+	+	+			╟	╟	╀	┢	+	+		
	+	+		$\parallel$		┝┼	+	+					ł		+	┥		+			╢	$\left  \right $	+	:	+		6		+		╢	╉	+	╞	+		+	╟	╟	+-			+		
30	Ħ					╟	+	+			-	╢	╀					+		┥	╫	$\left  \right $		+	+		┞		+		╢	+	┿	+-	+		+	╟	╟	╀	-	┢	+		
	$ \uparrow  $	+		$\parallel$		H	+		-		_		╈	$\left  \right $		-		╉		-	$\parallel$	╢	+	-	+		┢		+			+		+	+		-	╟	╢	+	$\left  \right $	+	+		
, 40	+					╟	╉	+			_	+	╉	┢	+			+		-	╢	╢	+		+	₩	-		+			+	+	+	+		-+	╢	╟	╀	+	╀	+		
	$\parallel$			$\parallel$		┝┤	╀	-	-			+	╎	╟	+	-		+		-			$\left  \right $	-	\$	#	+		+			╉	+	╀	+		-+	$\parallel$	╟	+-	┝	┢	-		
50		+		$\parallel$			╀	+-	-				╉					╀		-	╫	H	$\left  \right $	ĥ	ď	ŧ.	┢		╉	╟		╉	╉	+-			+		$\parallel$	+	┢	+-	+		
I	$\parallel$	+		$\parallel$		$\dagger$	+	-	_		_		╉					╉		-	$\parallel$	+	╞	8	ł	╢	┢		-	╢	H	+	┼	╈	┥		+	╢	╞┼	┢	╀╴	+	+		
60	$\parallel$			╢		╎┤	+	+-	-			$\ $	+	$\left  \right $				╉		-	Ĥ	ł	$\mathbf{k}^{+}$	ł	$\uparrow$		╞		-		H	+	╉	╋			+	╢		╉	┝	+-	+		
	$\left  \right $	+		╢	$\left  \right $	╢	+	╉	-			$\ $	+	┢				+	<u> </u>	$\left\{ \right\}$	$\parallel$	1	Ņ		$\left  \right $	$\vdash$	-		+		H	╉	+-	+			+		╢	╀	+	+	-		
70				$\parallel$		$\ $	+	+	-			#	-	$\ $		-		╀			₩	Ĥ	$\left  \right $		¥,	<b> </b>	-		-		+	+	+-	+	_	<u>.</u> .		╢	$\left  \right $	╉	+	+	-		
•	$\mathbb{H}$			╢		$\left  \right $	+	+	-			ł		$\left  \right $		_	 	$\frac{1}{4}$	4		╢	+	Ĥ	X	H				+			-+		┿				╢	┼┼	╉	+-	┢	-		
80	┢┿	+				$\ $	-	+	-				╞	$\left  \cdot \right $	-			$\frac{1}{1}$			ĥ	X			-		-		-			4	+	+				╫	$\left  \right $	╀	╀	+	-		
								+-	_				+	$\left  \cdot \right $	-			Ŧ	4	X		ŧ		<u> </u>	-				_			-	+	-				╢	$\parallel$	-	╀	-	_		
90				╢			-	+-											_	_				-	_		╞		_			_	+	+			_	$\parallel$	$\prod$	+	-		_		
			ļ	╢			+		_				ļ			-		4	-					-			-		-	H			4.	+			_		$\left  \right $	+					
00	' <b>r</b>	1	6	4	3	n	-h	1	3	4	Т		<u> </u>	П	'n	Ť	г'n	ΓT	Ť	Π	Î	Π		<del>T</del>	Ť	. /	<b>T</b>	T	T	'n	T T	П	- <b>T</b> -	T				Π	TT	Т	Т	Т	-		



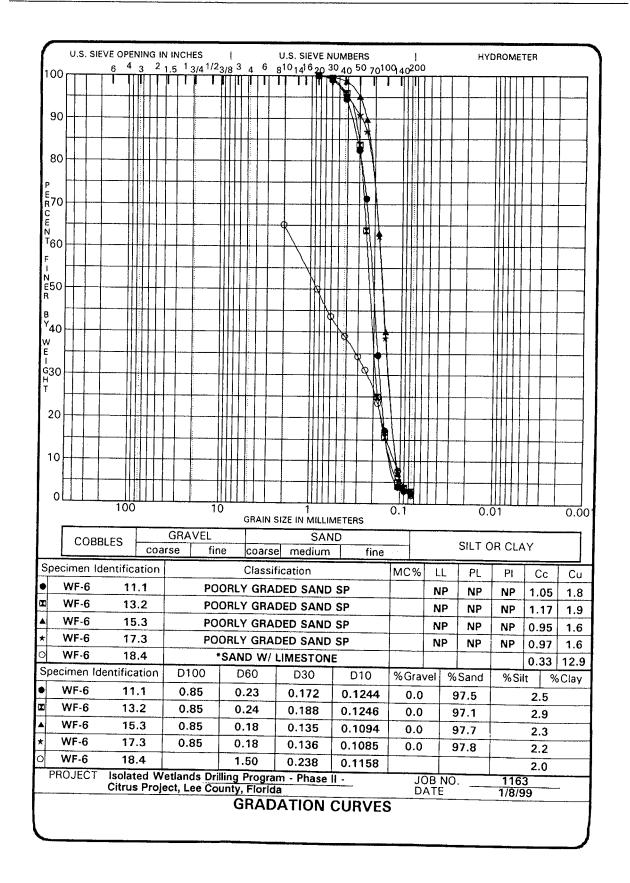
	0.9	s. sii	EVE OI 6	PEN 4					IES 3/4 <sup>1</sup>	1/2	 2/2	3	٨	6			5. SI						70	100	140	200	0			1		)HI	эм	ETI	ER			
00	Π	Τ	ŢŤ⁻	Π	Ň	Π	T	T	1	TÌ	Î	Ī	Ť	Π	Π	T	1	ΠÍ				T	Ϊ	Т	1	Į	Ī	T	Τ	T		Π		Π	Τ		<u> </u>	
	$\left  + \right $		-	╫		H	+-			_		$\parallel$		┢	+	+-		╢	110	$\left( \right)$	-	+			-#		+	-	+	╉		╢	$\left  \right $	$\left  \right $	+			
90					H	$\parallel$			÷		#	$\left  \right $	-	-	-	+			#	14	1	+	+									$\parallel$		$\left  \right $				
				╢			-	<u> </u>			Щ		1					Щ		1			1		[[	4						#						_
80		_																				V																
																						N																
	Π				ŀ		-				Ħ	Π				1					$\square$	$\uparrow\uparrow$	1				11			1		Ħ			-			
70	H	1				Ħ	+	-			╈	H	t.	┢		┫		╫				t 🕈	┉		+	++-	+	╈	+	-		$\parallel$		+	+			,
	╟	+		╫		┟┤	+-				╫	$\left  \right $		┢		╀	7	╢			$\vdash$	1	┽		╢	+	$\left  \cdot \right $		+	+		╢		+	-			
60	$\vdash$			╫		┝┼			-			╟╟	-	-		₳		╢		-			+-				$\prod$	╞	-			#		+	-			
				#		$\left  \right $	_								_		$\sum$	$\downarrow\downarrow$	ľ	Ą	_	1	ĮL.					_				Ш		-				
50									-			Ш		L					Ь		$\square$	$\square$					$\square$											
••																					K		ł		$\prod$	$\ $						$\prod$		T				
				T	:						$\parallel$	Π		1		T					Ľ	N	T				$\uparrow \uparrow$			1				$\dagger$	Π			_
40 '				$\parallel$			1		1			H	-	+-		+		$\parallel$		-+;	+		N-		╢		$\dagger$	+-	+	+		$\left  \right  \right $	╫	+	H		- <u></u>	
		-		+		$\left  \right $	+	-	:			+	+	$\vdash$		+		╢		┿	-	$\left  \cdot \right $	╫		╢		H	+					+	+	$\left  \cdot \right $			-
30										_		-	+-			╞		-		+	-				╢		$\square$	+		-			11		$\square$			_
		_				<b></b> _				_								Ш					N															_
20									-				1											1														
																								1			Π	T				$\square$	Π					
												T				Γ						<u> </u>	١		J.		h	$\uparrow$	1	1				T				-
10												╈				T		╢╢	Ħ			-	┢	Í.			-	┢		+			Ħ	$\top$	┝╴╎		•	-
		1				+	$\left  - \right $					$^{+}$				┢		₩	H				┢	Ĥ			$\left  \right $	+	-			$\parallel$	+	+	$\left  \right $			-
01		1	1	Ш 00			1. 1			10	))		:		··			 1		Ŀ			Ι.		<b>中</b> ).1		Ц.			1	0.0			Ц			0.	Ĭ
,					<b>,</b>								GF	A	N S	IZE	IN	МІ	.LII	MET	ΓEF	٦S								_	0.0	51					υ.	U
	C	сов	BLES		ļ				VE	~						τ—			A١	ID										SIL	го	R	CI	.A	Y			]
<u> </u>					-		ars	e		fin	e			oai			me		IM		_	f	in			1	-									-		
	wF		denti				-									_	tio								MC	2%	<u> </u>	LL		<u> </u>	-		ΡI	_	_C	С	С	u
	WF			11 13			-			PO														_			+-	NF	-+	N			NP	-+	1.		1.	
	WF			15			╀─			20							SH	_		5	Ρ						-	NF		N	2		NP	-+	0.		1.	
	WF			17				•			-	•					SH										+		+					+-	0.3		5.	
							+					-												┿			┼		-+-					+	0.	18	17	.4
pec	im	en le	dentif	ica	ati	on	+	D1	00			D	060	0	Ţ	-	D3	30		<u> </u>	r	010	)	+	%0	ire		1	%	San	d		%:		. 1		Cla	
	WF			11		_			85	_			.2		-+	(	0.1			1		14				0.0		+		7.2			/0 .					Y
	WF			13			$\uparrow$		85				.2		-+		0.2					152				0.0		┿	_	8.7					2.			
1	WF	-4		15			T						.8		-	_	).2			+		151						- -			-+			,	2.			
١	WF	-4		17	.2	-	1						.7		-+		0.1			<u>+</u>	_	)98		_			-	+			-				7.			
																	-	-						+				╋			-+					-		
PR	OJ	ECT	lso	lat	ec		/et	lan	ds   .ee	Dril	lin	g	Pr	og	rai	n	- P	ha	se	11 -	·					Ţ	Q	BN	Ю.	·	í	_	11	63	3		_	
			UI.			10	Jec	· , 1		0							TI									Ľ	JA	TE				1	/8	/9	9			

l	J.S.	SIE	VE O	PEN 4	111	١G	IN	iN	CH	ES	1/	2.	١	3			6				SI 1								-1	00		~2	1 00	I				ł	HY	DR	01	ΛE	TE	R				
<sup>00</sup> Г	Т		6	Ţ	3	Π		.5 	Ť	3/4 T		Π	1/8 	ŋ		T	ň		i†		ф Н	Ŭ	ĥ	Ň		Ĭ	Ţ		Ţ	T	1	Ť	ļ	Π	Т	T		-		Π	Π	Т	Π		<u> </u>			٦
┝				╢		╀	+	_				_	╢	H	-	-	-		+			-	ħ	Å	Ħ	Ā	+		╀			╢	+	┝╋	+	┽				╢	$\left  \right $	╋	┢			+-		-
90													Щ	Ц		-		_	$\downarrow$			_	Ц.		7	ġ	Į		+		_				4						+	+	╞		_			_
																											L)	J				1	-	Ц		_										.		
-					11111																					1																	1					
80	1			╢	T	T								T									Π	T			ļ	ł						Π		Τ												
				╢		╈	$\left  \cdot \right $			ł				t			_		+			+	╟	Ħ	+	+	Ĭ	1	1		_		t	┟╂	1	╈					T	T	t	ſ	┢	+		-
70				-	$\left  \right $	╋	$\left  \right $			-				╈	$\left  \right $	-		-	+			+	╢	H	+	+	4	N.	+					H	+	+		-		╢	+	-		-	┢	+		-
								_								-		-				+	$\parallel$		-	-		1	-					μ	_		••			$\parallel$	+		┢	┝	-	+		-
60										_												4	$\prod$											$\square$	_								-		L	+		
Ĩ																																																
1														T	Π			Γ					Π																									
50	+-			-#		+				-				1	H			t		-		1	Ħ		H		1	Î	1		_	Ħ			1			F		-11		Ħ	1	1	1	T		-
,		$\left  - \right $		+		╋	$\left  \cdot \right $							+	╢			$\left  \right $				+	$\left  \right $	+	H	+	-	\$	ł			H		╞┤	+	+		-		╢		╟	┢	-	$\vdash$	+		-
40				$\parallel$		$\parallel$				-				-		:		-		L		4	╢	$\parallel$		÷	-		1	<u> </u>			$\left  \right $	$\left  \right $	+	-+				+	$\parallel$	╟╋	┝	╞	-	+		-
	_					$\parallel$	Ц			1				1						-		_			$\parallel$							Щ						L		4	μ.		1	-	L	_		_
30																-																													ļ	_		
30																													ų	3								ł										
Ē	$\uparrow$			Ħ	÷				-	t				T		-		ſ					Ħ		H				ţ							-+					T		T		ľ			
20	+			╢	÷		$\vdash$	-						+	$\left  \right $		-	ŀ	-			+	╈	+	$\left  \right $	+	-		╢	$\left\  - \right\ $		H	+	┢	-	-+		-		+	╎	╟╋	┢	┢─	┢╌			-
-	-			+			-			-				+				ļ.,				-	$\left  \right $	$\parallel$		-	+		4			Ш		$\left  \right $	_	+			<b></b>				╀	┝	_	+		-
10	_	ŀ		_			Ц											_	_			_				+										_		_					1.			4.		
																														X	ľ.																	_
0														ľ																	T	Ċ,																
01				100	0		1			<u>r.</u>		1	0			~ ~			~			1									0	.1	<u>.</u>	1.1				<u></u>	0	.0	1	<u>ц</u>					0	0.0
Г					T	_			0	~ `	<u>/r</u>	1			_	GF T		IN	SI	126	11	1 1		-			EP	(S					1						_				_					
	C	ЮВ	BLE	S	$\left  \right $		07	ars	GR.	T	/E		ne			C	oa	irs	e	<u> </u>	m	ec	-			ך ד			fir	ne			$\left  \right $				\$	SIL	T.	0	R	С	LA	Y				
Spec	im	en l	den	tifi	 ca			T			-						-	-			ati		_		-	<u></u>				<u> </u>	Τn	Λ	29	6	1	LL	1	ſ	<u>ר</u>			ΡI			Co	;	(	<u></u> Cu
<u> </u>	WF					.3		╋				PC	00	R							D			NE	D	SF	2				$\dagger$			-	1	NP	-	N	νP	1		NF	)	1	.0	8	1	1.7
	WF		•••			.9		T	•									_			D			• •	-						t			1		NP	+		VP			NF			.1		1	1.8
, ,	WF	-5			6	.1		t			_					~~~		-	_		D	-									T									1				0	.9	9	1	1.7
, ,	WF	-5				.0		1											_	-	D			_	_						T	•		1	1	٧P	1	٢	١P	1	Ī	NF	>		.0			1.7
> '	WF	•5			9	.1		T	<u> </u>		1	PC	00	R	L١	1	GI	R/	۱C	)E	D	S	A	N	D	SF	2	•		• •	t				1	NP		ľ	IP		1	NF	,	1	.0	7	1	1.9
Spec	im	en l	den	tifi	ca	itic	n	Т	C	1	00	)			D	6	0				C	)3	0		Τ		C	21	0		9	%(	Gr	a١	/e		%	Sa	nd	ī		%	Si	lt	Τ	%	ЬC	lay
	WF	-5			1	.3			(	).8	35				0	.2	4		1		0.	1	89	)		(	).	13	88	7	1		0	0		T	9	8.	2						1.8	3		
3	WF	-5		~~~~~	2	.9		Τ	(	).8	35				0	.2	3				0.	1	83	3	-	(	).'	12	27	8	T		0.	0		T	9	7.	5						2.	5		
1	WF	•5			6	.1			2	2.0	0				0	.2	27			•	0.	2	07	7		(	).	15	59	7	T		0.	0		T	9	7.	2	-†					2.1	8		
1	WF	-5			7	.0			(	).8	35				0	.2	4				0.	1	89	)		(	).'	14	13	4	Ι		0.	0			9	7.	0			_			3.0	0		
	WF	_			_	.1			_		35					_	8		Ι	_	0.						_	14	9	1	Ι		0.			Ι		7.	3		_				2.	7		
PR	OJ	ECI	- <u>I</u> s	sol. itr	at	ed	V	Ve	tla	ne	is	D	ril	lin	g	P	ro	gi	a	m	-	P	ha	Se	e I	•								J	DE	N TE	10					1	16	3 99		-	_	
				- u	ua	» T*	10	je	ω,		ee	-	0	441							Т	1	ñ	N			1	P	$\overline{\mathbf{v}}$	E	c				<u>~</u>							1/	0/3	59				
															-		.,	-11		-				4 1				• •	۳	-	0																	

