

# HYDROLOGIC ASSOCIATES U.S.A., INC. ENVIRONMENTAL CONSULTANTS

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September 7, 1994

Mr. Gene McLoughlin, P.E.  
MDWASA  
P.O. Box 330316  
Miami, Florida 33233-0316

Dear Mr. McLoughlin,

The purpose of this letter report is to describe the procedures used and the results obtained from quantitative hydraulic analysis of a potential monitoring zone within the Floridan Aquifer system penetrated by Injection well I-17. The straddle packer test and subsequent hydraulic analysis were conducted in the zone of the aquifer between 1580 and 1610 feet below land surface (BLS).

## METHOD

A straddle packer was used to isolate the test zone for drawdown and recovery tests. The formation tested is under artesian pressure, and was allowed to flow at a rate of 65 gpm during the drawdown portion of the test. Water level changes were measured in the drill stem with a pressure transducer and recorded on a Hermit 1000-C data logger. Prior to testing, the well was developed by pumping the formation fluid until the specific conductance stabilized. Specific conductance readings taken during the test are included in Appendix I. The well was then allowed to recover from development before performing the test.

## **BACKGROUND**

A 17 inch pilot hole was drilled below casing to a depth of 1900 feet below land surface. A suite of geophysical logs were run and, together with the borehole cutting samples, the test zone was selected by the WASA project hydrogeologist. The zone was selected between 1580-1610 feet below land surface. The zone was isolated with an inflatable 30 foot straddle packer with 10 feet of perforated pipe, open to the formation, between the two packer elements.

The packer assembly was lowered on the drill stem into the original pilot hole to the tested interval of 1580-1610 feet B.L.S. The packer elements were then inflated. After more than 8 hours of artesian flow, a constant specific conductance of 9,000 umhos was reached. The well was allowed to recover to its initial antecedent conditions. After recovery, the well was allowed to flow for 1 hour while drawdown data was recorded. Recovery data were then recorded until the formation water level had again reached antecedent conditions. Background, drawdown and recovery water level data is graphed on Figure 1. The test was run at a flow rate of 65 gpm, and is analyzed as follows. Raw data are presented in Appendix II.

AQUIFER TEST, I-17 ZONE 1580-1610

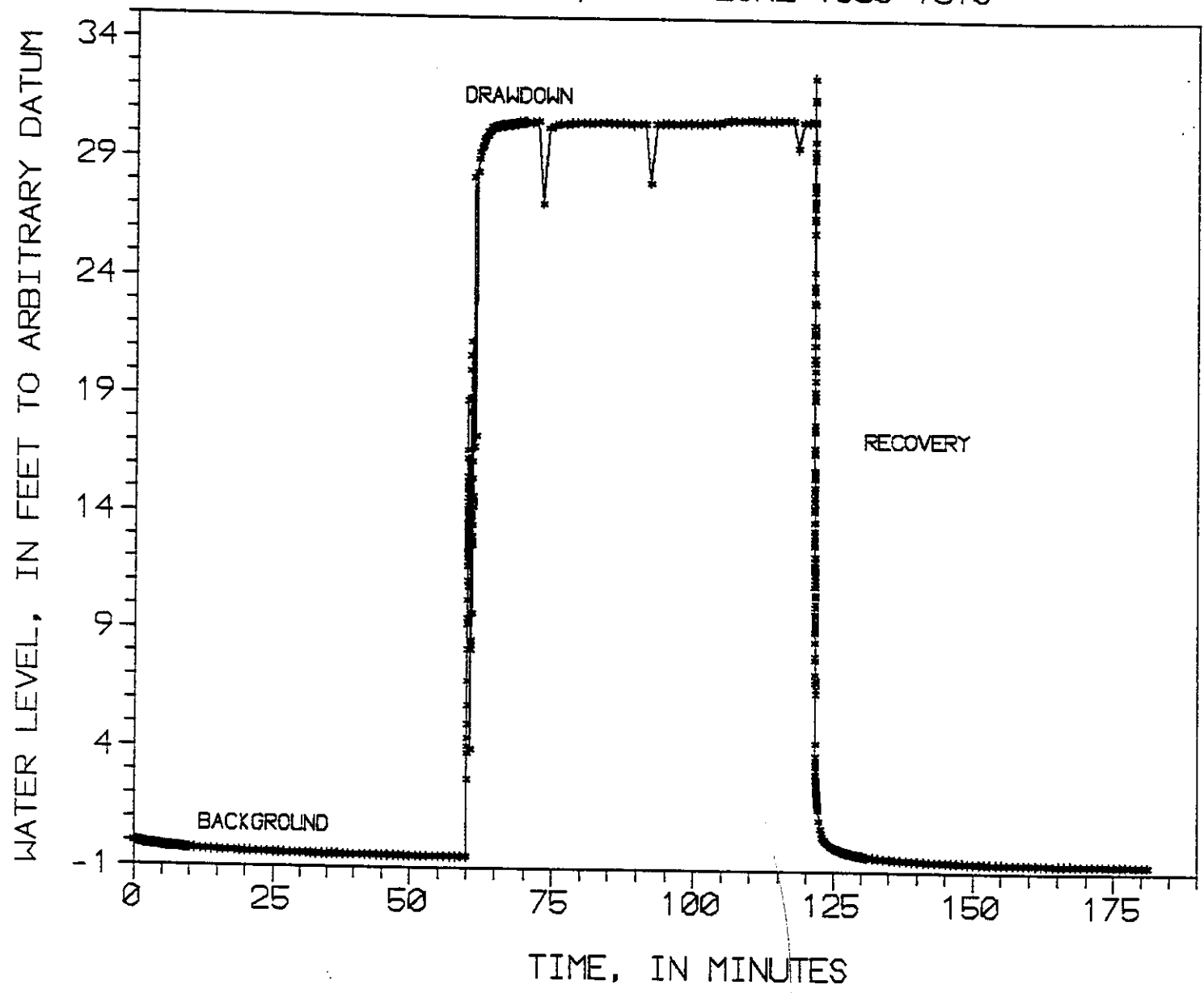


Figure 1.-- Background, drawdown and recovery water level data from I-17, zone 1580 to 1610.

## **DATA ANALYSIS**

Three methods of data analysis were tested for this zone.

