

McCARTY RANCH AQUIFER TEST REPORT

BY: GEORGE W. HILL

I. Summary

- A. Location. -- Lat. $N27^{\circ} 14' 40''$, Long. $W 080^{\circ} 29' 55''$,
Township 37 South, Range 38 East, in $NE\frac{1}{4}$,
 $SE\frac{1}{4}$, $NE\frac{1}{4}$ Section 23, 2.7 miles north of
the Martin-St. Lucie County line and
approximately 1.0 mile west of State
Road 609.
- B. Test Dates. -- March 28-29, 1979.
- C. Length of Test. -- Pumping: 24.5 hours;
Recovery: None
- D. Discharge. -- 123 GPM
- E. Hydraulic Coefficients. --
Transmissivity -- $1,350 \text{ ft}^2/\text{day}$
Storage Coefficient -- 1.0×10^{-4}
Leakance Coefficient -- $4.2 \times 10^{-4}/\text{day}$
- F. Analytical Model. -- Hantush-Jacob (leaky artesian, unsteady flow)
- G. Computations. -- Ralph Wilcox and George Hill
- H. Remarks. -- Results of Hantush I and DeGlee models were also
evaluated.
Test design and test drilling supervision was done
by Wes Miller.

II. Narrative

A. Introduction

1. Test Purpose. -- To determine aquifer properties of the best producing zone of the so-called shallow aquifer in this particular area. The test is part of a reconnaissance study of the aquifer properties of the Upper East Coast Planning Area which includes Martin and St. Lucie Counties and eastern Okeechobee County, Florida. The study is in cooperation with South Florida Water Management District.

2. Personnel. -- The test was designed and test drilling supervision was done by Wes Miller, SFSD office. Aquifer test was performed by George Hill, Ralph Wilcox, Bill Long, Wes Miller, and Jay Wendorf - all from the Jupiter Field Office except Mr. Miller.

B. Physical Aspects

1. Site Location. -- The test site is in Township 37 South, Range 38 East, in NE $\frac{1}{4}$, SE $\frac{1}{4}$, NE $\frac{1}{4}$ Section 23, 2.7 miles north of Martin-St. Lucie County line and about 1.0 mile west of State Road 609, on the property of McCarty Ranch (Exhibit I).

2. Test Drilling and Geophysical Logs. -- There are no geophysical logs related to the test in the Jupiter Field office file. Presumably, the pumped well and observation wells were set and screened according to the lithologic log of well SL-185 (Exhibit III).

3. Aquifer Description. -- The so-called shallow aquifer is mainly composed of sand, clay, silt and shell of Pleistocene and Pliocene epochs. Sediments forming the aquifer system are components of the Fort Thompson and Anastasia Formations overlain by Pamlico Sand (W. Miller, 1979). Shell and sand lenses in the Caloosahatchee Marl are also present. Many facies changes appear. Generally the aquifer system is unconfined and under water-table conditions, but localized artesian conditions have been noted by other investigators (Parker 1955) in the vicinity of Fort Pierce and Indiantown where discontinuous clay lenses act as confining units.

Wells set in the producing zone were screened in a zone consisting of unconsolidated shells and shell fragments with a minor component of sand, overlain by fine, gray sand with some shells and clay (Exhibits II and III).

4. Well Descriptions. -- See the table below for production and observation well data.

<u>Well No.</u>	<u>Radius, in Feet</u>	<u>Drilled Depth, in Feet (LSD)</u>	<u>Interval Screened, in Feet (LSD)</u>	<u>Diameter, in Inches</u>
PW	0	113	103-113	4
OWD-1	72	98	88-98	2
OWD-2	107	109	99-109	2
OWD-3	1140	120	Unknown	6
OWS-1	9	11	Open Hole	2
OWS-2	142	23	Open Hole	2

Please see Exhibit II.

5. Instrumentation. -- Three Keck/Stevens water-level recorder combinations were used to collect background, drawdown and recovery data. Steel tapes were used to collect water-level data in all other wells.

6. Pump. -- The production well was pumped with a four-inch centrifugal pump.

7. Background Water-Level Data. -- Background water-level data was obtained from well OWD-2 from March 8-20 and for 12 hours just prior to the test (Exhibit VI). There was a net decline of 0.05 feet during the 12 hour period just prior to the test. The earlier background W/L data shows a diurnal fluctuation of several hundredths superimposed on an overall declining trend. No adjustments were made to the drawdown data to correct for the slight decline in W/L which could have occurred during the test (Exhibit VI).

8. Measurement of Drawdown. -- Drawdown and recovery records for wells OWD-1, OWD-2, and OWS-1 were obtained with Keck surface followers in conjunction with Stevens F-type recorders (Exhibit VI) adjustments of W/L data were required because of mechanical factors. On OWD-2 the recorder pulley jammed against the housing and record was lost for 0.95 feet of drawdown. The chart trace was adjusted accordingly. Chart trace for well OWD-1 required adjustment of 0.18 ft. at 1227 minutes prorated back to zero at the beginning of the test.

No corrections were made for declining water levels or other cyclic phenomenon. These corrections would be insignificant compared to the corrections already made for mechanical problems.

Well OWD-3 was found by accident after the test was started and therefore, limited drawdown data could be obtained. See Exhibit VI for drawdown data.

9. Discharge. -- The production well was pumped at approximately 123 GPM. See Exhibit V for pumping data. During the early part of the test the rate was up to 131 GPM. After five hours of pumping the rate was 123 GPM and fluctuated between 123 and 122 GPM for the remainder of the test.

A 6-inch aluminum pipeline was used to route the discharge to a shallow ditch about 130 feet south of the production well.

10. Potential Surface Water Recharge. -- Shallow drainage ditches are located a short distance (within 130 ft.) to the south, west, and northeast. Underlying the ditches is a layer of clay and therefore, there shouldn't be a potential relationship of the ditches to the test; the C-23 land is approximately 2.7 miles south of the site and a large rock quarry is located about two miles west of the site. Here the shallow coquina strata is dewatered in large volumes and discharged into a drainage ditch running southward. No other data is available on the quarry and no computations were made to evaluate a discharging boundary (Image Well Theory).

A drawdown of only about 0.7 feet in the shallow wells is an indication that recharge from the shallow ditches was not a factor in the test.

C. Computations

1. Computations are included in Exhibit VIII. Three methods were considered - Hantush I, Thiem and Hantush-Jacob for leaky artesian, nonsteady flow. Since the drawdown in the shallow observation wells was very little compared to the pumped zone, there is an indication of semi-confined aquifer and therefore, all three methods are applicable. However, the Hantush-Jacob model is the most appropriate solution.

2. Type Curve Fitting. -- Drawdown data frames wells OWD-1 and OWD-2 were plotted against t/r^2 on log-log. A composite fit was achieved and a single match point selected. The fit is good.

Other solutions examined were semilog plots.

3. Transmissivity. -- Use $1,350 \text{ ft}^2/\text{day}$.
4. Storage Coefficient. -- Use 1.0×10^{-4} .
5. Leakance Coefficient. -- Use $4.2 \times 10^{-4}/\text{day}$.

Table 1
OWD-1

time	t(min)	s(ft)	s corrected (ft)	t/r^2 (d ft ⁻²)
1703	210	8.42	8.45	2.80×10^{-5}
1733	240	8.48	8.51	3.20×10^{-5}
1826	293	8.59	8.63	3.90×10^{-5}
1914	341	8.67	8.72	4.54×10^{-5}
2008	395	8.75	8.81	5.26×10^{-5}
2102	449	8.81	8.88	5.98×10^{-5}
2232	539	8.89	8.97	7.18×10^{-5}
3-29-79 2003	630	8.93	9.02	8.39×10^{-5}
0109	696	8.95	9.05	9.27×10^{-5}
0200	747	8.97	9.08	9.95×10^{-5}
0358	865	9.00	9.13	1.15×10^{-4}
0502	929	9.01	9.15	1.24×10^{-4}
0603	990	9.02	9.16	1.32×10^{-4}
0713	1060	9.04	9.19	1.41×10^{-4}
0800	1107	9.05	9.21	1.47×10^{-4}
0909	1176	9.07	9.24	1.57×10^{-4}
1000	1227	9.08	9.26	1.63×10^{-4}
1213	1360	9.30	—	1.81×10^{-4}
1302	1409	9.30	—	1.88×10^{-4}
1400	1467	9.30	—	1.95×10^{-4}

Table 1

OWD-1 $r = 72.2 \text{ ft}$

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time	t (min)	s (ft)	S corrected (ft)	T/r^2 (dft^{-2})
5-28-79 1334	1	1.95	1.95	1.33×10^{-7}
	2	2.95	2.95	2.66×10^{-7}
	3	3.47	3.47	4.00×10^{-7}
	4	3.84	3.84	5.33×10^{-7}
	5	4.12	4.12	6.66×10^{-7}
	7	4.62	4.62	9.33×10^{-7}
	10	5.07	5.07	1.33×10^{-6}
	15	5.65	5.65	2.00×10^{-6}
	20	6.05	6.05	2.66×10^{-6}
	26	6.31	6.31	3.46×10^{-6}
	30	6.70	6.70	4.00×10^{-6}
	35	6.93	6.94	4.66×10^{-6}
	40	7.10	7.11	5.33×10^{-6}
	45	7.22	7.23	5.99×10^{-6}
	50	7.33	7.34	6.66×10^{-6}
	55	7.41	7.42	7.33×10^{-6}
	60	7.49	7.50	7.99×10^{-6}
1448	75	7.68	7.69	9.99×10^{-6}
	90	7.82	7.83	1.20×10^{-5}
	105	7.95	7.97	1.40×10^{-5}
1534	121	8.05	8.07	1.61×10^{-5}
1556	143	8.16	8.18	1.91×10^{-5}
1633	180	8.32	8.35	2.40×10^{-5}

Table 2
 OWD-2 r = 107 ft

time (3-28-79)	t (min)	s (ft)	s corrected (ft)	t/r ² (d ft ⁻²)
1334	1	0.33	1.28	6.07×10^{-8}
	2	1.00	1.95	1.21×10^{-7}
	3	1.39	2.34	1.82×10^{-7}
	4	1.68	2.63	2.43×10^{-7}
	5	1.92	2.87	3.03×10^{-7}
	7	2.35	3.30	4.25×10^{-7}
	10	2.81	3.76	6.07×10^{-7}
	15	3.30	4.25	9.10×10^{-7}
	20	3.55	4.50	1.21×10^{-6}
	25	3.78	4.73	1.52×10^{-6}
	30	4.14	5.09	1.82×10^{-6}
	35	4.37	5.32	2.12×10^{-6}
	40	4.55	5.50	2.43×10^{-6}
	45	4.68	5.63	2.73×10^{-6}
	50	4.79	5.74	3.03×10^{-6}
	55	4.88	5.83	3.34×10^{-6}
	60	4.97	5.92	3.64×10^{-6}
1448	75	5.18	6.13	4.55×10^{-6}
	90	5.33	6.28	5.46×10^{-6}
	105	5.47	6.42	6.37×10^{-6}
1533	120	5.58	6.53	7.28×10^{-6}
1554	141	5.69	6.64	8.55×10^{-6}
1632	179	5.86	6.81	1.09×10^{-5}

Table 2
OWD-2

32

time	t (min)	s (ft)	S corrected (ft)	t/r^2 ($d \text{ ft}^{-2}$)
1702	209	5.96	6.91	1.27×10^{-5}
1733	240	6.05	7.00	1.46×10^{-5}
1827	294	6.18	7.13	1.78×10^{-5}
1911	338	6.24	7.19	2.05×10^{-5}
2008	395	6.32	7.27	2.40×10^{-5}
2102	449	6.40	7.35	2.72×10^{-5}
2234	541	6.48	7.43	3.28×10^{-5}
(3-29-79) 0010	637	6.53	7.48	3.86×10^{-5}
0115	702	6.55	7.50	4.26×10^{-5}
0205	752	6.57	7.52	4.56×10^{-5}
0359	866	6.60	7.55	5.25×10^{-5}
0504	931	6.62	7.57	5.65×10^{-5}
0558	985	6.64	7.59	5.97×10^{-5}
0713	1060	6.66	7.61	6.43×10^{-5}
0803	1110	6.68	7.63	6.73×10^{-5}
0908	1175	6.70	7.65	7.13×10^{-5}
1000	1227	6.71	7.66	7.44×10^{-5}
1038	1265	7.67	—	7.67×10^{-5}
1140	1327	7.68	—	8.05×10^{-5}
1213	1360	7.68	—	8.25×10^{-5}
1258	1405	7.68	—	8.52×10^{-5}
1400	1467	7.68	—	8.90×10^{-5}

OWS-2

Radius = 142 Ft 3-30-79
RWW

9-194
November 1949

UNITED STATES
DEPARTMENT OF THE INTERIOR
GEOLOGICAL SURVEY
WATER RESOURCES DIVISION

WATER LEVEL MEASUREMENTS (Field) Measured by GWH
Location of Project McCarty Ranch OWS-2

DATE	Minutes HOUR	WELL NO. MIN	TAPE READING AT—		DEPTH TO WATER	WATER LEVEL Ft(MSL)	REMARKS
			Meas. point	Water level			
	1324		6.0	2.30	3.70		
	1330		8.0	4.31	3.69		
	1335		8.0	4.30	3.70	0	
1337	3		9.0	5.29	3.71	.01	
1337	4		9.0	5.30	3.70	.0	
1338	5		"	5.31	3.71	+0.1	
1339	6		"	5.28	3.72	.02	
1339	7		"	5.26	3.74	.04	
1340	8		"	5.26	3.74	.04	
1340	9		"	5.25	3.75	.05	
1340	10			5.25	3.75	.05	
1341							
1341	12			5.23	3.77	.07	
1341	14			5.23	3.77	.07	
1341	17			5.24	3.76	.06	
1341	22			5.20	3.80	.10	
1341	25			5.20	3.80	.10	
1341	25			5.20	3.80	.10	
1341	30			5.18	3.82	.12	
1341	35			5.16	3.84	.14	
1341	45			5.12	3.88	.18	
1341	50			5.11	3.89	.19	
1341	60			5.09	3.91	.21	

9-194
November 1949

UNITED STATES
DEPARTMENT OF THE INTERIOR
GEOLOGICAL SURVEY
WATER RESOURCES DIVISION

B+

WATER LEVEL MEASUREMENTS (Field) Measured by _____
Location of Project _____

DATE	HOUR	WELL NO.	TAPE READING AT—		DEPTH TO WATER	Ft(MSL)	Remarks
			Meas. point	Water level			
1450	75		9.0	5.06	3.94	.24	
1505	90		9.0	5.02	3.98	.28	
1510	105		9.0	4.99	4.01	.31	
1515	120		9.0	4.96	4.04	.34	
1637	182		6.0	1.91	4.09	.39	
1700	205		5.0	.88	4.12	.42	
1745	250		6.0	1.29	4.16	.46	
1822	287		5.0	.81	4.19	.49	
1917	342		5.0	.79	4.21	.51	
2014	400		5.0	.77	4.23	.53	
21	448		5.0	.74	4.26	.56	
2336	542		5.0	.71	4.29	.59	
3/25/79	0003	6288	5.0	.69	4.31	.61	
	0113	6998	5.0	.68	4.32	.62	
	0203	7498	5.0	.66	4.34	.64	
	0401	8670	5.0	.67	4.33	.63	
	0507	9332	5.0	.65	4.35	.65	
	0600	9865	5.0	.66	4.34	.64	
	712	10587	5.0	.65	4.35	.65	
	0805	1110	5.0	0.63	4.37	.67	
	0925	11910	5.0	.64	4.36	.66	
	1005	12310	5.0	.64	4.36	.66	
	1103	12898	5.0	.62	4.38	.68	

Discharge Measurements

McCarty Ranch

QW field parameters 3/28/79 RWW-MAD-JSW

Temp = 25°C hardness (as CaCO₃) = 435 mg/l

Iron = 1 mg/l

sp. cond. = 1580 μ mhos/cm

HS \approx 400 μ g/l

SO₄ = < 50 mg/l

WMQ = 123 GPM

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WATER LEVEL MEASUREMENTS (Field) Measured by Wal RWU

