RETURN to Jim Andersen

M-135-

WELL COMPLETION REPORT FOR FLORIDAN AQUIFER WELL RO-4

Prepared for Martin County Environmental Services

September, 2000

Stemle, Andersen and Associates, Inc.

ENVIRONMENTAL \mathbf{g} HYDROLOGIC CONSULTANTS

FLORIDAN AQUIFER WELL COMPLETION REPORT **FOR PRODUCTION WELL RO-4**

MARTIN COUNTY ENVIRONMENTAL SERVICES

MARTIN COUNTY, FLORIDA

Prepared for

Hutcheon Engineers A Division of Kimley Horn and Associates, Inc. 4431 Embarcadero Drive West Palm Beach, Florida 33407

September, 2000

Prepared by Stemle, Andersen and Associates, Inc. 5307 Pennock Point Road Jupiter, Florida 33458

James L. Andersen, P.G. **Principal Hydrogeologist** Licensed Professional Geologist #1103

ENVIRONMENTAL AND HYDROLOGIC CONSULTANTS

7327 Catalina Club Circle Lake Worth, Florida 33467 $(561) 649 - 5369$ (561) 649-2390 FAX

5307 Pennock Point Road Jupiter, Florida 33458 (561) 745-9545 FAX (561) 745-9549

October 6, 2000

Ms. Dana Branscum, P.E. **Kimley-Horn and Associates** 4431 Embarcadero Drive West Palm Beach, FL 33407

Re: Martin County Environmental Services RO-4 Well Completion Report

Dear Dana:

We are pleased to transmit the final well completion report for Martin County Environmental Services Floridan Aquifer Well RO-4. A complete set of geophysical logs is included with the report as Appendix B.

We appreciate the opportunity to provide our services for this project. Please do not hesitate to call if we can be of further assistance.

Sincerely, Stemle, Andersen & Associates, Inc.

Imarke! trupe

Amanda Krupa, P.G. Senior Hydrogeologist

Enclosures

TABLE OF CONTENTS

TABLES

FIGURES

APPENDICES

LIST OF TABLES

LIST OF FIGURES

APPENDICES

1.0 **INTRODUCTION**

This report documents the procedures, testing, as-built construction details and recommendations for Floridan Aquifer production well RO-4 for Martin County Environmental Services. The project site is located in Jensen Beach, Martin County, Florida, in Section 17, Township 37 South, Range 41 East, as indicated on Figure 1. Well RO-4 is located north of Jensen Beach Boulevard, on the east side of the future extension of Deer Oak Drive. The well is less than one mile east of Federal Highway, and approximately 2,300 feet northeast of the North Martin County Treatment Plant as shown on Figure 2.

The North Martin County Water Treatment Plant produces potable water for Martin County using reverse osmosis treatment under South Florida Water Management District Water Use Permit No. 43000102-W. Well RO-4 increases Martin County's Floridan Aquifer brackish raw water capacity to approximately nine million gallons per day (MGD).

 $\mathbf 1$

WELL CONSTRUCTION AND TESTING 2.0

Hutcheon Engineers, a division of Kimley-Horn & Associates, Inc., and Stemle, Andersen and Associates, Inc. prepared technical specifications and conducted onsite observation during construction, well development, and aquifer performance testing.

2.1 **Drilling Methods**

Well RO-4 was constructed by Youngquist Brothers, Inc. of Fort Myers, Florida. Construction observation, development and testing were performed by Stemle, Andersen and Associates, Inc. (SAA) and Hutcheon Engineers. The methods and materials used by the drilling contractor were in accordance with 1) Technical specifications outlined in the contract document, 2) the standards of the American Water Works Association for Deep Wells (AWWA A100-90) and the National Water Well Association, and 3) South Florida Water Management District and Florida Department of Environmental Regulation rules and regulations. Well construction commenced on May 22, 2000 and was completed on August 25, 2000. The location of the well is shown in Figure 2. The drilling and casing depths are provided in Table 1. A schematic diagram of the well is provided as Figure 3. The drilling procedures used for the well are described below.