1. Cooper-Jacob Analysis
2. Theis Analysis (Leaky)
3. Theis recovery analysis

### **1. Cooper-Jacob Analysis**

The Cooper-Jacob method of analysis was not conducted due to large amounts of surging in the well during the free flow drawdown portion of the test (see Figure 2).

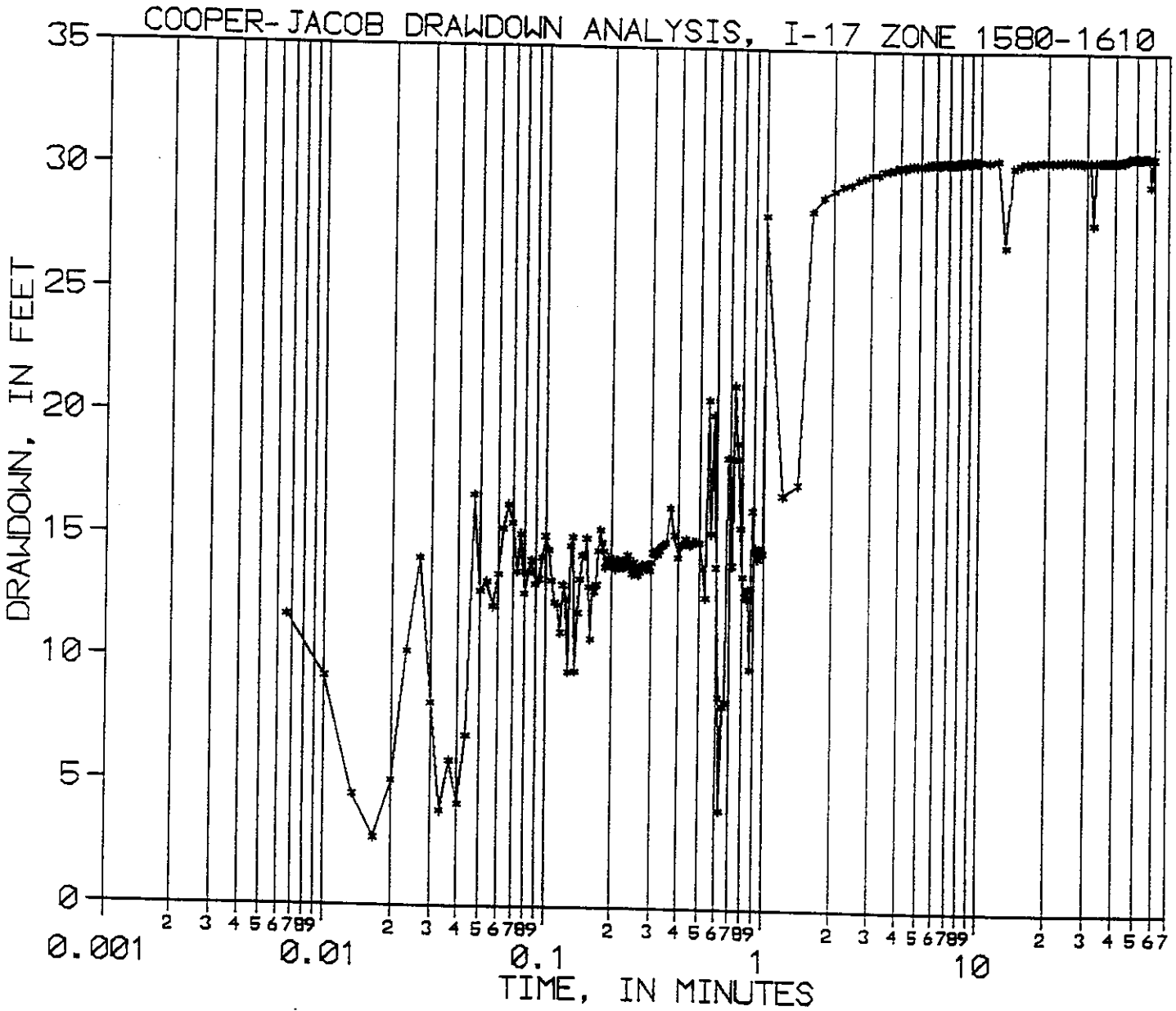


Figure 2.-- Cooper-Jacob Drawdown Analysis I-17, zone 1580 to 1610

## 2. Theis Analysis

The time-drawdown data for the packer test was analyzed using the Theis nonequilibrium equation given by (Todd, 1980, 123) as:

$$s = \frac{(Q) (W(u))}{(4) (\pi) (T)}$$

Where  $s$  is the drawdown,  $Q$  is the pumping rate and  $T$  is the transmissivity.

$W(u)$  is the well function and ( $u$  is the exponential integral function) where

$$u = \frac{(r^2) \cdot (S)}{(4) (\pi) (T) (t)}$$

Where  $r$  is the distance to the observation well ( $r$  = well radius for a single well test).