Location of Project 6" pipe 3" office

DATE	HOUR	WELL NO.	TAPE READING AT—		DEPTH TO WATER	REMARKS
			Meas. point	Water level		
3/28	1330				15" w	128
	1340				15"	128 } 127
	1355				14.5"	126 } 128
	1402				15.75	130 } 131
	1425				15.75	130 } 130
	1435				15.50	130 } 129
	1450				15.00	128 } 128
	1505				14.75	127 } 126
	1515				14.50	126 } 126
	1523				14.50	126
	1538				14.50	126
	1555				14.50	126 } 126
	1632				14.40	126
	1700				14.50	126
	1745				14.25	125
	1823				14.0	123 } 124
	1919				13 3/4	122
	2012				13 3/4	122
	2040				13 3/4	122
	2103				13 3/4	122 } 122

WATER LEVEL MEASUREMENTS (Field) Measured by _____

Location of Project _____

DATE	HOUR	WELL NO.	TAPE READING AT—		DEPTH TO WATER	REMARKS
			Meas. point	Water level		
223	2238				14.0	123
2/28/79	0007				13.8	122
	0102				13.8	122
	203				13.8	122
	401				14	123
	508				13 3/4	122
	600				13 3/4	
	712				13 3/4	
	0807				13.75	
	925				13 3/4	
	1100				13 3/4	
	1215				13 3/4	
	1304				13.75	
	1345				13 3/4	122

Computation of weighted mean Q:
 $2.67 \times 127 = 339.09$ $2.67 \times 126 = 336.42$
 $.12 \times 128 = 15.36$ $.03 \times 124 = 3.72$
 $.58 \times 131 = 75.98$ $19.36 \times 122 = 2361.92$
 $.17 \times 130 = 22.10$ 24.25
 $.25 \times 129 = 32.25$
 $.25 \times 128 = 32.00$
2981.29
 WMQ = 123 GPM

OWD-2 r = 107ft

time 73 1334	t (min)	s (ft)	s corrected (ft)	t/r ² (d ft ⁻²)
	1	0.33	1.28	6.07×10^{-8}
	2	1.00	1.95	1.21×10^{-7}
	3	1.39	2.34	1.82×10^{-7}
	4	1.68	2.63	2.43×10^{-7}
	5	1.92	2.87	3.03×10^{-7}
	7	2.35	3.30	4.25×10^{-7}
	10	2.81	3.76	6.07×10^{-7}
	15	3.30	4.25	9.10×10^{-7}
	20	3.55	4.50	1.21×10^{-6}
	25	3.78	4.73	1.52×10^{-6}
	30	4.14	5.09	1.82×10^{-6}
	35	4.37	5.32	2.12×10^{-6}
	40	4.55	5.50	2.43×10^{-6}
	45	4.68	5.63	2.73×10^{-6}
	50	4.79	5.74	3.03×10^{-6}
	55	4.88	5.83	3.34×10^{-6}
	60	4.97	5.92	3.64×10^{-6}
1448	75	5.18	6.13	4.55×10^{-6}
	90	5.33	6.28	5.46×10^{-6}
	105	5.47	6.42	6.37×10^{-6}
1533	120	5.58	6.53	7.28×10^{-6}
1554	141	5.69	6.64	8.55×10^{-6}
1632	179	5.86	6.81	1.09×10^{-5}

OWD-2

52

Time	t (min)	s (ft)	S corrected (ft)	t/r^2 ($d ft^{-2}$)
1702	209	5.96	6.91	1.27×10^{-5}
1733	240	6.05	7.00	1.46×10^{-5}
1827	294	6.18	7.13	1.78×10^{-5}
1911	338	6.24	7.19	2.05×10^{-5}
2008	395	6.32	7.27	2.40×10^{-5}
2102	449	6.40	7.35	2.72×10^{-5}
2234	541	6.48	7.43	3.28×10^{-5}
29-79) 600	637	6.53	7.48	3.86×10^{-5}
0115	702	6.55	7.50	4.26×10^{-5}
0205	752	6.57	7.52	4.56×10^{-5}
0359	866	6.60	7.55	5.25×10^{-5}
0504	931	6.62	7.57	5.65×10^{-5}
0558	985	6.64	7.59	5.97×10^{-5}
0713	1060	6.66	7.61	6.43×10^{-5}
0803	1110	6.68	7.63	6.73×10^{-5}
0908	1175	6.70	7.65	7.13×10^{-5}
1000	1227	6.71	7.66	7.44×10^{-5}
1038	1265	7.67	—	7.67×10^{-5}
1140	1327	7.68	—	8.05×10^{-5}
1213	1360	7.68	—	8.25×10^{-5}
1258	1405	7.68	—	8.52×10^{-5}
1400	1467	7.68	—	8.90×10^{-5}

Table 1

OWD-1

r = 72.2ft

29

time
1334

t (min)	s (ft)	S corrected (ft)	t/r ² (dft ⁻²)
1	1.95	1.95	1.33×10^{-7}
2	2.95	2.95	2.66×10^{-7}
3	3.47	3.47	4.00×10^{-7}
4	3.84	3.84	5.33×10^{-7}
5	4.12	4.12	6.66×10^{-7}
7	4.62	4.62	9.33×10^{-7}
10	5.07	5.07	1.33×10^{-6}
15	5.65	5.65	2.00×10^{-6}
20	6.05	6.05	2.66×10^{-6}
26	6.31	6.31	3.46×10^{-6}
30	6.70	6.70	4.00×10^{-6}
35	6.93	6.94	4.66×10^{-6}
40	7.10	7.11	5.33×10^{-6}
45	7.22	7.23	5.99×10^{-6}
50	7.33	7.34	6.66×10^{-6}
55	7.41	7.42	7.33×10^{-6}
60	7.49	7.50	7.99×10^{-6}
75	7.68	7.69	9.99×10^{-6}
90	7.82	7.83	1.20×10^{-5}
105	7.95	7.97	1.40×10^{-5}
121	8.05	8.07	1.61×10^{-5}
143	8.16	8.18	1.91×10^{-5}
180	8.32	8.35	2.40×10^{-5}

1448

1534

1556

1633

OWD-1

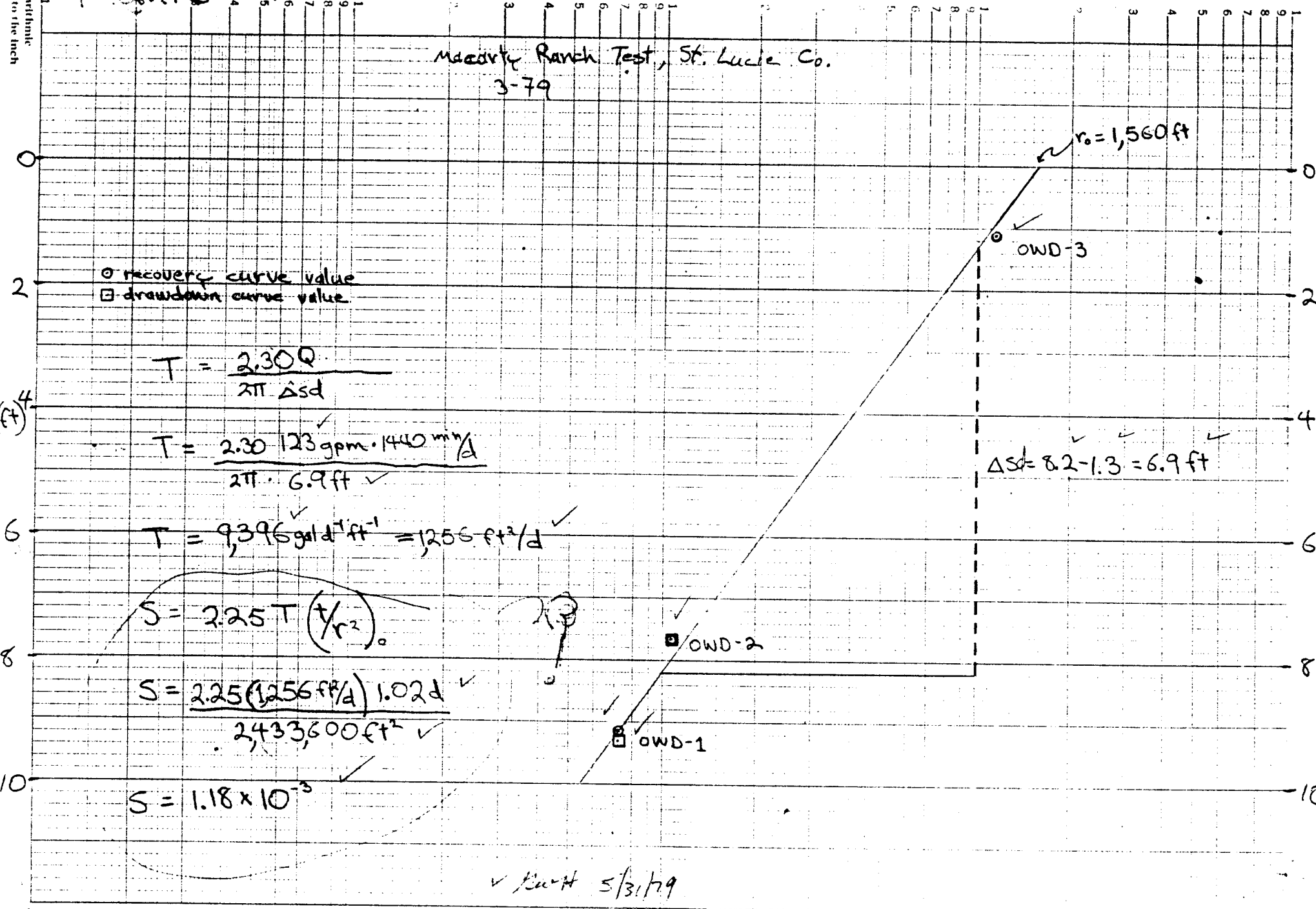
time	t(min)	s(ft)	S corrected (ft)	t/r^2 (d ft ⁻²)
1703	210	8.42	8.45	2.80×10^{-5}
1733	240	8.48	8.51	3.20×10^{-5}
1826	293	8.59	8.63	3.90×10^{-5}
1914	341	8.67	8.72	4.54×10^{-5}
2008	395	8.75	8.81	5.26×10^{-5}
2102	449	8.81	8.88	5.98×10^{-5}
2232	539	8.89	8.97	7.18×10^{-5}
1-79 0003	630	8.93	9.02	8.39×10^{-5}
0109	696	8.95	9.05	9.27×10^{-5}
0200	747	8.97	9.08	9.95×10^{-5}
0358	865	9.00	9.13	1.15×10^{-4}
0502	929	9.01	9.15	1.24×10^{-4}
0603	990	9.02	9.16	1.32×10^{-4}
0713	1060	9.04	9.19	1.41×10^{-4}
0800	1107	9.05	9.21	1.47×10^{-4}
0909	1176	9.07	9.24	1.57×10^{-4}
1000	1227	9.08	9.26	1.63×10^{-4}
1213	1360	9.30	—	1.81×10^{-4}
1302	1409	9.30	—	1.88×10^{-4}
1400	1467	9.30	—	1.95×10^{-4}

Figure 12

Thiem Method

RWW 4-13-79

Meadow Ranch Test, St. Lucie Co.
3-79



○ recovery curve value
□ drawdown curve value

$$T = \frac{2.30Q}{2\pi \Delta s d}$$

$$T = \frac{2.30 (123 \text{ gpm} \cdot 1440 \text{ min/d})}{2\pi \cdot 6.9 \text{ ft}}$$

$$T = 9396 \text{ gal/d ft} = 1256 \text{ ft}^2/\text{d}$$

$$S = 2.25 T \left(\frac{1}{r^2} \right)$$

$$S = \frac{2.25 (1256 \text{ ft}^2/\text{d}) (1.02 \text{ d})}{2,433,600 \text{ ft}^2}$$

$$S = 1.18 \times 10^{-3}$$

$$\Delta s = 8.2 - 1.3 = 6.9 \text{ ft}$$

✓ $K_{eff} = 5/31/79$

1 inch to the inch

Moritz Recovery pumping test, St. Lucie Co., FL

RWW 4-16-79

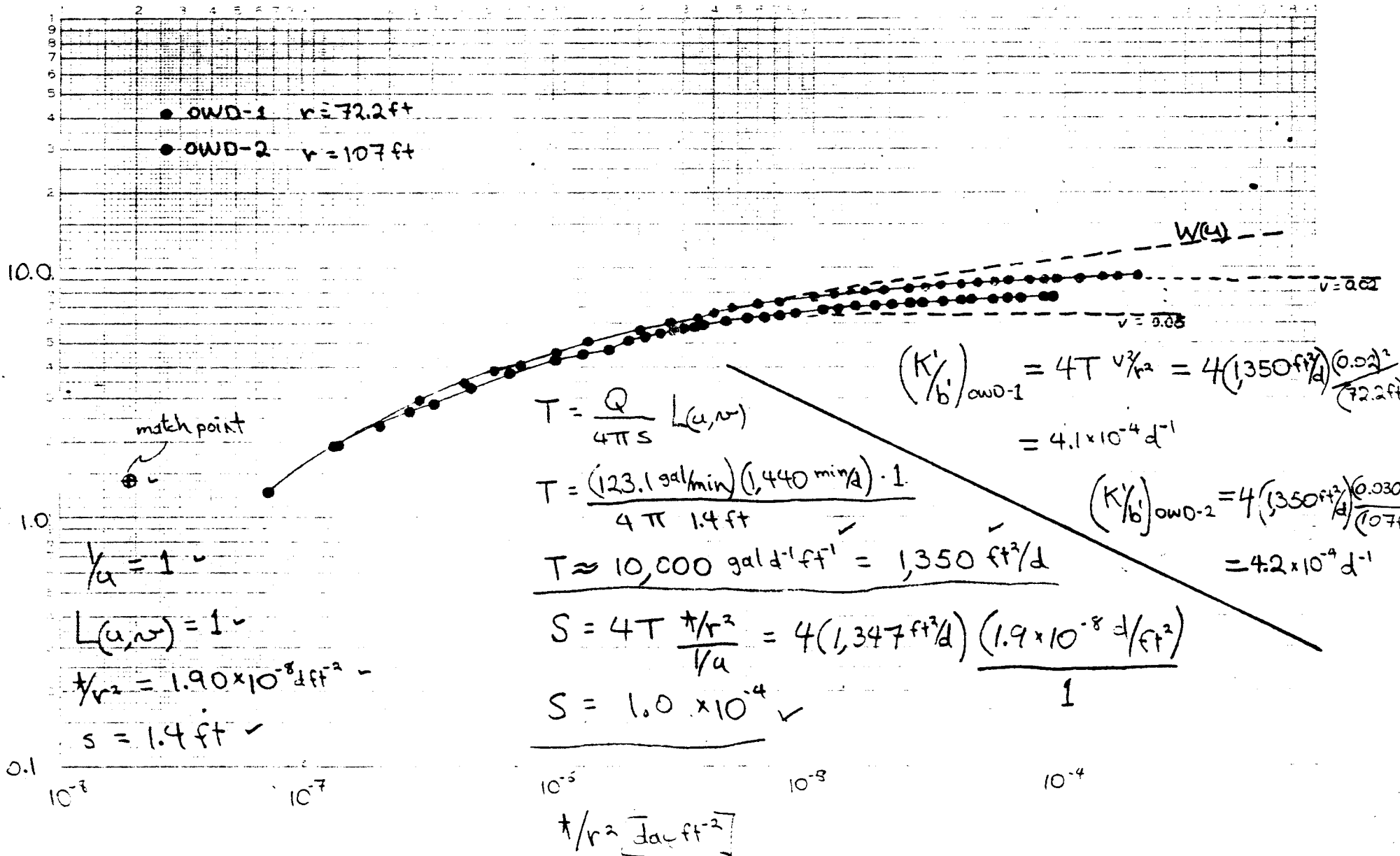
4-19-79

Hantush-Jacob method

method

from:
P.P. 708 pp 30-32

✓ MWH



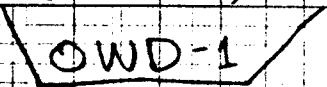
Handwritten Method I

RWW 7-13-79
 4-15-79

and evaluate on
 of pumping test data ILLRI
 p. 86

Macarty Ranch Test, St. Lucie Co., 3-79

- $Q = 123.1 \text{ gal/min}$ ✓
- $r = 72.2 \text{ ft}$ ✓
- $S_m = 9.30 \text{ ft}$ ✓
- $s_p = \frac{1}{2} S_m = 4.65 \text{ ft}$ ✓
- $t_p = 7.2 \text{ min}$ ✓
- $\Delta s_p = 3.12 \text{ ft}$ ✓