A nominal 36-inch diameter borehole was drilled to a depth of 203 feet below land surface (BLS) using the mud rotary method. The borehole was circulated to clear the cuttings from the mud and to prepare the hole for logging and setting of the surface casing. Geophysical logging (SP, resistivity, caliper, and gamma ray) was performed by Florida Geophysical Logging, Inc. as described in Section 2.7. The surface casing is 30-inch diameter, 0.375-inch thick steel pipe with factorybeveled ends. During installation, the ends were welded together, and centralizers were welded onto the casing at 40-foot intervals. Final depth of the

 $\overline{2}$

casing installation was 199 feet below land surface (BLS). Upon completion of the casing installation, the annular space surrounding the casing was pressure grouted in a single stage-using API Class B Portland Cement, with 118 barrels of a 6% bentonite mixture followed by 65 barrels of neat cement. The cement was allowed to cure before drilling was resumed.

After drilling out the cement plug, a nominal 12-inch pilot hole was advanced from the base of the surface casing to a depth of 900 feet BLS. The pilot hole was drilled using the mud rotary method and a 12 1/4-inch bit. Lithologic samples were collected during drilling from the circulating mud. A field lithologic log was maintained by SAA. Pilot hole drilling continued until suitable competent limestone was encountered near the top of the Floridan aquifer. The maximum drilled depth of the 12-inch pilot hole was 900 feet BLS. After the pilot hole was completed, drilling fluid was circulated to clear the hole of cuttings, and to prepare the hole for logging. Geophysical logging (SP, resistivity, caliper, and gamma ray) of the pilot hole was performed by Florida Geophysical Logging, Inc. as described in Section 2.7.

Following logging, the pilot hole was reamed to 24-inches in diameter using the mud rotary method and a staged bit assembly consisting of a 12-inch diameter lead bit and a nominal 24-inch diameter reamer bit. To keep the reamed hole from deviating from the pilot hole, weight on the bit was kept to a minimum; with the drill string held plumb by the drill collars and bit assembly. After circulating the drilled cuttings and conditioning the drilling fluid, the drilling tools were removed and Florida Geophysical Logging, Inc. conducted caliper logging on the 24-inch reamed hole, as described in Section 2.7. Logged depth of the reamed hole was 895 feet BLS.

The 18-inch diameter intermediate casing string was installed into the 24-inch diameter borehole to a depth of 895 feet BLS. The intermediate casing consisted of 0.375-inch steel pipe, with factory-beveled ends, which were arc-welded

together during installation. The top of the 18-inch casing string was completed at 176-feet BLS, and overlapped the 30-inch diameter surface casing by 23 feet. The intermediate casing was pressure-grouted using API Class B Portland cement. The initial grouting stage was neat cement for maximum strength near the base of the casing. Subsequent grouting stages included a 6% bentonite mixture. Grouting continued until the annular space between the 18-inch casing and the 24-inch borehole was completely filled with cement.

After the cement cured, drilling resumed using the reverse-air rotary method. Drilling was conducted using formation water with added clear water for drilling fluid. A nominal 17-inch diameter borehole was drilled from the bottom of the 18inch casing to a total depth of 1,375 feet BLS. Lithologic samples were collected during drilling, and the field lithologic log was maintained by Stemle, Andersen and Associates, Inc. Flow testing was conducted during drilling of the 17-inch borehole. Upon reaching the total depth, the driller cleared the borehole of drill cuttings. Florida Geophysical Logging, Inc. conducted borehole logging (SP, resistivity, caliper, gamma ray, fluid conductivity, flow velocity, and temperature) as described in Section 2.7.

The final casing depth of 1,065 feet BLS was determined based on lithologic samples, water quality data, flow test results, geophysical logs, and flow and water quality logs. The primary objective was to select an interval within the Floridan aquifer with the best water quality and high permeability. The selected interval must have competent formation material to minimize erosion and the subsequent contribution of particulate matter to the raw water. The interval that was selected is a flow zone sequence within the Avon Park formation (described in more detail in Section 3.1). The final casing string consisted of 140 feet of 16inch diameter PVC casing and 925 feet of 12-inch diameter PVC casing. The two casing strings were connected by a 16- by 12-inch reducer bushing. The PVC casing was Certainteed, Certa-Loc, SDR-17 lock coupling PVC casing. The annular space surrounding the PVC casing was grouted with neat cement to land

surface. Cementing was conducted in stages to minimize grouting stress on the PVC casing.