$S$  = Storage coefficient

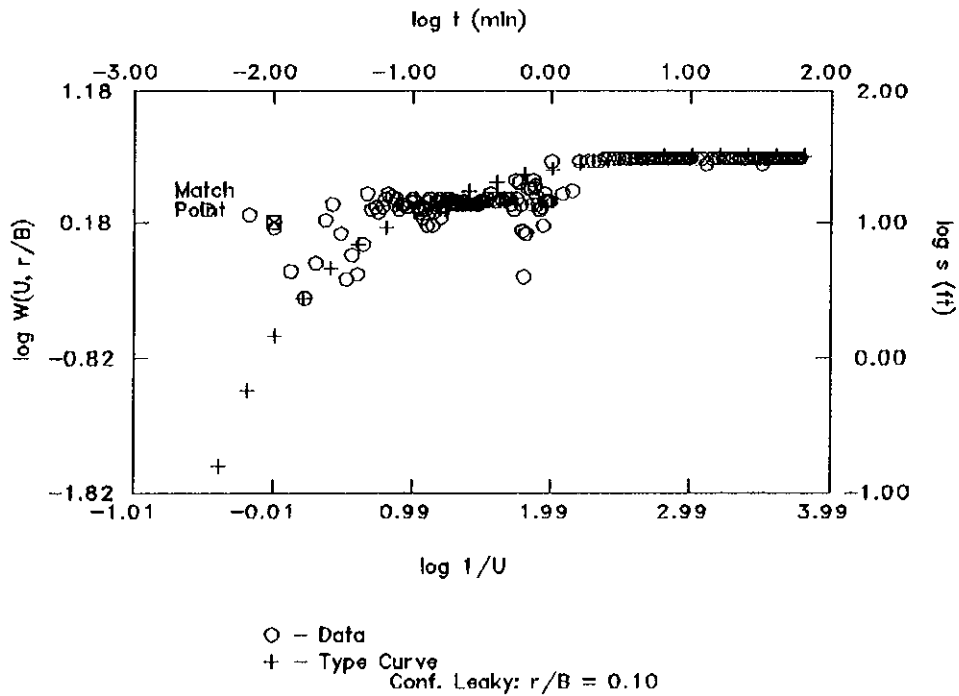
$t$  = Time since the start of pumping

Transmissivity and storage coefficient values were determined from the drawdown data by type - curve matching techniques as described in Todd (P125-128) and by using the computer package GWAP (Graphical Well Analysis Package). Figure 3 shows the type curve superimposed on the drawdown data plot and the resulting computed values for transmissivity, hydraulic conductivity and storativity (Storage coefficient divided by unit thickness). Values for horizontal hydraulic conductivity expressed in standard units are:

$$K = 37.6 \text{ gal/day/sq.ft.} \rightarrow 5 \text{ ft/d} \checkmark$$

$$K = 1.8 \times 10^{-3} \text{ cm/sec}$$

# I-17 ZONE 1580-1610



| MATCH POINT  |               | SOLUTION                   |                         |
|--|---------------|----------------------------|-------------------------|
| $t$  | = 1.000E-0002 | Transmissivity (T)         | = 1.127E+0003 gpd/ft    |
| $s$  | = 1.000E+0001 | Hydraulic Conductivity (K) | = 3.757E+0001 gpd/sq ft |
| $1/U$  | = 9.772E-0001 | Storativity (S)            | = 8.546E-0003           |
| $W(U, r/B)$  | = 1.514E+0000 | Leakage Factor (B)         | = 7.080E+0000 ft        |
| WELL INFORMATION                                   |               |                            |                         |
| WELL IDENTIFICATION                                |               | : I-17 158                 |                         |
| DATE OF AQUIFER TEST                               |               | : 7/31/94                  |                         |
| AQUIFER THICKNESS (b)                              |               | : 3.000E+0001 ft           |                         |
| DISCHARGE RATE (Q)                                 |               | : 6.500E+0001 gpm          |                         |
| PUMPING WELL RADIUS (r)                            |               | : 7.080E-0001 ft           |                         |
| DISTANCE OF OBSERVATION WELL FROM PUMPING WELL (d) |               | : 7.080E-0001 ft           |                         |

Figure 3.--Theis Leaky Curve Analysis I-17, zone 1580 to 1610

### 3. Theis Recovery Analysis

The Theis Method was used to analyze recovery in the well after the flow was stopped by shutting in the well, using the method as described in Todd (1980 p. 133). Residual drawdown,  $s'$ , was plotted against the log of the ratio of time from the start of flow to the time of shut down ( $t/t'$ ) (see Figure 4).

A straight line was fitted to the early time data and the change in residual drawdown over a single log cycle ( $s'$ ) was calculated. Transmissivity was then determined from the equation: Todd (1980, p.134):

$$T = \frac{(2.30) (12512.5) \text{ ft}^3/\text{day}}{(4) (3.1416) (25.5 \text{ ft})}$$

$$T = 89.8 \text{ ft}^2/\text{day}$$

Horizontal hydraulic conductivity is calculated by dividing T by the unit thickness of 30.0 ft.

$$K = 3.0 \times 10^{-1} \text{ ft/day}$$

$$K = 1.1 \times 10^{-3} \text{ cm/sec}$$

Analytical results of the tests are summarized as follows:

#### **Hydraulic Conductivity**

$$\begin{array}{l} \text{Theis} = 1.8 \times 10^{-3} \text{ cm/sec} \\ \text{Theis Recovery Analysis} = 1.1 \times 10^{-3} \text{ cm/sec} \end{array}$$