$$KD = T = \frac{2.30 Q}{4\pi \Delta s_p} e^{-r/L}$$

$$T = \frac{2.30 (123.1 \text{ gal/min}) (1,440 \text{ min/d})}{4\pi (3.12 \text{ ft})} e^{-0.042}$$

$$T = 9,971 \text{ gal ft}^2 \text{d}^{-1} = 1,333 \text{ ft}^2 \text{d}^{-1} \checkmark$$

$$2.30 \frac{s_p}{\Delta s_p} = e^{-r/L} K_0(r/L)$$

$$2.30 \frac{4.65 \text{ ft}}{3.12 \text{ ft}} = e^{-r/L} K_0(r/L) = 3.43 \checkmark$$

$$r/L = 0.042 \checkmark$$

$$\frac{72.2 \text{ ft}}{0.042} = L = 1,719 \text{ ft} \checkmark$$

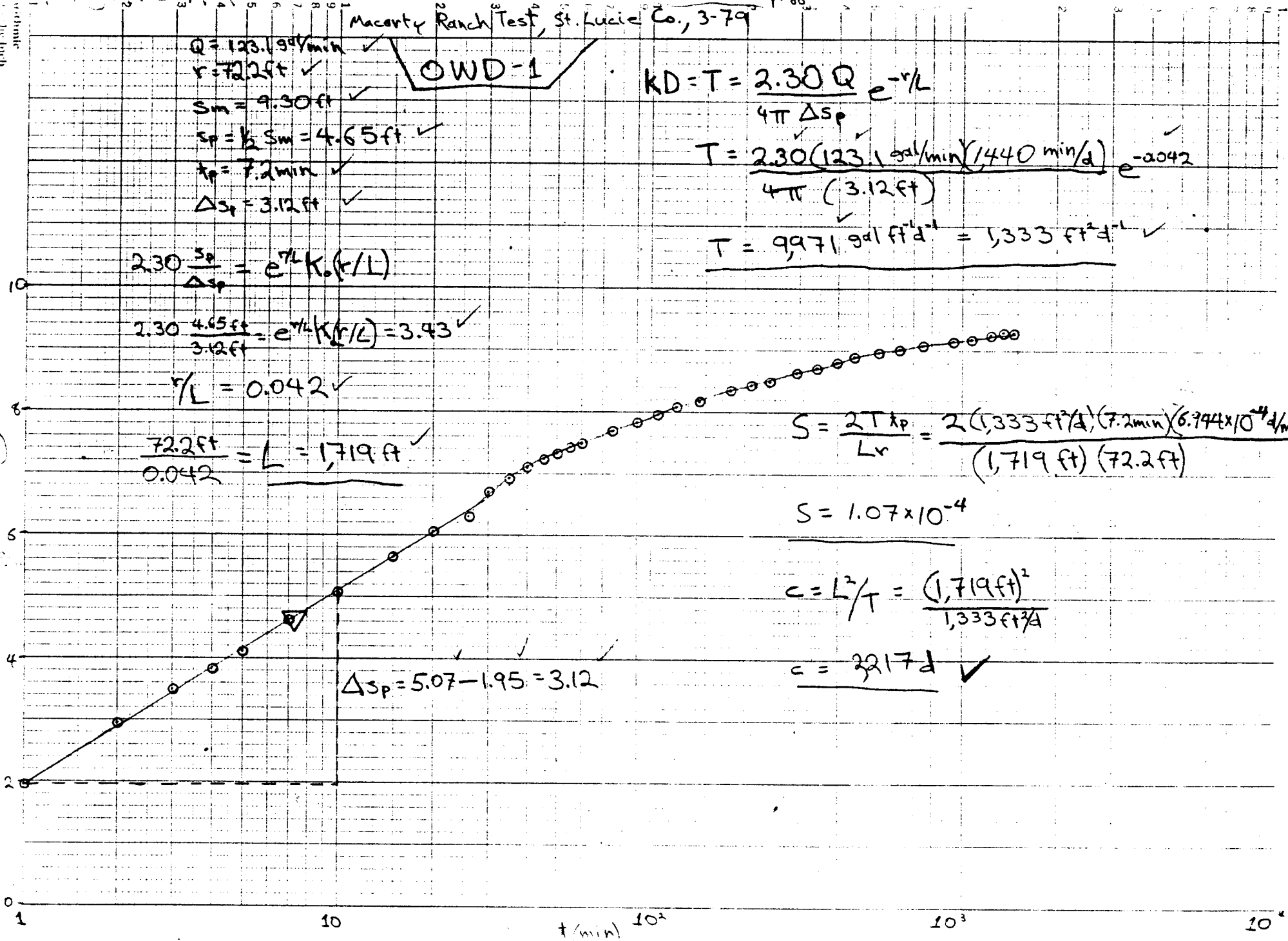
$$S = \frac{2 T t_p}{L r} = \frac{2 (1,333 \text{ ft}^2/\text{d}) (7.2 \text{ min}) (6.744 \times 10^{-4} \text{ d/min})}{(1,719 \text{ ft}) (72.2 \text{ ft})}$$

$$S = 1.07 \times 10^{-4}$$

$$c = \frac{L^2}{T} = \frac{(1,719 \text{ ft})^2}{1,333 \text{ ft}^2/\text{d}}$$

$$c = 2,217 \text{ d} \checkmark$$

$$\Delta s_p = 5.07 - 1.95 = 3.12 \checkmark$$



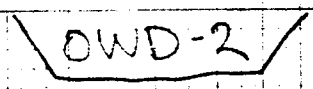
Scale: 1 inch = 100 ft

Figure 1

Alameda Co., St. Lucie Co., 3-79

YWW 4-13-79

4-18-79



$Q = 123.1 \text{ gal/min}$
 $r = 107 \text{ ft}$
 $s_m = 7.68$
 $s_p = \frac{1}{2} s_m = 3.84$
 $t_p = 10.8 \text{ min}$
 $\Delta s_p = 2.87 \text{ ft}$

$$T = \frac{2.30 Q e^{-r/L}}{4\pi \Delta s_p}$$

$$T = \frac{2.30 (123.1 \text{ gal/min}) (440 \text{ min/d}) e^{-0.062}}{4\pi (2.87 \text{ ft})}$$

$$T = 10,625 \text{ gal ft}^2 \text{ d}^{-1} = 1,420 \text{ ft}^2 \text{ d}^{-1}$$

$$2.30 \frac{s_p}{\Delta s_p} = e^{-r/L} K_a (r/L)$$

$$2.30 \frac{3.84}{2.87} = 3.08$$

$$r/L = 0.062$$

$$L = \frac{107 \text{ ft}}{0.062} = 1,726 \text{ ft}$$

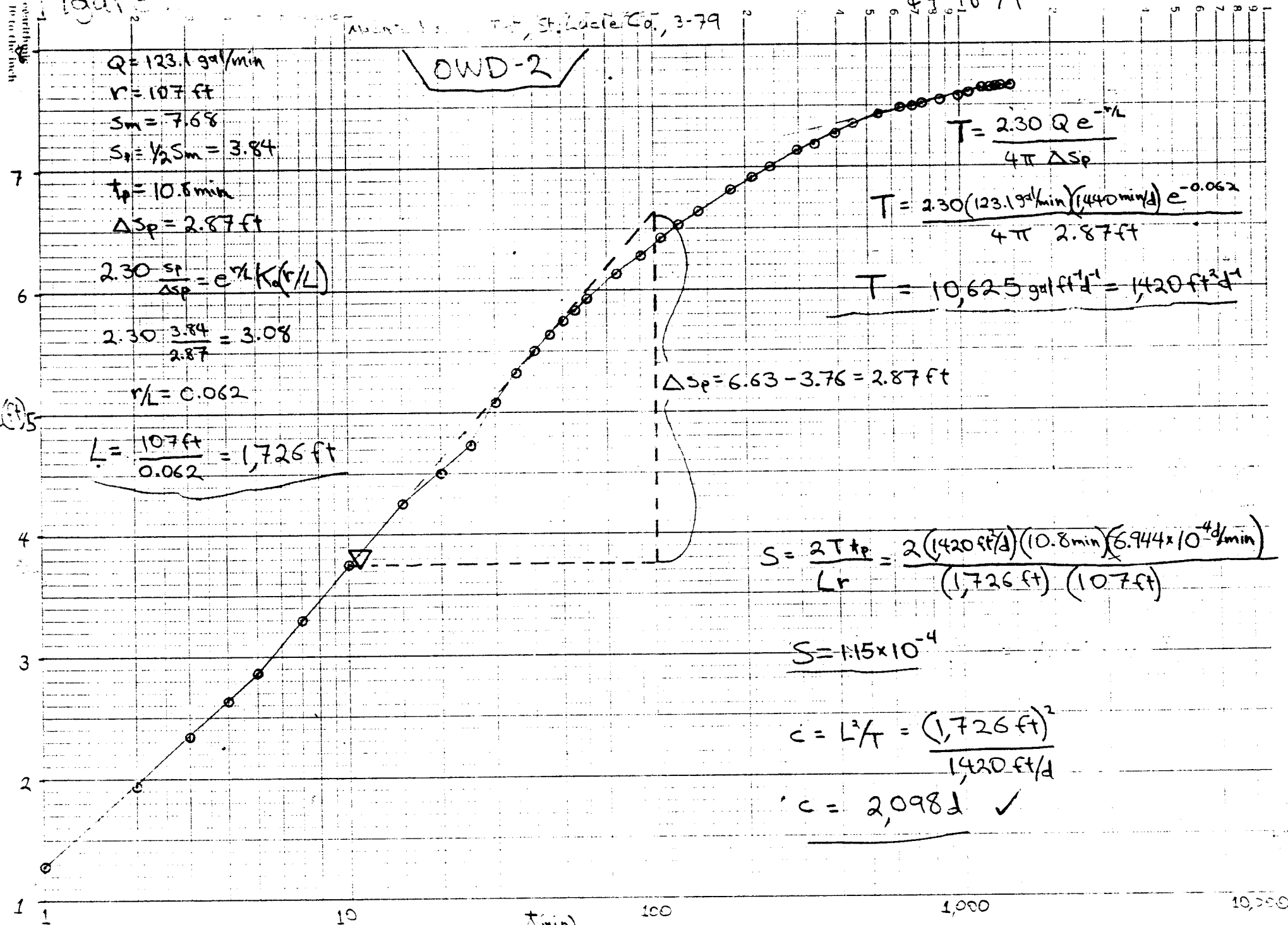
$$\Delta s_p = 6.63 - 3.76 = 2.87 \text{ ft}$$

$$S = \frac{2Tt_p}{Lr} = \frac{2 (1,420 \text{ ft}^2/\text{d}) (10.8 \text{ min}) (6.944 \times 10^{-4} \text{ d/min})}{(1,726 \text{ ft}) (107 \text{ ft})}$$

$$S = 1.15 \times 10^{-4}$$

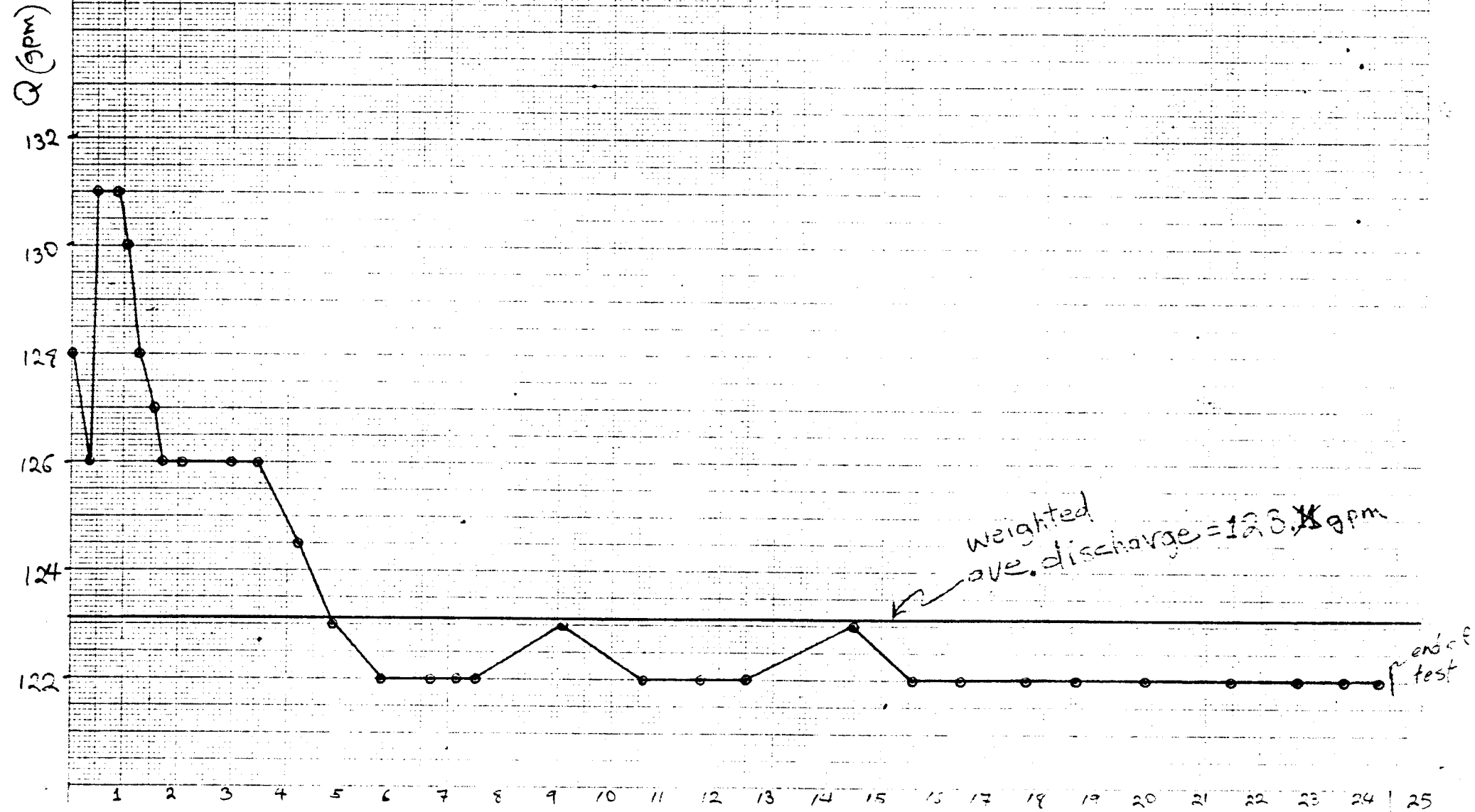
$$c = L^2/A = \frac{(1,726 \text{ ft})^2}{1,420 \text{ ft}^2/\text{d}}$$

$$c = 2,098 \text{ d} \quad \checkmark$$



RWW 4-11-79

Figure 10a Discharge vs. time
(Macarty Ranch test 3-79)



Discharge Measurements

McCarty Ranch

QW field parameters 3/28/79 RWU-MAD-JSW

Figure 20

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Temp = 25°C hardness (as CaCO₃) = 435 mg/l
Iron = 1 mg/l
sp. cont. = 158
HS = 400 mg/l
SO₄ = < 50 mg/l

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WATER LEVEL MEASUREMENTS (Field)

Measured by W.R. IRUW

Location of Project

6" pipe 3" office inside

DATE	HOUR	WELL NO.	TAPE READING AT—		DEPTH TO WATER	REMARKS
			Mean point	Top of pipe		
3/28	01330	Start at @			15.5"	128
	13340				15"	128
	1355				14.5"	126
	1402				15.75	130
	1428				15.75	130
	1435				15.50	129
	1450				15.00	128
	1505				14.75	
	1515		4050		14.50	
	1523		2050		14.50	
	1538				14.50	15.75 = 131
	1555				14.50	15.5 = 130
	1632				14.00	15.25 = 129
	1700				14.50	15.00 = 128
	1745				14.25	14.5 = 126
	1823				14.0	14.25 = 125
	1919				13.75	13.5 = 124
	2012				13.75	
	2040				13.75	
	2103				13.75	

WATER LEVEL MEASUREMENTS (Field)

Measured by _____

Location of Project _____

DATE	HOUR	WELL NO.	TAPE READING AT—		DEPTH TO WATER	REMARKS
			Mean point	Water level		
2/23	2238				14.0	✓
2/29/79	0007				13.8	✓
	0102				13.8	✓
	203				13.8	✓
	401				14	✓
	508				13.75	✓
	600				13.75	✓
	712				13.75	✓
	0807				13.75	✓
	925				13.75	✓
	1100				13.75	✓
	1215				13.75	✓
	1304				13.75	✓
	1345				13.75	✓

a gate valve was not used to regulate the discharge. The production well was pumped to its capacity, and flow remained fairly constant throughout the test (figure 10a,b).