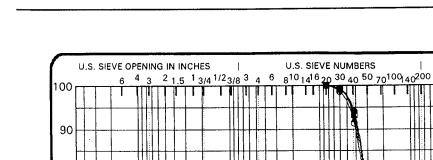
.



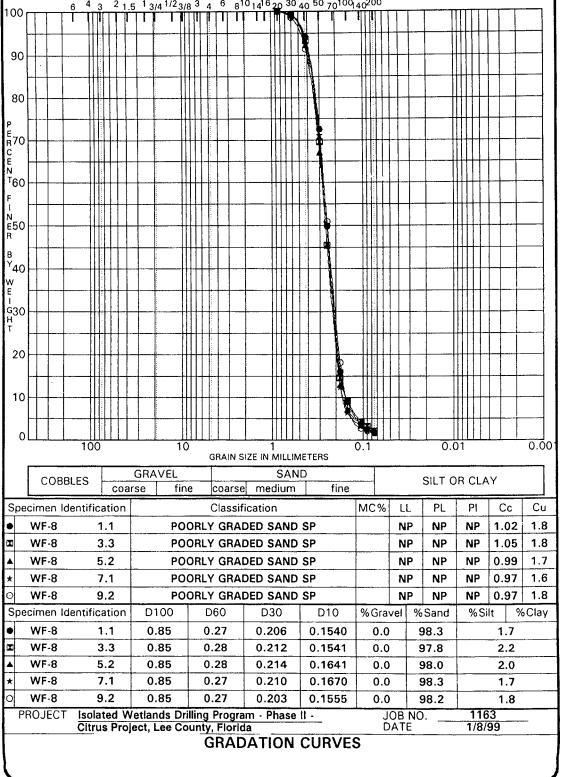
			4	3	3	$\frac{2}{1}$	.5	T	3/4	1/2;	3/8	3 11	4	U TT		B,	11	410	20	יט (	U 4	10	20	77	סיי	η,	40	20	<u> </u>	<del>.</del>							· · ·	-				
		-					'	1		•				1		IT				Т	4	I	Т	Ĥ	ř٩			H		1 1	- 1						11					
							-+				Ш			Ľ		1			Ш	$\parallel$		Ą					1		+		_						$\left  \right $	+	-			
																						N	A																			
				Π	Ħ		-				ttt	11	1	T								1	X		<b> </b>		T	Π	T													
	-			╫	+		+		:		┼┼┼	H	+	┼╴		┥			┟┼┥	+	$\left  \right $	+	đ	-			╢		$^{+}$	┝╍			┼─				Ħ	╈	╋	-		
	1	<u> </u>						<b>.</b>	ļ		Ш	$\downarrow$	-	1		-				+		-	-1	-			#		+	$\left  \cdot \right $					╢	+	┢╍┝	_		+		
																								Ł							_		L		Щ			$\downarrow$	_			
+-																								T									1									
1	†	1							<u> </u>			Ħ	1	t	T	1				T			1	å			11	T	T	Π	-				1			T				
		+			++				-		H	+		+	+	+	_		$\left  \right  \right $	+	$\left  \cdot \right $	+	+	╉	-		╫		+	$\left  \cdot \right $	-		$\left  \right $		$\mathbf{H}$	╟	$  \uparrow$	┽	+	-		
					-	$\left  \cdot \right $			ļ		Щ	$\downarrow$	_		$\downarrow$	-				_	$\left  \cdot \right $	+	-	-	$\vdash$		$\parallel$	$\left  \right $	+		_		-		⋕	╟	╇	+	╇	-+		
																								1			Ш								Ш		$\square$	╡	_			
				$\ $	$\left  \right $		T				$\ $																															
+	t	1				$\parallel$			-			$\dagger$	-	$\uparrow$	+	+					Ħ	1	+	-1			$\parallel$		1						$\parallel$	Ħ	Ħ	T	1			
+	-	$\vdash$			$\parallel$	H			-		╢╢	+		╀	+	+			$\ $	+	╟	+	+				╢	╢	╉	$\left  \cdot \right $	-		-		$\parallel$	$\parallel$	╟	+	╉	-		
		<u> </u>			1							$\parallel$		+						-	↓	:	4						+-	$\left  \cdot \right $		_	ļ		#	#	╢	-+		-		
											Ш																										Ш					
					T	Π					Π	Π		T		T			$\ $		IT	1	T		ſ												$\ $					
+	1			$\square$					1				-		$^{+}$						Ħ		1		r		╢		+		-					IT	Ħ	1	1			
						+					$\left\{ \right\}$		+		╞	-			╫	+-	$\mathbb{H}$	┽	+				╢	╢	+	$\left  \right $	-				╫	$\parallel$	H	-+	+			
	ļ	ļ											-	╞	+				Щ	-		4	$\downarrow$						4.	Ц						Щ			-			
																_																										
				$\left  \right $	$\prod$	Π					Π	Π		T	T	T			[]		Π	-	T			I.	Π		T							IT				Ī		
+-	1	1				$\dagger$					$\parallel \parallel$	$\dagger$		1	+-	-†					Ħ		╡		1	1/			╞				t		Ħ	Ħ	$\uparrow\uparrow$	†	+			-
+	┢			$\left  \right $	+	+	$\left  - \right $				╢╢	+		+	+-	+			╢	$\left  \right $	H	+	╉		┢	A	6	į.	+	+			+		$\parallel$	╟	+	+	╋			
	L		10	$\prod_{i=1}^{n}$						- 1	Щ	Ш							$\prod_{1}$						L.		Ţ						<u> </u>		Й	ĻL						).(
			п	0						I	0		G	RA	٩N	SI	ZE	IN	I MI	LLI	íM	ЕT	ER	s		Ľ	J. (	1						0.	.0	1					`	<i>.</i>
 C	·		<b></b>				G	iR/	١V	EL									S	A	N	)									-		211	т	<u>ог</u>			<u> </u>	~~~			
	.08	BL	<u> </u>		0	02	ars	e		fi	ne		(	0	ars	se	r	ne	diı	un	n			f	ine	2		1					21			{	-L	A .	r			
im	en	ldei	ntif	ic	ati	on							(	Cla	ss	ifi	са	tio	n			_					М	C	%		٤L		F	۶Ļ		{	P		С	c	1	Сι
WF	-6			1	.2					P	20	R	LY	G	R/	۱D	E	) (	SA	N	D	SF	>							1	NF	>	Ν	IP	Τ	N	IP		1.	17		1.8
WF	•6			3	3.0		1			P	00	R	LY	G	R/	٩D	E	5 5	SA	N	D	SF	)							I	NF	>	Ν	IP		N	IP	T	1.	16		1.8
WF	-6			5	5.1		T			P	20	R	LY	G	R/	٩D	)E[	5 5	SA	N	D	SF	>					-		1	NF	,	N	ĮΡ		N	IP		1.	17	T	1.8
WF	-6			7	.2		T			P	20	R	ĹY	G	R/	١D	E	) 5	SA	N	D	SF	>			1				1	NF	,	N	IP	Ť	٨	IP	1	1.	08		1.(
WF	-6			9	).2		1	-		P	00	R	LY	G	R/	١D	E	5 5	SA	N	D	SF	>			1					NF	,	N	IP	Ť	٨	IP	1	1.	03	1	1.
im	en	Ide	ntii	ici	ati	on		D	10	0	Т		D	60	)	Т		D	30			_	D	)1(	0		%	G	ra	ve	1	%	Sa	nd	+	(	%5	Silt	:	9	%0	la
WF	-6			1	.2		+	0	.8!	5	-		0.	23	}	1	(	).1	8	1	-1	C	).1	12	36	-		0	.0	)	╡	9	6.	9	+		-		3	.1		-
				3	3.0		$\uparrow$				╈					╈					╡							•	•	· · ·	╈		· · ·		$^+$		~~					
							+-				+			_	-	+					+							_			+				+							
							+				+					┥					+					-+				_	╉				+		•					
							┢				+			_		╈					-+					-					+				+	_						
		Ţ	Isc				Ve				ril					rar					e I							_	J	ŌĒ	1 6	NO					11	63	3			
			Cit	ru	s F	ro	jeo	ct,	Le	e C	oī																		D	)A'	TE					1	/8	/9	9			
	WF WF WF WF	WF-6 WF-6 WF-6 WF-6 WF-6 WF-6 WF-6 WF-6	WF-6 WF-6 WF-6 WF-6 WF-6 WF-6 WF-6 WF-6	COBBLES imen Identif WF-6 WF-6 WF-6 WF-6 imen Identif WF-6 WF-6 WF-6 WF-6 WF-6 WF-6	WF-6         1           WF-6         3           WF-6         5           WF-6         9           WF-6         1           WF-6         2           WF-6         2           WF-6         2           WF-6         7           WF-6         7           WF-6         7           WF-6         9           WF-6         9	COBBLES         c           cimen Identification         c           WF-6         1.2           WF-6         3.0           WF-6         5.1           WF-6         7.2           WF-6         9.2           cimen Identification         WF-6           WF-6         1.2           WF-6         3.0           WF-6         3.0	COBBLES         coal           cimen Identification         wF-6         1.2           WF-6         3.0         wF-6         5.1           WF-6         7.2         wF-6         9.2           cimen Identification         wF-6         1.2           WF-6         9.2         control of the second secon	COBBLES         Coars           coars         coars           coars         coars           wF-6         1.2           WF-6         3.0           WF-6         5.1           WF-6         7.2           WF-6         9.2           cimen Identification           WF-6         1.2           WF-6         3.0           WF-6         5.1           WF-6         3.0           WF-6         5.1           WF-6         5.1           WF-6         7.2           WF-6         7.2           WF-6         9.2	COBBLES         GR/ coarse           imen Identification            WF-6         1.2           WF-6         3.0           WF-6         5.1           WF-6         9.2           imen Identification         D           WF-6         1.2           WF-6         9.2           imen Identification         D           WF-6         3.0           WF-6         1.2           WF-6         3.0           WF-6         5.1           WF-6         5.1           WF-6         7.2           WF-6         7.2           WF-6         7.2           WF-6         7.2           WF-6         7.2           WF-6         7.2           WF-6         9.2	COBBLES         GRAV/ coarse           imen Identification	COBBLES         GRAVEL coarse         fi           cimen Identification             WF-6         1.2         PG           WF-6         3.0         PG           WF-6         5.1         PG           WF-6         7.2         PG           WF-6         9.2         PG           wF-6         1.2         0.85           WF-6         3.0         2.00           WF-6         5.1         0.85           WF-6         7.2         0.85           WF-6         7.2         0.85           WF-6         9.2         0.85	GRAVEL           coarse         fine           timen Identification         time           WF-6         1.2         POO           WF-6         3.0         POO           WF-6         5.1         POO           WF-6         7.2         POO           WF-6         9.2         POO           WF-6         1.2         0.85           WF-6         3.0         2.00           WF-6         3.0         2.00           WF-6         5.1         0.85           WF-6         7.2         0.85           WF-6         7.2         0.85           WF-6         9.2         0.85	GRAVEL           coarse         fine           imen Identification            WF-6         1.2         POOR           WF-6         3.0         POOR           WF-6         5.1         POOR           WF-6         7.2         POOR           WF-6         9.2         POOR           WF-6         1.2         0.85           WF-6         3.0         2.00           WF-6         3.0         2.00           WF-6         5.1         0.85           WF-6         7.2         0.85           WF-6         9.2         0.85           WF-6         9.2         0.85           WF-6         9.2         0.85           WF-6         9.2         0.85           OJECT         Isolated Wetlands Drillin           Citrus Project, Lee Coun         Citrus Project, Lee Coun	GRAVEL         GRAVEL           coarse         fine           imen Identification         0           WF-6         1.2         POORLY           WF-6         3.0         POORLY           WF-6         5.1         POORLY           WF-6         7.2         POORLY           WF-6         9.2         POORLY           WF-6         1.2         0.85         0.           WF-6         3.0         2.00         0.           WF-6         1.2         0.85         0.           WF-6         3.0         2.00         0.           WF-6         3.0         2.00         0.           WF-6         5.1         0.85         0.           WF-6         9.2         0.85         0.           WF-6         9.2         0.85         0.           WF-6         9.2         0.85         0.           WF-6         9.2         0.85         0.           OJECT         Isolated Wetlands Drilling I         Citrus Project, Lee County,	GRAVEL           COBBLES         GRAVEL         coarse         fine         coarse           imen Identification         Classification         Classification         Classification         Classification           WF-6         1.2         POORLY G         WF-6         S.0         POORLY G           WF-6         5.1         POORLY G         WF-6         G           WF-6         7.2         POORLY G         G           WF-6         9.2         POORLY G         G           WF-6         1.2         0.85         0.23           WF-6         3.0         2.00         0.24           WF-6         5.1         0.85         0.23           WF-6         5.1         0.85         0.23           WF-6         7.2         0.85         0.23           WF-6         9.2         0.85         0.24           WF-6         9.2         0.85         0.24           OJECT         Isolated Wetlands Drilling Project, Lee County, F	GRAIN           GRAVEL           GRAVEL           coarse         fine         coarse           simen Identification         Class           WF-6         1.2         POORLY GRA           WF-6         3.0         POORLY GRA           WF-6         5.1         POORLY GRA           WF-6         7.2         POORLY GRA           WF-6         9.2         POORLY GRA           wF-6         1.2         0.85         0.23           WF-6         5.1         D100         D60           WF-6         3.0         2.00         0.24           WF-6         5.1         0.85         0.23           WF-6         7.2         0.85         0.23           WF-6         9.2         0.85         0.24           OJECT         Isolated Wetlands Drilling Program         Citrus Project, Lee County, Flor	GRAIN SI       GRAVEL       COBBLES       GRAVEL       coarse       fine       coarse       MPF-6       1.2     POORLY GRAD       WF-6     9.2     POORLY GRAD       WF-6     9.2     POORLY GRAD       WF-6     1.2     0.85     0.23       WF-6     3.0     2.00     0.24       WF-6     7.2     0.85     0.23       WF-6     9.2     0.85     0.24       OJECT     Isolated Wetlands Drilling Program       Citrus Project, Lee County, Floridad	GRAIN SIZE         GRAVEL         COBBLES       GRAVEL         coarse       fine	GRAIN SIZE IN           GRAVEL           COBBLES         GRAVEL           coarse         fine         coarse         me           coarse         fine         classification           WF-6         3.0           WF-6         7.2         POORLY GRADED S           wF-6         1.2         0.85         0.23         0.1           WF-6         1.2         0.85         0.23         0.1           wF-6         3.0         0         0         0	GRAIN SIZE IN MI           GRAVEL         S           COBBLES         GRAVEL         S           coarse         fine <th< td=""><td>GRAIN SIZE IN MILLCOBBLESGRAVELSAcoarsefinecoarsemediumsimen IdentificationClassificationWF-61.2POORLY GRADED SANWF-63.0POORLY GRADED SANWF-65.1POORLY GRADED SANWF-67.2POORLY GRADED SANWF-69.2POORLY GRADED SANWF-61.20.850.230.181WF-63.02.00WF-61.20.850.23WF-65.10.850.23WF-65.10.850.23WF-67.20.850.23WF-69.20.850.24OJECTIsolated Wetlands Drilling Program - Phas Citrus Project, Lee County, Florida</td><td>GRAIN SIZE IN MILLIMCOBBLESGRAVELSANIcoarsefinecoarsemediumcimen IdentificationClassificationWF-61.2POORLY GRADED SANDWF-63.0POORLY