THEIS RECOVERY ANALYSIS I-17, ZONE 1580-1610

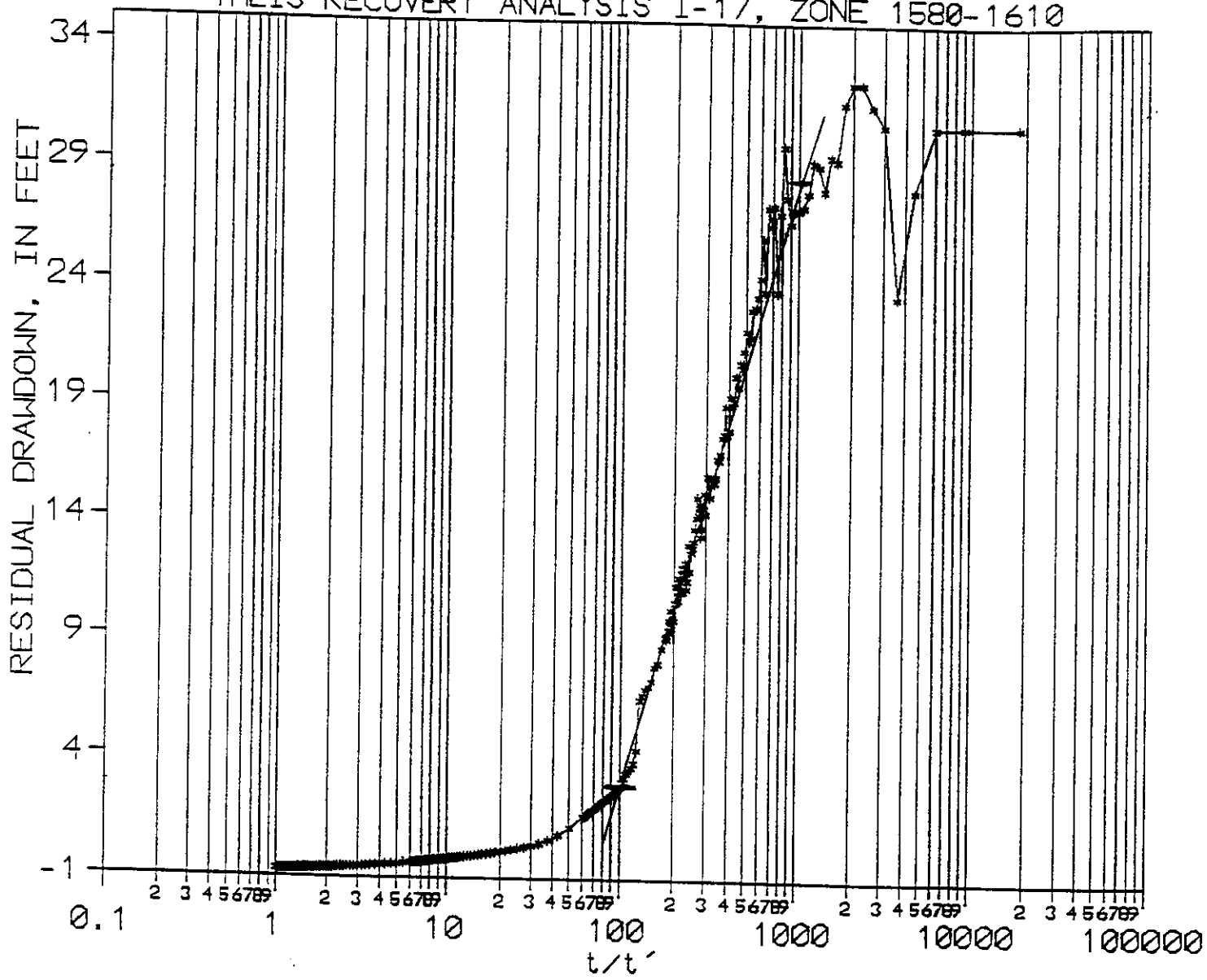
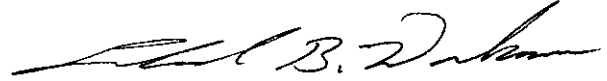


Figure 4.-- Theis Recovery Analysis I-17, zone 1580 to 1610

If you have any questions or comments please feel free to contact me or Leo

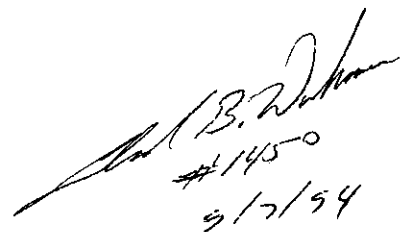
Swayze.

Sincerely,

A handwritten signature in black ink, appearing to read "Ed B. Workman". The signature is fluid and cursive, with a long horizontal stroke at the beginning.

Edmand B. Workman, P.G.

EBW:na

A handwritten signature in black ink, appearing to read "Ed B. Workman". Below the signature, there are two lines of handwritten text: "#1450" and "9/7/94".

**Appendix I**  
**Specific Conductance Stabilization Data**

Packer Test (I-17)  
Zone 1580-1610

| <u>TIME</u> | <u>TEMP °C</u> | <u>SALINITY</u> | <u>CONDUCTIVITY umhos</u> |
|-------------|----------------|-----------------|---------------------------|
| 2400        | 26.5           | 12              | .20                       |
| 0030        | 26.5           | 11              | .19                       |
| 0230        | 25.5           | 7               | .12                       |
| 0300        | 25.5           | 7               | .12                       |
| 0330        | 25.5           | 6               | .11                       |
| 0400        | 25             | 6               | .10                       |
| 0430        | 25             | 6               | .10                       |
| 0500        | 25             | 6               | .10                       |
| 0530        | 25             | 6               | .10                       |
| 0600        | 25             | 5.5             | .09                       |
| 0630        | 24.5           | 5.5             | .09                       |
| 0700        | 24.5           | 5.5             | .09                       |
| 9:15        | 26             | 9.0             | .1                        |
| 9:30        | 26.5           | 8.5             | .09                       |
| 9:45        | 26.5           | 9.0             | .09                       |
| 10:00       | 27             | 8.7             | .09                       |
| 10:15       | 26             | 9.0             | .09                       |

**Appendix II**  
**Raw Aquifer Test Data**

SE1000C  
Environmental Logger  
08/31 12:44

Unit# 01513 Test 0

-----  
Setups: INPUT 1  
-----  
Type Level (F)  
Mode TOC  
I.D. 00000  
  
Reference 0.000  
Linearity 0.280  
Scale factor 29.990  
Offset 0.120  
Delay mSEC 50.000

Step 0 08/31 07:14:19

-----  
Elapsed Time INPUT 1  
-----  
0.0000 -0.019  
0.0033 -0.009  
0.0066 0.000  
0.0100 -0.009  
0.0133 -0.009  
0.0166 -0.009  
0.0200 -0.009  
0.0233 -0.019  
0.0266 -0.009  
0.0300 0.000  
0.0333 -0.019  
0.0366 -0.009  
0.0400 -0.019  
0.0433 -0.019  
0.0466 -0.009  
0.0500 0.000  
0.0533 -0.019  
0.0566 -0.019  
0.0600 -0.009  
0.0633 -0.009  
0.0666 -0.009  
0.0700 -0.009  
0.0733 -0.019  
0.0766 -0.019  
0.0800 -0.009  
0.0833 -0.009  
0.0866 -0.019  
0.0900 -0.009  
0.0933 -0.019  
0.0966 -0.009  
0.1000 -0.009  
0.1033 -0.019  
0.1066 -0.009  
0.1100 -0.019  
0.1133 -0.009  
0.1166 -0.019  
0.1200 -0.019