Water Quality Testing During Drilling 2.2

During reverse-air drilling in the Floridan aquifer, temperature, specific conductance and chloride concentration of the formation water were measured at regular intervals. Water samples were collected from the reverse-air discharge after the bit drilled at the desired sampling depth. Lag time (time it takes for the fluid or cuttings to be brought to the surface) was monitored at the onset of drilling following each drill rod change to ensure that samples were being obtained from the desired depths. At approximately every ten feet during drilling, temperature and specific conductance of the formation water were recorded. Additionally, after every ten feet or significant change in specific conductance, a water sample was collected for chloride analysis. Temperature and specific conductance measurements were conducted using a YSI model 3000 SCT meter. Performance of the meter was checked on a regular basis against reference standards. Chloride analysis was performed using a Hach titrator and silver nitrate titrant. A summary of the water quality data collected during drilling is provided in Table 2.

2.3 **Flow Testing During Drilling**

During reverse air drilling through the Floridan aquifer, flow tests were performed to evaluate the specific capacity of the penetrated open interval. The tests were performed after every drill rod change (approximately every 30 feet). To perform the test, a construction header was fitted to the flanged 30-inch diameter surface casing and sealed to the drilling tools with a rotating head. The header and rotating head effectively sealed the wellhead so that the well could be drilled under "live" artesian conditions. The construction header was equipped with a valve, a 12-inch diameter flow port, a 2-inch diameter port for adding brine "kill" water, and a %-inch manometer fitting. A manometer tube was fitted to the

construction header to measure the potentiometric (or static) water level which reached as high as 22 feet above land surface (39.75 ft NGVD).

During testing, the flow rate was measured using an in-line flow meter installed in the 12-inch diameter PVC line that discharged to a lined pond. Water levels in the well were measured during the pump test and compared to static, no-flow conditions measured at the beginning of each day and after each test. Measurement of flow rate (Q) and drawdown in the well (Δh) allowed calculation of specific capacity (C_s) of the well to be approximated using the formula C_s = $Q/\Delta h$ (Freeze and Cherry, 1979).

Table 2 includes a summary of the static and flowing water levels from flow tests conducted during the reverse air drilling phase.

2.4 **Well Acidization**

Well RO-4 was acid-treated on July 11, 2000 to increase specific capacity. The acidization procedure involved inserting 1,200 feet of drop tubing in the well, pumping 5,000 gallons of 32 percent hydrochloric acid into the open interval at a rate of 120 gallons per minute (gpm). Following the acid injection, approximately 2,500 gallons of potable chase water were pumped into the well at a rate of 47 gpm. During pumping, the wellhead was sealed and fitted with a pressure gauge to monitor pressure within the casing. A relief valve and gas discharge hose was in place on the wellhead to vent off excess pressure in the well if needed. Pressures were monitored continually during the process. Following the procedure, the well remained undisturbed until July 12 when well development was resumed.

Prior to acidization, the specific capacity was measured to be 56.6 gpm/ft at an artesian flow rate of 840 gpm. A pump was not yet installed in the well so the specific capacity could not be determined at a higher rate. To determine the percent improvement resulting from acid treatment, the first step of the step

drawdown test is used for the comparison. At the 830 gpm pumping rate, the specific capacity was 104.4 gpm/ft. This represents an 84 percent increase in specific capacity resulting from the acid treatment.

Well Development Pumping 2.5

The well was developed using a diesel-powered, vertical turbine test pump equipped with a ten-inch diameter pump and column pipe. Formation water was discharged to a lined pond via an underground 12-inch diameter PVC raw water main. The pond was regularly discharged to a nearby creek via stormwater discharge piping along Jensen Beach Boulevard.

Initially, the well was pumped at a maximum steady rate until the discharge water was visibly free of solids and turbidity. The maximum flow rate attained was approximately 2,800 gpm. Following the steady flow period, the well was pumped intermittently with surge and rest periods. Development progress was measured by performing silt density index (SDI) testing of the raw water. Additionally, the specific capacity of the well was measured on a daily basis during development to evaluate progress of improvement in well performance. Development began on July 14, 2000 and continued until July 21, 2000. SDI test results at the end of development had dropped to a value of 3.7. It is recommended that the utility continue pumping the well after the permanent pump is installed, and monitor SDI values until they are reduced to a value less than one (1).