GRADED SANDWF-65.1POORLY GRADED SANDWF-67.2POORLY GRADED SANDWF-69.2POORLY GRADED SANDWF-61.20.850.230.181WF-63.02.00WF-61.20.850.23WF-65.10.850.23WF-65.10.850.23WF-69.20.850.23WF-69.20.850.24OJECTIsolated Wetlands Drilling Program - Phase Citrus Project, Lee County, FlorIda</td><td>GRAIN SIZE IN MILLIMETCOBBLESGRAVELSANDcoarsefinecoarsemediumcimen IdentificationClassificationWF-61.2POORLY GRADED SAND SFWF-63.0POORLY GRADED SAND SFWF-65.1POORLY GRADED SAND SFWF-67.2POORLY GRADED SAND SFWF-69.2POORLY GRADED SAND SFWF-61.20.850.23output0.000.240.190WF-65.10.850.230.181WF-61.20.850.230.1860WF-65.10.850.230.1860WF-69.20.850.240.1930WF-69.20.850.240.1930OJECTIsolated Wetlands Drilling Program - Phase II - Citrus Project, Lee County, Florida-</td><td>GRAIN SIZE IN MILLIMETERCOBBLESGRAVELSANDcoarsefinecoarsemediumimen IdentificationClassificationWF-61.2POORLY GRADED SAND SPWF-63.0POORLY GRADED SAND SPWF-65.1POORLY GRADED SAND SPWF-67.2POORLY GRADED SAND SPWF-69.2POORLY GRADED SAND SPWF-61.20.850.230.181WF-63.02.000.240.1900.1WF-65.10.850.230.1860.1WF-65.10.850.230.1860.1WF-65.10.850.230.1860.1WF-69.20.850.240.1930.1OJECTIsolated Wetlands Drilling Program - Phase II - Citrus Project, Lee County, FloridaPoint of the second se</td><td>GRAIN SIZE IN MILLIMETERSGRAVELSANDcoarsefinecoarsemediumfcimen IdentificationClassificationWF-61.2POORLY GRADED SAND SPWF-63.0POORLY GRADED SAND SPWF-65.1POORLY GRADED SAND SPWF-67.2POORLY GRADED SAND SPWF-69.2POORLY GRADED SAND SPWF-61.20.850.230.160.130.12WF-65.10.850.23WF-65.10.850.23WF-67.20.850.23WF-67.20.850.23WF-69.20.850.240.150.150.150JECTIsolated Wetlands Drilling Program - Phase II - Citrus Project, Lee County, Florida</td><td>GRAIN SIZE IN MILLIMETERSGRAVELSANDcoarsefinemediumfinecoarsefinemediumfinecoarsefinemediumfinecoarsefinemediumfinecoarseimen IdentificationDORLY GRADED SAND SPWF-6<th coarse<="" td=""><td>GRAIN SIZE IN MILLIMETERSGRAVELSANDcoarsefinecoarsemediumfinecoarsefinecoarsemediumfinecoarsefinecoarsemediumfinecoarsefinecoarsemediumfinecoarsefinecoarsemediumfinecoarsefinecoarsemediumfineClassificationWF-61.2POORLY GRADED SAND SPWF-65.1POORLY GRADED SAND SPWF-69.2POORLY GRADED SAND SPWF-61.20.850.230.1810.1236WF-63.02.000.240.1900.1317WF-65.10.850.230.1860.1300WF-67.20.850.230.1870.1435WF-69.20.850.240.1930.1532OJECTIsolated Wetlands Drilling Program - Phase II - Citrus Project, Lee County, Floridacitrus Project, Lee County, Florida</td><td>GRAIN SIZE IN MILLIMETERS           COBBLES         GRAVEL         SAND           coarse         fine         coarse         medium         fine           imen Identification         Classification         M           WF-6         1.2         POORLY GRADED SAND SP         M           WF-6         3.0         POORLY GRADED SAND SP         M           WF-6         5.1         POORLY GRADED SAND SP         M           WF-6         7.2         POORLY GRADED SAND SP         M           WF-6         9.2         POORLY GRADED SAND SP         M           wF-6         1.2         0.85         0.23         0.181         0.1236           WF-6         1.2         0.85         0.23         0.186         0.1300         M           WF-6         5.1         0.85         0.23         0.186         0.1300         M           WF-6         5.1         0.85         0.23         0.187         0.1435         M           WF-6         7.2         0.85         0.24         0.193         0.1532         M</td><td>GRAIN SIZE IN MILLIMETERS         COBBLES       GRAVEL       SAND         coarse       fine       coarse       medium       fine         imen Identification       Classification       MC         WF-6       1.2       POORLY GRADED SAND SP       MC         WF-6       3.0       POORLY GRADED SAND SP       MC         WF-6       5.1       POORLY GRADED SAND SP       MC         WF-6       7.2       POORLY GRADED SAND SP       MC         WF-6       9.2       POORLY GRADED SAND SP       MC         wF-6       1.2       POORLY GRADED SAND SP       MC         wF-6       9.2       POORLY GRADED SAND SP       MC         wF-6       1.2       POORLY GRADED SAND SP       MC         wF-6       3.0       2.00       D100       %G         WF-6       1.2       0.85       0.23       0.181       0.1236       0         WF-6       5.1       0.85       0.23       0.186       0.1300       0         WF-6       7.2       0.85       0.23       0.187       0.1435       0         WF-6       9.2       0.85       0.24       0.193       0.1532       0</td><td>GRAIN SIZE IN MILLIMETERS         COBBLES       GRAVEL       SAND         coarse       fine       coarse       medium       fine         imen Identification       Classification       MC%         WF-6       1.2       POORLY GRADED SAND SP       MC%         WF-6       3.0       POORLY GRADED SAND SP       MC%         WF-6       5.1       POORLY GRADED SAND SP       MC%         WF-6       7.2       POORLY GRADED SAND SP       MF-6         WF-6       9.2       POORLY GRADED SAND SP       MG%         wF-6       1.2       0.85       0.23       0.181       0.1236       0.00         WF-6       1.2       0.85       0.23       0.186       0.1300       0.00         WF-6       3.0       2.00       0.24       0.190       0.1317       0.00         WF-6       5.1       0.85       0.23       0.187       0.1435       0.00         WF-6       7.2       0.85       0.23       0.187       0.1435       0.00         WF-6       9.2       0.85       0.24       0.193       0.1532       0.00         WF-6       9.2       0.85       0.24       0.193</td><td>GRAIN SIZE IN MILLIMETERS         COBBLES       GRAVEL       SAND         coarse       fine       coarse       medium       fine         imen Identification       Classification       MC%         WF-6       1.2       POORLY GRADED SAND SP       MC%         WF-6       3.0       POORLY GRADED SAND SP       MC%         WF-6       5.1       POORLY GRADED SAND SP       MC%         WF-6       7.2       POORLY GRADED SAND SP       MC%         WF-6       9.2       POORLY GRADED SAND SP       MC%         wimen Identification       D100       D60       D30       D10       %Grave         WF-6       1.2       0.85       0.23       0.181       0.1236       0.0         WF-6       3.0       2.00       0.24       0.190       0.1317       0.0         WF-6       5.1       0.85       0.23       0.187       0.1435       0.0         WF-6       9.2       0.85       0.24       0.193       0.1532       0.0         WF-6       9.2       0.85       0.24       0.193       0.1532       0.0         WF-6       9.2       0.85       0.24       0.193       0.1532&lt;</td><td>GRAVEL       SAND         COBBLES       GRAVEL       SAND         coarse       fine       coarse       medium       fine         coarse       fine       coarse       medium       fine         coarse       fine        medium       fine         coarse       fine        medium       fine         coarse       fine        medium       fine         coarse       fine         medium       fine         WF-6       1.2       POORLY GRADED SAND SP       NF         WF-6       7.2       POORLY GRADED SAND SP       NF         WF-6       9.2       POORLY GRADED SAND SP       NF         WF-6       7.2       0.85       0.23       0.181       0.1236       0.0       OV</td></th></td></th<> <td>GRAIN SIZE IN MILLIMETERS         COBBLES       GRAVEL       SAND         coarse       fine       coarse       medium       fine         imen Identification       Classification       MC%       LL         WF-6       1.2       POORLY GRADED SAND SP       NP         WF-6       3.0       POORLY GRADED SAND SP       NP         WF-6       5.1       POORLY GRADED SAND SP       NP         WF-6       7.2       POORLY GRADED SAND SP       NP         WF-6       9.2       POORLY GRADED SAND SP       NP         wF-6       1.2       0.85       0.23       0.181       0.1236       0.0       9         wF-6       3.0       2.00       0.24       0.190       0.1317       0.0       9         wF-6       5.1       0.85       0.23       0.186       0.1300       0.0       9         wF-6       3.0       2.00       0.24       0.190       0.1317       0.0       9         wF-6       7.2       0.85       0.23       0.186       0.1300       0.0       9         wF-6       9.2       0.85       0.24       0.193       0.1532       0.0       9      &lt;</td> <td>GRAVEL       SAND         GRAVEL       SAND         COBBLES       GRAVEL       SAND         coarse       fine       coarse       medium       fine         COBBLES       GRAVEL       SAND         coarse       fine       coarse       medium       fine         COBBLES       GRAVEL       SAND         immen Identification       MPOORLY GRADED SAND SP       NP       N         WF-6       3.0       POORLY GRADED SAND SP       NP       N         WF-6       7.2       POORLY GRADED SAND SP       NP       N         WF-6       9.2       POORLY GRADED SAND SP       NP       N         WF-6       9.2       POORLY GRADED SAND SP       NP       N         WF-6       9.2       0.85       0.23       0.181       0.1236       0.0       97</td> <td>GRAIN SIZE IN MILLIMETERS         GRAVEL       SAND         COBBLES       GRAVEL       SAND         coarse       fine       coarse       medium       fine       SILT         timen Identification       Classification       MC %       LL       PL         WF-6       1.2       POORLY GRADED SAND SP       MP       NP       NP         WF-6       3.0       POORLY GRADED SAND SP       NP       NP       NP         WF-6       5.1       POORLY GRADED SAND SP       NP       NP       NP         WF-6       7.2       POORLY GRADED SAND SP       NP       NP       NP         WF-6       9.2       POORLY GRADED SAND SP       NP       NP       NP         wf-6       1.2       0.85       0.23       0.181       0.1236       0.0       96.9         WF-6       1.2       0.85       0.23       0.186       0.1300       0.0       95.7         WF-6       5.1       0.85       0.23       0.187       0.1435       0.0       97.1         WF-6       7.2       0.85       0.24       0.193       0.1532       0.0       97.1      <t< td=""><td>GRAIN SIZE IN MILLIMETERS         GRAVEL       SAND         COBBLES       GRAVEL       SAND         coarse       medium       fine       SILT OF         COBBLES       fine       coarse       medium       fine       SILT OF         coarse       fine       coarse       medium       fine       SILT OF         MP       Classification       MC%       LL       PL         WF-6       1.2       POORLY GRADED SAND SP       NP       NP         WF-6       7.2       POORLY GRADED SAND SP       NP       NP         WF-6       7.2       POORLY GRADED SAND SP       NP       NP         WF-6       9.2       POORLY GRADED SAND SP       NP       NP       Sand         WF-6       9.2       0.85       0.23       0.1010       %         WF-6</td><td>GRAIN SIZE IN MILLIMETERS         GRAVEL       SAND         SILT OR O         COBBLES       GRAVEL       SAND         coarse       medium       fine       SILT OR O         coarse       fine       coarse       medium       fine         coarse       medium       fine       SILT OR O         coarse       medium       fine       SILT OR O         Classification       MC%       LL       PL       SILT OR O         WF-6       1.2       POORLY GRADED SAND SP       NP       NP       N         WF-6       7.2       POORLY GRADED SAND SP       NP       NP         WF-6       9.2       POORLY GRADED SAND SP       NP       NP         WF-6       9.2       0.85       0.23       0.181       0.123       0.123</td><td>GRAIN SIZE IN MILLIMETERSGRAVELSANDCOBBLESGRAVELSANDcoarsemediumfinecoarsefinecoarsemediumfinemediumfinecoarsefinemediumfinecoarsefinemediumfineClassificationMC %LPLPIWF-61.2POORLY GRADED SAND SPNPNPNPWF-69.2POORLY GRADED SAND SPNPNPNPWF-69.2POORLY GRADED SAND SPNPNPNPNPNPWF-69.2POORLY GRADED SAND SPNPNPWF-69.2POORLY GRADED SAND SPNPNPWF-69.20.850.230.1810.12360.096.9WF-61.0.850.230.186</td></t<></td>	GRAIN SIZE IN MILLCOBBLESGRAVELSAcoarsefinecoarsemediumsimen IdentificationClassificationWF-61.2POORLY GRADED SANWF-63.0POORLY GRADED SANWF-65.1POORLY GRADED SANWF-67.2POORLY GRADED SANWF-69.2POORLY GRADED SANWF-61.20.850.230.181WF-63.02.00WF-61.20.850.23WF-65.10.850.23WF-65.10.850.23WF-67.20.850.23WF-69.20.850.24OJECTIsolated Wetlands Drilling Program - Phas Citrus Project, Lee County, Florida	GRAIN SIZE IN MILLIMCOBBLESGRAVELSANIcoarsefinecoarsemediumcimen IdentificationClassificationWF-61.2POORLY GRADED SANDWF-63.0POORLY GRADED SANDWF-65.1POORLY GRADED SANDWF-67.2POORLY GRADED SANDWF-69.2POORLY GRADED SANDWF-61.20.850.230.181WF-63.02.00WF-61.20.850.23WF-65.10.850.23WF-65.10.850.23WF-69.20.850.23WF-69.20.850.24OJECTIsolated Wetlands Drilling Program - Phase Citrus Project, Lee County, FlorIda	GRAIN SIZE IN MILLIMETCOBBLESGRAVELSANDcoarsefinecoarsemediumcimen IdentificationClassificationWF-61.2POORLY GRADED SAND SFWF-63.0POORLY GRADED SAND SFWF-65.1POORLY GRADED SAND SFWF-67.2POORLY GRADED SAND SFWF-69.2POORLY GRADED SAND SFWF-61.20.850.23output0.000.240.190WF-65.10.850.230.181WF-61.20.850.230.1860WF-65.10.850.230.1860WF-69.20.850.240.1930WF-69.20.850.240.1930OJECTIsolated Wetlands Drilling Program - Phase II - Citrus Project, Lee County, Florida-	GRAIN SIZE IN MILLIMETERCOBBLESGRAVELSANDcoarsefinecoarsemediumimen IdentificationClassificationWF-61.2POORLY GRADED SAND SPWF-63.0POORLY GRADED SAND SPWF-65.1POORLY GRADED SAND SPWF-67.2POORLY GRADED SAND SPWF-69.2POORLY GRADED SAND SPWF-61.20.850.230.181WF-63.02.000.240.1900.1WF-65.10.850.230.1860.1WF-65.10.850.230.1860.1WF-65.10.850.230.1860.1WF-69.20.850.240.1930.1OJECTIsolated Wetlands Drilling Program - Phase II - Citrus Project, Lee County, FloridaPoint of the second se	GRAIN SIZE IN MILLIMETERSGRAVELSANDcoarsefinecoarsemediumfcimen IdentificationClassificationWF-61.2POORLY GRADED SAND SPWF-63.0POORLY GRADED SAND SPWF-65.1POORLY GRADED SAND SPWF-67.2POORLY GRADED SAND SPWF-69.2POORLY GRADED SAND SPWF-61.20.850.230.160.130.12WF-65.10.850.23WF-65.10.850.23WF-67.20.850.23WF-67.20.850.23WF-69.20.850.240.150.150.150JECTIsolated Wetlands Drilling Program - Phase II - Citrus Project, Lee County, Florida	GRAIN SIZE IN MILLIMETERSGRAVELSANDcoarsefinemediumfinecoarsefinemediumfinecoarsefinemediumfinecoarsefinemediumfinecoarseimen IdentificationDORLY GRADED SAND SPWF-6 <th coarse<="" td=""><td>GRAIN SIZE IN MILLIMETERSGRAVELSANDcoarsefinecoarsemediumfinecoarsefinecoarsemediumfinecoarsefinecoarsemediumfinecoarsefinecoarsemediumfinecoarsefinecoarsemediumfinecoarsefinecoarsemediumfineClassificationWF-61.2POORLY GRADED SAND SPWF-65.1POORLY GRADED SAND SPWF-69.2POORLY GRADED SAND SPWF-61.20.850.230.1810.1236WF-63.02.000.240.1900.1317WF-65.10.850.230.1860.1300WF-67.20.850.230.1870.1435WF-69.20.850.240.1930.1532OJECTIsolated Wetlands Drilling Program - Phase II - Citrus Project, Lee County, Floridacitrus Project, Lee County, Florida</td><td>GRAIN SIZE IN MILLIMETERS           COBBLES         GRAVEL         SAND           coarse         fine         coarse         medium         fine           imen Identification         Classification         M           WF-6         1.2         POORLY GRADED SAND SP         M           WF-6         3.0         POORLY GRADED SAND SP         M           WF-6         5.1         POORLY GRADED SAND SP         M           WF-6         7.2         POORLY GRADED SAND SP         M           WF-6         9.2         POORLY GRADED SAND SP         M           wF-6         1.2         0.85         0.23         0.181         0.1236           WF-6         1.2         0.85         0.23         0.186         0.1300         M           WF-6         5.1         0.85         0.23         0.186         0.1300         M           WF-6         5.1         0.85         0.23         0.187         0.1435         M           WF-6         7.2         0.85         0.24         0.193         0.1532         M</td><td>GRAIN SIZE IN MILLIMETERS         COBBLES       GRAVEL       SAND         coarse       fine       coarse       medium       fine         imen Identification       Classification       MC         WF-6       1.2       POORLY GRADED SAND SP       MC         WF-6       3.0       POORLY GRADED SAND SP       MC         WF-6       5.1       POORLY GRADED SAND SP       MC         WF-6       7.2       POORLY GRADED SAND SP       MC         WF-6       9.2       POORLY GRADED SAND SP       MC         wF-6       1.2       POORLY GRADED SAND SP       MC         wF-6       9.2       POORLY GRADED SAND SP       MC         wF-6       1.2       POORLY GRADED SAND SP       MC         wF-6       3.0       2.00       D100       %G         WF-6       1.2       0.85       0.23       0.181       0.1236       0         WF-6       5.1       0.85       0.23       0.186       0.1300       0         WF-6       7.2       0.85       0.23       0.187       0.1435       0         WF-6       9.2       0.85       0.24       0.193       0.1532       0</td><td>GRAIN SIZE IN MILLIMETERS         COBBLES       GRAVEL       SAND         coarse       fine       coarse       medium       fine         imen Identification       Classification       MC%         WF-6       1.2       POORLY GRADED SAND SP       MC%         WF-6       3.0       POORLY GRADED SAND SP       MC%         WF-6       5.1       POORLY GRADED SAND SP       MC%         WF-6       7.2       POORLY GRADED SAND SP       MF-6         WF-6       9.2       POORLY GRADED SAND SP       MG%         wF-6       1.2       0.85       0.23       0.181       0.1236       0.00         WF-6       1.2       0.85       0.23       0.186       0.1300       0.00         WF-6       3.0       2.00       0.24       0.190       0.1317       0.00         WF-6       5.1       0.85       0.23       0.187       0.1435       0.00         WF-6       7.2       0.85       0.23       0.187       0.1435       0.00         WF-6       9.2       0.85       0.24       0.193       0.1532       0.00         WF-6       9.2       0.85       0.24       0.193</td><td>GRAIN SIZE IN MILLIMETERS         COBBLES       GRAVEL       SAND         coarse       fine       coarse       medium       fine         imen Identification       Classification       MC%         WF-6       1.2       POORLY GRADED SAND SP       MC%         WF-6       3.0       POORLY GRADED SAND SP       MC%         WF-6       5.1       POORLY GRADED SAND SP       MC%         WF-6       7.2       POORLY GRADED SAND SP       MC%         WF-6       9.2       POORLY GRADED SAND SP       MC%         wimen Identification       D100       D60       D30       D10       %Grave         WF-6       1.2       0.85       0.23       0.181       0.1236       0.0         WF-6       3.0       2.00       0.24       0.190       0.1317       0.0         WF-6       5.1       0.85       0.23       0.187       0.1435       0.0         WF-6       9.2       0.85       0.24       0.193       0.1532       0.0         WF-6       9.2       0.85       0.24       0.193       0.1532       0.0         WF-6       9.2       0.85       0.24       0.193       0.1532&lt;</td><td>GRAVEL       SAND         COBBLES       GRAVEL       SAND         coarse       fine       coarse       medium       fine         coarse       fine       coarse       medium       fine         coarse       fine        medium       fine         coarse       fine        medium       fine         coarse       fine        medium       fine         coarse       fine         medium       fine         WF-6       1.2       POORLY GRADED SAND SP       NF         WF-6       7.2       POORLY GRADED SAND SP       NF         WF-6       9.2       POORLY GRADED SAND SP       NF         WF-6       7.2       0.85       0.23       0.181       0.1236       0.0       OV</td></th>	<td>GRAIN SIZE IN MILLIMETERSGRAVELSANDcoarsefinecoarsemediumfinecoarsefinecoarsemediumfinecoarsefinecoarsemediumfinecoarsefinecoarsemediumfinecoarsefinecoarsemediumfinecoarsefinecoarsemediumfineClassificationWF-61.2POORLY GRADED SAND SPWF-65.1POORLY GRADED SAND SPWF-69.2POORLY GRADED SAND SPWF-61.20.850.230.1810.1236WF-63.02.000.240.1900.1317WF-65.10.850.230.1860.1300WF-67.20.850.230.1870.1435WF-69.20.850.240.1930.1532OJECTIsolated Wetlands Drilling Program - Phase II - Citrus Project, Lee County, Floridacitrus Project, Lee County, Florida</td> <td>GRAIN SIZE IN MILLIMETERS           COBBLES         GRAVEL         SAND           coarse         fine         coarse         medium         fine           imen Identification         Classification         M           WF-6         1.2         POORLY GRADED SAND SP         M           WF-6         3.0         POORLY GRADED SAND SP         M           WF-6         5.1         POORLY GRADED SAND SP         M           WF-6         7.2         POORLY GRADED SAND SP         M           WF-6         9.2         POORLY GRADED SAND SP         M           wF-6         1.2         0.85         0.23         0.181         0.1236           WF-6         1.2         0.85         0.23         0.186         0.1300         M           WF-6         5.1         0.85         0.23         0.186         0.1300         M           WF-6         5.1         0.85         0.23         0.187         0.1435         M           WF-6         7.2         0.85         0.24         0.193         0.1532         M</td> <td>GRAIN SIZE IN MILLIMETERS         COBBLES       GRAVEL       SAND         coarse       fine       coarse       medium       fine         imen Identification       Classification       MC         WF-6       1.2       POORLY GRADED SAND SP       MC         WF-6       3.0       POORLY GRADED SAND SP       MC         WF-6       5.1       POORLY GRADED SAND SP       MC         WF-6       7.2       POORLY GRADED SAND SP       MC         WF-6       9.2       POORLY GRADED SAND SP       MC         wF-6       1.2       POORLY GRADED SAND SP       MC         wF-6       9.2       POORLY GRADED SAND SP       MC         wF-6       1.2       POORLY GRADED SAND SP       MC         wF-6       3.0       2.00       D100       %G         WF-6       1.2       0.85       0.23       0.181       0.1236       0         WF-6       5.1       0.85       0.23       0.186       0.1300       0         WF-6       7.2       0.85       0.23       0.187       0.1435       0         WF-6       9.2       0.85       0.24       0.193       0.1532       0</td> <td>GRAIN SIZE IN MILLIMETERS         COBBLES       GRAVEL       SAND         coarse       fine       coarse       medium       fine         imen Identification       Classification       MC%         WF-6       1.2       POORLY GRADED SAND SP       MC%         WF-6       3.0       POORLY GRADED SAND SP       MC%         WF-6       5.1       POORLY GRADED SAND SP       MC%         WF-6       7.2       POORLY GRADED SAND SP       MF-6         WF-6       9.2       POORLY GRADED SAND SP       MG%         wF-6       1.2       0.85       0.23       0.181       0.1236       0.00         WF-6       1.2       0.85       0.23       0.186       0.1300       0.00         WF-6       3.0       2.00       0.24       0.190       0.1317       0.00         WF-6       5.1       0.85       0.23       0.187       0.1435       0.00         WF-6       7.2       0.85       0.23       0.187       0.1435       0.00         WF-6       9.2       0.85       0.24       0.193       0.1532       0.00         WF-6       9.2       0.85       0.24       0.193</td> <td>GRAIN SIZE IN MILLIMETERS         COBBLES       GRAVEL       SAND         coarse       fine       coarse       medium       fine         imen Identification       Classification       MC%         WF-6       1.2       POORLY GRADED SAND SP       MC%         WF-6       3.0       POORLY GRADED SAND SP       MC%         WF-6       5.1       POORLY GRADED SAND SP       MC%         WF-6       7.2       POORLY GRADED SAND SP       MC%         WF-6       9.2       POORLY GRADED SAND SP       MC%         wimen Identification       D100       D60       D30       D10       %Grave         WF-6       1.2       0.85       0.23       0.181       0.1236       0.0         WF-6       3.0       2.00       0.24       0.190       0.1317       0.0         WF-6       5.1       0.85       0.23       0.187       0.1435       0.0         WF-6       9.2       0.85       0.24       0.193       0.1532       0.0         WF-6       9.2       0.85       0.24       0.193       0.1532       0.0         WF-6       9.2       0.85       0.24       0.193       0.1532&lt;</td> <td>GRAVEL       SAND         COBBLES       GRAVEL       SAND         coarse       fine       coarse       medium       fine         coarse       fine       