|        |        |
|--------|--------|
| 0.1233 | -0.019 |
| 0.1266 | -0.009 |
| 0.1300 | -0.009 |
| 0.1333 | -0.019 |
| 0.1366 | -0.019 |
| 0.1400 | -0.009 |
| 0.1433 | -0.009 |
| 0.1466 | -0.019 |
| 0.1500 | -0.019 |
| 0.1533 | -0.019 |
| 0.1566 | -0.009 |
| 0.1600 | -0.009 |
| 0.1633 | -0.019 |
| 0.1666 | -0.019 |
| 0.1700 | -0.019 |
| 0.1733 | -0.019 |
| 0.1766 | -0.009 |
| 0.1800 | -0.009 |
| 0.1833 | -0.019 |
| 0.1866 | -0.019 |
| 0.1900 | -0.009 |
| 0.1933 | -0.009 |
| 0.1966 | -0.019 |
| 0.2000 | -0.019 |
| 0.2033 | -0.019 |
| 0.2066 | -0.009 |
| 0.2100 | -0.019 |
| 0.2133 | -0.019 |
| 0.2166 | -0.019 |
| 0.2200 | -0.009 |
| 0.2233 | -0.019 |
| 0.2266 | -0.019 |
| 0.2300 | -0.019 |
| 0.2333 | -0.019 |
| 0.2366 | -0.019 |
| 0.2400 | -0.019 |
| 0.2433 | -0.019 |
| 0.2466 | -0.019 |
| 0.2500 | -0.019 |
| 0.2533 | -0.019 |
| 0.2566 | -0.019 |
| 0.2600 | -0.019 |
| 0.2633 | -0.019 |
| 0.2666 | -0.019 |
| 0.2700 | -0.009 |
| 0.2733 | -0.028 |
| 0.2766 | -0.019 |
| 0.2800 | -0.019 |
| 0.2833 | -0.019 |
| 0.2866 | -0.028 |
| 0.2900 | -0.019 |
| 0.2933 | -0.028 |
| 0.2966 | -0.009 |
| 0.3000 | -0.019 |
| 0.3033 | -0.019 |
| 0.3066 | -0.019 |
| 0.3100 | -0.019 |
| 0.3133 | -0.019 |
| 0.3166 | -0.019 |
| 0.3200 | -0.019 |

|        |        |
|--------|--------|
| 0.3233 | -0.019 |
| 0.3266 | -0.019 |
| 0.3300 | -0.028 |
| 0.3333 | -0.019 |
| 0.3500 | -0.019 |
| 0.3666 | -0.019 |
| 0.3833 | -0.028 |
| 0.4000 | -0.019 |
| 0.4166 | -0.028 |
| 0.4333 | -0.019 |
| 0.4500 | -0.028 |
| 0.4666 | -0.028 |
| 0.4833 | -0.028 |
| 0.5000 | -0.028 |
| 0.5166 | -0.038 |
| 0.5333 | -0.038 |
| 0.5500 | -0.028 |
| 0.5666 | -0.028 |
| 0.5833 | -0.038 |
| 0.6000 | -0.038 |
| 0.6166 | -0.028 |
| 0.6333 | -0.028 |
| 0.6500 | -0.038 |
| 0.6666 | -0.038 |
| 0.6833 | -0.038 |
| 0.7000 | -0.038 |
| 0.7166 | -0.038 |
| 0.7333 | -0.038 |
| 0.7500 | -0.047 |
| 0.7666 | -0.038 |
| 0.7833 | -0.038 |
| 0.8000 | -0.047 |
| 0.8166 | -0.038 |
| 0.8333 | -0.038 |
| 0.8500 | -0.047 |
| 0.8666 | -0.047 |
| 0.8833 | -0.047 |
| 0.9000 | -0.047 |
| 0.9166 | -0.038 |
| 0.9333 | -0.047 |
| 0.9500 | -0.047 |
| 0.9666 | -0.047 |
| 0.9833 | -0.057 |
| 1.0000 | -0.047 |
| 1.2000 | -0.057 |
| 1.4000 | -0.076 |
| 1.6000 | -0.086 |
| 1.8000 | -0.086 |
| 2.0000 | -0.095 |
| 2.2000 | -0.095 |
| 2.4000 | -0.105 |
| 2.6000 | -0.114 |
| 2.8000 | -0.124 |
| 3.0000 | -0.124 |
| 3.2000 | -0.133 |
| 3.4000 | -0.133 |
| 3.6000 | -0.143 |
| 3.8000 | -0.152 |
| 4.0000 | -0.152 |
| 4.2000 | -0.162 |



|         |        |
|---------|--------|
| 4.4000  | -0.162 |
| 4.6000  | -0.171 |
| 4.8000  | -0.171 |
| 5.0000  | -0.181 |
| 5.2000  | -0.191 |
| 5.4000  | -0.191 |
| 5.6000  | -0.200 |
| 5.8000  | -0.200 |
| 6.0000  | -0.200 |
| 6.2000  | -0.210 |
| 6.4000  | -0.210 |
| 6.6000  | -0.219 |
| 6.8000  | -0.210 |
| 7.0000  | -0.229 |
| 7.2000  | -0.229 |
| 7.4000  | -0.238 |
| 7.6000  | -0.238 |
| 7.8000  | -0.238 |
| 8.0000  | -0.238 |
| 8.2000  | -0.248 |
| 8.4000  | -0.248 |
| 8.6000  | -0.248 |
| 8.8000  | -0.248 |
| 9.0000  | -0.257 |
| 9.2000  | -0.267 |
| 9.4000  | -0.267 |
| 9.6000  | -0.267 |
| 9.8000  | -0.277 |
| 10.0000 | -0.267 |
| 11.0000 | -0.286 |
| 12.0000 | -0.305 |
| 13.0000 | -0.305 |
| 14.0000 | -0.325 |
| 15.0000 | -0.334 |
| 16.0000 | -0.344 |
| 17.0000 | -0.353 |
| 18.0000 | -0.363 |
| 19.0000 | -0.372 |
| 20.0000 | -0.382 |
| 21.0000 | -0.382 |
| 22.0000 | -0.391 |
| 23.0000 | -0.401 |
| 24.0000 | -0.401 |
| 25.0000 | -0.411 |
| 26.0000 | -0.411 |
| 27.0000 | -0.420 |
| 28.0000 | -0.430 |
| 29.0000 | -0.430 |
| 30.0000 | -0.430 |
| 31.0000 | -0.439 |
| 32.0000 | -0.449 |
| 33.0000 | -0.449 |
| 34.0000 | -0.458 |
| 35.0000 | -0.458 |
| 36.0000 | -0.449 |
| 37.0000 | -0.458 |
| 38.0000 | -0.468 |
| 39.0000 | -0.468 |
| 40.0000 | -0.468 |
| 41.0000 | -0.478 |

|         |        |
|---------|--------|
| 42.0000 | -0.478 |
| 43.0000 | -0.478 |
| 44.0000 | -0.487 |
| 45.0000 | -0.487 |
| 46.0000 | -0.487 |
| 47.0000 | -0.497 |
| 48.0000 | -0.497 |
| 49.0000 | -0.497 |
| 50.0000 | -0.506 |
| 51.0000 | -0.506 |
| 52.0000 | -0.506 |
| 53.0000 | -0.516 |
| 54.0000 | -0.516 |
| 55.0000 | -0.516 |
| 56.0000 | -0.516 |
| 57.0000 | -0.525 |
| 58.0000 | -0.525 |
| 59.0000 | -0.516 |
| 60.0000 | -0.525 |