2.6 **Drawdown Testing**

After completion of acidification and well development, a step-drawdown test was performed on the well using the development pump and discharge setup. The completed well was pump-tested to assess well yield and anticipated drawdown, and to aid in final pump selection. The flow rates for the test were measured by SAA with an in-line flow meter that was calibrated just prior to the start of the project. Prior to starting the test, the static water level was measured with the use of an elevated manometer tube. The measured static water level was 24.10 feet

 $\overline{7}$

above land surface (41.85 feet NGVD) on July 24, 2000. The step-drawdown test was conducted at 830, 1210, 1575, 2210 and 2980 gpm. These rates generally bracketed the proposed pumping rate of 1580 gpm for the well upon its completion. Water quality samples, including temperature, specific conductance, and chloride were collected at the end of each test step. SDI testing was also performed by SAA staff. . The results of the step drawdown test and water quality results are included in Table 3. SDI results ranged from 3.8 to 5.3 during the drawdown test. The results indicate that the well needs additional pumping to remove silt.

The drawdown data were used in conjunction with the pumping rates to obtain an estimated specific capacity value of 68 gpm/ft for the well at the proposed pumping rate of 1580 gpm. It is estimated that at a pumping rate of 1580 gpm. the water level will drop to approximately land surface, as seen during testing.

2.7 **Geophysical Logging**

Various borehole logs were conducted at each stage of well construction. The logs were used to aid in the decision-making and data-gathering process to determine hole dimensions, casing setting depths, geologic formation characteristics, water quality, and flow zone and aquifer characteristics.

An initial series of downhole logs was run on May 24, 2000, following the drilling of the 36-inch diameter hole to 199 feet BLS. The logs included spontaneous potential (SP), resistivity, caliper, and gamma ray.

A second series of logs was run on May 31, 2000, following the completion of the 12-inch pilot hole to 900 feet BLS. The second set included SP, gamma ray, resistivity, and caliper logs. On June 6, 2000, after the pilot hole was reamed to 24 inches in diameter, a caliper log was run on the reamed hole for installation of the intermediate casing.

On June 21, 2000, a final series was run after completion of the open interval from the bottom of the 18-inch casing to 1,375 feet BLS. These logs included SP, resistivity, caliper, gamma ray, fluid conductivity, flow velocity, and temperature.

The flow velocity log revealed the most productive zone from approximately 1190 to 1290 feet BLS. These results correlate well to the location of the production zone predicted from geophysical logging of nearby production wells.

All geophysical, flow, and video logs were recorded by Florida Geophysical Logging, Inc. Supervision was performed by an SAA hydrogeologist. Copies of the geophysical logs are included in Appendix B.

2.8 **Video Log**

A downhole television survey was run on the entire depth of the completed well on July 28, 2000. The video was performed by Florida Geophysical Logging, Inc. The video survey enabled inspection of the condition of the final casing string as well as the open-hole interval to the 1375-foot total depth of the well. The video showed that the PVC casing was in good condition, aside from some vertical scrape marks on the casing walls. The reduction from 16-inch to 12-inch diameter casing was apparent at 144 feet BLS, and the bottom of the 12-inch casing was noted at 1068 feet BLS. (These depths are slightly deeper than the actual depths verified by other methods.)

Just beneath the bottom of the casing, the open hole at 1074 feet BLS showed evidence of smooth cement that apparently invaded through the gravel during grouting of the casing. The borehole was clear to a depth of 1255 feet, with wide areas noted at 1093 and 1155 feet BLS. Smooth, uniform areas were noted at 1136-1137, 1160-1161, and 1188-1199 feet BLS. A large slab of rock was noted at 1202 feet, which sloughed off during video logging. At 1230 to 1232 feet, the color of the formation changed to dark gray. Below 1260 feet turbidity increased, in conjunction with a significant decrease in flow. The highly turbid, low-flow

condition persisted throughout the remaining interval. At 1374.6 feet BLS, the video went black as the camera reached the bottom. A copy of the video log is included with this report.