After a pumping period of 24 hours water level fluctuations became negligible, and the test was shut down. Water level recovery was closely monitored for the first two hours after shutdown, and the charts were pulled the next day. There was no precipitation during the test, and the microbarograph was malfunctioning, so there is no on site record of barometric pressure changes.

Computations

- Figure 11a,b — Hantush method I
- Figure 12 — Thiem method
- Figure 13 — Hantush-Jacob method
- Tables 1 and 2 — plotted values

Drawdowns in both shallow observation wells OWS-1 and OWS-2 were about 0.7 feet at the end of the test. This indicates that the aquifer is semiconfined. Therefore, all three of these methods are applicable to this test. Calculated transmissivity values are nearly the same for all methods, and calculated storage coefficients are close for the Hantush I and Hantush-Jacob methods. The values of $T = 10,000 \text{ gal/d}^2 \text{ ft}$, and $S = 1 \times 10^{-4}$ have thus been adopted for this test. (also $K/b = 4.15 \times 10^{-4} \text{ d}^{-1}$)

RWW
6-29-79

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OW 2 - 6" well, depth = 12
m.p. - top of casing

WATER LEVEL MEASUREMENTS (Field) Measured by JSW-U.A.-R.W.W.

Location of Project _____

DATE	HOUR	WELL NO.	TAPE READING AT—		DEPTH TO WATER	M.P. EIV.	W.L. EIV.
			Meas. point	Water level			
3-29-79	0715				4.01		drg. down
	0845		4.00	0.03	3.97		
	1012		5.0	.97	4.03		
	1120				4.02		
	1400		5.0	1.0	4.0		
	1401				4.0		1.02
	1402				4.0		1.0
	1403				4.0		
	1404				4.0		
	1405				4.0		
	1406				4.0		
	1407				4.0		
	1408				4.0		
	1409				4.0		
	1410				4.0		
	1412				4.0		1.05
	1415				4.0		1.02
	1420		5.0	1.01	3.99		1.01
	1425				3.99		1.01
	1430		5.0	1.02	3.98		1.00
	1435		5.0	1.02	3.98		1.00
	1440		5.0	1.05	3.95		1.07

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WATER LEVEL MEASUREMENTS (Field) Measured by _____

Location of Project _____

DATE	HOUR	WELL NO.	TAPE READING AT—		DEPTH TO WATER	M.P. EIV.	W.L. EIV.
			Meas. point	Water level			
	1445		5.0	1.08	3.92		1.02
	1450		5.0	1.09	3.91		1.02
	1455			1.11	3.89		1.01
	1500			1.13	3.87		0.99
	1510			1.16	3.84		0.96
	1520			1.18	3.82		0.94
	1530		5.0	1.25	3.75		0.87
	1545		5.0	1.30	3.70		0.85
	1600		5.0	1.33	3.67		0.79
3-30-79	0910		3.10	0.22	2.88		0

assigned for complete recovery

1.02

1.02

1.01

0.99

0.96

0.94

0.87

0.85

0.79

OWS -

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WATER LEVEL MEASUREMENTS (Field) Measured by G. K. H.
Location of Project McCarty Ranch OWS-2

DATE	MINUTES	WELL NO. MIN	TAPE READING AT—		DEPTH TO WATER	WATER LEVEL (Feet)	REMARKS
			Mean point	Water level			
	1324		6.0	2.30	3.70		
	1330		8.0	4.31	3.69		
	1335		8.0	4.30	3.70	0	
	3		9.0	5.29	3.71	.01	
	4		9.0	5.30	3.70	.0	
	5		"	5.31	3.71	+01	
	6		"	5.28	3.72	.02	
	7		"	5.26	3.74	.04	
	8		"	5.26	3.74	.04	
	9		"	5.25	3.75	.05	
	10			5.25	3.75	.05	
	11						
	12			5.23	3.77	.07	
	14			5.23	3.77	.07	
	17			5.24	3.76	.06	
	22			5.20	3.80	.10	
	25			5.20	3.80	.10	
	25			5.20	3.80	.10	
	30			5.18	3.82	.12	
	35			5.16	3.84	.14	
	45			5.12	3.88	.18	
	50			5.11	3.89	.19	
	60			5.09	3.91	.21	

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WATER LEVEL MEASUREMENTS (Field) Measured by _____
Location of Project _____

DATE	HOUR	WELL NO.	TAPE READING AT—		DEPTH TO WATER	Feet (msl)	Remarks
			Mean point	Water level			
	75		9.0	5.06	3.94	.24	
	90		9.0	5.02	3.98	.28	
	105		9.0	4.99	4.01	.31	
	120		9.0	4.96	4.04		
	1637		6.0	1.91	4.09		
	1700		5.0	.88	4.12		
	1822		5.0	.81	4.19		
	1917		5.0	.79	4.21		
	2014		5.0	.77	4.23		
	21		5.0	.74	4.26		
	2336		5.0	.71	4.29		
	0003		5.0	.69	4.31		
	0113		5.0	.68	4.32		
	0203		5.0	.66	4.34		
	0401		5.0	.67	4.33		
	0507		5.0	.65	4.35		
	0600		5.0	.66	4.34		
	0712		5.0	.65	4.35		
	0805		5.0	0.63	4.37		
	0925		5.0	.64	4.36		
	1005		5.0	.65	4.36		
	1103		5.0	.62	4.38		

OWD-3

Macarty Ranch - St. Lucie Co.

OWD-3 - 6" well, depth = 120', r = 1140' south of production well

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m.p. = top of casing

5.00
.97
4.03

WATER LEVEL MEASUREMENTS (Field)

Measured by JSW-WAL-RWW

Location of Project _____

WATER LEVEL MEASUREMENTS (Field)

Measured by _____

Location of Project _____

pump
off

DATE	HOUR	WELL NO.	TAPE READING AT—		DEPTH TO WATER	M. P. Elev.	W. L. Elev.
			Meas. point	Water level			
3-27-79	0715				4.01		
	0845		4.00	0.03	3.97		
	1012		5.0	.97	4.03		
	1120				4.02		
	1400		5.0	1.0	4.0		
	1401				4.0		
	1402				4.0		
	1403				4.0		
	1404				4.0		
	1405				4.0		
	1406				4.0		
	1407				4.0		
	1408				4.0		
	1409				4.0		
	1410				4.0		
	1412				4.0		
	1415				4.0		
	1420		5.0	1.01	3.99		
	1425				3.98		
	1430		5.0	1.02	3.98		
	1435		5.0	1.02	3.98		
	1440		5.0	1.05	3.95		
					3.95		

DATE	HOUR	WELL NO.	TAPE READING AT—		DEPTH TO WATER	M. P. Elev.	W. L. Elev.
			Meas. point	Water level			
	1445		5.0	1.08	3.92		
	1450		5.0	1.09	3.91		
	1455			1.11	3.89		
	1500			1.13	3.87		
	1510			1.16	3.84		
	1520			1.18	3.82		
	1530		5.0	1.25	3.75		
	1545		5.0	1.30	3.70		
	1600		5.0	1.33	3.67		
3-30-79	0910		3.10	0.22	2.88		

Discharge Measurements

McCarty Ranch

QW field parameters 3/28/79 RWU-MAD-JSW

Temp = 25°C hardness (as CaCO₃) = 435 mg/l

Iron = 1 mg/l

sp. cond. = 1580 μ m/cm

H₂S = 400 μ g/l

SO₄ = < 50 μ g/l

WMQ = 123 GPM

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WATER LEVEL MEASUREMENTS (Field)

Measured by

Wal RWU

Location of Project

6" pipe 3" office indicator

DATE	HOUR	WELL NO.	TAPE READING AT—		DEPTH TO WATER	REMARKS
			Meas. point	Water level		
3/28	01330	that's it @			15" in	128
	13340			Same	15"	128 } 127
	1355	.42 hrs			14.5"	126 } 128
	1402	.17 hrs			15.75	130 } 131
	1425	.38 hrs			15.75	130 } 130
	1435	.17 hrs			15.50	130 } 129
	1450	.25			15.00	128 } 128
	1505	.25			14.75	127 } 126
	1515		up out 50		14.20	126 } 126
	1523		Down 50		14.50	126
	1538				14.50	126
	1555		2.67 hrs		14.50	126 } 126
	1632				14.40	126
	1700				14.50	126
	1745				14.25	125 } 124
	1823				14.0	123 } 124
	1919	.63			13.75	122
	2012				13.75	122
	2040				13.75	122
	2103		19.36		13.75	122 } 122

WATER LEVEL MEASUREMENTS (Field)

Measured by

Location of Project

DATE	HOUR	WELL NO.	TAPE READING AT—		DEPTH TO WATER	REMARKS
			Meas. point	Water level		
223	2238				14.0	123
2/29/79	0007				13.8	122
	0102				13.8	122
	203				13.8	122
	401				14	123
	508				13.75	122
	600				13.75	
	712				13.75	
	0807				13.75	
	925				13.75	
	1100				13.75	
	1215				13.75	
	1304				13.75	
	1345				13.75	122

Computation of weighted mean Q:
 $.42 \times 127 = 53.34$ $2.67 \times 126 = 336.42$
 $.12 \times 128 = 15.36$ $.63 \times 124 = 78.12$
 $.58 \times 131 = 75.98$ $19.36 \times 122 = 2361.92$
 $.17 \times 130 = 22.10$ 24.25
 $.25 \times 129 = 32.25$
 $.25 \times 128 = 32.00$

WMQ = 123 GPM

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WATER LEVEL MEASUREMENTS (Field)

Measured by GWH FOTHERS

Location of Project

McCarty Ranch OWS-2

DATE	HOUR	WELL NO.	TAPE READING AT—		DEPTH TO WATER	REMARKS
			Mess. point	Water level		
3/29/49	1214		5.0	.63	4.37	.67
	1304		5.0	.62	4.38	.68
	1340		5.0	.61	4.39	.69
	1359	1465	5.0	.60	4.40	.70
1400	0		5.0	.60	4.40	.70
	1			.61	4.39	.69
	2			.61	4.39	.69
	3			.63	4.37	.67
	4			.63	4.37	.67
	5			.63	4.37	.67
	7			.64	4.36	.66
	9			.64	4.36	.66
	12			.66	4.34	.64
	15			.67	4.33	.63
	20			.69	4.31	.61
	25			.72	4.28	.58
	30			.73	4.27	.57
	40			.75	4.25	.55
	50			.78	4.22	.52
	60			.82	4.18	.48
1519	79			.85	4.15	.45
1605	125			.92	4.08	.38

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WATER LEVEL MEASUREMENTS (Field)

Measured by _____

Location of Project _____

DATE	HOUR	WELL NO.	TAPE READING AT—		DEPTH TO WATER	REMARKS
			Mess. point	Water level		
3-30-49	1010		4.00	0.34	3.66	

OWS-2

Radios = 142 Ft 3-30-79
RWW

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WATER LEVEL MEASUREMENTS (Field) Measured by GWH

Location of Project McCarty Ranch OWS-2

DATE	Minutes HOUR	WELL NO. MIN	TAPE READING AT—		DEPTH TO WATER	WATER LEVEL Ft (MSL)	REMARKS
			Meas. point	Water level			
	1324		6.0	2.30	3.70		
	1330		8.0	4.31	3.69		
	1335		8.0	4.30	3.70	0	
1338	3		9.0	5.29	3.71	.01	
1342	4		9.0	5.30	3.70	.0	
1343	5		"	5.31	3.71	+01	
1344	6		"	5.28	3.72	.02	
1345	7		"	5.26	3.74	.04	
1346	8		"	5.26	3.74	.04	
1347	9		"	5.25	3.75	.05	
1348	10		"	5.25	3.75	.05	
1349							
1350	12			5.23	3.77	.07	
1351	14			5.23	3.77	.07	
1352	17			5.24	3.76	.06	
1353	22			5.20	3.80	.10	
1354	25			5.20	3.80	.10	
1355	25			5.20	3.80	.10	
1356	30			5.18	3.82	.12	
1357	35			5.16	3.84	.14	
1358	45			5.12	3.88	.18	
1359	50			5.11	3.89	.19	
1360	60			5.09	3.91	.21	

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November 1949

UNITED STATES
DEPARTMENT OF THE INTERIOR
GEOLOGICAL SURVEY
WATER RESOURCES DIVISION

B+

WATER LEVEL MEASUREMENTS (Field) Measured by _____

Location of Project _____

DATE	HOUR	WELL NO.	TAPE READING AT—		DEPTH TO WATER	Ft (MSL)	Remarks
			Meas. point	Water level			
1450	75		9.0	5.06	3.94	.24	
1505	90		9.0	5.02	3.98	.28	
1520	105		9.0	4.99	4.01	.31	
1535	120		9.0	4.96	4.04	.34	
1637	182		6.0	1.91	4.09	.39	
1700	205		5.0	.88	4.12	.42	
1745	250		6.0	1.21	4.16	.46	
1822	287		5.0	.81	4.19	.49	
1917	342		5.0	.79	4.21	.51	
2014	399		5.0	.77	4.23	.53	
21	448		5.0	.74	4.26	.56	
2336	542		5.0	.71	4.29	.59	
3/29/79	0003	628	5.0	.69	4.31	.61	
	0113	699	5.0	.68	4.32	.62	
	0203	749	5.0	.66	4.34	.64	
	0401	867	5.0	.67	4.33	.63	
	0507	933	5.0	.65	4.35	.65	
	0600	986	5.0	.66	4.34	.64	
	712	1058	5.0	.65	4.35	.65	
	0805	1110	5.0	0.63	4.37	.67	
	0925	1191	5.0	.64	4.36	.66	
	1005	1231	5.0	.64	4.36	.66	
	1103	1289	5.0	.62	4.38	.68	

McCart~~r~~ Ranch Pumping Test

Summary sheet

Date test begun — 3-28-79

Length of test — 24 hrs 27 min

Discharge — 123 gal/min

Hydraulic coefficient results

Hantush method I (semiconfined, unsteady-state)

well OWD-1 $\rightarrow T = 9,971 \text{ gal d}^{-1} \text{ ft}^{-1}$

$\rightarrow S = 1.07 \times 10^{-4}$

well OWD-2 $\rightarrow T = 10,625 \text{ gal d}^{-1} \text{ ft}^{-1}$

$\rightarrow S = 1.15 \times 10^{-4}$

Theim method (confined, steady-state)

$T = 9,396 \text{ gal d}^{-1} \text{ ft}^{-1}$

$S = 1.18 \times 10^{-3}$

Hantush - Jacob method (semiconfined, unsteady-state)

$$T = 10,000 \text{ gal d}^{-1} \text{ ft}^{-1}$$

$$S = 1.0 \times 10^{-4}$$

$$\text{well OWD-1} \rightarrow K'/b' = 4.1 \times 10^{-4} \text{ d}^{-1}$$

$$\text{well OWD-2} \rightarrow K'/b' = 4.2 \times 10^{-4} \text{ d}^{-1}$$

Field observations of drawdown in shallow observation wells, plus data plots of deep observation wells indicate this is a semiconfined aquifer. Therefore, the following results are adopted for this test.

$$T = 10,000 \text{ gal d}^{-1} \text{ ft}^{-1}$$

$$S = 1 \times 10^{-4}$$

$$K'/b' = 4.15 \times 10^{-4} \text{ d}^{-1}$$

Preparer — Ralph Wilcox

Introduction

The purpose of this test is to determine the transmissivity and storage coefficient of the main producing zone of the so-called shallow aquifer at this site. Determination of these parameters in Martin and St. Lucie Counties, Florida is an objective of the Upper East Coast Project (459826800). This is a cooperative project with South Florida Water Management District.

Personnel conducting test

- George Hill
- Wes Miller
- Bill Long
- Ralph Wilcox
- Jay Wendorf

Physical Conditions

The test site is located about 2.7 miles north of the Martin-St. Lucie County line, and about 1 mile west of State Road 609 (figure 1). The lat-long of the production well is $N27^{\circ}14'40"$, $W080^{\circ}29'55"$ (T37S, R38E, Sec 23, NE SE NE).

Wells used in this test are described on figure 2. It should be noted that the screened intervals are not known on wells OWS-2 and OWD-3, but well depths are known.

The tested aquifer consists of unconsolidated shells and shell fragments with a minor component of sand (figure 3).

