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**April 18, 1994**

**Mr. Gene McLoughlin, P.E.  
MDWASA  
P.O. Box 330316  
Miami, Florida 33233-0316**

**Dear Mr. McLoughlin,**

The purpose of this letter report is to describe the procedures used and the results obtained from quantitative hydraulic analysis of a potential monitoring zone within the Floridan Aquifer system penetrated by Injection well I-15. The straddle packer test and subsequent hydraulic analysis were conducted in the zone of the aquifer between 1530 and 1560 feet below land surface (BLS).

**METHOD**

A straddle packer was used to isolate the test zone for drawdown and recovery tests. The formation tested is under artesian pressure, and was allowed to free flow during the drawdown portion of the test. Discharge was maintained at a constant rate by continuously opening a valve on the well head. Water level changes were measured in the drill stem with a pressure transducer and recorded on a Hermit 1000-C data logger. Prior to testing, the well was developed by pumping the formation fluid until the specific conductance stabilized. Specific conductance readings taken during the test are included in Appendix I. The well was then allowed to recover from development before performing the test.

## BACKGROUND

A 12 1/4 inch pilot hole was drilled below casing to a depth of 1900 feet below land surface. A suite of geophysical logs were run and, together with the borehole cutting samples, the test zone was selected by the WASA project hydrogeologist. The zone was selected between 1530-1560 feet below land surface. The zone was isolated with an inflatable 30 foot straddle packer with 10 feet of perforated pipe, open to the formation, between the two packer elements.

The packer assembly was lowered on the drill stem into the original pilot hole to the tested interval of 1530-1560 feet B.L.S. The packer elements were then inflated. After more than six hours of free flow, a constant specific conductance of 14,000 umhos was reached. The well was allowed to recover to its initial antecedent conditions and then allowed to flow for 1 hour while drawdown data was recorded. Recovery data were recorded until formation water level had again reached antecedent conditions. Background, drawdown and recovery water level data is graphed on Figure 1. The test was run at a flow rate of 130.4 gpm, and is analyzed as follows. Raw data are presented in Appendix II.