SE1000C  
Environmental Logger  
08/31 12:22

Unit# 01513 Test 1

-----  
Setups:           INPUT 1  
-----  
Type              Level (F)  
Mode              TOC  
I.D.              00000

Reference         0.000  
Linearity         0.280  
Scale factor      29.990  
Offset            0.120  
Delay mSEC        50.000

Step 0 08/31 08:16:17

-----  
Elapsed Time      INPUT 1  
-----  
0.0000            18.801  
0.0033            12.585  
0.0066            11.728  
0.0100            9.250  
0.0133            4.461  
0.0166            2.713  
0.0200            5.033  
0.0233            10.298  
0.0266            14.099  
0.0300            8.191  
0.0333            3.811  
0.0366            5.835  
0.0400            4.088  
0.0433            6.866  
0.0466            16.708  
0.0500            12.776  
0.0533            13.157  
0.0566            12.138  
0.0600            13.462  
0.0633            15.337  
0.0666            16.327  
0.0700            15.566  
0.0733            13.604  
0.0766            15.118  
0.0800            12.700  
0.0833            13.547  
0.0866            14.033  
0.0900            13.081  
0.0933            13.300  
0.0966            14.166  
0.1000            15.052  
0.1033            14.481  
0.1066            13.243  
0.1100            12.347  
0.1133            12.214  
0.1166            11.118  
0.1200            13.061

|        |        |
|--------|--------|
| 0.1233 | 12.462 |
| 0.1266 | 9.498  |
| 0.1300 | 14.671 |
| 0.1333 | 15.023 |
| 0.1366 | 9.536  |
| 0.1400 | 11.938 |
| 0.1433 | 13.309 |
| 0.1466 | 14.281 |
| 0.1500 | 14.319 |
| 0.1533 | 14.985 |
| 0.1566 | 13.005 |
| 0.1600 | 10.870 |
| 0.1633 | 12.985 |
| 0.1666 | 12.833 |
| 0.1700 | 13.109 |
| 0.1733 | 14.471 |
| 0.1766 | 15.328 |
| 0.1800 | 14.842 |
| 0.1833 | 14.490 |
| 0.1866 | 13.833 |
| 0.1900 | 14.081 |
| 0.1933 | 14.195 |
| 0.1966 | 13.957 |
| 0.2000 | 13.900 |
| 0.2033 | 14.138 |
| 0.2066 | 13.747 |
| 0.2100 | 14.128 |
| 0.2133 | 14.090 |
| 0.2166 | 13.862 |
| 0.2200 | 14.099 |
| 0.2233 | 13.823 |
| 0.2266 | 13.871 |
| 0.2300 | 14.128 |
| 0.2333 | 14.328 |
| 0.2366 | 13.890 |
| 0.2400 | 13.947 |
| 0.2433 | 13.557 |
| 0.2466 | 13.823 |
| 0.2500 | 14.043 |
| 0.2533 | 13.795 |
| 0.2566 | 13.671 |
| 0.2600 | 13.509 |
| 0.2633 | 13.623 |
| 0.2666 | 13.652 |
| 0.2700 | 13.852 |
| 0.2733 | 13.947 |
| 0.2766 | 13.938 |
| 0.2800 | 13.833 |
| 0.2833 | 13.814 |
| 0.2866 | 13.928 |
| 0.2900 | 13.823 |
| 0.2933 | 13.823 |
| 0.2966 | 13.700 |
| 0.3000 | 14.052 |
| 0.3033 | 14.433 |
| 0.3066 | 14.471 |
| 0.3100 | 14.376 |
| 0.3133 | 14.471 |
| 0.3166 | 14.509 |
| 0.3200 | 14.376 |

|        |        |
|--------|--------|
| 0.3233 | 14.566 |
| 0.3266 | 14.519 |
| 0.3300 | 14.690 |
| 0.3333 | 14.709 |
| 0.3500 | 14.861 |
| 0.3666 | 16.280 |
| 0.3833 | 15.166 |
| 0.4000 | 14.261 |
| 0.4166 | 14.776 |
| 0.4333 | 15.033 |
| 0.4500 | 14.757 |
| 0.4666 | 14.909 |
| 0.4833 | 14.909 |
| 0.5000 | 14.871 |
| 0.5166 | 13.795 |
| 0.5333 | 12.623 |
| 0.5500 | 20.721 |
| 0.5666 | 15.252 |
| 0.5833 | 20.094 |
| 0.6000 | 13.881 |
| 0.6166 | 8.573  |
| 0.6333 | 3.974  |
| 0.6500 | 8.191  |
| 0.6666 | 8.372  |
| 0.6833 | 18.335 |
| 0.7000 | 18.344 |
| 0.7166 | 13.957 |
| 0.7333 | 21.310 |
| 0.7500 | 18.953 |
| 0.7666 | 18.287 |
| 0.7833 | 15.490 |
| 0.8000 | 13.509 |
| 0.8166 | 12.719 |
| 0.8333 | 12.614 |
| 0.8500 | 13.005 |
| 0.8666 | 9.746  |
| 0.8833 | 16.222 |
| 0.9000 | 14.547 |
| 0.9166 | 14.719 |
| 0.9333 | 14.261 |
| 0.9500 | 14.490 |
| 0.9666 | 14.576 |
| 0.9833 | 14.490 |
| 1.0000 | 28.213 |
| 1.2000 | 16.841 |
| 1.4000 | 17.307 |
| 1.6000 | 28.422 |
| 1.8000 | 29.001 |
| 2.0000 | 29.285 |
| 2.2000 | 29.475 |
| 2.4000 | 29.541 |
| 2.6000 | 29.740 |
| 2.8000 | 29.854 |
| 3.0000 | 29.968 |
| 3.2000 | 29.987 |
| 3.4000 | 30.129 |
| 3.6000 | 30.148 |
| 3.8000 | 30.224 |
| 4.0000 | 30.338 |
| 4.2000 | 30.271 |