Anticipated boundaries exist both south and west of the pumping test site (figure 1). Along the county line approximately 2.7 miles south of the test site is the C-23 canal. About 2 miles west of the test site is a rock quarry. Within this

LOCAL WELL NUMBER: SL-185

LOCATION: Two and one-half miles east of SR 609 extension, on McCarty Ranch. 4" production well

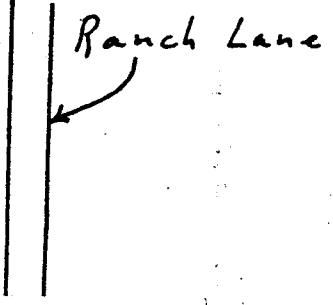
<u>Depth</u> Feet (Below Land Surface)	<u>Geologic Description</u>
0-1	Fine sand, black organic material
1-3	Red sand, some gray clay
3-6	Blue-gray clay and fine sand
6-10	Gray, sandy Ls and shell, some clay
10-15	Gray, sandy, Ls cement, 90% quartz sand
15-20	Shells, poorly cemented
20-27	Shells (coquina)
27-35	Shells (coquina)
35-40	Fine gray sand
40-46	Hard, cemented shell and Ls
46-50	Shell, sandy Ls (20% quartz) some clay
50-57	Fine gray sand
57-63	Fine gray sand, some shell
63-73	Sand, shell, clay
73-78	Very fine gray sand
78-88	Sand (75%), shell, clay
88-92	Sand on top of shell bed
92-103	Fine gray sand
103-107	Poorly cemented shell, lost mud
107-118	Shells (unconsolidated) some sand


113
↑
103
↓
92

Lat. - Long. 271440 0802955
 Top 37s Rg 38e Sac 24 SE 4, NE 4

Agwifer test: Goals Actual
 24 hrs pumping
 24 hrs recovery
 Q of 150-200 gpm

Observation Well #1
 2 inch diameter
 98.4 ft deep (below LS)
 1.6 ft MP (above LS)
 88.4 - 98.4 ft screened (below LS)



ROUTING AND TRANSMITTAL SLIP		ACTION
1	TO (Name, office symbol or location) George Hill, WRD Jupiter	CIRCULATE
2		COORDINATION
3		FILE
4		INFORMATION
		NOTE AND RETURN
		PER CONVERSATION
		SEE ME
		SIGNATURE
REMARKS		
<p>Enclosed is the info. on the McCarty test well you requested. Bill Long has been to the site and should be able to find it again. Be sure to call John McCarty in advance and stop at the house before going to the wells.</p> <p>Also enclosed are pumping test data for the old Ft. Pierce well field. This is original data and field notes so guard it closely.</p>		
FROM (Name, office symbol or location)		DATE
		3/12/79
		PHONE

OPTIONAL FORM 41
 AUGUST 1967
 GSA FPMR (41CFR) 100-11.206

GPO 648-16-81418-1 410-016 5041-101

Observation Well #2
 2 inch diameter
 98.4 ft deep (below LS)
 1.6 ft MP (above LS)
 88.4 - 98.4 ft screened (below LS)

Mc Carty Ranch Test Well
Lat.-Long. 271440 0802955
Twp 37s Rg 38e S4c 24 SE4, NE4

Aquifer test: Goals Actual
24 hrs pumping
24 hrs recovery
Q of 150-200 gpm

Observation Well #1
2 inch diameter
98.4 ft deep (below LS)
1.6 ft MP (above LS)
88.4-98.4 ft screened (below LS)

$r = 72.2 \text{ ft (22.0 m)}$

Test Well
4 inch diameter
113 ft deep (below LS)
2.8 ft MP (above LS)
103-113 ft screened (below LS)

$r = 107.0 \text{ ft (32.6 m)}$

Ranch Lane

Observation Well #2
2 inch diameter
109.2 ft deep (below LS)
1.8 ft MP (above LS)
99.2-109.2 screened (below LS)

Figure 2 Mcarty Ranch pumping test site description

N
↑

(SL-185)
Production well — 4" diameter, 113' deep (below L_s),
103'-113 ft screened (below L_s), L_s elev ~ 27 ft
assumed, m.p. elev. 29.7', m.p. ~ 2.7'
above L_s.

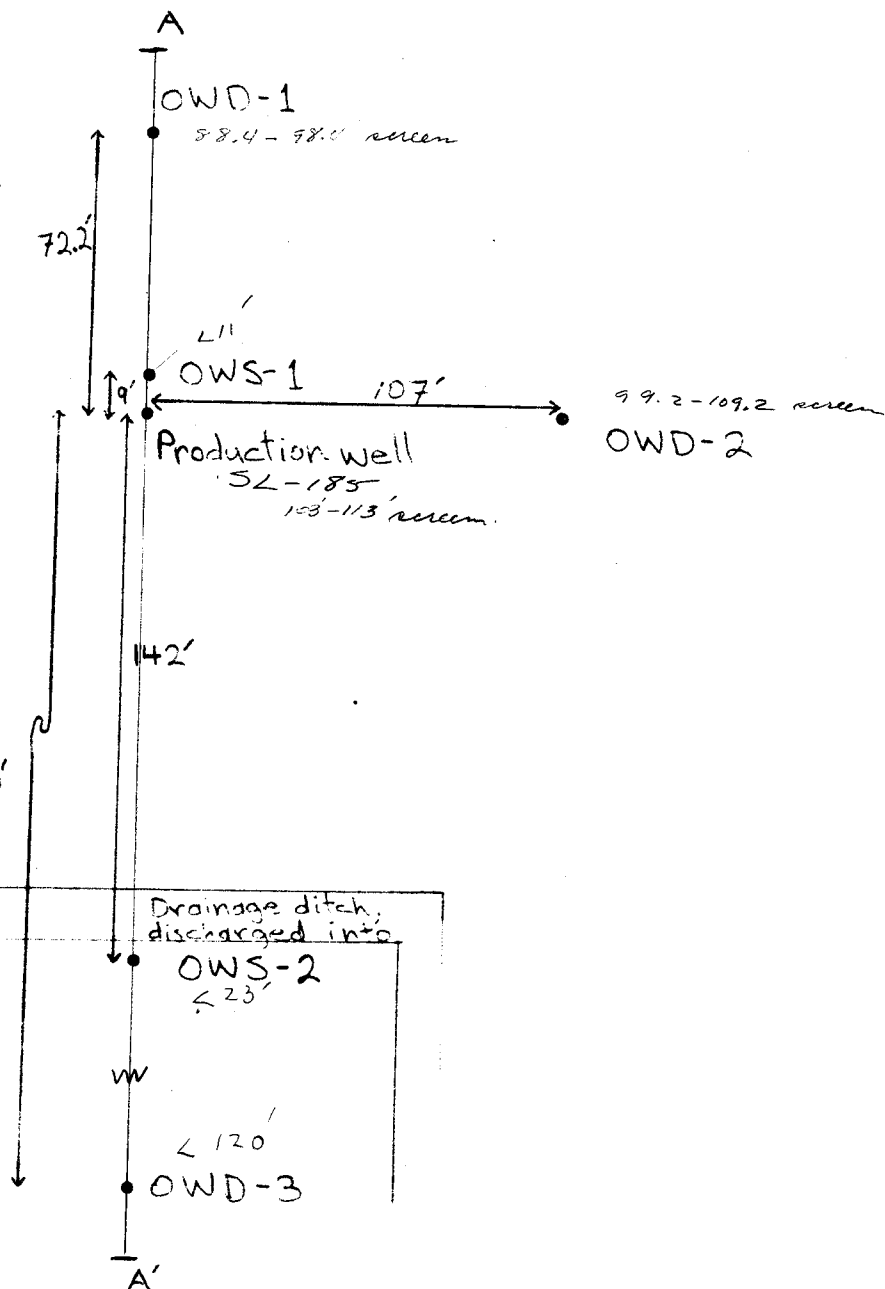
OWD-1 — 2" diameter, 93.4' deep (below L_s)
88.4-98.4 ft screened (below L_s), m.p. elev 29.01,
m.p. ~ 1' above L_s.

OWD-2 — 2" diameter, 109.2' deep (below L_s)
99.2-109.2 ft screened (below L_s),
m.p. elev 29.33, m.p. ~ 1.5' above L_s.

OWD-3 — 6" diameter, 120' deep (below m.p.)
m.p. ~ 1' above L_s, elev. m.p. 27.60

OWS-1 — 2" diameter, 11' deep (below L_s)
open hole, m.p. elev. 29.04', m.p. ~ 1' above
L_s.

OWS-2 — 2" diameter, 23' deep
(below m.p.), m.p. elev. 28.42',
m.p. ~ 2' above L_s.



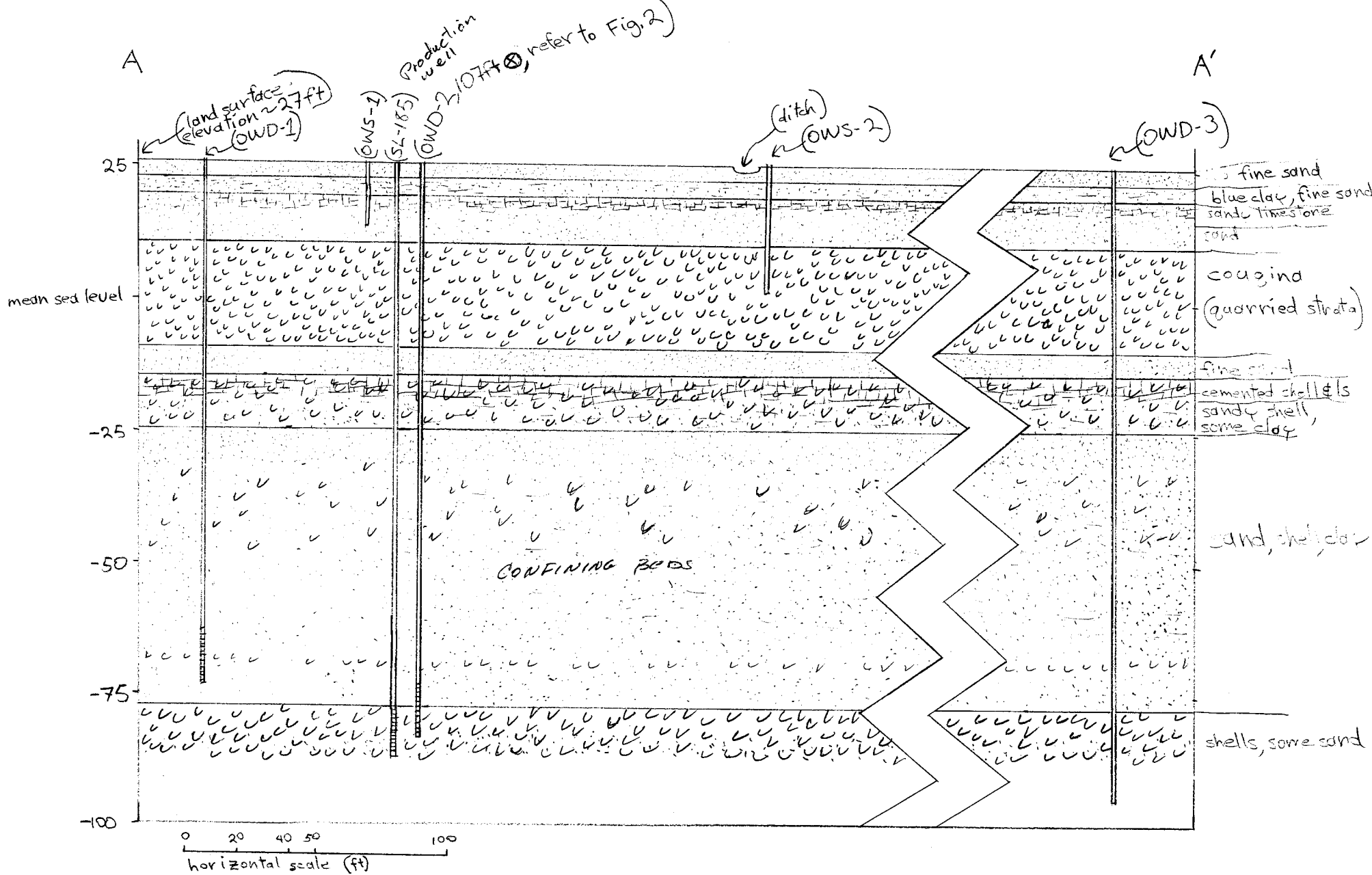


Figure 3

Cross sectional view of McCarty Ranch pumping test site.
 (cross section constructed with lithologic log of SL-185 only)

7

LOCAL WELL NUMBER: SL-185

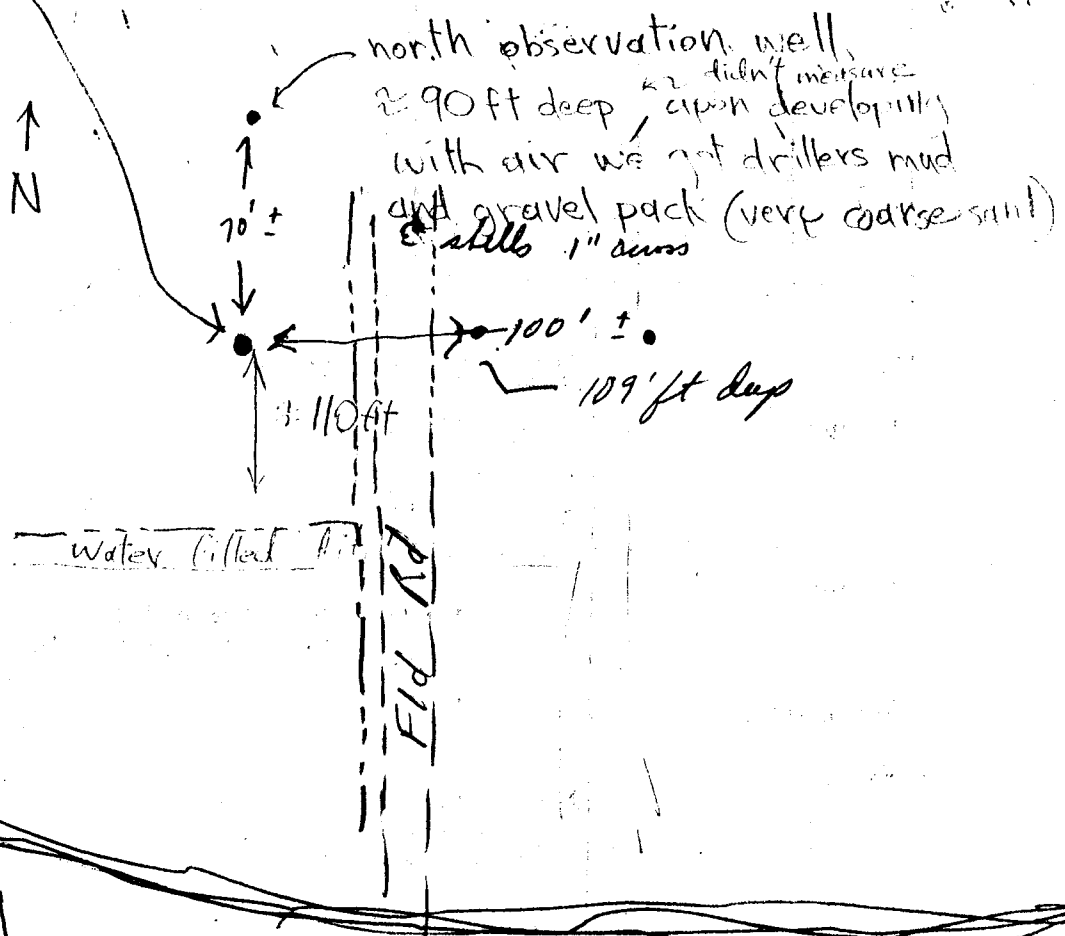
LOCATION: Two and one-half miles east of SR 609 extension, on McCarty Ranch.

