

UNITED STATES  
DEPARTMENT OF THE INTERIOR  
GEOLOGICAL SURVEY

HYDROGEOLOGIC DATA FOR THE SOUTH CROSS BAYOU SUBSURFACE-  
INJECTION TEST SITE, PINELLAS COUNTY, FLORIDA

By John J. Hickey

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Open-File Report 78-575

Prepared in cooperation with  
PINELLAS COUNTY, FLORIDA



Tallahassee, Florida

1979

UNITED STATES DEPARTMENT OF THE INTERIOR

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## CONVERSION FACTORS

For use of those readers who may prefer to use metric units rather than U.S. inch-pound units, the conversion factors for the terms used in this report are listed below:

| <u>U.S. inch-pound units</u>                                | <u>Multiply by</u>     | <u>To obtain metric units</u>                  |
|---|------------------------|--|
| inch (in)   | $2.540 \times 10^1$    | millimeter (mm)                                |
| inch squared ( $in^2$ )                                     | 6.452                  | centimeter squared ( $cm^2$ )                  |
| foot (ft)   | $3.048 \times 10^{-1}$ | meter (m)                                      |
| mile (mi)   | 1.609                  | kilometer (km)                                 |
| gallon (gal)  | 3.785                  | liter (L)                                      |
| gallon per minute<br>(gal/min)                              | $3.785 \times 10^{-3}$ | cubic meter ( $m^3$ )                          |
| gallon per minute<br>(gal/min)                              | $6.309 \times 10^{-1}$ | liter per second (L/s)                         |
| foot squared per day<br>(ft <sup>2</sup> /d)                | $9.290 \times 10^{-2}$ | meter squared per day<br>(m <sup>2</sup> /d)   |
| pound per square inch<br>(lb/in <sup>2</sup> )              | $6.894 \times 10^3$    | Newton per square<br>meter (N/m <sup>2</sup> ) |
| pound per square foot<br>(lb/ft <sup>2</sup> )              | $4.788 \times 10^1$    | Newton per square<br>meter (N/m <sup>2</sup> ) |
| foot per day (ft/d)   | $3.048 \times 10^1$    | meter per day (m/d)                            |
| gallon per minute per<br>foot of drawdown<br>[(gal/min)/ft] | $2.070 \times 10^1$    | liter per second per<br>meter [(L/s)/m]        |
| microsecond per foot<br>(ms/ft)                             | 3.280                  | microsecond per meter<br>(ms/m)                |
| $^{\circ}F = 9/5(^{\circ}C) + 32$                           |                        | $^{\circ}C = 5/9(^{\circ}F - 32)$              |

HYDROGEOLOGIC DATA FOR THE SOUTH CROSS BAYOU SUBSURFACE-  
INJECTION TEST SITE, PINELLAS COUNTY, FLORIDA

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ABSTRACT

One exploratory hole, a test injection well, and nine monitor wells were constructed at the South Cross Bayou test-injection site between January 1973 and October 1975. The exploratory hole was drilled to a depth of 3,280 feet below land surface. The test injection well, 856 feet distant from the exploratory hole, is uncased from 961 to 1,080 feet. Four of the monitor wells were constructed within the exploratory hole and range in depth from 520 to 1,224 feet and two of the monitor wells, within 140 feet of the exploratory hole, are 35 and 94 feet deep. The remaining three monitor wells are within 106 feet of the test injection well and range in depth from 250 to 800 feet.

At the test site, the first 125 feet below land surface is predominantly limestone and clay; from 125 to 3,280 feet it is mostly limestone and dolomite. Gypsum is also present below 1,260 feet.

During the 33-hour withdrawal test in which well A1 was pumped at a rate of 5,000 gallons per minute, the water level in well B2, uncorrected for environmental factors and 856 feet from the pumped well, declined 0.9 foot, from 1.5 to 2.4 feet below mean sea level. During the 96-hour injection test, injecting at an average rate of 4,350 gallons per minute, uncorrected water levels in well B2 rose 0.4 foot, from 2.0 feet to 1.6 feet below mean sea level. Well B2 is open to the injection test zone.

Water containing 19,000 milligrams per liter of chloride is estimated to be from a depth of about 370 feet below land surface. After completion of the injection test, the chloride concentration in water from well A2 decreased from 19,000 to 8,800 milligrams per liter. Chloride concentration in water from 16 additional wells near the test site and 25 to 302 feet deep, ranged from about 10 to 290 milligrams per liter.

## INTRODUCTION

Pinellas County, in the Tampa Bay area, is experiencing a rapid population growth with an accompanying increase in environmental regulation. Limits have been placed on ground-water withdrawals, and standards regulating the quality of sewage treatment plant effluent that can be discharged to the Gulf of Mexico and Tampa Bay have been imposed. These limits and standards have resulted in a marked interest by Pinellas County in investigating subsurface storage of waste-treatment plant effluent. The benefits Pinellas County expects to gain are a reduction in the cost of their current waste-treatment plant expansion program and the creation of a potential water resource for future nonpotable reuse.