|         |        |
|---------|--------|
| 4.4000  | 30.347 |
| 4.6000  | 30.366 |
| 4.8000  | 30.357 |
| 5.0000  | 30.366 |
| 5.2000  | 30.376 |
| 5.4000  | 30.423 |
| 5.6000  | 30.442 |
| 5.8000  | 30.451 |
| 6.0000  | 30.413 |
| 6.2000  | 30.423 |
| 6.4000  | 30.442 |
| 6.6000  | 30.480 |
| 6.8000  | 30.470 |
| 7.0000  | 30.480 |
| 7.2000  | 30.461 |
| 7.4000  | 30.451 |
| 7.6000  | 30.470 |
| 7.8000  | 30.499 |
| 8.0000  | 30.499 |
| 8.2000  | 30.499 |
| 8.4000  | 30.499 |
| 8.6000  | 30.565 |
| 8.8000  | 30.508 |
| 9.0000  | 30.518 |
| 9.2000  | 30.518 |
| 9.4000  | 30.575 |
| 9.6000  | 30.537 |
| 9.8000  | 30.546 |
| 10.0000 | 30.565 |
| 11.0000 | 30.527 |
| 12.0000 | 30.594 |
| 13.0000 | 27.103 |
| 14.0000 | 30.309 |
| 15.0000 | 30.423 |
| 16.0000 | 30.518 |
| 17.0000 | 30.470 |
| 18.0000 | 30.527 |
| 19.0000 | 30.556 |
| 20.0000 | 30.546 |
| 21.0000 | 30.527 |
| 22.0000 | 30.556 |
| 23.0000 | 30.546 |
| 24.0000 | 30.594 |
| 25.0000 | 30.556 |
| 26.0000 | 30.556 |
| 27.0000 | 30.565 |
| 28.0000 | 30.556 |
| 29.0000 | 30.499 |
| 30.0000 | 30.546 |
| 31.0000 | 30.537 |
| 32.0000 | 28.043 |
| 33.0000 | 30.537 |
| 34.0000 | 30.565 |
| 35.0000 | 30.575 |
| 36.0000 | 30.556 |
| 37.0000 | 30.556 |
| 38.0000 | 30.584 |
| 39.0000 | 30.584 |
| 40.0000 | 30.565 |
| 41.0000 | 30.565 |

|         |        |
|---------|--------|
| 42.0000 | 30.603 |
| 43.0000 | 30.613 |
| 44.0000 | 30.584 |
| 45.0000 | 30.679 |
| 46.0000 | 30.736 |
| 47.0000 | 30.717 |
| 48.0000 | 30.717 |
| 49.0000 | 30.755 |
| 50.0000 | 30.707 |
| 51.0000 | 30.736 |
| 52.0000 | 30.726 |
| 53.0000 | 30.726 |
| 54.0000 | 30.736 |
| 55.0000 | 30.745 |
| 56.0000 | 30.745 |
| 57.0000 | 30.745 |
| 58.0000 | 29.579 |
| 59.0000 | 30.669 |
| 60.0000 | 30.698 |

SE1000C  
Environmental Logger  
08/31 12:26

Unit# 01513 Test 2

-----  
Setups: INPUT 1  
-----  
Type Level (F)  
Mode TOC  
I.D. 00000

Reference 0.000  
Linearity 0.280  
Scale factor 29.990  
Offset 0.120  
Delay mSEC 50.000

Step 0 08/31 09:17:46

-----  
Elapsed Time INPUT 1  
-----  
0.0000 30.669  
0.0033 30.726  
0.0066 30.717  
0.0100 30.698  
0.0133 28.033  
0.0166 23.591  
0.0200 30.745  
0.0233 31.560  
0.0266 32.508  
0.0300 32.527  
0.0333 31.665  
0.0366 29.295  
0.0400 29.456  
0.0433 28.052  
0.0466 29.076  
0.0500 29.219  
0.0533 27.948  
0.0566 27.359  
0.0600 27.189  
0.0633 27.236  
0.0666 26.676  
0.0700 27.739  
0.0733 29.883  
0.0766 27.075  
0.0800 23.809  
0.0833 27.397  
0.0866 26.543  
0.0900 27.322  
0.0933 23.828  
0.0966 26.012  
0.1000 24.388  
0.1033 23.581  
0.1066 23.154  
0.1100 23.021  
0.1133 21.881  
0.1166 21.767  
0.1200 22.147



|        |        |
|--------|--------|
| 0.1233 | 21.310 |
| 0.1266 | 20.550 |
| 0.1300 | 20.759 |
| 0.1333 | 19.809 |
| 0.1366 | 20.227 |
| 0.1400 | 19.152 |
| 0.1433 | 19.010 |
| 0.1466 | 19.343 |
| 0.1500 | 17.954 |
| 0.1533 | 17.745 |
| 0.1566 | 18.943 |
| 0.1600 | 17.773 |
| 0.1633 | 17.631 |
| 0.1666 | 16.946 |
| 0.1700 | 16.679 |
| 0.1733 | 16.746 |
| 0.1766 | 15.946 |
| 0.1800 | 15.718 |
| 0.1833 | 15.927 |
| 0.1866 | 15.623 |
| 0.1900 | 15.109 |
| 0.1933 | 15.908 |
| 0.1966 | 15.985 |
| 0.2000 | 14.385 |
| 0.2033 | 15.252 |
| 0.2066 | 14.614 |
| 0.2100 | 13.776 |
| 0.2133 | 13.424 |
| 0.2166 | 14.823 |
| 0.2200 | 14.347 |
| 0.2233 | 15.071 |
| 0.2266 | 14.214 |
| 0.2300 | 13.728 |
| 0.2333 | 13.223 |
| 0.2366 | 12.947 |
| 0.2400 | 12.728 |
| 0.2433 | 12.881 |
| 0.2466 | 11.947 |
| 0.2500 | 13.071 |
| 0.2533 | 11.518 |
| 0.2566 | 11.166 |
| 0.2600 | 12.290 |
| 0.2633 | 11.737 |
| 0.2666 | 12.071 |
| 0.2700 | 11.842 |
| 0.2733 | 11.023 |
| 0.2766 | 11.118 |
| 0.2800 | 11.661 |
| 0.2833 | 10.689 |
| 0.2866 | 11.451 |
| 0.2900 | 10.613 |
| 0.2933 | 11.290 |
| 0.2966 | 10.594 |
| 0.3000 | 9.850  |
| 0.3033 | 10.136 |
| 0.3066 | 9.526  |
| 0.3100 | 10.308 |
| 0.3133 | 9.774  |
| 0.3166 | 9.355  |
| 0.3200 | 9.850  |