<u>Depth</u> Feet (Below Land Surface)	<u>Geologic Description</u>
0-1	Fine sand, black organic material
1-3	Red sand, some gray clay
3-6	Blue-gray clay and fine sand
6-10	Gray, sandy Ls and shell, some clay
10-15	Gray, sandy, Ls cement, 90% quartz sand
15-20	Shells, poorly cemented
20-27	Shells (coquina)
27-35	Shells (coquina)
35-40	Fine gray sand
40-46	Hard, cemented shell and Ls
46-50	Shell, sandy Ls (20% quartz) some clay
50-57	Fine gray sand
57-63	Fine gray sand, some shell
63-73	Sand, shell, clay
73-78	Very fine gray sand
78-88	Sand (75%), shell, clay
88-92	Sand on top of shell bed
92-103	Fine gray sand
103-107	Poorly cemented shell, lost mud
107-118	Shells (unconsolidated) some sand

3-8-79 RWW/WAL

Test of wells at Mearly Ranch for pumping test on following week

production well — 160-180 gpm-max
113 ft deep



3-12-79

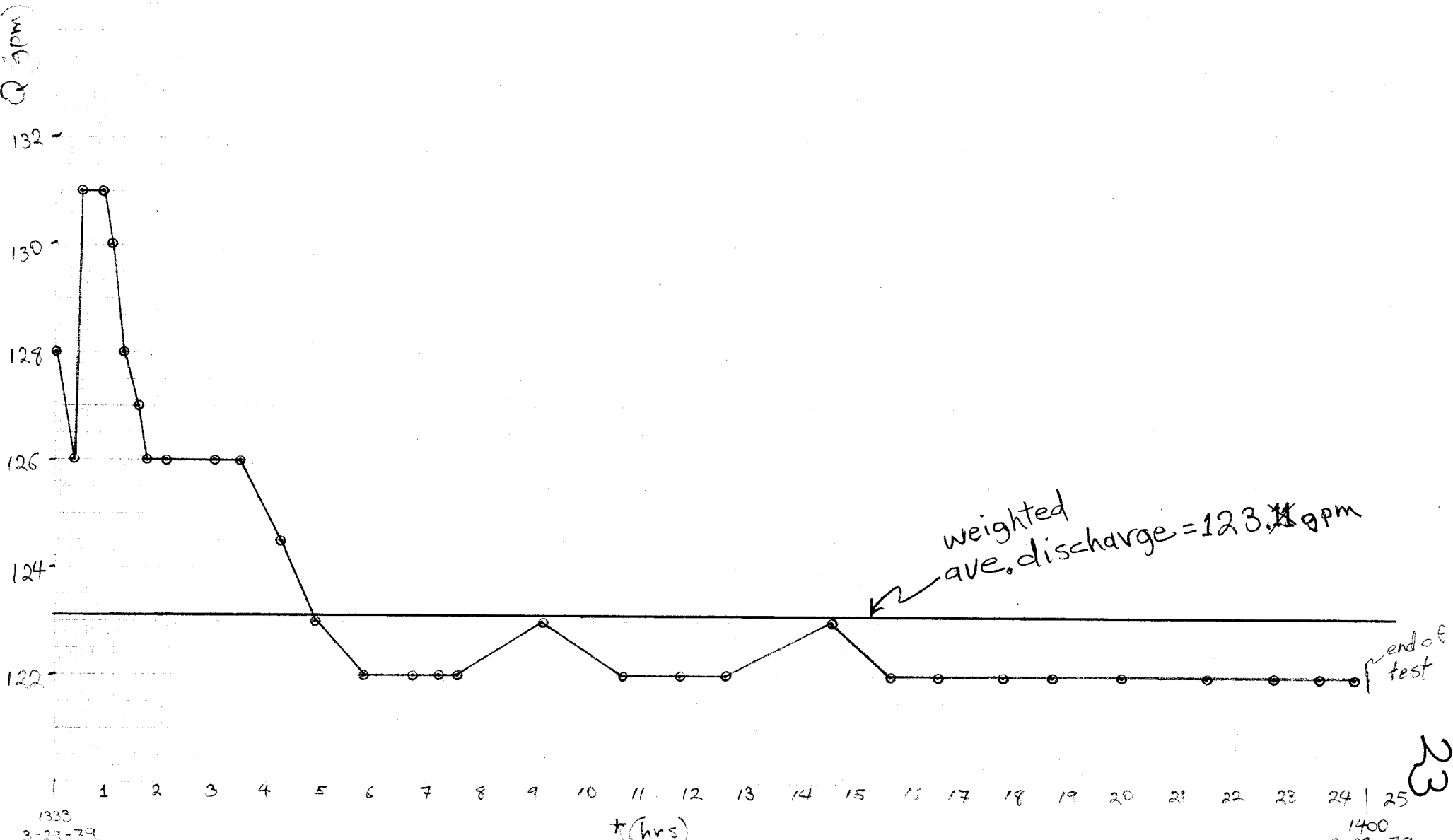
	head	read	dtw	
North Obs well	32.0	0.68	31.32	m.p. @ 6:10 after developing $\frac{5.00}{1.10} = 3.90$
Production well	5.0	0.48	4.52	m.p. } top of coupling
East Obs well	6.0	1.57	4.43	m.p. } remeasure 4.32

before development

RWW 4-11-79

Figure 10a

Discharge vs. time
(Macarty Ranch test 3-79)



Discharge Measurements

McCarty Ranch

QW field parameters 3/28/79 RWU-MAD-JSW

Figure 10b

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WATER RESOURCES DIVISION

Temp = 25°C

Iron = 1 mg/l

sp. cond. = 158

hardness (as CaCO₃) = 435 mg/l

HS = 400 µ/l

SO₄ = < 50 mg/l

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WATER RESOURCES DIVISION

discharge measurements

WATER LEVEL MEASUREMENTS (Field)

Measured by

WAL RWU

Location of Project

6" pipe 3" office in back

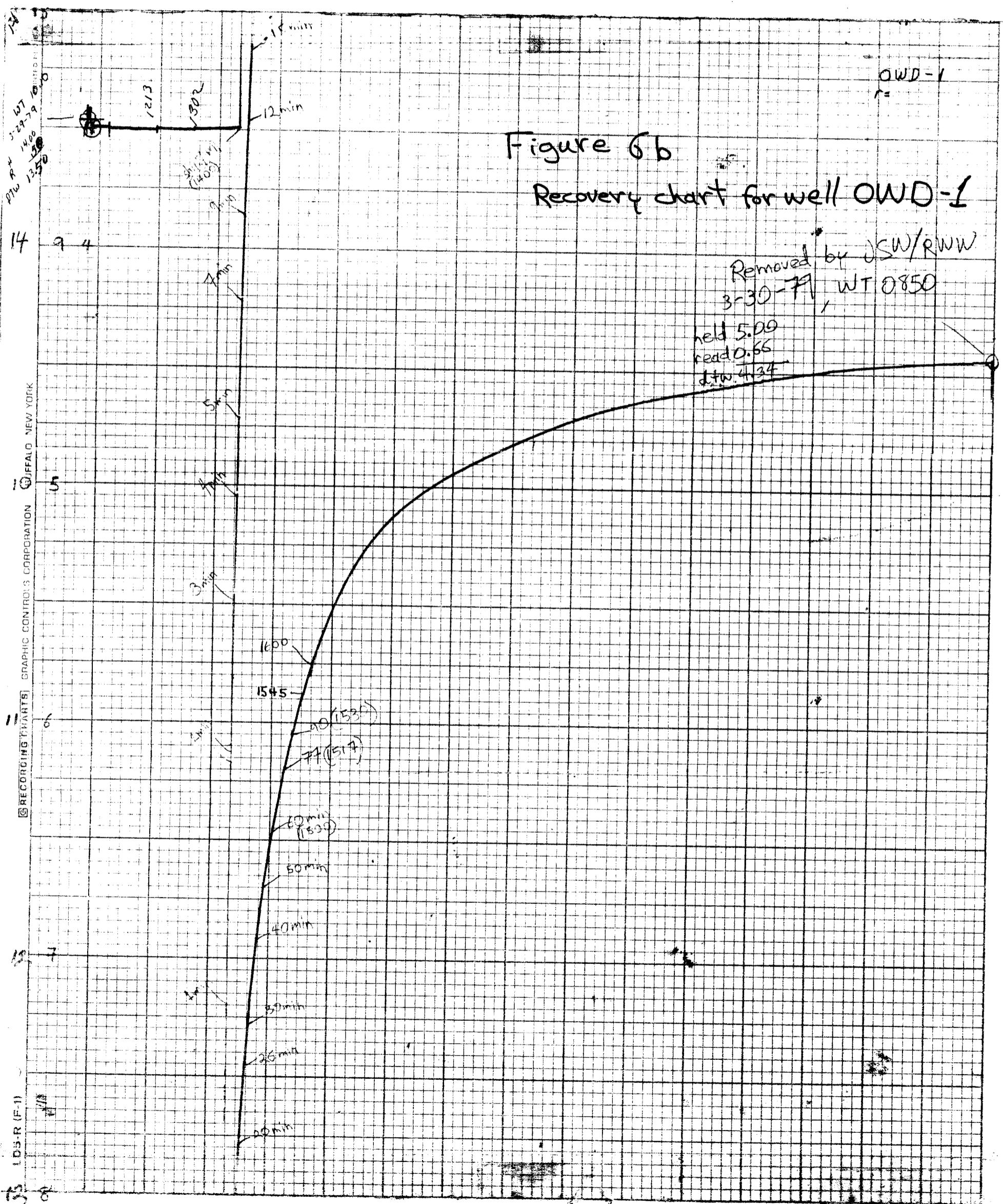
WATER LEVEL MEASUREMENTS (Field)

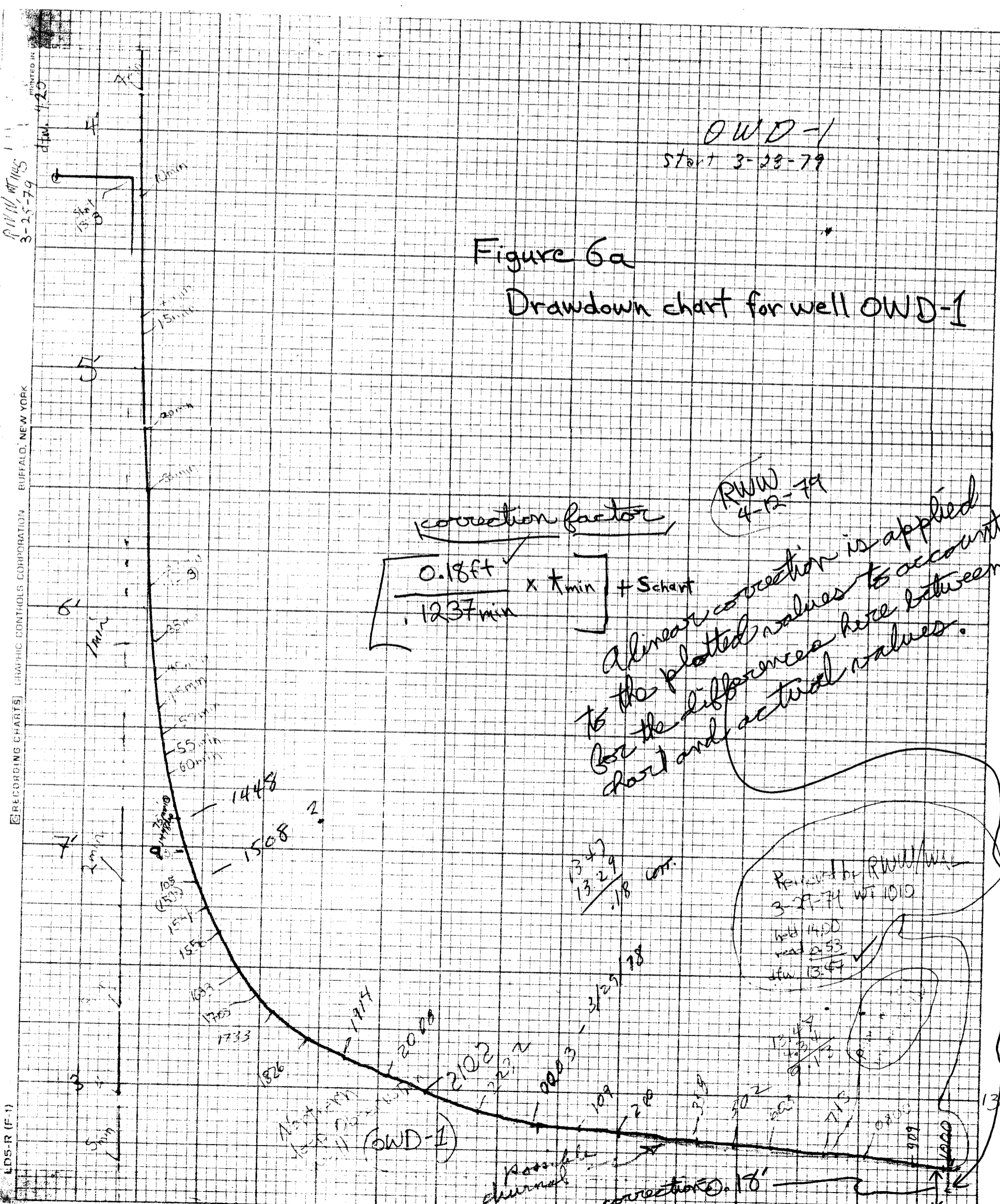
Measured by

Location of Project

DATE	HOUR	WELL NO.	TAPE READING AT—		DEPTH TO WATER	REMARKS
			Meas. point	Water level		
3/28	01330	Start @			15" in	128
	13340			Same	15"	128
	1355				14.5"	126
	1402				15.75"	130
	1425				15.75"	130
	1435				15.50"	129
	1450				15.00"	128
	1505				14.75"	
	1515		up at 50		14.75"	
	1523		down 50		14.50"	
	1538				14.50"	15.75" = 131
	1555				14.50"	15.5" = 130
	1632				14.40"	15.25" = 129
	1700				14.50"	15.00" = 128
	1745				14.25"	14.5" = 126
	1823				14.0"	14.25" = 125
	1919				13.75"	13.5" = 121
	2012				13.75"	
	2040				13.75"	
	2103				13.75"	

DATE	HOUR	WELL NO.	TAPE READING AT—		DEPTH TO WATER	REMARKS
			Meas. point	Water level		
2/23	2238				14.0	✓
2/29/79	0007				13.8	✓
	0102				13.8	✓
	203				13.8	✓
	401				14	✓
	508				13.75	✓
	600				13.75	✓
	712				13.75	✓
	0807				13.75	✓
	925				13.75	✓
	1100				13.75	✓
	1215				13.75	✓
	1304				13.75	✓
	1345				13.75	✓





OWS-2

Figure 8a - Drown-down measurements made on well OWS-2.

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WATER LEVEL MEASUREMENTS (Field) Measured by G.W.H.
Location of Project McCarty Ranch OWS-2

DATE	Minutes HOUR	WELL NO. MIN	TAPE READING AT-		DEPTH TO WATER	WATER LEVEL Ft(MSL)	REMARKS
			Meas. point	Water level			
	1324		6.0	2.30	3.70		
	1330	X	8.0	4.31	3.69		
	1335		8.0	4.30	3.70	0	
1340	3		9.0	5.29	3.71	.01	
1343	4		9.0	5.30	3.70	.0	
1346	5		"	5.31	3.71	+01	
1349	6		"	5.28	3.72	.02	
1352	7		"	5.26	3.74	.04	
1355	8		"	5.26	3.74	.04	
1358	9		"	5.25	3.75	.05	
1401	10			5.25	3.75	.05	
1404							
1407	12			5.23	3.77	.07	
1410	14			5.23	3.77	.07	
1413	17			5.24	3.76	.06	
1416	22			5.20	3.80	.10	
1419	25			5.20	3.80	.10	
1422	25			5.20	3.80	.10	
1425	30			5.18	3.82	.12	
1428	35			5.16	3.84	.14	
1431	45			5.12	3.88	.18	
1434	50			5.11	3.89	.19	
1437	60			5.09	3.91	.21	

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GEOLOGICAL SURVEY
WATER RESOURCES DIVISION

WATER LEVEL MEASUREMENTS (Field) Measured by _____
Location of Project _____

DATE	HOUR	WELL NO.	TAPE READING AT-		DEPTH TO WATER	Ft(MSL)	Remarks
			Meas. point	Water level			
1430	75		9.0	5.06	3.94	.24	
1435	90		9.0	5.02	3.98	.28	
1440	105		9.0	4.99	4.01	.31	
1445	120		9.0	4.96	4.04	.34	
1637			6.0	1.91	4.09	.39	
1700			5.0	.88	4.12	.42	
1711							
1822			5.0	.81	4.19	.49	
1917			5.0	.79	4.21	.51	
2014			5.0	.77	4.23	.53	
21			5.0	.74	4.26	.56	
2336			5.0	.71	4.29	.59	
3/29/79	0003		5.0	.69	4.31	.61	
	0113		5.0	.68	4.32	.62	
	0203		5.0	.66	4.34	.64	
	0401		5.0	.67	4.33	.63	
	0507		5.0	.65	4.35	.65	
	0600		5.0	.66	4.34	.64	
	712		5.0	.65	4.35	.65	
	0805		5.0	0.63	4.37	.67	
	0925		5.0	.64	4.36	.66	
	1005		5.0	.64	4.36	.66	
	1103		5.0	.62	4.38	.68	

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WATER LEVEL MEASUREMENTS (Field) Measured by GWH FOTHERS
Location of Project McCarty Ranch OWS-2

DATE	HOUR	WELL NO.	TAPE READING AT—		DEPTH TO WATER	REMARKS
			Meas. point	Water level		
3/29/79	1214		5.0	.63	4.37	.67
	1304		5.0	.62	4.38	.68
	1340		5.0	.61	4.39	.69
	1359		5.0	.60	4.40	.70
1400	0		5.0	.60	4.40	
	1			.61	4.39	
	2			.61	4.39	
	3			.63	4.37	
	4			.63	4.37	
	5			.63	4.37	
	7			.64	4.36	
	9			.64	4.36	
	12			.66	4.34	
	15			.67	4.33	
	20			.69	4.31	
	25			.72	4.28	
	30			.73	4.27	
	40			.75	4.25	
	50			.78	4.22	
	60			.82	4.18	
	79			.85	4.15	
1605				.92	4.08	

Figure 8b - Recovery measurements made on well OWS-2.