3.0 **HYDROGEOLOGY**

Beneath northern Martin County, there are two major aquifer systems, the Surficial Aquifer System (SAS), and the deeper Floridan Aquifer System (FAS). They are separated by a thick confining unit. The drilling of RO-4 penetrated the full thickness of the SAS, and partially penetrated the FAS. Well RO-4 was drilled to a total depth of 1,375 feet BLS. A hydrogeologist from Stemle, Andersen & Associates, Inc. was present during key phases of the drilling to collect lithologic samples and log the geologic formation materials encountered. The resulting lithologic log is provided in Appendix A. A generalized hydrostratigraphic section showing the typical lithologies, aquifers and formations encountered during drilling is provided as Figure 4.

3.1 **Surficial Aquifer System**

In descending order from land surface, the SAS formations include the Pamlico Sand, Anastasia, Fort Thompson, and the Tamiami Formation (Lichtler, 1960).

The thin covering of sand present over most of South Florida is known as the Pamlico Sand. It consists of fine- to medium-grained loose quartz sand grains, loose detrital clay and shell, and may be cemented as cap rock near the top of the present or previous water table surface. At RO-4, sand extends to a depth of about 40 feet beneath the site where it becomes interbedded with sandstone and shell. Because the Pamlico Formation does not have a distinct lower boundary, the exact depth is not known. The Anastasia Formation underlies the Pamlico Formation and comprises the majority of the SAS in this region. The Anastasia Formation ranges in composition from coquina ("beach rock") to pure quartz sand, often with varying mixtures of shell, sandy limestone, and sandstone as

well. In Martin County, the Anastasia Formation is composed of sand, shell beds, and thin, discontinuous layers of sandy limestone or sandstone (Lichtler, 1960). Here, vertical changes in lithology tend to follow a downward progression from unconsolidated sand and shell to calcareous sandstone and limestone. Sandstone and limestone units in the Anastasia make up the water-producing zone of the surficial aquifer in this area.

Underlying the Anastasia Formation in this area is the Tamiami Formation (Pliocene age), and/or the formations of the Hawthorn Group (Miocene age). Specific depths and even presence of these units are unclear in the available literature, as it is difficult to distinguish between the Tamiami and the Hawthorn Group. With depth, the sand, shell, sandy limestone and sandstone underlying this site undergo a downward fining trend and become the underlying confinement of the SAS. At this site, the basal confining unit of the SAS occurs at a depth of approximately 180 feet, where marl, clay and interbedded sandstone predominate.

Intermediate Confining Unit 3.2

The intermediate confining unit consists of the relatively impermeable calcareous clays and silts of the Hawthorn Group. The Miocene-aged Hawthorn sediments consist of dense, olive gray, clayey, unlithified lime mud, fine- to very-fine-grained quartz and phosphate sand and silt. Also present are beds of shell and sandy limestone within the upper and lower reaches of the unit. Here, the intermediate confining unit is approximately 560 feet thick, extending to a depth of 737 feet beneath the site. The predominately clayey upper section of the unit is known as the Peace River Formation.

The sandy-phosphatic limestones and phosphatic lime muds and that underlie the Peace River Formation are of the Arcadia Formation. These occur to a depth of 860 feet and although they are part of the Hawthorn Group, the permeable

beds are considered to be part of the Floridan aquifer and may produce considerable amounts of water.

3.3 **Floridan Aquifer System**

The Floridan Aquifer System (FAS) is a confined aquifer that underlies the lowpermeability beds of the intermediate confining unit. The brackish upper portion, referred to as the upper Floridan aquifer, has been classified by the Florida Department of Environmental Regulation as an underground source of drinking water (USDW) because it has a total dissolved solids (TDS) concentration of less than 10,000 mg/l.

The upper Floridan is composed predominantly of interbedded limestones and dolomites of late Miocene to middle Eocene age. Four primary rock units comprise the upper Floridan aquifer. From approximately 737 feet beneath the site, in descending order, these units are the Arcadia Formation limestones (Miocene age), Suwannee Limestone (Oligocene age), Ocala Group and the Avon Park Limestone (Eocene age). The uppermost rock unit (Arcadia) was cased off by the intermediate casing string because of poor consolidation.