AQUIFER TEST I-15 ZONE 1530 - 1560

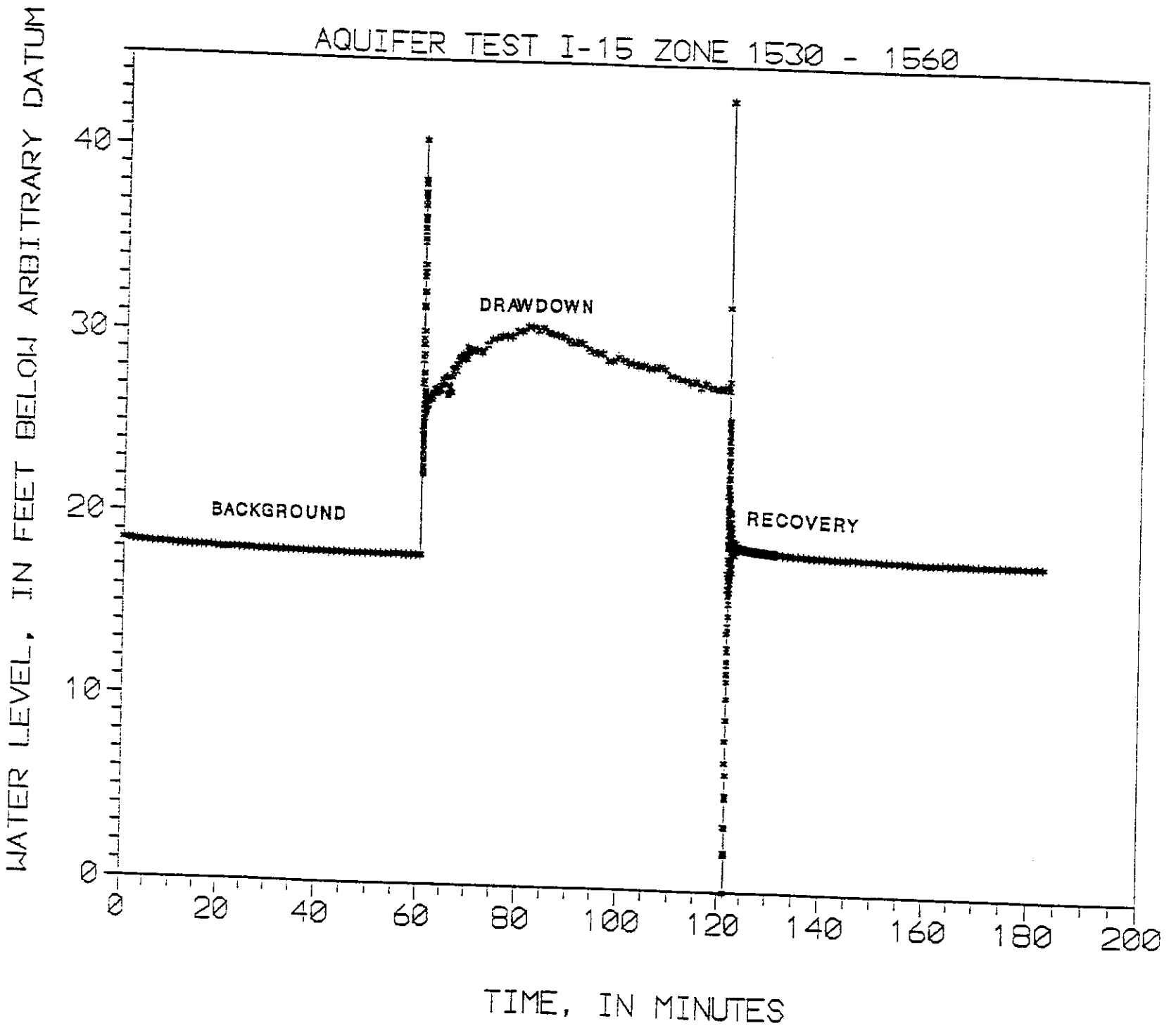


Figure 1-- Background, drawdown and recovery data from I-15, from 1530 to 1560 zone, arbitrary datum.

## DATA ANALYSIS

Three methods of data analysis were tested for this zone. The Theis curve analysis method yielded no data matches with any appropriate curves. The Theis Recovery method was tested but due to large amounts of surging after the well was closed, this data was not useable. This surging resulted from the water over recovering then stabilizing in the stand pipe. This rebounding is typical in high permeability formations. Only the Cooper-Jacob analysis method of drawdown was used for the test analysis to calculate the transmissivity for the packer setting between 1530 and 1560 feet below land surface.

### 1. Cooper-Jacob Analysis

The Cooper-Jacob method (figure 2) (Todd, 1980 p. 129) was used to compute a transmissivity value. The equation is as follows:

$$T = \frac{(2.3) (Q)}{(4) (\pi) (\Delta s_t)}$$

where

Q = discharge in cubic feet per day

$s_t$  = drawdown over one log cycle of time

The data were plotted on semi-log paper (s verses log t) and a straight line is fitted to the data.