|        |        |
|--------|--------|
| 0.3233 | 9.440  |
| 0.3266 | 9.050  |
| 0.3300 | 9.193  |
| 0.3333 | 9.136  |
| 0.3500 | 8.649  |
| 0.3666 | 8.029  |
| 0.3833 | 7.905  |
| 0.4000 | 7.304  |
| 0.4166 | 7.037  |
| 0.4333 | 6.923  |
| 0.4500 | 6.675  |
| 0.4666 | 6.474  |
| 0.4833 | 4.355  |
| 0.5000 | 3.830  |
| 0.5166 | 3.639  |
| 0.5333 | 3.515  |
| 0.5500 | 3.410  |
| 0.5666 | 3.238  |
| 0.5833 | 3.057  |
| 0.6000 | 2.837  |
| 0.6166 | 2.751  |
| 0.6333 | 2.713  |
| 0.6500 | 2.646  |
| 0.6666 | 2.474  |
| 0.6833 | 2.465  |
| 0.7000 | 2.407  |
| 0.7166 | 2.331  |
| 0.7333 | 2.302  |
| 0.7500 | 2.245  |
| 0.7666 | 2.188  |
| 0.7833 | 2.130  |
| 0.8000 | 2.083  |
| 0.8166 | 2.035  |
| 0.8333 | 1.997  |
| 0.8500 | 1.930  |
| 0.8666 | 1.891  |
| 0.8833 | 1.844  |
| 0.9000 | 1.796  |
| 0.9166 | 1.758  |
| 0.9333 | 1.720  |
| 0.9500 | 1.662  |
| 0.9666 | 1.634  |
| 0.9833 | 1.605  |
| 1.0000 | 1.557  |
| 1.2000 | 1.118  |
| 1.4000 | 0.812  |
| 1.6000 | 0.611  |
| 1.8000 | 0.468  |
| 2.0000 | 0.372  |
| 2.2000 | 0.315  |
| 2.4000 | 0.258  |
| 2.6000 | 0.200  |
| 2.8000 | 0.162  |
| 3.0000 | 0.133  |
| 3.2000 | 0.095  |
| 3.4000 | 0.066  |
| 3.6000 | 0.028  |
| 3.8000 | 0.000  |
| 4.0000 | -0.019 |
| 4.2000 | -0.038 |

|         |        |
|---------|--------|
| 4.4000  | -0.066 |
| 4.6000  | -0.076 |
| 4.8000  | -0.095 |
| 5.0000  | -0.114 |
| 5.2000  | -0.133 |
| 5.4000  | -0.143 |
| 5.6000  | -0.152 |
| 5.8000  | -0.181 |
| 6.0000  | -0.191 |
| 6.2000  | -0.200 |
| 6.4000  | -0.210 |
| 6.6000  | -0.229 |
| 6.8000  | -0.238 |
| 7.0000  | -0.238 |
| 7.2000  | -0.257 |
| 7.4000  | -0.267 |
| 7.6000  | -0.277 |
| 7.8000  | -0.277 |
| 8.0000  | -0.296 |
| 8.2000  | -0.296 |
| 8.4000  | -0.305 |
| 8.6000  | -0.315 |
| 8.8000  | -0.325 |
| 9.0000  | -0.334 |
| 9.2000  | -0.334 |
| 9.4000  | -0.344 |
| 9.6000  | -0.353 |
| 9.8000  | -0.353 |
| 10.0000 | -0.363 |
| 11.0000 | -0.382 |
| 12.0000 | -0.420 |
| 13.0000 | -0.430 |
| 14.0000 | -0.449 |
| 15.0000 | -0.478 |
| 16.0000 | -0.487 |
| 17.0000 | -0.497 |
| 18.0000 | -0.506 |
| 19.0000 | -0.525 |
| 20.0000 | -0.535 |
| 21.0000 | -0.544 |
| 22.0000 | -0.554 |
| 23.0000 | -0.554 |
| 24.0000 | -0.573 |
| 25.0000 | -0.573 |
| 26.0000 | -0.582 |
| 27.0000 | -0.582 |
| 28.0000 | -0.602 |
| 29.0000 | -0.602 |
| 30.0000 | -0.611 |
| 31.0000 | -0.611 |
| 32.0000 | -0.621 |
| 33.0000 | -0.621 |
| 34.0000 | -0.621 |
| 35.0000 | -0.630 |
| 36.0000 | -0.630 |
| 37.0000 | -0.640 |
| 38.0000 | -0.640 |
| 39.0000 | -0.649 |
| 40.0000 | -0.649 |
| 41.0000 | -0.649 |

|         |        |
|---------|--------|
| 42.0000 | -0.649 |
| 43.0000 | -0.669 |
| 44.0000 | -0.659 |
| 45.0000 | -0.659 |
| 46.0000 | -0.659 |
| 47.0000 | -0.669 |
| 48.0000 | -0.678 |
| 49.0000 | -0.678 |
| 50.0000 | -0.669 |
| 51.0000 | -0.678 |
| 52.0000 | -0.669 |
| 53.0000 | -0.688 |
| 54.0000 | -0.678 |
| 55.0000 | -0.688 |
| 56.0000 | -0.678 |
| 57.0000 | -0.678 |
| 58.0000 | -0.688 |
| 59.0000 | -0.688 |
| 60.0000 | -0.688 |