coarse       medium       fine         coarse       fine        medium       fine         coarse       fine        medium       fine         coarse       fine        medium       fine         coarse       fine         medium       fine         WF-6       1.2       POORLY GRADED SAND SP       NF         WF-6       7.2       POORLY GRADED SAND SP       NF         WF-6       9.2       POORLY GRADED SAND SP       NF         WF-6       7.2       0.85       0.23       0.181       0.1236       0.0       OV</td>	GRAIN SIZE IN MILLIMETERSGRAVELSANDcoarsefinecoarsemediumfinecoarsefinecoarsemediumfinecoarsefinecoarsemediumfinecoarsefinecoarsemediumfinecoarsefinecoarsemediumfinecoarsefinecoarsemediumfineClassificationWF-61.2POORLY GRADED SAND SPWF-65.1POORLY GRADED SAND SPWF-69.2POORLY GRADED SAND SPWF-61.20.850.230.1810.1236WF-63.02.000.240.1900.1317WF-65.10.850.230.1860.1300WF-67.20.850.230.1870.1435WF-69.20.850.240.1930.1532OJECTIsolated Wetlands Drilling Program - Phase II - Citrus Project, Lee County, Floridacitrus Project, Lee County, Florida	GRAIN SIZE IN MILLIMETERS           COBBLES         GRAVEL         SAND           coarse         fine         coarse         medium         fine           imen Identification         Classification         M           WF-6         1.2         POORLY GRADED SAND SP         M           WF-6         3.0         POORLY GRADED SAND SP         M           WF-6         5.1         POORLY GRADED SAND SP         M           WF-6         7.2         POORLY GRADED SAND SP         M           WF-6         9.2         POORLY GRADED SAND SP         M           wF-6         1.2         0.85         0.23         0.181         0.1236           WF-6         1.2         0.85         0.23         0.186         0.1300         M           WF-6         5.1         0.85         0.23         0.186         0.1300         M           WF-6         5.1         0.85         0.23         0.187         0.1435         M           WF-6         7.2         0.85         0.24         0.193         0.1532         M	GRAIN SIZE IN MILLIMETERS         COBBLES       GRAVEL       SAND         coarse       fine       coarse       medium       fine         imen Identification       Classification       MC         WF-6       1.2       POORLY GRADED SAND SP       MC         WF-6       3.0       POORLY GRADED SAND SP       MC         WF-6       5.1       POORLY GRADED SAND SP       MC         WF-6       7.2       POORLY GRADED SAND SP       MC         WF-6       9.2       POORLY GRADED SAND SP       MC         wF-6       1.2       POORLY GRADED SAND SP       MC         wF-6       9.2       POORLY GRADED SAND SP       MC         wF-6       1.2       POORLY GRADED SAND SP       MC         wF-6       3.0       2.00       D100       %G         WF-6       1.2       0.85       0.23       0.181       0.1236       0         WF-6       5.1       0.85       0.23       0.186       0.1300       0         WF-6       7.2       0.85       0.23       0.187       0.1435       0         WF-6       9.2       0.85       0.24       0.193       0.1532       0	GRAIN SIZE IN MILLIMETERS         COBBLES       GRAVEL       SAND         coarse       fine       coarse       medium       fine         imen Identification       Classification       MC%         WF-6       1.2       POORLY GRADED SAND SP       MC%         WF-6       3.0       POORLY GRADED SAND SP       MC%         WF-6       5.1       POORLY GRADED SAND SP       MC%         WF-6       7.2       POORLY GRADED SAND SP       MF-6         WF-6       9.2       POORLY GRADED SAND SP       MG%         wF-6       1.2       0.85       0.23       0.181       0.1236       0.00         WF-6       1.2       0.85       0.23       0.186       0.1300       0.00         WF-6       3.0       2.00       0.24       0.190       0.1317       0.00         WF-6       5.1       0.85       0.23       0.187       0.1435       0.00         WF-6       7.2       0.85       0.23       0.187       0.1435       0.00         WF-6       9.2       0.85       0.24       0.193       0.1532       0.00         WF-6       9.2       0.85       0.24       0.193	GRAIN SIZE IN MILLIMETERS         COBBLES       GRAVEL       SAND         coarse       fine       coarse       medium       fine         imen Identification       Classification       MC%         WF-6       1.2       POORLY GRADED SAND SP       MC%         WF-6       3.0       POORLY GRADED SAND SP       MC%         WF-6       5.1       POORLY GRADED SAND SP       MC%         WF-6       7.2       POORLY GRADED SAND SP       MC%         WF-6       9.2       POORLY GRADED SAND SP       MC%         wimen Identification       D100       D60       D30       D10       %Grave         WF-6       1.2       0.85       0.23       0.181       0.1236       0.0         WF-6       3.0       2.00       0.24       0.190       0.1317       0.0         WF-6       5.1       0.85       0.23       0.187       0.1435       0.0         WF-6       9.2       0.85       0.24       0.193       0.1532       0.0         WF-6       9.2       0.85       0.24       0.193       0.1532       0.0         WF-6       9.2       0.85       0.24       0.193       0.1532<	GRAVEL       SAND         COBBLES       GRAVEL       SAND         coarse       fine       coarse       medium       fine         coarse       fine       coarse       medium       fine         coarse       fine        medium       fine         coarse       fine        medium       fine         coarse       fine        medium       fine         coarse       fine         medium       fine         WF-6       1.2       POORLY GRADED SAND SP       NF         WF-6       7.2       POORLY GRADED SAND SP       NF         WF-6       9.2       POORLY GRADED SAND SP       NF         WF-6       7.2       0.85       0.23       0.181       0.1236       0.0       OV	GRAIN SIZE IN MILLIMETERS         COBBLES       GRAVEL       SAND         coarse       fine       coarse       medium       fine         imen Identification       Classification       MC%       LL         WF-6       1.2       POORLY GRADED SAND SP       NP         WF-6       3.0       POORLY GRADED SAND SP       NP         WF-6       5.1       POORLY GRADED SAND SP       NP         WF-6       7.2       POORLY GRADED SAND SP       NP         WF-6       9.2       POORLY GRADED SAND SP       NP         wF-6       1.2       0.85       0.23       0.181       0.1236       0.0       9         wF-6       3.0       2.00       0.24       0.190       0.1317       0.0       9         wF-6       5.1       0.85       0.23       0.186       0.1300       0.0       9         wF-6       3.0       2.00       0.24       0.190       0.1317       0.0       9         wF-6       7.2       0.85       0.23       0.186       0.1300       0.0       9         wF-6       9.2       0.85       0.24       0.193       0.1532       0.0       9      <	GRAVEL       SAND         GRAVEL       SAND         COBBLES       GRAVEL       SAND         coarse       fine       coarse       medium       fine         COBBLES       GRAVEL       SAND         coarse       fine       coarse       medium       fine         COBBLES       GRAVEL       SAND         immen Identification       MPOORLY GRADED SAND SP       NP       N         WF-6       3.0       POORLY GRADED SAND SP       NP       N         WF-6       7.2       POORLY GRADED SAND SP       NP       N         WF-6       9.2       POORLY GRADED SAND SP       NP       N         WF-6       9.2       POORLY GRADED SAND SP       NP       N         WF-6       9.2       0.85       0.23       0.181       0.1236       0.0       97	GRAIN SIZE IN MILLIMETERS         GRAVEL       SAND         COBBLES       GRAVEL       SAND         coarse       fine       coarse       medium       fine       SILT         timen Identification       Classification       MC %       LL       PL         WF-6       1.2       POORLY GRADED SAND SP       MP       NP       NP         WF-6       3.0       POORLY GRADED SAND SP       NP       NP       NP         WF-6       5.1       POORLY GRADED SAND SP       NP       NP       NP         WF-6       7.2       POORLY GRADED SAND SP       NP       NP       NP         WF-6       9.2       POORLY GRADED SAND SP       NP       NP       NP         wf-6       1.2       0.85       0.23       0.181       0.1236       0.0       96.9         WF-6       1.2       0.85       0.23       0.186       0.1300       0.0       95.7         WF-6       5.1       0.85       0.23       0.187       0.1435       0.0       97.1         WF-6       7.2       0.85       0.24       0.193       0.1532       0.0       97.1 <t< td=""><td>GRAIN SIZE IN MILLIMETERS         GRAVEL       SAND         COBBLES       GRAVEL       SAND         coarse       medium       fine       SILT OF         COBBLES       fine       coarse       medium       fine       SILT OF         coarse       fine       coarse       medium       fine       SILT OF         MP       Classification       MC%       LL       PL         WF-6       1.2       POORLY GRADED SAND SP       NP       NP         WF-6       7.2       POORLY GRADED SAND SP       NP       NP         WF-6       7.2       POORLY GRADED SAND SP       NP       NP         WF-6       9.2       POORLY GRADED SAND SP       NP       NP       Sand         WF-6       9.2       0.85       0.23       0.1010       %         WF-6</td><td>GRAIN SIZE IN MILLIMETERS         GRAVEL       SAND         SILT OR O         COBBLES       GRAVEL       SAND         coarse       medium       fine       SILT OR O         coarse       fine       coarse       medium       fine         coarse       medium       fine       SILT OR O         coarse       medium       fine       SILT OR O         Classification       MC%       LL       PL       SILT OR O         WF-6       1.2       POORLY GRADED SAND SP       NP       NP       N         WF-6       7.2       POORLY GRADED SAND SP       NP       NP         WF-6       9.2       POORLY GRADED SAND SP       NP       NP         WF-6       9.2       0.85       0.23       0.181       0.123       0.123</td><td>GRAIN SIZE IN MILLIMETERSGRAVELSANDCOBBLESGRAVELSANDcoarsemediumfinecoarsefinecoarsemediumfinemediumfinecoarsefinemediumfinecoarsefinemediumfineClassificationMC %LPLPIWF-61.2POORLY GRADED SAND SPNPNPNPWF-69.2POORLY GRADED SAND SPNPNPNPWF-69.2POORLY GRADED SAND SPNPNPNPNPNPWF-69.2POORLY GRADED SAND SPNPNPWF-69.2POORLY GRADED SAND SPNPNPWF-69.20.850.230.1810.12360.096.9WF-61.0.850.230.186</td></t<>	GRAIN SIZE IN MILLIMETERS         GRAVEL       SAND         COBBLES       GRAVEL       SAND         coarse       medium       fine       SILT OF         COBBLES       fine       coarse       medium       fine       SILT OF         coarse       fine       coarse       medium       fine       SILT OF         MP       Classification       MC%       LL       PL         WF-6       1.2       POORLY GRADED SAND SP       NP       NP         WF-6       7.2       POORLY GRADED SAND SP       NP       NP         WF-6       7.2       POORLY GRADED SAND SP       NP       NP         WF-6       9.2       POORLY GRADED SAND SP       NP       NP       Sand         WF-6       9.2       0.85       0.23       0.1010       %         WF-6	GRAIN SIZE IN MILLIMETERS         GRAVEL       SAND         SILT OR O         COBBLES       GRAVEL       SAND         coarse       medium       fine       SILT OR O         coarse       fine       coarse       medium       fine         coarse       medium       fine       SILT OR O         coarse       medium       fine       SILT OR O         Classification       MC%       LL       PL       SILT OR O         WF-6       1.2       POORLY GRADED SAND SP       NP       NP       N         WF-6       7.2       POORLY GRADED SAND SP       NP       NP         WF-6       9.2       POORLY GRADED SAND SP       NP       NP         WF-6       9.2       0.85       0.23       0.181       0.123       0.123	GRAIN SIZE IN MILLIMETERSGRAVELSANDCOBBLESGRAVELSANDcoarsemediumfinecoarsefinecoarsemediumfinemediumfinecoarsefinemediumfinecoarsefinemediumfineClassificationMC %LPLPIWF-61.2POORLY GRADED SAND SPNPNPNPWF-69.2POORLY GRADED SAND SPNPNPNPWF-69.2POORLY GRADED SAND SPNPNPNPNPNPWF-69.2POORLY GRADED SAND SPNPNPWF-69.2POORLY GRADED SAND SPNPNPWF-69.20.850.230.1810.12360.096.9WF-61.0.850.230.186			