COOPER-JACOB DRAWDOWN ANALYSIS 1-15 ZONE 1530-1560

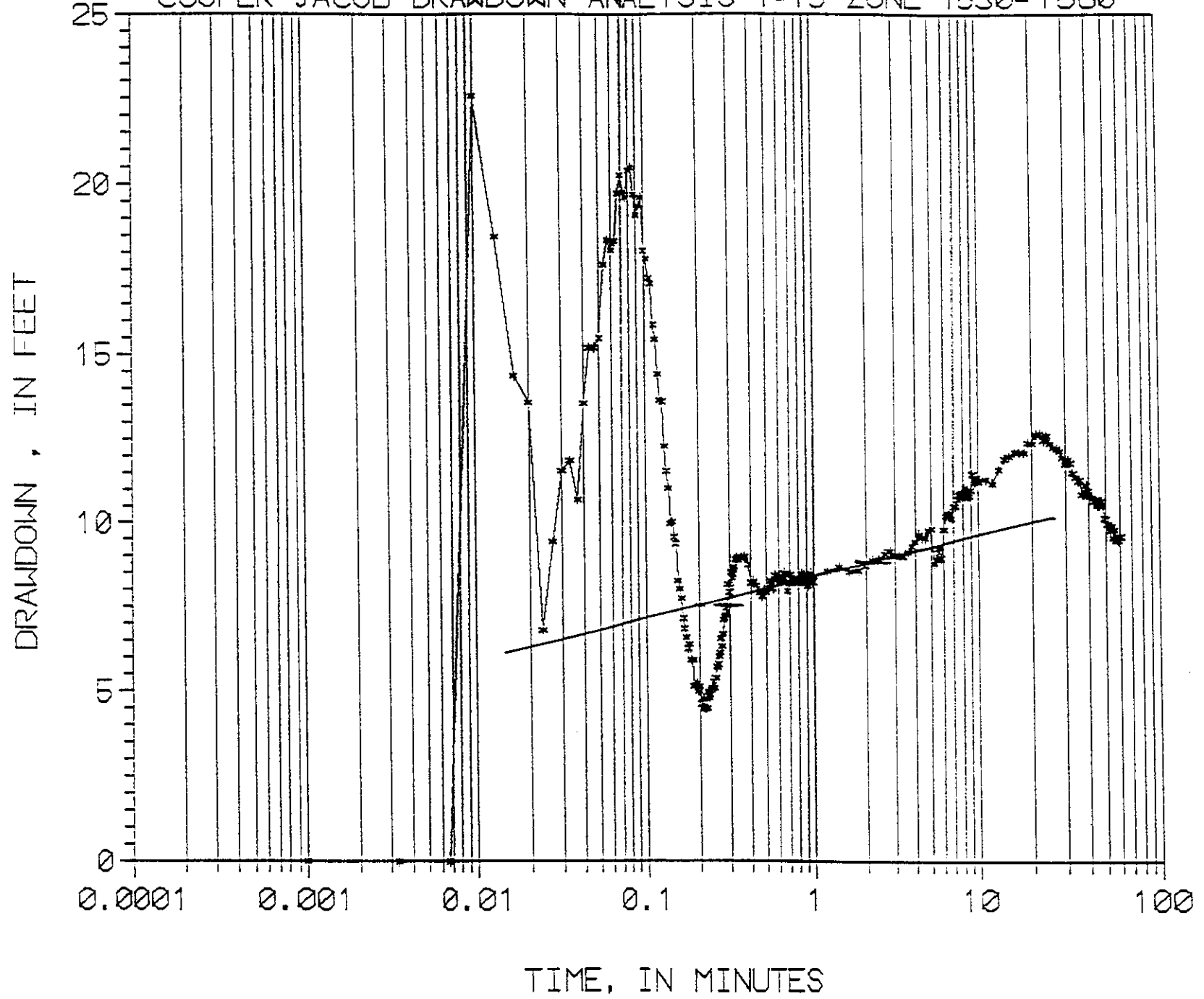


Figure 2.-- Cooper-Jacob Drawdown Analysis 1-15, zone 1530 to 1560

Using the observed drawdown over a single log cycle, (s), the transmissivity can be determined from the equation given by Todd (1980, p. 130) as:

$$T = \frac{2.3 (25100 \text{ ft}^3/\text{day})}{(4) (3.1416) (1.25 \text{ ft})}$$

$$T = 3677 \text{ ft}^2/\text{D}$$

Using a unit thickness of 30 ft., the horizontal hydraulic conductivity is:

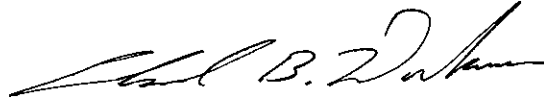
$$K = 122.5 \text{ ft/D}$$

$$K = 4.3 \times 10^{-2} \text{ cm/sec.}$$

This hydraulic conductivity is similar to the hydraulic conductivity in I-14, zone 1510-1540, which was  $3.2 \times 10^{-2}$  cm/sec.

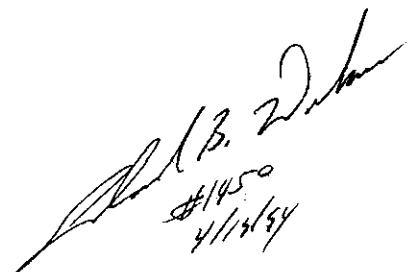
If you have any questions or comments please feel free to contact me or Leo Swayze.

Sincerely,

A handwritten signature in black ink, appearing to read "Edmand B. Workman". The signature is fluid and cursive, with a prominent initial "E".

Edmand B. Workman, P.G.

EBW/na

A handwritten signature in black ink, appearing to read "Edmand B. Workman". Below the signature, there are handwritten notes: "#1450" and "4/12/54".