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WATER LEVEL MEASUREMENTS (Field) Measured by _____
Location of Project _____

DATE	HOUR	WELL NO.	TAPE READING AT—		DEPTH TO WATER	REMARKS
			Meas. point	Water level		
3-30-79	1010		4.00	0.34	3.66	

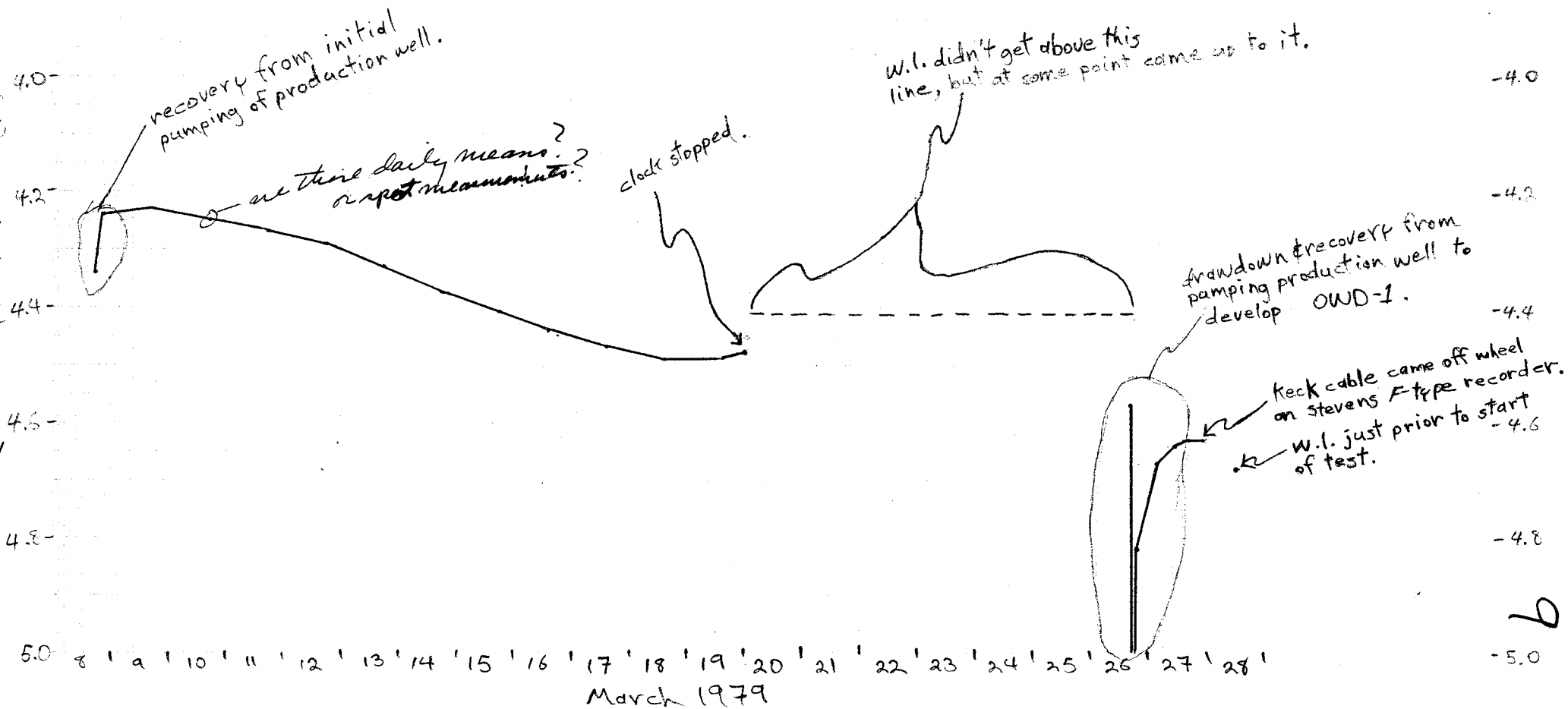
19

RWW 4-11-79

Figure 4a

Background water level (OWD-2)
(Macarty Ranch test 3-79)

any possibility that other wells were pumping in the area?



OWD-3

Macarty Ranch - St. Lucie Co.

OWD-3 - 6" well, depth = 120', r = 1140' south of production well

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m.p. = top of casing

WATER LEVEL MEASUREMENTS (Field)

Measured by JSW-UXL-RWC

Location of Project _____

DATE	HOUR	WELL NO.	TAPE READING AT--		DEPTH TO WATER	M.P. EIV.	W.L. EIV.
			Meas. point	Water level			
3-27-49	0715				4.01		drawdown (ft)
	0845		4.00	2.23	3.97		
	1012		5.0	1.97	4.03		
	1120				4.02		
	1400		5.0	1.0	4.0		↑
	1401				4.0	1.12	
	1402				4.0		
	1403				4.0		
	1404				4.0		
	1405				4.0		
	1406				4.0		
	1407				4.0		
	1408				4.0		
	1409				4.0		
	1410				4.0		
	1412				4.0	1.12	
	1415				4.0	1.12	
	1420		5.0	1.01	3.99	1.11	
	1425				3.99	1.11	
	1430		5.0	1.02	3.98	1.10	
	1435		5.0	1.02	3.98	1.10	
	1440		5.0	1.05	3.95	1.07	

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WATER RESOURCES DIVISION

WATER LEVEL MEASUREMENTS (Field)

Measured by _____

Location of Project _____

DATE	HOUR	WELL NO.	TAPE READING AT--		DEPTH TO WATER	M.P. EIV.	W.L. EIV.
			Meas. point	Water level			
	1445		5.0	1.08	3.92		drawdown (ft)
	1450		5.0	1.09	3.91	1.04	
	1455			1.11	3.89	1.03	
	1500			1.13	3.87	1.01	
	1510			1.16	3.84	0.99	
	1520			1.18	3.82	0.96	
	1530		5.0	1.25	3.75	0.94	
	1545		5.0	1.30	3.70	0.87	
	1600		5.0	1.33	3.67	0.82	
						0.79	
3-30-49	0910		3.10	0.22	2.88	0	

Figure 9

Drawdown and Recovery measurements for well OWD-3.

20

OWS-1
start 3-28-79
11 ft deep

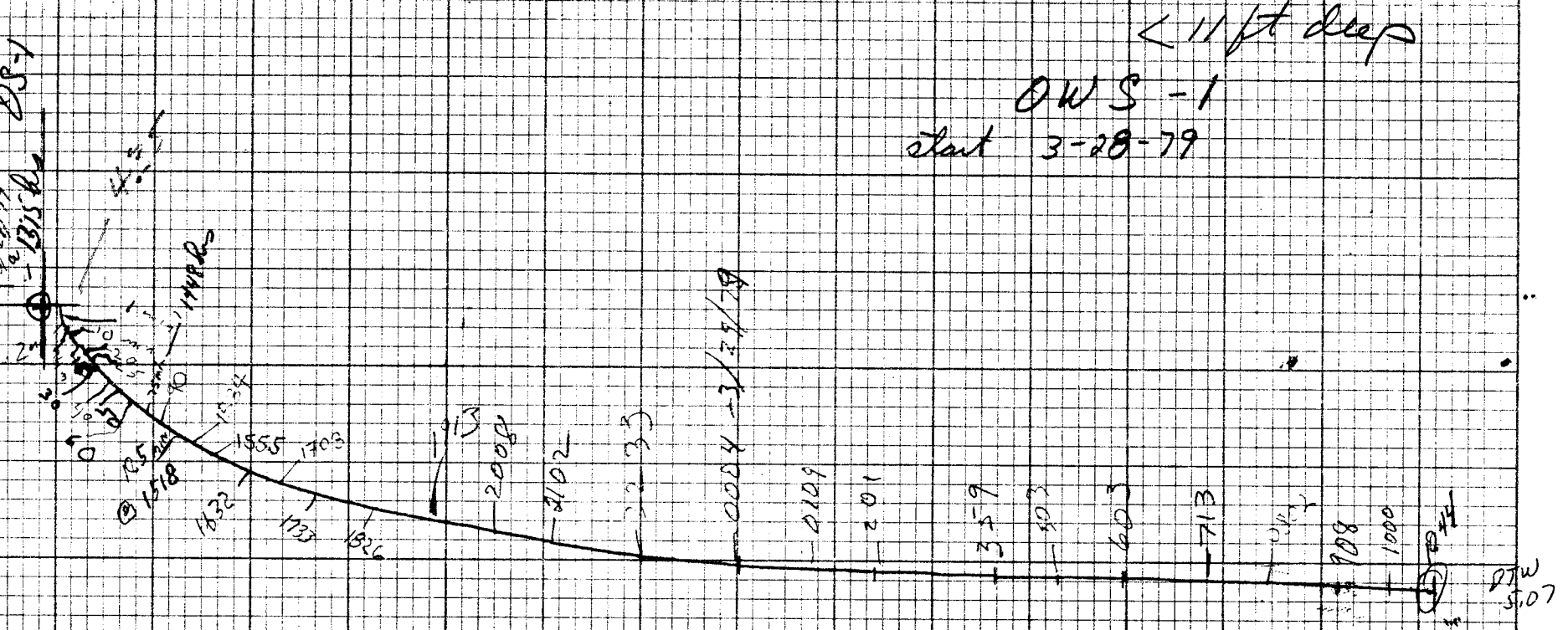


Figure 7a

Drawdown chart for well OWS-1

Loop
PUMP IN
WATER
3-29-77
PT 105.0

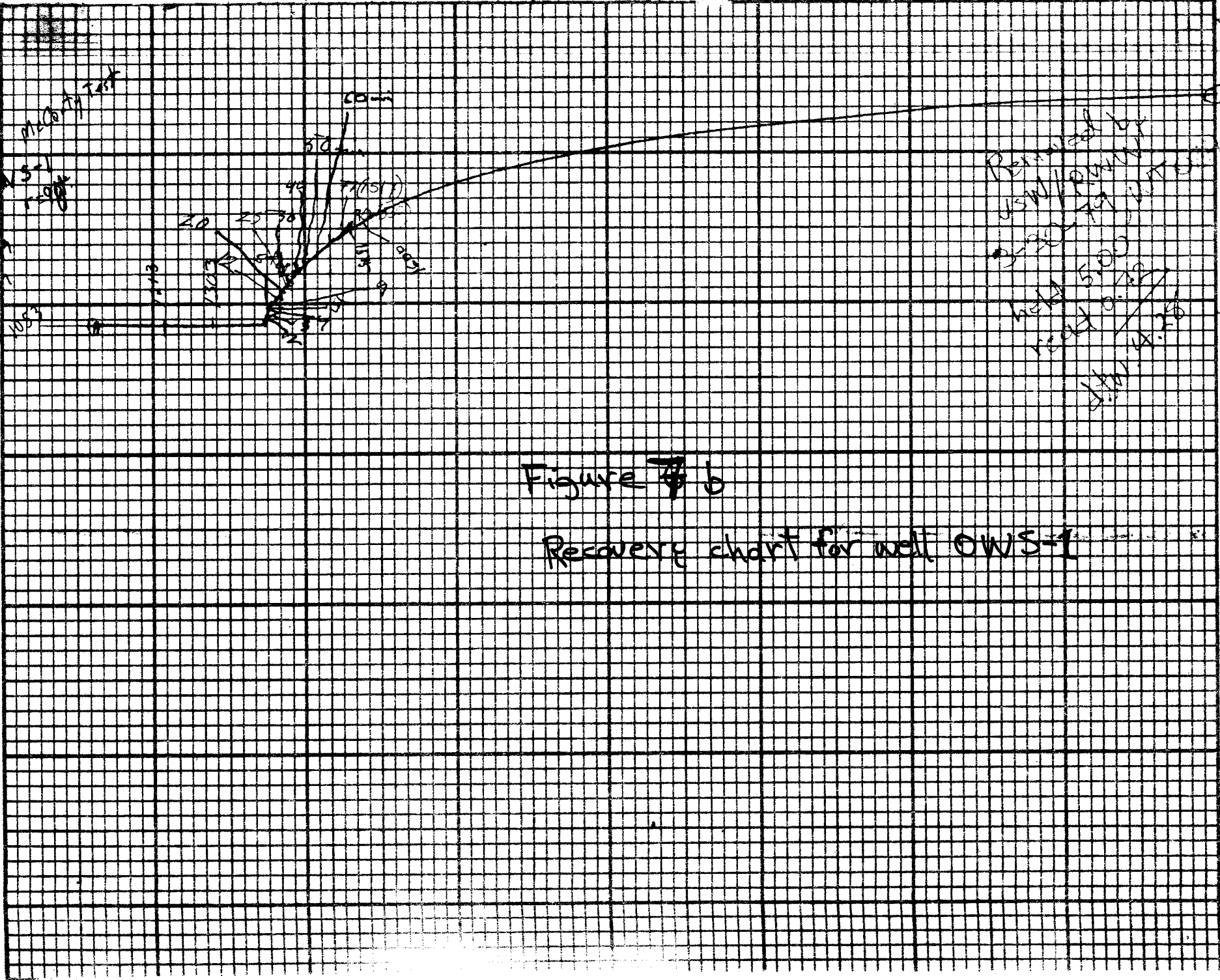


Figure 7 b

Recovery chart for well OWS-1

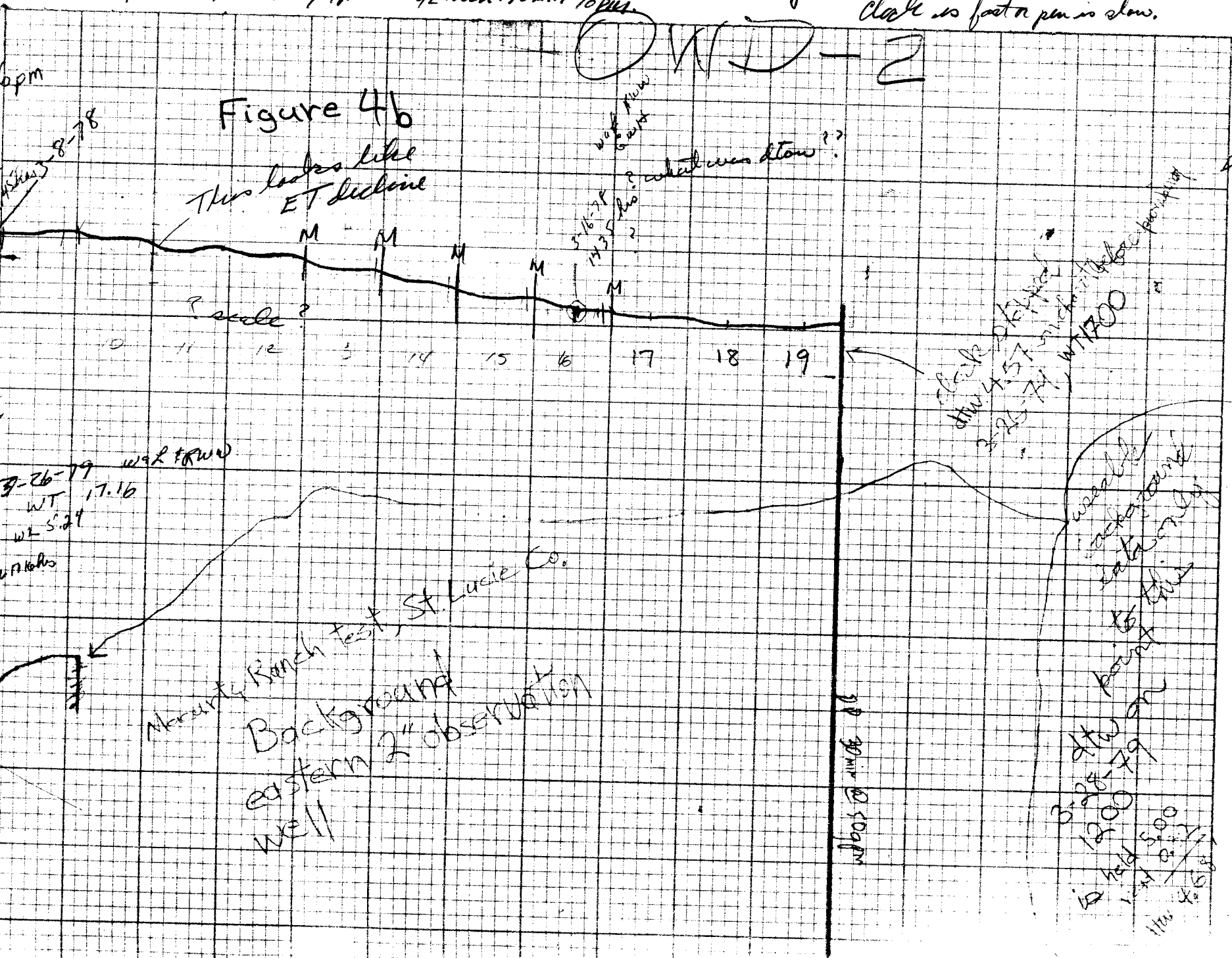
atmospheric tide is semidiurnal.
 u/L max. 4am & 4pm u/L min. 10AM 10PM

slow days - looks as though
 clock is fast or pen is slow.