The maximum depth penetrated during drilling was 1,375 feet. The lithology approaching the terminus of the well consists of interbedded, microcrystalline limestone, dolomitic limestone, and dolomite.

The producing zones within the Floridan aquifer can generally be referred to as "flow zones". A flow zone is typically a thin sequence of highly solutioned rock where water, flowing within the aquifer, is concentrated. Numerous thin flow zones may convey water to the open interval of a well and quite often, a high percentage of the water produced by the well comes from one or two thin flow zones.

Based on the lithologic logs, geophysical logs and wellhead flow data, the most productive flow zones occurred between approximately 1,190 feet and 1,290 feet BLS. These depths correspond to the same highly productive zones of the Avon Park limestone found in wells RO-1, RO-2, and RO-3. For the purposes of this report, this interval will be referred to as the mid-Floridan production zone.

Because the flow zones are typically separated from each other by continuous sequences of low permeability strata, water quality may very significantly with depth. As was found in similar wells drilled for Martin County water quality improves slightly with depth in the open interval of the well.

3.4 **Floridan Aquifer Head Pressures**

The aquifer artesian head was measured while drilling RO-4 to determine static head within the aquifer. Static head measurements were obtained using a manometer tube that was connected to the construction wellhead assembly and elevated by fastening the tube to the rig derrick. Static water levels were monitored during drilling; the measurements are summarized in Table 2. Upon completion of drilling and before commencement of the step-drawdown test, RO-4 had a static water level of 24.10 feet above land surface (approximately 41.85) feet NGVD). Results of the step-drawdown test are summarized in Table 3.

An increase in head was expected after penetrating the mid-Floridan production zone, as was the case in RO-3, where there was a significant change in head. However, that trend was not clearly evident during drilling of RO-4. It may be possible that there has been a decrease in head in the aquifer due to regional withdrawals.

PREDICATED DRAWDOWNS 4.0

Well RO-4 will experience two types of drawdown when it is pumped during the useful life of the well. The first type of drawdown is due pumping the well. The amount of drawdown in the well is a function of its specific capacity (pumping / drawdown rate). The second type of drawdown RO-4 will experience is the overall drawdown in the aquifer resulting from the withdrawals of surrounding existing and future wells completed in the same depth interval. This is known as wellfield drawdown or well interference effect. The amount of interference is dependent on the proximity of the surrounding wells. Based on the drawdown test results upon the completion of the well, RO-4 should maintain a pumping head approximately one foot above ground level at a pumping rate of 1580 GPM for now, although it may decrease as the aquifer yield decreases with the addition of more users.

5.0 **CONCLUSIONS**

The following conclusions are made based on results of the drilling and testing conducted during wellfield construction.

- Floridan aguifer production well, RO-4, was constructed for Martin County $1₁$ Environmental Services between May 22, 2000 and August 25, 2000. The well was constructed in three casing strings, which enabled testing of the upper Floridan aquifer for productivity and water quality prior to installation of the final PVC casing string. Total depth of RO-4 is 1,375 feet.
- At the design pumping rate of 1,580 gpm, the specific capacity value for $2.$ well RO-4 is expected to be 68 gpm/ft, with a pumping water level of one foot above ground surface.
- The chloride concentration in the groundwater sample collected from well 3. RO-4 after pump testing was 775 mg/l. Average chloride concentration of all samples collected during pump testing was 756 mg/l.
- The SDI test result at the end of development was 3.7. The SDI value can 4. be expected to decrease to less than 1 with continued pumping using the permanent well pump before the well is placed into operation.
- During testing, the static head in RO-4 was 24.1 feet above land surface. 5. or approximately 41.85 feet above MSL (NGVD).
- Most of the flow entering the well is produced from a 100-foot thick 6. sequence of dolomite and limestone beds in the Avon Park Limestone. The best flow zones were encountered at an upper depth of 1,190 feet in the well. This interval correlates to the same zones found in wells RO-1, $RO-2$ and $RO-3$.