## **Appendix I**

### **Specific Conductance Stabilization Data**



Packer Test (I-15)  
Zone 1530-1560

| <u>TIME</u> | <u>TEMP °C</u> | <u>CONDUCTIVITY umhos</u> |
|-------------|----------------|---------------------------|
| 11:20       | 23             | 13,100                    |
| 11:30       | 23             | 14,000                    |
| 11:45       | 24             | 14,000                    |
| 12:00       | 24             | 13,800                    |
| 12:15       | 22.5           | 14,000                    |
| 12:30       | 23             | 14,100                    |
| 12:45       | 25             | 15,000                    |
| 1:00        | 25             | 15,000                    |
| 1:15        | 25             | 15,000                    |
| 1:30        | 25.5           | 15,000                    |
| 1:45        | 25.5           | 15,000                    |
| 2:00        | 25.5           | 14,900                    |
| 2:15        | 25.5           | 14,900                    |
| 2:30        | 25.5           | 14,900                    |
| 2:45        | 25.5           | 14,800                    |
| 3:00        | 25.5           | 14,800                    |
| 3:15        | 25.5           | 14,500                    |
| 3:30        | 25.5           | 14,800                    |
| 3:45        | 25.5           | 14,800                    |
| 4:00        | 25.5           | 14,500                    |
| 4:15        | 25             | 14,500                    |
| 4:30        | 25             | 14,500                    |
| 4:45        | 25             | 14,500                    |
| 5:00        | 25             | 14,500                    |
| 5:15        | 25             | 14,500                    |
| 5:30        | 25             | 14,500                    |
| 5:45        | 25             | 14,500                    |
| 6:00        | 25             | 14,500                    |
| 6:15        | 25             | 14,200                    |
| 6:30        | 25             | 14,200                    |
| 6:45        | 24             | 14,000                    |

SE1000C  
Environmental Logger  
04/04 15:50

Unit# 01513 Test 0

-----  
Setups:           INPUT 1  
-----  
Type              Level (F)  
Mode              TOC  
I.D.              00000

Reference           0.000  
Linearity           0.280  
Scale factor        29.990  
Offset              0.120  
Delay mSEC         50.000

Step 0 04/02 21:09:49

-----  
Elapsed Time       INPUT 1  
-----  
0.0000            18.462  
1.0000            18.472  
2.0000            18.443  
3.0000            18.405  
4.0000            18.375  
5.0000            18.375  
6.0000            18.328  
7.0000            18.318  
8.0000            18.318  
9.0000            18.328  
10.0000           18.261  
11.0000           18.261  
12.0000           18.251  
13.0000           18.241  
14.0000           18.212  
15.0000           18.232  
16.0000           18.212  
17.0000           18.222  
18.0000           18.212  
19.0000           18.184  
20.0000           18.145  
21.0000           18.136  
22.0000           18.145  
23.0000           18.165  
24.0000           18.155  
25.0000           18.136  
26.0000           18.145  
27.0000           18.126  
28.0000           18.136  
29.0000           18.097  
30.0000           18.117  
31.0000           18.107  
32.0000           18.088  
33.0000           18.088  
34.0000           18.097  
35.0000           18.068  
36.0000           18.078

**Appendix II**  
**Raw Aquifer Test Data**

|         |        |
|---------|--------|
| 37.0000 | 18.059 |
| 38.0000 | 18.088 |
| 39.0000 | 18.039 |
| 40.0000 | 18.068 |
| 41.0000 | 18.068 |
| 42.0000 | 18.011 |
| 43.0000 | 18.049 |
| 44.0000 | 18.068 |
| 45.0000 | 18.011 |
| 46.0000 | 18.021 |
| 47.0000 | 18.039 |
| 48.0000 | 18.021 |
| 49.0000 | 18.011 |
| 50.0000 | 18.021 |
| 51.0000 | 18.021 |
| 52.0000 | 18.039 |
| 53.0000 | 17.992 |
| 54.0000 | 18.039 |
| 55.0000 | 18.049 |
| 56.0000 | 18.011 |
| 57.0000 | 18.001 |
| 58.0000 | 18.011 |
| 59.0000 | 18.001 |
| 60.0000 | 17.992 |

SE1000C  
Environmental Logger  
04/04 15:53

Unit# 01513 Test 1

-----  
Setups:           INPUT 1  
-----  
Type              Level (F)  
Mode              TOC  
I.D.              00000

Reference           0.000  
Linearity           0.280  
Scale factor        29.990  
Offset              0.120  
Delay mSEC         50.000