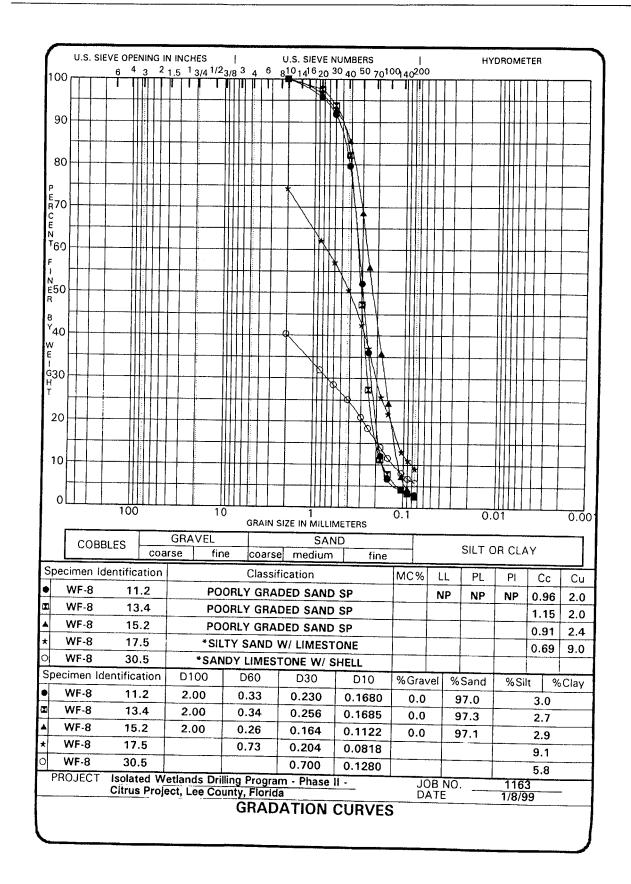
D-13

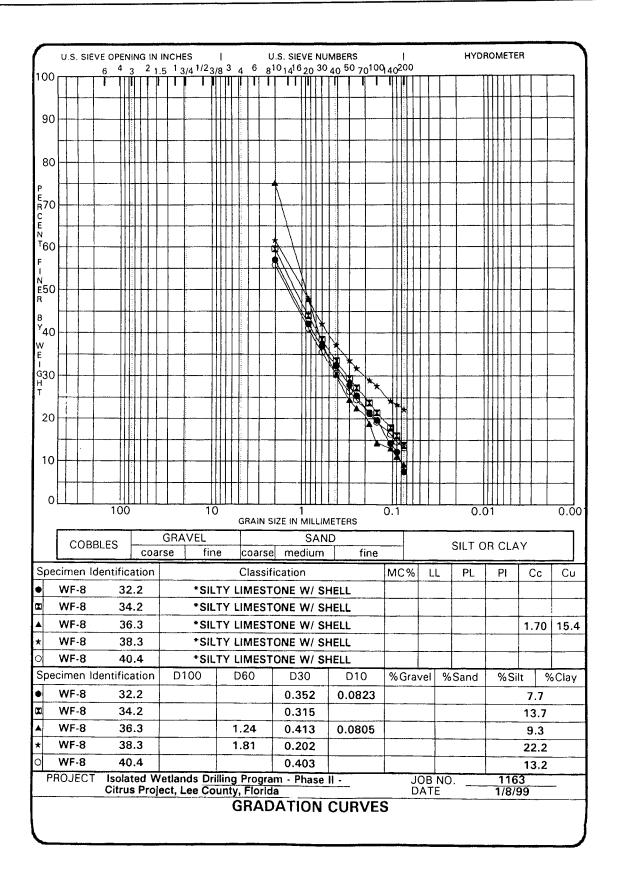


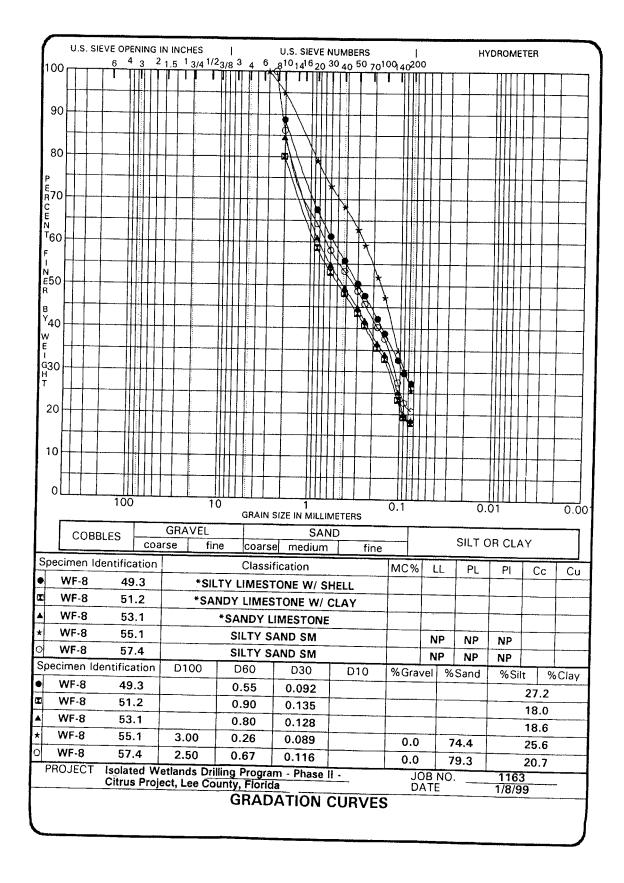
APPENDIX D - Citrus Project Field Notes



HYDROMETER







	U.S	i. SI		E OP 6 '	'EN 4	IIN 3	G 2	IN 2 1	IN .5	сн 1	ES 3/4	1/2	3/	 8 3	3	4	6					EVE 3 20						'0 <sup>1</sup>	00	14	ا 20	00					ΗY	DF	10	M	ETE	ER				
<sup>00</sup> [		Τ	T	ŕ	Π	Ĭ	Π	ή	Π	T	Ī	Т	Ĩ	ĪП	Γ	Ì	T	h	Í		Ē		Ŕ	h	Ţ	٦		Ť	Т	T	Ťſ	Π	Τ	Τ		Τ		T	Π		T	T	Γ			
ł	╈	+-	+		Η	H	Ħ	-+		_			╢	╫	┢			1	┥			fſ	X	R	蘭			╈		1	Ħ	Ħ	┢	1		+		╡	Ħ	Ħ	╀	╋	╀╴	+		
90		+	╋		H		॑┤	-+					╉	╢	┢	-		┢	+			╟	+	H	H	Н		+		-		╟	+-	┢		+		+	╢	+	+	+	+-	+		
}	+		+				Н	+	_				╢	$\left  \right $	╞	_		┝	-					H	ł	Щ		-					+	╞		+-		+	╢	+	╋	+-	-	-		
80	_		-			-		_			-		4			-		_							_	Ц							1	_	L					$\parallel$	╞					
					Ш	-					-																																L			
-						1																				K	4	ł																		
70			1		Ш		Ħ						╢	Ħ	T			1	1			I		Π		ļ					Ħ	Ħ			1	T			Ħ	Π	1		-			
Ì	+	-	╈		₩		Ħ						╫	Ħ	╀╌		-	+	┥			╢	Ħ	t				1			Ħ	Ħ	+	+-	†	╈	•••••	+	Ħ	Ħ	╉	T	ſ	╉		
60	+	┼─	+				Η	-+	-	-	-	<b></b>	╢	╟	┢	-	-	-	┥			╢	$\left  \right $	$\frac{1}{1}$	+			╀			╫	$\left  \right $	╀	┢	+-	╈		-+	╢	$\parallel$	+	┼	┢	+		
	+		+-		Щ		H	+					╢	╢	-	-			+				$\left  \right $		-	_		+		_		$\parallel$	┢	┢		+		-	╢	$\parallel$	╀	+-	┝	+		_
50	+				Щ		Ц	_	_		-		$\parallel$	$\parallel$	╞	-	L	$\vdash$	_			⋕	-		4		1	+			1		$\downarrow$			$\downarrow$			$\parallel$	$\parallel$	$\downarrow$	<b>_</b>	-	_		
					Ш		$\square$							$\parallel$																									$\parallel$							
40														$\ $	ľ												Ţ			ļ																
40			T		$\prod$		Π		1					Ħ	T			1						Π			Ţ	ľ				Ħ		T					Π	Ħ	T	T	1	-		
ł	+	+	+		₩			-+	+		ţ.		╫	╢	┢	-		<b> </b>	+			╢	╟	Η		-	-	t		┥		$\left  \right $	+	+	1-	+			╢	╢	╈	+	1-	╈		
30	┼		+				Η	-					╫	╢	┢			╞	-			╫	+	$\left  \right $						-+	#	╟	+	+		+			╢	H	+-	┢	╀			
ł	╀	-	╉		$\left  \right  \right $		H	-	-	. <u> </u>			╢	╟	+				-				+		-	_		₩	)	$\downarrow$			+-	$\vdash$	╞	-			$\parallel$	╢	+	-	╞	-		
20			$\downarrow$				μ	1			_		1	$\parallel$			_		4				_			_						$\prod$	_			_		_	1	Ш	1	1	ļ			
							Ш									1.11												Ň	l																	
10													$\prod$																ľ			Π							Π	Π						
10			Γ		Π		Π						11	Π	Τ				T	-		Π	T					T		$\langle  $			T	Γ		1		1		Π	T	T		T		
		1	1		Ħ	T	††	1					╢		T	-			$\dagger$				f				•	┢	-6		26		t	┢	┢─	╈		1	Ħ	Ħ	-	╞	<u> </u>		-	
οL	- <u> </u>	J		1(	ш 50	<u>  </u>	LL				ŀ	1	10	ш.				L	1			1111 1	1					1		0.	Г <b>с</b> 1	Ш	<u> </u>	L.	I	L	C	).C	)1	Ш.	<u> </u>				C	0.0
r						Т										GF	۹A	IN :	SIZ	ZE	IN				_	EΡ	S							_									,		_	
	C	O	3BL	ES		-	<u> </u>	าล	G rsi				ine					irs				S diu			2 T			in			4					SI	T	0	R	С	LA	١Y				
 pec	im	en	Ide	ntif	fic	<u></u>	-	_		_		-		_			-	ssi	-		-	_			1				с —	N		0/.	Г	LL	_	-	PL	-	-	PI		<b>—</b>	Co			Сι
	NF				-	1.3	•••	-	-			P	00	)R				RA	_				MI		<b>c</b> 1	<u> </u>						/0	⊢	NF	•••		NP	1		NF	-	┝──	.9			1.8
	NF					3.0						P		_											-					-		•		NF			NP	+		NF		+	.0			1.8
1	NF	-9			E	5.2	2										_	٦A		• •	_		_						-				<del> </del>	NF			NP	-+	_	NF			.0		-	1.6
	NF					7.1						P			_		-						_						_				+	NF			NP		_	NF		+	.9			1.9
١	٨F	-9			9	).2	2					P	20	R	L١	1	GI	R	D	EC	) 5	5A	NI	D	SF	>		_							-			-				1	.0	5	2	2.2
bec	im	en	lde	ntif	ic	at	ioi	n		D	10	0	Τ		С	6	0		I		D	30		٦		C	)1(	C		%	G	ra	ve	el	%	Sa	nç	1		%	Si	÷	T	_	6C	_
۱	٨F	-9			1	1.3	3			2	.00	)			0	.2	9		T	0	.2	12	2		(	).'	15	77	1		0	.0	)		ç	97.	7						2.3	3		
_	NF				3	3.0	)			0	.85	5		_	0	.2	6		Γ	0	.1	99	)		(	).'	14	54	ŀ			.0		1		8.			_				1.9			
	NF					5.2				0	.8	5			0	.2	5			0	1.1	97	1		(	).'	15	63	3		0	0.0	)		5	98	1	1					1.9	)		
	NF				-	7.1					.00	_				.2					_	99			(	).'	14	68	3		0	.0	)		9	97.	3		_		_		2.7	7		
	NF		<del>~ -</del>	<u> </u>		).2					.00					.2						9(					2	66	3		0	.0				96.	4		_				3.6	3		
PR	υJ	ЕC	1	Iso Cit	la ru	te s l	d Pr	W oli	et ec	lar t. I	nds Lef	D C	ril	lin In	g tv	Pi F	ro In	gra oriz	ne 1e	۱ -	Ρ	ha	se	<u>  </u>	-							J		B N TE	١Ö				-	1	16 R/9	3 99			_	
		-				-		~1		•, 1			-									~											-	10						1/1	513	23				

e

•

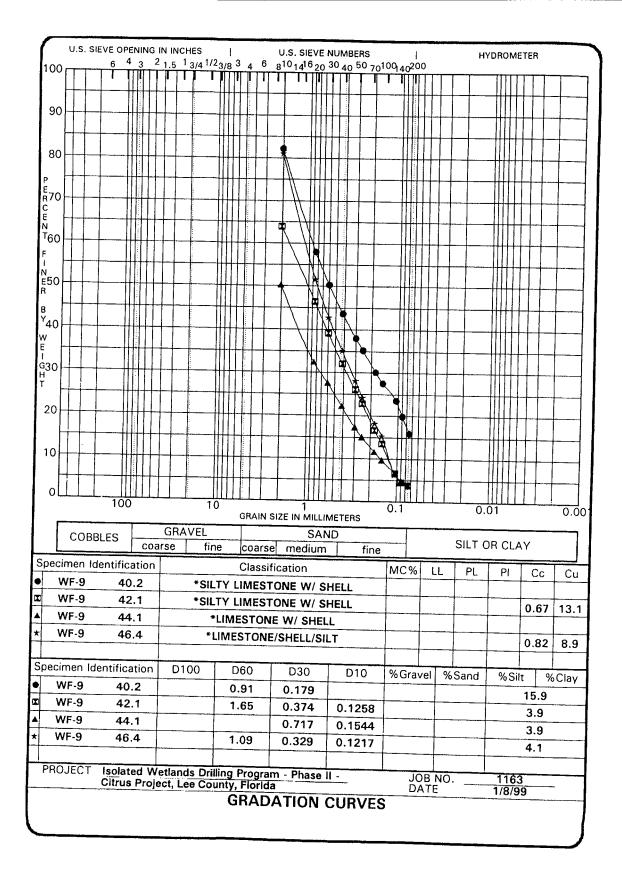
.