RECOMMENDATIONS 6.0

- Before placement into operation, the well should be pumped to waste to $1₁$ reduce SDI values to less than one (1). The permanent well pump fitted to RO-4 will be satisfactory for this purpose and may be accomplished during the typical pre-startup testing of the well.
- At the design flow rate of 1,580 gpm and without significant interference $2.$ from other wells, the pumping water level in the well should be above land surface. The South Florida Water Management District (SFWMD) requires that Floridan aquifer wells in Martin County only be pumped at their land surface artesian flow rate. The operation of other nearby wells will lower the static water level in RO-4 and thereby lower the pumping level. A computer model impact analysis should be performed to evaluate the amount of drawdown this well will experience so that an appropriate pump setting depth can be determined.
- In time, incrustation of the borehole may cause the specific capacity to $3.$ degrade and pumping levels to decline. The incrustation is primarily composed of calcium carbonate, and hydrochloric acid treatment is typically an effective remedy for this condition. Acid treatment should be performed on the well if the specific capacity falls more than ten percent.
- Water levels should be monitored in RO-4 and existing wells RO-1, RO-2 $\overline{4}$. and RO-3. Water levels should be collected weekly on pumping wells and at least monthly on non-pumping wells. Not only will this confirm that pumping equipment is operating within design criteria, but it will allow tracking of well performance and forecasting of well problems.

- A monitoring program will also provide background Floridan aquifer water 5. levels, as competition for the resource escalates over time.
- Water quality samples should be collected monthly from pumping wells 6. and at a minimum, analyzed for chloride and specific conductance. Well pumping should be rotated so that all wells are used and monitored. Any time a water sample is collected, a minimum of three casing volumes of water should be purged from the well prior to sample collection. The Floridan aquifer is a leaky aquifer with varying water quality both vertically and horizontally. Additionally, water quality within the open interval of the well varies with depth and ranges from 725 mg/l to 1810 mg/l chloride. Given this, water quality at RO-4 is expected to vary. We anticipate that the chloride concentration will be at the low end of this range, but monitoring will better establish the actual range. Rotation of well usage minimizes the stress on the aquifer in any one area and will help to limit degradation of water quality.
- The well construction method specified for this project has proven to be 7. reliable, with fewer construction problems encountered than with alternate techniques on similar wells. This method allows testing of the aquifer at depth for collection of reliable data on aquifer properties and water quality. This method is recommended for future wells constructed for Martin **County Environmental Services.**

7.0 **REFERENCES**

- Freeze, R.A. and Cherry, J.A., 1979. Groundwater. Prentice-Hall, Inc. Englewood, N.J., 604 pp.
- Lichtler, W.F., 1960, Geology and Groundwater Resources of Martin County. Florida. U.S. Geological Survey Report of Investigations No. 23.
- Lukasiewicz, J. and Smith, K., 1996. Hydrogeologic Data and Information Collected from the Surficial and Floridan Aquifer Systems, Upper East Coast Planning Area. South Florida Water Management District Technical Publication 96-02, West Palm Beach, Florida. 224 pp.
- Miller, W.L. 1980. Geologic Aspects of the Surficial Aquifer in the Upper East Coast Planning Area, Southeast Florida. U.S. Geological Survey Open File Report 80-586. 2 sheets.
- Nealon, D., Shih, D., Trost, S., and others, 1987. Martin County Water Resource Assessment, Martin, Florida. South Florida Water Management District, **Resource Planning Department.**
- Parker, G.G., Ferguson, G.E., Love, S.K., 1955. Water Resources of Southeastern Florida. Water Supply Paper 1255. United States Geological Survey. Washington D.C. 965p.
- Stemle, Andersen & Associates, Inc., 1998. Floridan Aquifer Wellfield Expansion, Results Of Existing Water Use Inventory And Aquifer Drawdown Modeling For The North Martin County Reverse Osmosis Plant, Jensen Beach, Florida.
- Stemle, Andersen & Associates, Inc., 1999. Well Completion Report for Floridan Aquifer Well RO-3. Prepared for Martin County Utilities and Hutcheon Engineers. 20 pp.

WELL CONSTRUCTION DETAILS

MARTIN COUNTY ENVIRONMENTAL SERVICES PRODUCTION WELL RO-4

Abbreviations:

Ft. - feet DIAM. - Diameter INT. - Interval

 $in. - inches$ PVC - Polyvinyl chloride

SCH 80 - Schedule 80

Depths are feet below land surface.