Step 0 04/02 22:12:32

-----  
Elapsed Time       INPUT 1  
-----  
0.0000            18.030  
0.0033            18.021  
0.0066            18.021  
0.0100            40.599  
0.0133            36.501  
0.0166            32.399  
0.0200            31.595  
0.0233            24.814  
0.0266            27.449  
0.0300            29.575  
0.0333            29.882  
0.0366            28.704  
0.0400            31.566  
0.0433            33.231  
0.0466            33.231  
0.0500            33.509  
0.0533            35.660  
0.0566            36.386  
0.0600            36.071  
0.0633            36.348  
0.0666            37.743  
0.0700            38.269  
0.0733            37.772  
0.0766            37.629  
0.0800            38.403  
0.0833            38.488  
0.0866            37.715  
0.0900            37.103  
0.0933            37.390  
0.0966            37.638  
0.1000            36.062  
0.1033            35.832  
0.1066            35.278  
0.1100            35.115  
0.1133            33.891  
0.1166            33.461  
0.1200            32.428

|        |        |
|--------|--------|
| 0.1233 | 31.662 |
| 0.1266 | 31.614 |
| 0.1300 | 30.294 |
| 0.1333 | 29.556 |
| 0.1366 | 29.039 |
| 0.1400 | 27.986 |
| 0.1433 | 28.043 |
| 0.1466 | 27.584 |
| 0.1500 | 27.392 |
| 0.1533 | 26.290 |
| 0.1566 | 26.041 |
| 0.1600 | 25.753 |
| 0.1633 | 25.169 |
| 0.1666 | 24.862 |
| 0.1700 | 24.594 |
| 0.1733 | 24.277 |
| 0.1766 | 24.392 |
| 0.1800 | 23.932 |
| 0.1833 | 23.922 |
| 0.1866 | 23.155 |
| 0.1900 | 23.174 |
| 0.1933 | 23.232 |
| 0.1966 | 23.011 |
| 0.2000 | 23.145 |
| 0.2033 | 22.637 |
| 0.2066 | 22.685 |
| 0.2100 | 22.772 |
| 0.2133 | 22.522 |
| 0.2166 | 22.483 |
| 0.2200 | 22.512 |
| 0.2233 | 22.982 |
| 0.2266 | 22.829 |
| 0.2300 | 22.906 |
| 0.2333 | 23.097 |
| 0.2366 | 23.097 |
| 0.2400 | 23.280 |
| 0.2433 | 23.097 |
| 0.2466 | 23.395 |
| 0.2500 | 23.730 |
| 0.2533 | 23.711 |
| 0.2566 | 23.807 |
| 0.2600 | 24.047 |
| 0.2633 | 24.143 |
| 0.2666 | 24.565 |
| 0.2700 | 24.354 |
| 0.2733 | 24.699 |
| 0.2766 | 25.130 |
| 0.2800 | 25.197 |
| 0.2833 | 25.255 |
| 0.2866 | 25.379 |
| 0.2900 | 25.542 |
| 0.2933 | 26.175 |
| 0.2966 | 25.820 |
| 0.3000 | 25.964 |
| 0.3033 | 26.079 |
| 0.3066 | 26.539 |
| 0.3100 | 26.366 |
| 0.3133 | 26.491 |
| 0.3166 | 26.616 |
| 0.3200 | 26.702 |

|        |        |
|--------|--------|
| 0.3233 | 26.932 |
| 0.3266 | 26.913 |
| 0.3300 | 26.989 |
| 0.3333 | 26.922 |
| 0.3500 | 26.970 |
| 0.3666 | 27.009 |
| 0.3833 | 26.779 |
| 0.4000 | 26.223 |
| 0.4166 | 26.271 |
| 0.4333 | 26.146 |
| 0.4500 | 25.936 |
| 0.4666 | 25.820 |
| 0.4833 | 25.993 |
| 0.5000 | 25.945 |
| 0.5166 | 26.089 |
| 0.5333 | 26.290 |
| 0.5500 | 26.060 |
| 0.5666 | 26.443 |
| 0.5833 | 26.405 |
| 0.6000 | 26.213 |
| 0.6166 | 26.271 |
| 0.6333 | 26.357 |
| 0.6500 | 26.520 |
| 0.6666 | 26.271 |
| 0.6833 | 25.993 |
| 0.7000 | 26.213 |
| 0.7166 | 26.472 |
| 0.7333 | 26.309 |
| 0.7500 | 26.348 |
| 0.7666 | 26.204 |
| 0.7833 | 26.319 |
| 0.8000 | 26.252 |
| 0.8166 | 26.280 |
| 0.8333 | 26.501 |
| 0.8500 | 26.261 |
| 0.8666 | 26.482 |
| 0.8833 | 26.261 |
| 0.9000 | 26.136 |
| 0.9166 | 26.146 |
| 0.9333 | 26.405 |
| 0.9500 | 26.520 |
| 0.9666 | 26.309 |
| 0.9833 | 26.252 |
| 1.0000 | 26.434 |
| 1.2000 | 26.568 |
| 1.4000 | 26.702 |
| 1.6000 | 26.577 |
| 1.8000 | 26.606 |
| 2.0000 | 26.750 |
| 2.2000 | 26.913 |
| 2.4000 | 26.932 |
| 2.6000 | 27.105 |
| 2.8000 | 27.181 |
| 3.0000 | 27.037 |
| 3.2000 | 27.037 |
| 3.4000 | 27.028 |
| 3.6000 | 27.152 |
| 3.8000 | 27.315 |
| 4.0000 | 27.468 |
| 4.2000 | 27.689 |