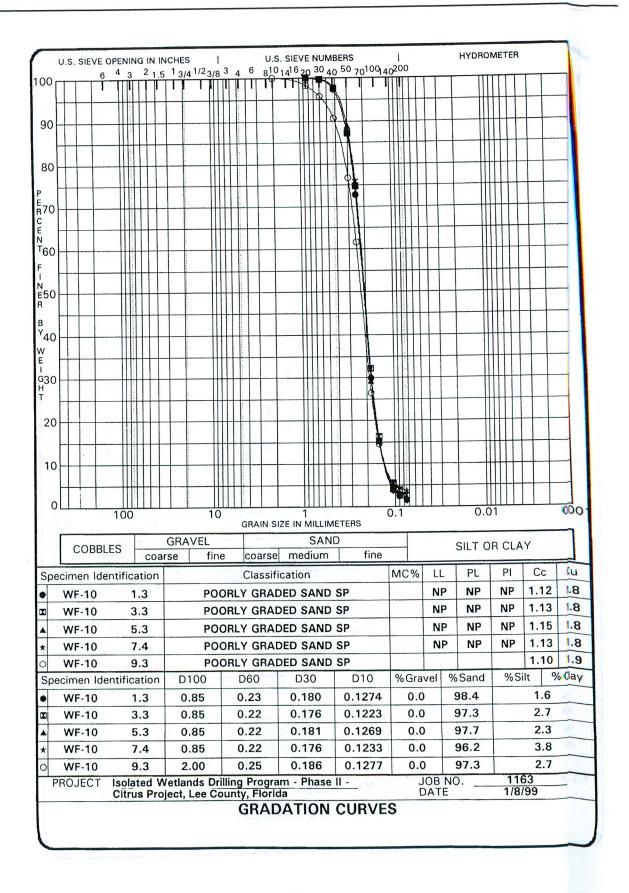
100		5. 51	EVE O 6					INC 5 1			23	 /8 ·	3	4	6	<u>,</u>	U.S 10	:. S 1/1	IE\   6 -	/E	NU 30	) м (	BEI n 5	RS 50 ·	701	100	<b>.</b> .	ا مرير	ეი					HY	DR	ON	٨E٦	TEF	٦			
100		Τ	ΤŤ	T	Ť	Π	Ť	Ť	Ť	-	ſĬ	Ť	η	Ī	٦ <sup>0</sup>	۲	1	Ŧ	Ĥ		Π	Ţ		Γ	Î	Т	14		Π			[	1		П	Π	Π	Π	-r			-
		+		-		+	┽	╉	-				+	-	┝		+		-		N		-	-	╀				$\left  \right $	+	┝		+		╢		$\parallel$	4	-			
90	·  -	+			4	$\left  \right $	_		-	_		$\parallel$	-				1		_	Ш	ľ	Ŷ		Ì.	1		_		Ц		<b>.</b>											
																						X	Å																			
80												$\ $											N.		Τ											Π	11	1				-
00						T	T	1	ŀ			††	T				1				+	T.	Ą		+				Ħ	+		_	$\uparrow$		╢	$\parallel$	╢	╈	+	_		-
-		1	<u> </u>	-#	+	Ħ	+	+	+		-#	╢	╀				+-	_	╢		-		4	-	╞		_		H						╢	╢	╀┦					
70			<u> </u>	•#		$\left  \right $			_			#	+	: 	_									Ł	$\downarrow$		_								4	1			$\perp$	_		
		_	 	-								$\parallel$							X					1									ļ		$\ $							
1 60																				$\left \right $	¥			٩ ۱											Π		Π		Τ			
												Π					T			Ť	1	V		T	$\parallel$		1						1		Ħ	Ħ	Ħ	+	+	-		-
1	Ħ	1		++	Ħ		+	+			╢	$^{\dagger}$	H		-		┼╴		╢	╢	+	H	$\forall$	+	╀		+		╋	$\left  \right $	-		-		╢	╟	╟╟	+	+	+		
50	$\left  - \right  $			╢	╢	╟	+-	+	+		-#	╢	$\left  \right $		-		╞		╢	$\parallel$	+	H		$\left( - \right)$	-		+	Щ	4						$\parallel$		Ц.	-	_	_		
	μ_	<u> </u>	 	Щ	<u>  </u>		+	<b> </b>	-		#	Щ	$\parallel$		_					$\parallel$	1			ľ																		
40				$\parallel$	:							$\parallel$	[			_		1	$\downarrow$					1	ŀ						Ţ			_	$\left[ \right]$		T	Τ		T		
,											$\Pi$	Π	Π	Τ				- ~	N				Ť		Ħ			Ħ	Ť		1	_			$\parallel$			$\uparrow$	+	┥		-
	$\square$			╢		$ \uparrow$	1	1	†		╢	†	$\uparrow$	֠	+		+		Ŧf	Ҟ	$\frac{1}{2}$	X	+		N		-+		+	$\left  \cdot \right $	+				$\parallel \mid$	$\left  \right $	+	+	+-			
30				╫	:	┝┼	+-	$\vdash$	+	• • • •	╫	$\left  \right $	┼┼	+			┞		╢	₽	Å	2	Å			ŀ—	_	-	╞		-			_			_	+	_	1		
		$\vdash$		#	-						#		$\parallel$				1		Щ			Å.	V.	1	Ц	ł																
20			·																			-	Î	đ		$\mathbb{N}$									Π				Γ	T		
																	Γ			IT	Ħ		1	-1			1	Ħ			1					$\dagger$	╈	┢	┢	╈		-
						╈			1-		Ш	ħ		+	+				╫	╟	$\ $	+	+	_	λ.	£∏ €	$\mathbb{H}$	∦	Η	+	┿	-			++	╢	+	┢		+		
10						+-					╢	+		╋			_		#			-			$\square$		Å.	-	$\downarrow$		_			_	4	$\parallel$			_			
							ļ	-	-		$\left  \right $	4			_				4					_			ЯĮ															
ol									1.91.1																		Î													Τ		]
			1(	00						1	0		G	84	۱۸۱	5	ZE	IN	1			стI				С	).1						(	<u>.</u> c	)1		-ł		<u> </u>	-	0.0	0
ſ							Ċ	R/	ν	EL.			Ť					IN		A	_	_	-	<u> </u>	_			-					-						_			7
		OBE	BLES		(	202	ars		Ť		ne			20	ars	sei	r	ne				, T		fi	ne			-				S	ILT	0	R	CI	LA	Y				
pec	ime	n lo	lentif	ica	ati	on	T				-						cai					<u> </u>	-	-			M	- 0/	Ť	L	(	T	PL	-						-		1
1	WF-	9		11	.1		1			PC	00	RL				_	E			Νſ		20				+	vi (		+		L	+	PL	-		PI	-			+	Cu	
1	WF-	9		13	.2		$\uparrow$					_	_		_		EC		_	_	_		_			+			+							_	-	-	.00		2.(	-
١	WF-	9		15	.1		1					_			_		1/ 5				_								┽		_	+		+	_		-	1	.08	\$	2.(	<u> </u>
١	WF-	9		17	.1		$\uparrow$		*	SH	EL									_	Т	70	E			+-			+			+					-	~		+		_
١	WF-	9		19	· · · ·		$\square$			SH																+			╇			+		-+			$\downarrow$	0.	51	+	5.8	Ĵ 
bec	imei	n Id	entif	-		n	†	D1			T	_	De	_	_	T		D3	_		Ť	-	D1	0			%(	311	1	1	0/		anc	_+		%			<b>—</b>			
	NF-			11			1		00		+	_	).2			+-		.1			+			10		+		-	_		_			+		70			<u> </u>	%(	Clay	/
١	NF-	9		13.			1		00		$\uparrow$		).2			+-		.1			+			22		╉		0.0 0.0		-	· · · ·	96	· · · · · ·	+					.2			-
٧	NF-9	9		15		<b></b> ,	1-		-		$^{+}$					╋		.3	~		+	_		16	_	+			, 	-+		97.	.9	+					.5	-		
٧	VF-S	}		17.	_		-				Ť	C	).5	53		+	-	.10	_	• •	+	_		<del>)</del> 6		+		_	-	+				-				· · ·	.0			
	VF-S			9.	_		ŀ				1-					$\dagger$		.49	_		+			)8		+				+				+					.8	_		
PRO	DJE	CT	Isol	at	ed	W	et	lan	ds	Dr	illi	١g	Ρ	ro	gra	an	<u> </u>				1	-			-	1			ō	BI	NO		_			11	67		.3			-
			Citr	us	P	roj	ec	t, L	.ee	Cd	110	ity	/, I	Fic	prie	da							- 					Ĕ	Ň	TE		•		_	1	/8	/9	9				
												- (	۶F	ł٨	٩Ľ	)/	١T	1(	٦C	L.	C	11	R	V	F	S																-

00	- <del></del>	6		3	- 2	1	ក់	12	1 1	122	/9	3	٨	6		01	014	16	20	. 30	0 /	BE 0 (		70	10	0.	~2	00													
ł		ŢŤ		Ň	Π	ή	Ţ	η		Π	Î	Π	Ţ	Π	<b>—</b>	ΪŢ	T	Π	ĨĬ	Π	Ţ	Ĭ	T	Ť	T	1	Ĩ	Π	Т					Ш	M	Π	Т	T	T		
Ĩ	╶┼╼┽╌	+			+	+	+-	$\neg$		+	╟	╟	+	┢	┢	+		-	╢	╢	+	+	╀	+			╢		-			+	-	₩		H	╀	+-	+		
90		+			$\left  \right $		+	_		_	#			╞	-				╢	Н				_			$\left  \right  \right $	$\parallel$	-			-		Щ		μ.	╀	+-			
ļ							_						_	L	ļ.,				╢		1													Ш		Ц	$\bot$		_		
80																																									
																				Π				T			Ш	Π						Π		Π	T	Τ	Τ		_
P E					Ħ	T	1			-	tt	Ħ		t	T	1		-	Ħ			Γ		┢	•										П			1	+		
	++-	-	╢		$^{\dagger}$	╈	+-	-		+	╫		╞	┢	╞	4	<u>}</u>		H	┢		-	+	╋					-				_	₩	+	┢╋	+	+	+		
E N		-	-		$\left\{ \cdot \right\}$	+	+			+	╟	$\left  \right $	+-	┝	-	4	<i>\\</i>	$\neg$	╢	$\left  \right $		-	+	+			H	-	-		-			╢	$\left  \right $	╟┼	+	+	+		_
<sup>7</sup> 60			-#		$\left  \cdot \right $	+		_		_	1				-	4	$\mathcal{H}$	$\mathbb{A}$	$\parallel$	$\downarrow$		-		_			Ш		_					Щ	Щ	$\parallel$	╞	+	_		
F			[]														7	$\square$	X															Ш							
E50																	,	Ń	١ľ	Ņ											-										
<b>a</b>			Π	T	Π	T	Γ				Π	Π		-		T	$\backslash$			Ĩ.	X		T	Ť				$\parallel$	1							T	T	T	1		
в			+	Ħ	$\parallel$	T	+-	-ŀ		+		$\left  \right $	ľ	+-	┢	+	$\uparrow$	-	Ħ	谨	N	1	$\mathbf{t}$	╉				$\dagger$	+	+		-	-	₩		$\uparrow$	+	+	╉		
<sup>4</sup> 40					┼┼	╉	+-			+	╢	+	-	┢	┢	+		H	╢	╢	ł)		k	,				$\left  \right $	+	-			_	╢	+	+	╀	+-	+		
				-	+	+	+	-				4	+-	Ļ.		-		_	Į.	$\parallel$	Ì	$\left  \right\rangle$	<b>\</b>	Ą.				$\prod$	4.							_	+	-	_		
30			_				$\bot$			_					ļ	_		_	₽	ļ		$\square$			<b>_</b>									Ш							
r l																				Ì		'	Ĩ,	X	Ø	2										;					
20																Τ			Π		Ì			V	¥	Ĩ								Π	Π	T		1	T		
20					Ħ	1		1						1		1			Ħ	Ħ			1	b	2	Ĵ		┢┟	+				-		$^{\dagger \dagger}$	╈	-	+	+		
ł	<u>+                                    </u>			ļ†-	H	┢	+-	_		+		+		-	$\vdash$	╉		+	╂	╟		-	-	┣	Æ	Ľ.,	H	╢					-	₩	╫	╈	+	+			
10	┥┝╍	+	-#		╎┼	+	+	+		-+	+	+				+	••••	+	╢					+	_	$\theta$	Ű	┦┤	+						╢	╀	$\vdash$		+		
-	+				$\left  \cdot \right $	╀		_		_	4	+	<b> </b>	-	_	_		_			-			$\downarrow$		6			-					Ш	Ц	$\downarrow$	L	$\bot$	$\downarrow$		_
οĹ														_							L													Ш							
			100	)						10	)		GF	٩AI	N :	SIZ	ZE II	1 N N	/IL	Lin	NE.	τει	RS			0.	1					(	0.0	)1						0.	. C
Γ		BBLE	 C	1			GR	A١	VEI			_	Τ	_	-	-			S		-			-			1										-			- <b></b>	7
		BBLE	5		co	ar	se			fin	e		С	oa	rs	e	m	ec	liu	m	Τ			fin	e						5	SILT	0	)R	С	LΑ	١Y				
Spec	imen	lden	tific	at	ior	1		_					С	las	ssi	fic	ati	or	1							N	1C	%		LL	Τ	PL		Γ	PI			Сс		(	շե
	NF-9		2	5.5	5				*S	AN	ID	Y	LI	M	ES	Т	ON	E	W	1 5	SH	EL	L.			T															
	NF-9		2	7.5	5				*S	A٨	D	Y	LI	M	ES	T	ON	E	W	/ 5	SH	EL	L						1								0	.6	0	13	3.
· ·	NF-9		34	1.5	5				*5	SIL	T١	<u>′ 1</u>	.11	٨E	S٦	ГС	NE	V	V/	S	HE	LL							1								0	.3	3	14	<b>1</b> .
	<b>NF-9</b>		36	3.3	}				* 5	SIL.	TΥ	ί μ	.11	/IE	ST	ГО	NE	E V	V/	S	HE	LL	_						Γ								+	.34		20	).
	NF-9			3.2	_				*5	SIL.	T١	1	.11	/E	ST	го	NE	: V	V/	S	HE	LL	•														0	.3	5	11	1.1
7	imen	Iden	tific	ati	ior		0	010	00			C	26	0			C	)3	0			(	D1	0		9	6G	ra	ve	1	%5	San	t		%	Si	lt	Τ	%	Cla	aγ
	NF-9			5.5		_										Ĺ	0.		_			0.	13	0	1												3	3.7	,		
	NF-9			7.5								1	.4	6			0.	3	0	_		0.	10	93	3	Γ											E	5.6	;		_
<u> </u>	VF-9			1.5								1	.0	8			0.	16	6	_		0.	07	58	3					T							ç	9.5	; ;		
+	VF-9			5.3	_			_				1	.8	3			0.	23	39			0.0	09	15	5	Γ			-	Τ		-					Ę	5.4	ŀ		
	VF-9		38								-		.0				0.						09	09	}				_								7	7.4	ŀ		
PR(	OJEC.	T le C	itru	teo Is	d \ Pri	N€ oi≉	tla	nc	ls I ee	Dri Co	llir	1g	Pi		gra	am	<u>ı</u> -	Ph	as	se	I	•	•							N	0.			<u> </u>	1	16	3			_	
				-		-10		-			u						L L						D	V		2			A	<u> </u>					1/8	5/5	19				

r

.