OWD-2

Figure 4b

This looks like
 ET decline



6pm

8-78

? scale?

what was slow??

5-16-78
 1435

DTW
 4/4.0

3-26-79
 WT 17.16
 WT 5.24

Merritts Ranch test, St. Lucie Co.
 Background
 eastern 2" observation
 well

clock checked
 time 4:57
 3-25-79
 WT 17.00

5.0

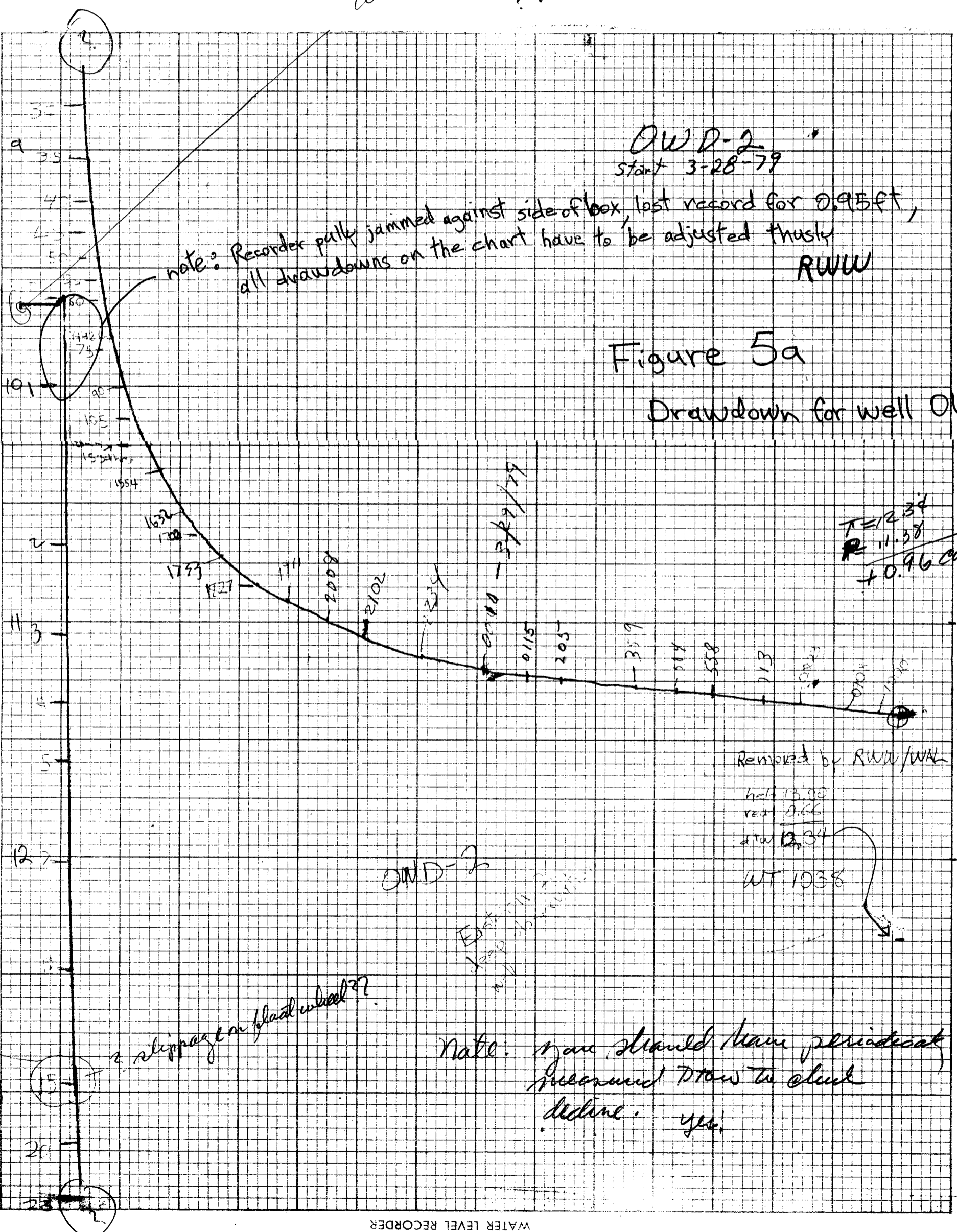
water
 background
 12:00
 3-25-79
 is held 5.00
 WT 4.6

WT 3.0 @ 5:00pm

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RECORDING CHARTS
LDS-R (F-1)

98,750

what was beginning DTOW??
? 4.67?



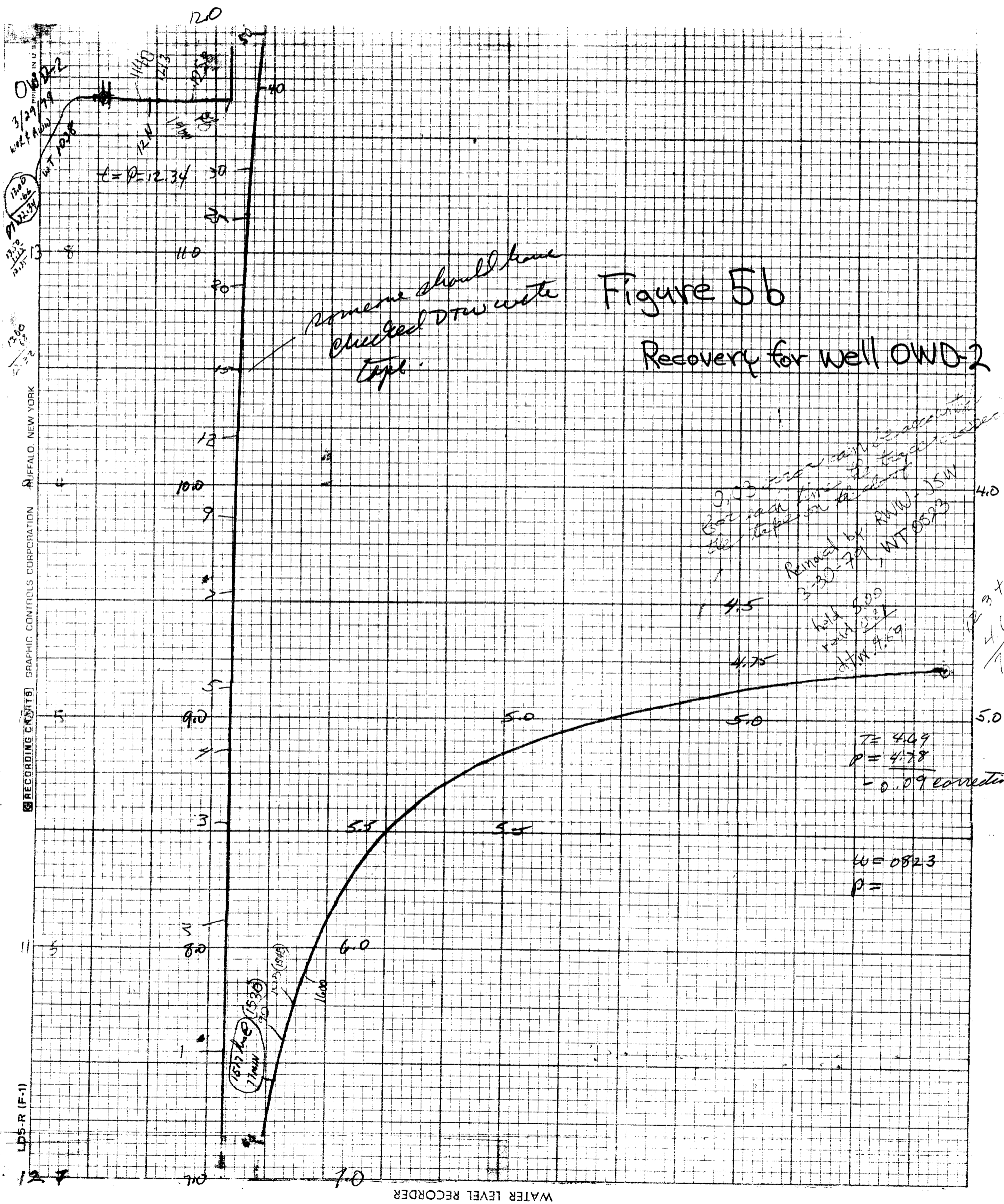


Figure 5b
Recovery for well OWD-2

someone should have
checked DTW with
tape.

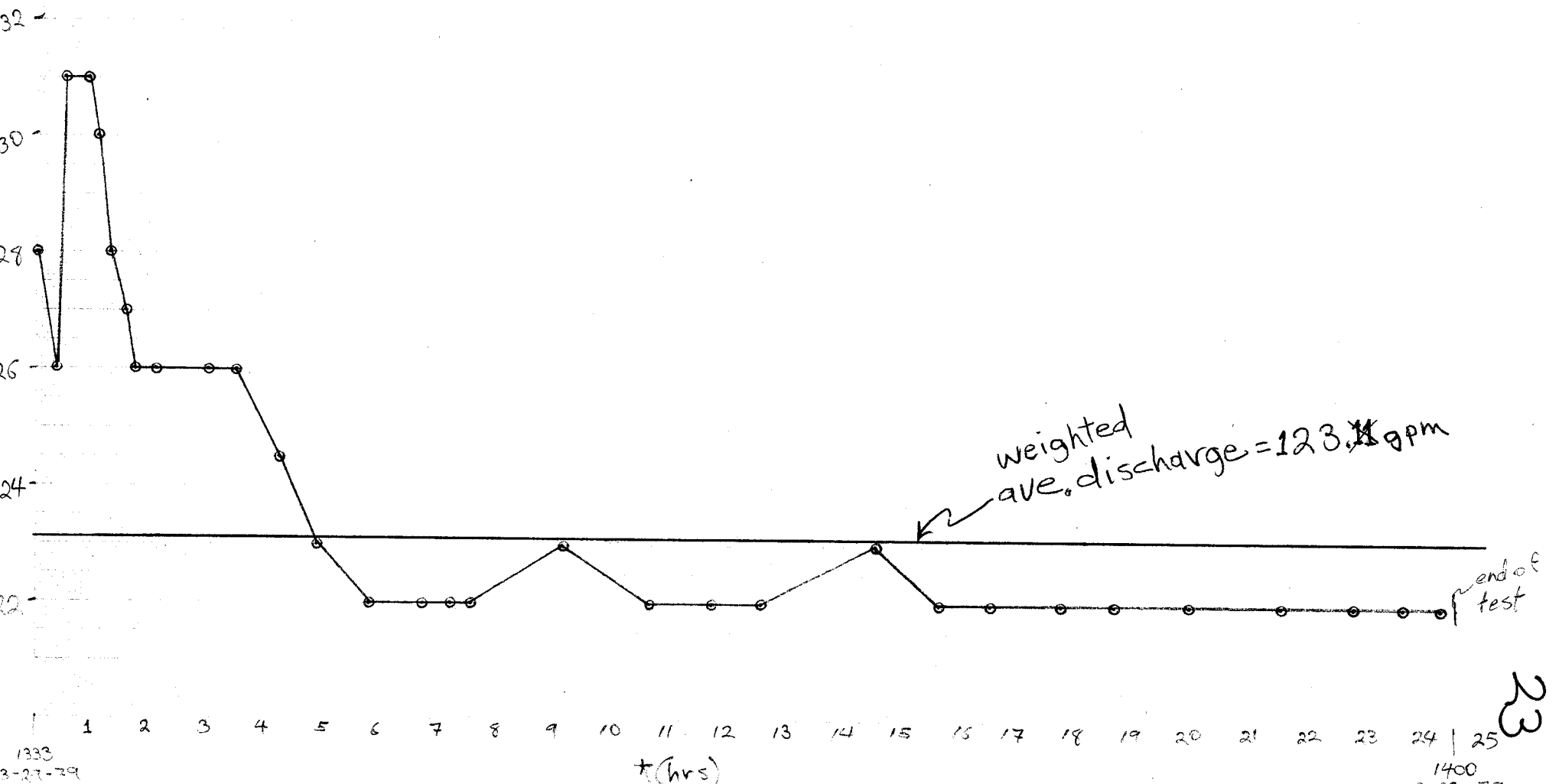
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T = 4.69
P = 4.78
- 0.09 correction

W = 0823
P =

RWW 4-11-79

Figure 10a Discharge vs. time
(Macarty Ranch test 3-79)



Discharge Measurements

McCarty Ranch

QW field parameters 3/28/79 RWV-MAD-JSW

Figure 10b

discharge measurements

9-194
November 1949

UNITED STATES
DEPARTMENT OF THE INTERIOR
GEOLOGICAL SURVEY
WATER RESOURCES DIVISION

Temp = 25°C

hardness (as CaCO₃) = 435 mg/l

Iron = 1 mg/l

9-194
November 1949

UNITED STATES
DEPARTMENT OF THE INTERIOR
GEOLOGICAL SURVEY
WATER RESOURCES DIVISION

sp. cont. = 158

HS = 400 u/l

SO₄ = < 50 mg/l

WATER LEVEL MEASUREMENTS (Field)

Measured by W.R. / RWV

Location of Project 6" pipe 3" office inside

DATE	HOUR	WELL NO.	TAPE READING AT—		DEPTH TO WATER	REMARKS
			Meas. point	Water level		
3/28	1330	Blattal @			15" in	128
	1334			Sand	15"	128
	1355				14.5"	126
	1402				15.75	130
	1425				15.75	130
	1435				15.50	129
	1450				15.00	128
	1505				14.75	
	1515		up at 50		14.75	
	1523		Down 50		14.50	
	1538				14.50	15.75" = 131
	1555				14.50	15.5 = 130
	1632				14.40	15.25 = 129
	1700				14.50	15.00 = 128
	1745				14.25	14.5 = 126
	1823				14.0	14.25 = 125
	1919				13.75	13.5 = 121
	2012				13.75	
	2040				13.75	
	2103				13.75	

WATER LEVEL MEASUREMENTS (Field)

Measured by _____

Location of Project _____

DATE	HOUR	WELL NO.	TAPE READING AT—		DEPTH TO WATER	REMARKS
			Meas. point	Water level		
2/23	2238				14.0	✓
2/29/79	0007				13.8	✓
	0102				13.8	✓
	203				13.8	✓
	401				14	✓
	508				13.75	✓
	600				13.75	✓
	712				13.75	✓
	0807				13.75	✓
	925				13.75	✓
	1100				13.75	✓
	1215				13.75	✓
	1304				13.75	✓
	1345				13.75	✓