|         |        |
|---------|--------|
| 4.4000  | 27.593 |
| 4.6000  | 27.564 |
| 4.8000  | 27.794 |
| 5.0000  | 27.842 |
| 5.2000  | 26.827 |
| 5.4000  | 26.942 |
| 5.6000  | 27.267 |
| 5.8000  | 26.970 |
| 6.0000  | 27.823 |
| 6.2000  | 28.235 |
| 6.4000  | 28.264 |
| 6.6000  | 28.311 |
| 6.8000  | 28.158 |
| 7.0000  | 28.522 |
| 7.2000  | 28.513 |
| 7.4000  | 28.723 |
| 7.6000  | 28.876 |
| 7.8000  | 28.915 |
| 8.0000  | 28.771 |
| 8.2000  | 29.068 |
| 8.4000  | 28.991 |
| 8.6000  | 28.829 |
| 8.8000  | 28.829 |
| 9.0000  | 29.001 |
| 9.2000  | 29.470 |
| 9.4000  | 29.240 |
| 9.6000  | 29.240 |
| 9.8000  | 29.384 |
| 10.0000 | 29.250 |
| 11.0000 | 29.327 |
| 12.0000 | 29.192 |
| 13.0000 | 29.605 |
| 14.0000 | 29.920 |
| 15.0000 | 29.987 |
| 16.0000 | 30.131 |
| 17.0000 | 30.121 |
| 18.0000 | 30.102 |
| 19.0000 | 30.409 |
| 20.0000 | 30.389 |
| 21.0000 | 30.657 |
| 22.0000 | 30.667 |
| 23.0000 | 30.466 |
| 24.0000 | 30.628 |
| 25.0000 | 30.389 |
| 26.0000 | 30.274 |
| 27.0000 | 30.226 |
| 28.0000 | 30.160 |
| 29.0000 | 29.958 |
| 30.0000 | 29.767 |
| 31.0000 | 29.901 |
| 32.0000 | 29.805 |
| 33.0000 | 29.518 |
| 34.0000 | 29.374 |
| 35.0000 | 29.278 |
| 36.0000 | 29.307 |
| 37.0000 | 28.886 |
| 38.0000 | 28.886 |
| 39.0000 | 29.145 |
| 40.0000 | 28.982 |
| 41.0000 | 28.819 |



|         |        |
|---------|--------|
| 42.0000 | 28.800 |
| 43.0000 | 28.666 |
| 44.0000 | 28.733 |
| 45.0000 | 28.541 |
| 46.0000 | 28.551 |
| 47.0000 | 28.666 |
| 48.0000 | 28.532 |
| 49.0000 | 28.168 |
| 50.0000 | 28.139 |
| 51.0000 | 27.986 |
| 52.0000 | 27.986 |
| 53.0000 | 27.784 |
| 54.0000 | 27.929 |
| 55.0000 | 27.564 |
| 56.0000 | 27.813 |
| 57.0000 | 27.622 |
| 58.0000 | 27.526 |
| 59.0000 | 27.497 |
| 60.0000 | 27.603 |
| 61.0000 | 27.612 |

SE1000C  
Environmental Logger  
04/04 15:58

Unit# 01513 Test 2

-----  
Setups:           INPUT 1  
-----  
Type             Level (F)  
Mode             TOC  
I.D.             00000