PVC casings used in RO-4 were Certa-Lok (TM) type, manufactured by CertainTeed Corporation, Social Circle, Georgia.

WATER QUALITY AND WELL FLOW CAPACITY SUMMARY

MARTIN COUNTY ENVIRONMENTAL SERVICES PRODUCTION WELL RO-4 DRILLING DATA (FROM 930 TO 1375 FEET BLS) Reference elevation: +17.75 feet NGVD

WATER QUALITY AND WELL FLOW CAPACITY SUMMARY

MARTIN COUNTY ENVIRONMENTAL SERVICES PRODUCTION WELL RO-4 DRILLING DATA (FROM 930 TO 1375 FEET BLS) Reference elevation: +17.75 feet NGVD

WATER QUALITY AND WELL FLOW CAPACITY SUMMARY

MARTIN COUNTY ENVIRONMENTAL SERVICES PRODUCTION WELL RO-4 DRILLING DATA (FROM 930 TO 1375 FEET BLS) Reference elevation: +17.75 feet NGVD

Notes:

mg/l - milligrams per liter, chloride concentration determined by the silver nitrate titration method. µmos/cm - micromhos per cubic centimeter

°C - degrees Celsius

gpm - gallons per minute

orf - orifice weir flow measurement method

vm - timed volume flow measurement method

 \sim

FIGURES

 $\sim 10^{-1}$

 \mathcal{L}^{\pm}

 $\mathcal{A}^{\mathcal{A}}$

 \bar{z}

 ϵ

FOR: PROJECT
NUMBER: FIGURE
NUMBER: 4 FIGURE
TITLE: TYPICAL HYDROSTRATRIGRAPHIC SECTION IN THE VICINITY OF THE NO. MARTIN COUNTY TREATMENT PLANT

APPENDICES

APPENDIX A

RO-4 LITHOLOGIC LOG

l,

 \sim

RO-4 Lithologic Log Page 1 of 7

 $\bar{\mathcal{L}}$

MARTIN COUNTY ENVIRONMENTAL SERVICES **REVERSE OSMOSIS WELL NO. RO-4**

RO-4 Lithologic Log Page 2 of 7

 $\ddot{}$

MARTIN COUNTY ENVIRONMENTAL SERVICES REVERSE OSMOSIS WELL NO. RO-4

RO-4 Lithologic Log Page 3 of 7

MARTIN COUNTY ENVIRONMENTAL SERVICES **REVERSE OSMOSIS WELL NO. RO-4**

RO-4 Lithologic Log Page 4 of 7

 $\bar{\mathbf{v}}$

MARTIN COUNTY ENVIRONMENTAL SERVICES REVERSE OSMOSIS WELL NO. RO-4

RO-4 Lithologic Log Page 5 of 7

MARTIN COUNTY ENVIRONMENTAL SERVICES **REVERSE OSMOSIS WELL NO. RO-4**

RO-4 Lithologic Log Page 6 of 7

MARTIN COUNTY ENVIRONMENTAL SERVICES **REVERSE OSMOSIS WELL NO. RO-4**

Description

 \bar{z}

 \sim

APPENDIX B

GEOPHYSICAL LOGS

FLORIDA

MAIN PASS

BIT SIZE (in)

55

一、大小 一、大

y

Dual Induction Calibration Report Serial-Model: 1510-C Thu Apr 29 16:47:18 1999 Surface Cal Performed: Downhole Cal Performed: Wed Jun 21 09:15:45 2000 Wed Jun 21 09:46:07 2000 After Survey Verification Performed: Surface Calibration

References

REPEAT PASS

Database File: Dataset Pathname: Presentation Format: grxyc.prs Dataset Creation: Charted by:

run4/pass2 Wed Jun 21 08:07:24 2000 by Log VER_5.4

Depth in Feet scaled 1:240

jensbro4.db

REPEAT PASS

Database File: Dataset Pathname: Presentation Format: dil prs Dataset Creation.

FLORIDA

GEOPHYSICAL LOGGING, INC.

jensbro4.db run2/pass5

MERGED PASSES

Database File: Dataset Pathname:

 \mathbf{h}

jensbro4.db run4/pass16

 $\alpha_{\perp\parallel\parallel}$