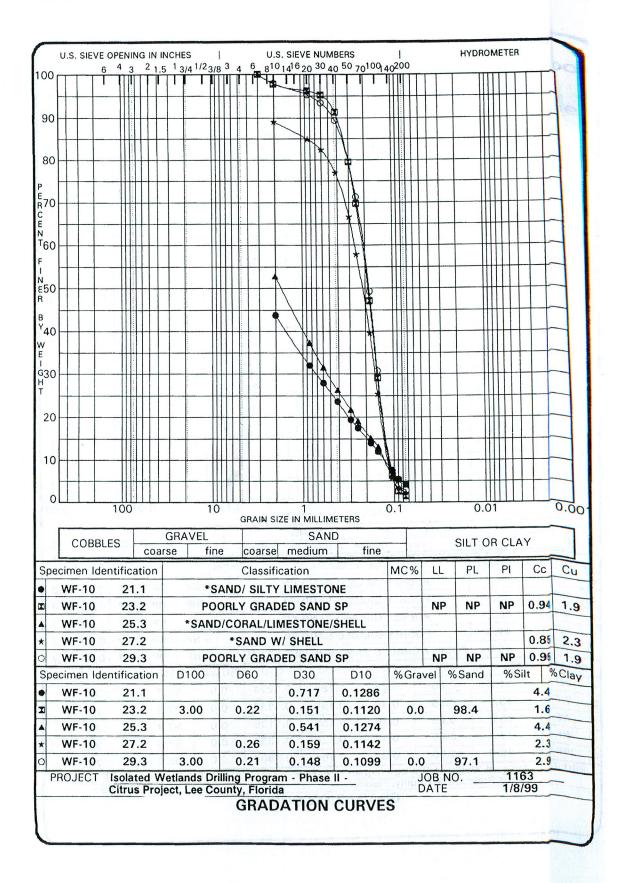




2

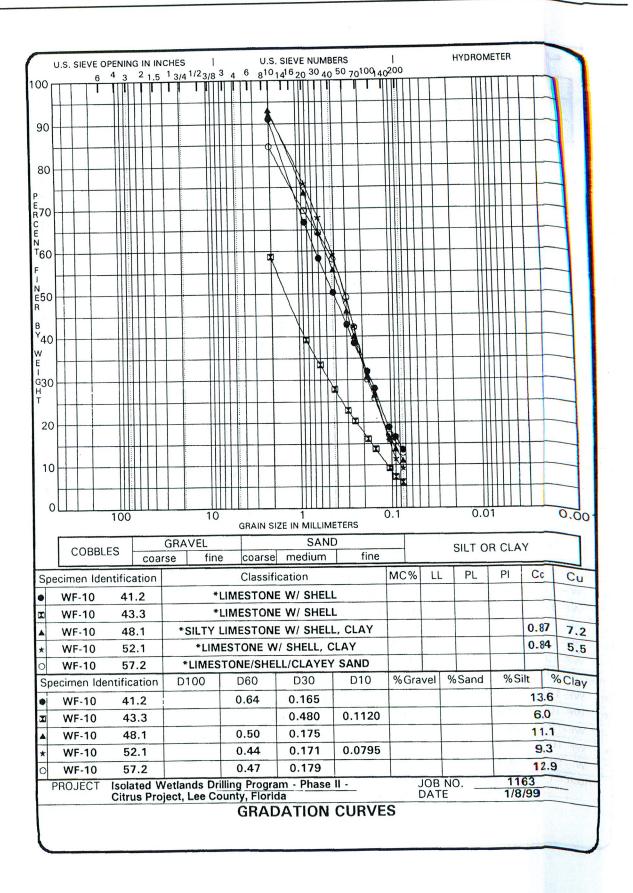
		.s. s	IEVE					IN				1/2		1	3			6			s.∶									<u>_1</u>	იი		-26						Н	Y	DR	٥N	ΛE	TE	R			
100	Π	-	Τ.		İ	3	Ē	T	7	Π	14	T	3/	'8 T	л П	4	T	19	8 ۲	T			TI	0 N≣	30 T		0 *	T	7	0' 	T	140	γ Π	Ш	П	Τ-	-				П	Π	Т	П	<b></b>	r	Т	
	$\left  \right $				╢	;	$\left  \right $		-	_			-	+		-	+	_	7	Ť			#	4	Ŧ	Ņ		Ļ		<b> </b>		_	Ц				_				Щ		Ļ				4	
90																				R	\				Į		N			ł																		
00													Π	Π		ļ	T			T	1	\	T	11	T		N	٩ <u>,</u>				1		TI		T		-			11	Ħ	ϯ	Π			T	
	Ħ			-				┢	T	-			$^{\dagger\dagger}$	Ħ	+	t	╈	+		$\dagger$		-/	Ħ	Ħ	$^{+}$	┢	Н	t,	Ĭ			+		H	+	╀	+	+			╢	╢	+	Η	-		╈	
80	$\left  \right $					-	-	+-	+	-			╢	+		╞	+	+	_	╉		_	fk	╢	╀			ľ	Į/	_		4		μ	-	-					#	#	$\downarrow$					
	H		_			:	_		1	_				Ц				_					╢	L)	¢			I	1																_			
- 70																												ľ	Ì	l.																		
2					Ш								T	Π	T	i.	T	T		T			Ħ	Ħ		à	5	Ħ		T				Ħ	1	T	1	1			Ħ			1	-		1	_
E Vi	Ħ		+		₩		+	+	+-	-			╫	╢	╋		+-	+		╀			$\ $	╟	+		-			Ĥ			-	╢	+	+	╉	-			╢	╟	H	_	-		+	
60	H					$\left  \right $	-	+	+	-			╢	$\left  \right $	┽		╞	+		╀							-{	μ	$\left  \right $			-			+	+	╞	-			#		$\square$	4	4		-	
<del>.</del> I	$\mid$				$\ $		-	$\downarrow$	-	_		•	#	Ц	1			1		1			Щ	$\parallel$			2	¥																				-
50	Ш				Ш																	1			$\ $			N	$\left \right $														Ī	T	T	_		
100						IT				T			Π	Π	Τ	-	T	T		T				T	Π			9	211	1		$\parallel$		Ħ	T	t	1	╈					Ħ	$\dagger$	+		1	
1	$ \uparrow$	+	+	-			╉		1-	-			tŀ	╟	$\dagger$		-	+		+				+				┝	╢	ݱ	-	╢		+	+	$\vdash$	┢	+		_	$\ $	+	$\left  + \right $	+	+		+	·
40	╟┼		+		$\parallel$	$\parallel$	╀	+		-			$\left  \right $	╟	+		┞	+		┞		_	+	╀	$\parallel$		-		4		_	$\parallel$		-	+		-				Щ	$\parallel$	$\mid \mid$	+	$\downarrow$			
V	$\mid \downarrow$		-	_	Ц.		-			_			Щ				L	1		L			$\parallel$							FI.						L												
30											_																					$\prod$	I	Γ	Γ	Γ		T			Π	Π		T		i		
						Π	Т	Ι		ŀ							Γ	T		ſ			Ħ							Ľ		╢	Ħ	t	1			+				$\dagger$	+	-	┢			
		+	1		Ħ	Ħ	╀	+		+		-		$\dagger$		-	-	+-	_	$\vdash$		-	╢	+		+	-		f	łá	}	╢		╉	$\left  \right $		<u> </u>	+		_	╢	+	+	╉	-	_		
20			+	-+		╟	+			-		-		+	Η		-	-				-	$\prod$	$\left  \right $		4	_		_	Ţ		#		-						_	$\parallel$	$\downarrow \downarrow$		1	-			
			ļ	_	$\parallel$	11			_			_							_												N																	
10		·																												J		Ŷ.						Τ			Π	Π	T		T			
											-		Π					Γ				T	Π	Π	T	1	1		T		Ţ	R	¢	t				┢		1	Ħ	Ħ	╞	1	╈			
		T	1						-		_		Ħ	t					-			+	Ħ	Ħ	╉		┥		╋		-			+	$\left  \cdot \right $	-	_	+-		╉	╢	╟	╀	╀	-	-		
0[		- <u>L</u>	I	10	0	Ц.	1			1		1	Щ	1		.		Ľ				1		11	1	1			_		0	Щ	3	1							<u>[]</u>			!				<u> </u>
r															(	GR	A	N	SI	ZE	IN	1 N	11L	LI	M	ET (	ER	s			U	• •							U	.0	1						(	0.0
	C	ОВ	BLE	s	+					<u>4</u> \	/El				_								S	41	١C	)	_	_		_			Γ					211	.T	0	0	~		v			-	
						_	-	irs	e		-	fir	e	_		co	ba	rs	e		me	ed	iu	m	_		_	f	fin	e	_					_	`	511	. 1		н —			ι Υ				
			den		-		n	_			•					-	_				tic	_									N	٨C	:%	6	ł	L		F	۲Ľ			ΡI			Сс	;		Сι
		-10			1.			-				o		_				_				-		_	_	_	_								N	١P		N	IP		١	٧P	,	1	.1	6		2.(
		-10			3.		_	-				0			_	_				_		_													N	IP		N	IP	Τ	١	١P		1	.0	4		1.7
		-10			5.			L				0			_				-		_		-	_	_		-								Ν	١P		N	IP	T	r	ΙP		1	.0	7	-	1.7
		-10			7.	_		-				0																							٨	ĮΡ		N	IP		N	IP		0	.9	2	1	1.6
		•10			9.			P			LY		R					s/			_		_	S	IL	_	-			M	-			I		IP		N	P		٨	IP		0	.9	1		3.7
		· · · · · · · · · · · · · · · · · · ·	den				n		D						D				1		D		_				D	10	)		9	60	àra	aν	el	[	%§	Sar	١d		(	%5	Sil	t		%	C	lay
		•10			1.:					.8	_				Э.					_0	).1	8	5			0	.1	22	24	ŀ		_0	).(	0	_		9	3.'	1			_		3	3.9	)	-	
		10			3.					.8				_	).				1.	C	).1	15	0			0	.1	13	33	5	Ĺ	C	).(	0			9	7.5	5	1					2.5			
		10		_	5.2					.8					).:		_				).1			_	<b></b>	· · · ·	1		-	-		C	).(	5			9	7.4	Ļ	+-					2.6		÷	
		10		·	7.3				_	.8				_	).	_	_				).1	_			-		.10		-			C	).(	)			97	7.5	5	Ţ					2.5			
PRC	_	10	1		9.0					.0				0	).:	33	3			0	).1	6	5			0.	0	90	)7			0	).(	_			92	2.2	2	T			_	7	.8			
r n(	JJE	-U I	Ci	ola tru	ite s l	a Pri	w ole	eti ect	lar I, L	id: .ee	s £ ∋ C	)ri	llír Jn	1g tv	F /.	rc Fli	or	ra	im la	1 -	P	ha	IS	e	11	-	-						J	0	B	N	0.	_		<u> </u>	1	1	63	3	_			
										-	-			1	<u></u>	_	A	-		_	_												_ L	A		C					1.	/8	/9	9				

ł



100	U.S	s. sie	VE O 6		NIN 3					s 4 <sup>1</sup>	/23	 /8	3	4	6	5	U.: <sub>B</sub> 10	s. ว <sub>1</sub> .	518 4 <sup>1 6</sup>	EVE 3 20	: N 3	UN 10 2	/BI 10	ER5 50	5 7(	010	00	4	ا 20						HY	DR	٥N	/E1	FEF	1			
100	Π		T	Π	Ţ		Ť	רן	Ť		ΠŤ	ÍŤ	Π	Ţ	Π	Г	ŤΤ		П	Ĩ	'n	Π	Ť	Т	Î	Ĕ	Г	Ĩ	Ť	Π	Т	T	r-			П	Π	Π	Т				
	$\mathbb{H}$			╢		╢	-+-	+	+				┝┼			┼─	$\frac{1}{4}$				-	$\left  \right $		+	-			-	╢				-	+		$\parallel$	$\parallel$	+			_		
90	Ц.							_							L		<u>a</u>	<u>۱</u>																									
•••																	ſ	X			Π			Ţ					Π		Τ	Τ				Π	Π	Π		Τ			
				╢	11	Ħ	+	1	-					ľ	┢	1	*	1	`		$\dagger$		-	+	-			-			+	+		+		╫	Ħ		-	+			
80	H-			╢	╟	╟	-	+-	-		+		╟	┝	╞	┼─	+	Ŧ.	ť	H	H	$\left  \right $	-					+	╢	H			<u> </u>	+		╢	╢	H	+				
5	$\square$				ļ			_	÷			11-				ļ		\ 	$\overline{1}$	ľ		1		_						Ц													
70					÷												ľ			N		Ŋ															11						
	Π			Т		Π			1				T			ſ	T	1		Ŋ	V	Ť	4	1					Ħ	Ħ	+			1	•••••	╢	Ħ	11	Ť	$\dagger$			
1				╢			╈	+	t		-1		+	ŀ	┢	┢┈	+	+		h	М	+	Υ	+	-			+	╢	H	+-	-		+		╫	╫	$\mathbb{H}$	╉		$\rightarrow$		
60	-			╢			╀	╞	╇		_			-	┞	ļ	+		f		Ŋ	<b>\</b>	-	¥.	-			_		$\left  \right $						#	11	11	+	_			_
											_											$\langle \rangle$		Τ																			
50																	ſ			M		N	Å		NT.			T		Π	Τ					Π	Π	Π	T				
50		†		11		T	$\uparrow$	1	1		-	$\parallel$	$\uparrow$		-	1	$\dagger$			ħ	Ħ	┦	N/	t	H			+	H	H	+	┞┤		+-		╢	╟	$\left  \right $	+	+	+		-
		$\left  - \right $		╢		+	+	+	╉		+	$\left  \right $	+	i.	<u> </u>	-	╀			╢	X	+	4	R	ł				H.		+-	┟╌┤		-		#	$\parallel$		+	+			
40	-	┣ ┃		#		4	-		-			$\parallel$			-		$\downarrow$			$\parallel$	<u>ال</u>			φq.	ŢĮ												Ш						
'																				$\ $		N			2)	6												IT			T		7
									T			11	Π		_		T			Ħ	Ħ		K		A,	T	<u> </u>	╢			$\uparrow$			1				Ħ	╋	╈	+	• • •	-
30		╞╌┨		$\parallel$	+	+	+	+	╞		+	╢	H				+		-	╢	╟	+	μ	+	╢	1	ᡏ᠆	╢		+	┢	$\vdash$		-		#	4	+	+	+	+		_
				$\parallel \mid$		+			+			$\parallel$	$\parallel$	_			$\downarrow$			Щ	$\mu$			1	Ĩ	ţ,	7	Щ								Ш		Ц					
20					:																			`	V	Å		ľ															
20									Τ			Π	Π				T			Ħ	Π	T	1	1	þ	7	T	ĥ	g	ϯ	T			-		111	$\dagger$		╋	$\uparrow$	+		┨
			<u> </u>			-	+	_	+	• • •	╢	Ħ	+		-		┢		-	╢	╟╋	+		$\vdash$	╉		$\emptyset$			╀	$\mathbb{H}$	+					+	-	┼╌	+		• •	4
10	+			╢		+-	$\vdash$		╞		-#	₽	$\left  \right $	-	_		_		_	μ.			_	L	-		Ì	Ŋ	U	1	$\square$	$\square$				Ш		_				_	
ļ				Ш								Ц															2	Į.					i										
o		Í																										Π		T	Π						11			1	T		
			1(	00					-L		10		<u></u>		_ 1		4	_	1		-1-	1.3		1	-		0	.1	1.1	1	Ц	l			0.0	<u>ш</u> 01	П	1	1	L	1	0.	] 00
r													) 	GR.	All	V S	IZE	11 E	1 1	11L		ΛE	TEF	٦S																		•.	•
	C	OBB	LES			_		iR/	<u>+</u> V				_				r-			<u>S/</u>		D											c	SIL 1	r c	)R	ſ	1 0	v				7
	<u>.</u>					_	ars	e	L	t	ine	)	_	-		se		m	-		n				fin	e	_			_	_						_						
			entif			on										sif											٨	10	29	6	ł	_L		Pl	-		ΡI			Сс		С	u
	WF-			31	.2					*S/	٩N	D	W	1	Sł	ίE	LL,	, L	.11	1E	<u>S1</u>	0	NE	Ξ															0	.6:	3	6.	3
	WF-			33			ļ			*S/						_			_	_	_									T			T						0	.7	1	6.	
	NF-			35	.4				*	'S/	٩N	D	W	1	Sŀ	łEl	LL,	, L	.IN	1E	ST	0	NE	-			Γ		-				T						0	.7	;	2.	-
	NF-			_	.3						*L	.IN	1E	Sī	го	N	E١	N	S	H	EL	L					1			1			ϯ							.85	-+	12	
	NF-	_			.4			* (	ŝA	NC	)/L	IN	E	ST	0	NE	١V	N/	S	HE	L	L F	R	AG	ì.		$\uparrow$		-	+			+					-			+		
bec	imer	n Id	entif	ica	tic	n		_	10	_	T	_	D	_	_	1		_	30	_			•••••	010		-	9	60	Gra	av	rel	9	6S	an	d		%	Sil	t	Т	%	Cla	v
V	NF-	10	3	31.	.2		1						0.0	64	ŀ	1	(	0.:	20	4		(		10:			$\vdash$					+-	_		-					⊥_ 5.1	, 0		,
٧	VF-	10	3	33.	2		1						0.	_			·	D. 1			-	_	_	08			$\vdash$			_													
٧	VF-	10		35.			┢				+	-	0.:			-+		).'	_		+			110									-		_		_			.8			
V	VF-1	10		37.							+		1.2		_	╉		).:			+			)98	_		-						·,							.3			
	VF-1			39.							+	_	0.1			╉		).'			┦						-										_			.3			
_	DJE		Iso	at	ed	W	/et	lan	ids	D	i rilli	ind	1 F	210	a	lar	n		- 0 2h:	, ac.		1.	-							10		NC	-				1 4	~		7.9			
			Cit	rus	P	ro	jec	t, I	Lec	e C	ou	Int	y,	FI	lor	id	a												ĭ	D/	٦R ۲	E	J.			1	11/8	6: 3/9	3 19				
												(	GĪ	R	A	D,	Δ.	ΤI	ī	N	1		1	21	/ 0	20	2									_		-	-				

4



1