Reference        0.000  
Linearity        0.280  
Scale factor     29.990  
Offset           0.120  
Delay mSEC       50.000

Step 0 04/02 23:15:17

-----  
Elapsed Time     INPUT 1  
-----  
0.0000           27.631  
0.0033           27.421  
0.0066           0.000  
0.0100           16.551  
0.0133           14.129  
0.0166           8.212  
0.0200           0.000  
0.0233           3.558  
0.0266           7.018  
0.0300           0.000  
0.0333           31.930  
0.0366           0.000  
0.0400           2.006  
0.0433           2.141  
0.0466           43.128  
0.0500           0.000  
0.0533           0.000  
0.0566           17.415  
0.0600           21.688  
0.0633           13.100  
0.0666           3.482  
0.0700           23.558  
0.0733           0.000  
0.0766           25.485  
0.0800           12.561  
0.0833           16.186  
0.0866           0.000  
0.0900           27.919  
0.0933           20.613  
0.0966           5.236  
0.1000           9.367  
0.1033           18.030  
0.1066           22.042  
0.1100           5.187  
0.1133           18.980  
0.1166           6.353  
0.1200           17.358

|        |        |
|--------|--------|
| 0.1233 | 14.494 |
| 0.1266 | 18.232 |
| 0.1300 | 5.052  |
| 0.1333 | 11.936 |
| 0.1366 | 22.138 |
| 0.1400 | 12.388 |
| 0.1433 | 11.878 |
| 0.1466 | 10.512 |
| 0.1500 | 22.244 |
| 0.1533 | 11.465 |
| 0.1566 | 19.307 |
| 0.1600 | 13.302 |
| 0.1633 | 17.175 |
| 0.1666 | 16.407 |
| 0.1700 | 21.994 |
| 0.1733 | 17.022 |
| 0.1766 | 13.100 |
| 0.1800 | 22.215 |
| 0.1833 | 21.016 |
| 0.1866 | 20.171 |
| 0.1900 | 14.177 |
| 0.1933 | 24.785 |
| 0.1966 | 20.238 |
| 0.2000 | 22.608 |
| 0.2033 | 18.827 |
| 0.2066 | 23.491 |
| 0.2100 | 21.668 |
| 0.2133 | 24.450 |
| 0.2166 | 23.385 |
| 0.2200 | 20.919 |
| 0.2233 | 24.181 |
| 0.2266 | 25.399 |
| 0.2300 | 25.667 |
| 0.2333 | 20.036 |
| 0.2366 | 25.715 |
| 0.2400 | 25.351 |
| 0.2433 | 25.840 |
| 0.2466 | 21.313 |
| 0.2500 | 24.977 |
| 0.2533 | 24.613 |
| 0.2566 | 25.063 |
| 0.2600 | 23.567 |
| 0.2633 | 22.733 |
| 0.2666 | 23.673 |
| 0.2700 | 24.056 |
| 0.2733 | 24.881 |
| 0.2766 | 20.594 |
| 0.2800 | 22.618 |
| 0.2833 | 23.059 |
| 0.2866 | 24.268 |
| 0.2900 | 19.806 |
| 0.2933 | 21.169 |
| 0.2966 | 21.668 |
| 0.3000 | 22.061 |
| 0.3033 | 20.142 |
| 0.3066 | 19.355 |
| 0.3100 | 20.018 |
| 0.3133 | 19.662 |
| 0.3166 | 20.526 |
| 0.3200 | 17.761 |

|        |        |
|--------|--------|
| 0.3233 | 18.174 |
| 0.3266 | 17.992 |
| 0.3300 | 19.893 |
| 0.3333 | 16.868 |
| 0.3500 | 15.744 |
| 0.3666 | 15.080 |
| 0.3833 | 16.272 |
| 0.4000 | 16.589 |
| 0.4166 | 16.368 |
| 0.4333 | 17.512 |
| 0.4500 | 18.856 |
| 0.4666 | 20.929 |
| 0.4833 | 21.524 |
| 0.5000 | 21.831 |
| 0.5166 | 21.515 |
| 0.5333 | 21.620 |
| 0.5500 | 20.785 |
| 0.5666 | 19.701 |
| 0.5833 | 18.251 |
| 0.6000 | 17.540 |
| 0.6166 | 17.069 |
| 0.6333 | 16.906 |
| 0.6500 | 16.877 |
| 0.6666 | 17.185 |
| 0.6833 | 17.886 |
| 0.7000 | 18.779 |
| 0.7166 | 19.662 |
| 0.7333 | 20.248 |
| 0.7500 | 20.670 |
| 0.7666 | 20.824 |
| 0.7833 | 20.718 |
| 0.8000 | 20.238 |
| 0.8166 | 19.576 |
| 0.8333 | 18.904 |
| 0.8500 | 18.299 |
| 0.8666 | 17.809 |
| 0.8833 | 17.512 |
| 0.9000 | 17.473 |
| 0.9166 | 17.694 |
| 0.9333 | 18.039 |
| 0.9500 | 18.597 |
| 0.9666 | 19.125 |
| 0.9833 | 19.643 |
| 1.0000 | 19.989 |
| 1.2000 | 19.442 |
| 1.4000 | 18.500 |
| 1.6000 | 18.443 |
| 1.8000 | 18.875 |
| 2.0000 | 19.125 |
| 2.2000 | 18.942 |
| 2.4000 | 18.702 |
| 2.6000 | 18.712 |
| 2.8000 | 18.827 |
| 3.0000 | 18.846 |
| 3.2000 | 18.788 |
| 3.4000 | 18.721 |
| 3.6000 | 18.731 |
| 3.8000 | 18.731 |
| 4.0000 | 18.760 |
| 4.2000 | 18.750 |

|         |        |
|---------|--------|
| 4.4000  | 18.721 |
| 4.6000  | 18.693 |
| 4.8000  | 18.702 |
| 5.0000  | 18.664 |
| 5.2000  | 18.693 |
| 5.4000  | 18.673 |
| 5.6000  | 18.683 |
| 5.8000  | 18.654 |
| 6.0000  | 18.635 |
| 6.2000  | 18.654 |
| 6.4000  | 18.635 |
| 6.6000  | 18.635 |
| 6.8000  | 18.644 |
| 7.0000  | 18.625 |
| 7.2000  | 18.616 |
| 7.4000  | 18.616 |
| 7.6000  | 18.616 |
| 7.8000  | 18.597 |
| 8.0000  | 18.597 |
| 8.2000  | 18.606 |
| 8.4000  | 18.587 |
| 8.6000  | 18.587 |
| 8.8000  | 18.568 |
| 9.0000  | 18.568 |
| 9.2000  | 18.587 |
| 9.4000  | 18.558 |
| 9.6000  | 18.568 |
| 9.8000  | 18.558 |
| 10.0000 | 18.558 |
| 11.0000 | 18.510 |
| 12.0000 | 18.500 |
| 13.0000 | 18.481 |
| 14.0000 | 18.443 |
| 15.0000 | 18.462 |
| 16.0000 | 18.405 |
| 17.0000 | 18.405 |
| 18.0000 | 18.395 |
| 19.0000 | 18.405 |
| 20.0000 | 18.366 |
| 21.0000 | 18.347 |
| 22.0000 | 18.357 |
| 23.0000 | 18.337 |
| 24.0000 | 18.357 |
| 25.0000 | 18.357 |
| 26.0000 | 18.318 |
| 27.0000 | 18.308 |
| 28.0000 | 18.328 |
| 29.0000 | 18.308 |
| 30.0000 | 18.280 |
| 31.0000 | 18.289 |
| 32.0000 | 18.289 |
| 33.0000 | 18.270 |
| 34.0000 | 18.261 |
| 35.0000 | 18.251 |
| 36.0000 | 18.241 |
| 37.0000 | 18.232 |
| 38.0000 | 18.241 |
| 39.0000 | 18.174 |
| 40.0000 | 18.222 |
| 41.0000 | 18.184 |

|         |        |
|---------|--------|
| 42.0000 | 18.241 |
| 43.0000 | 18.212 |
| 44.0000 | 18.193 |
| 45.0000 | 18.193 |
| 46.0000 | 18.222 |
| 47.0000 | 18.203 |
| 48.0000 | 18.174 |
| 49.0000 | 18.184 |
| 50.0000 | 18.174 |
| 51.0000 | 18.203 |
| 52.0000 | 18.174 |
| 53.0000 | 18.184 |
| 54.0000 | 18.203 |
| 55.0000 | 18.165 |
| 56.0000 | 18.203 |
| 57.0000 | 18.165 |
| 58.0000 | 18.165 |
| 59.0000 | 18.155 |
| 60.0000 | 18.203 |
| 61.0000 | 18.165 |