The U.S. Geological Survey, in cooperation with Pinellas County, is investigating storage of waste-treatment plant effluent in permeable saline water zones within the carbonate rocks that underlie the Pinellas County South Cross Bayou waste treatment plant (fig. 1). The U.S. Geological Survey's principal goal in this investigation is to better understand the hydrodynamic and chemical behavior of the stored water. This data for the South Cross Bayou test site will assist in that understanding.

### Purpose and Scope

This report presents the hydrogeologic data collected during the drilling of wells and withdrawal and injection testing at the South Cross Bayou site. These data include lithologic descriptions and laboratory analyses of drill cuttings and cores, results of withdrawal and injection tests, hydrographs, geophysical logs, and chemical analyses.

Data were collected at the test site to assist in the evaluation of the following objectives: (1) Determine if transmissive zones exist in the subsurface which can accept large volumes of waste effluent; (2) determine the water-quality profile at the site; (3) evaluate local effects of well injection on freshwater; and (4) design a long-term monitoring program. These and other determinations will be given in a subsequent interpretive report.

To provide data for these objectives, one exploratory hole and 10 wells were constructed; withdrawal and injection tests were performed; and water from the wells at the test site and from selected wells near the site were sampled and analyzed.

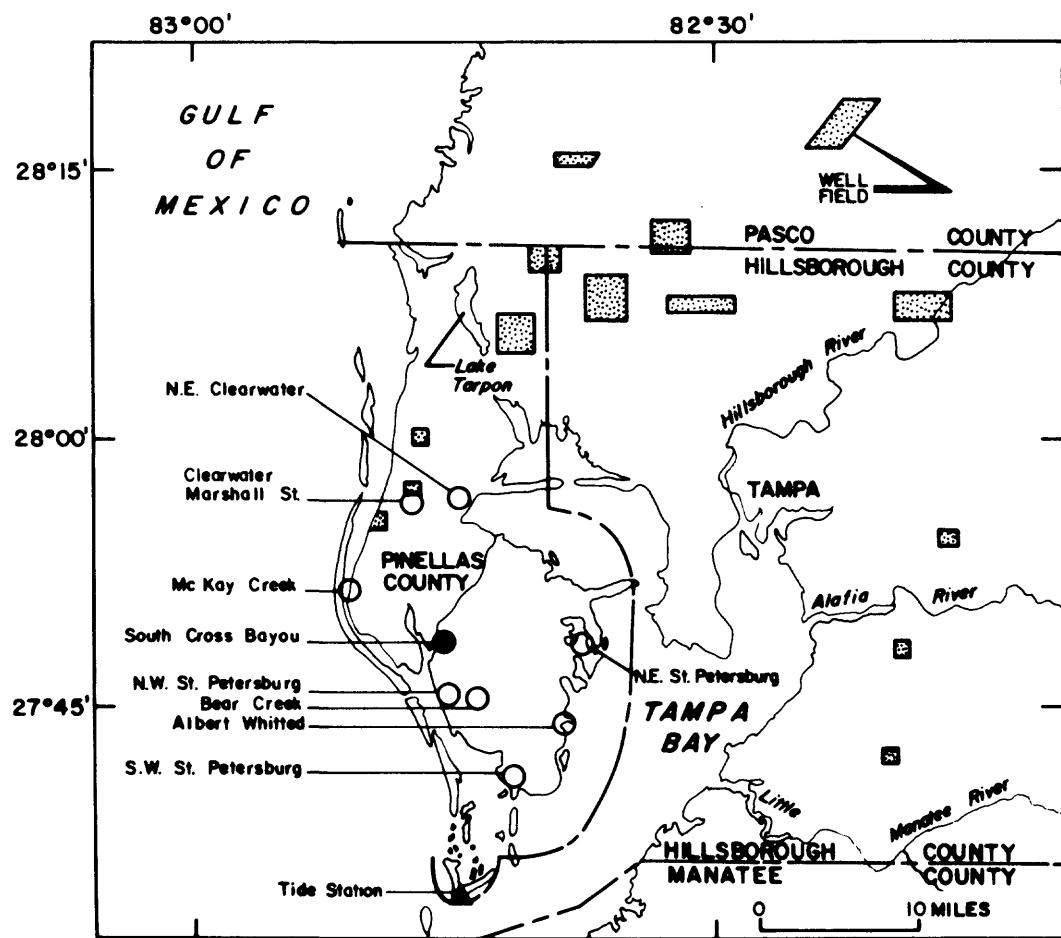


Figure 1.--Location of the South Cross Bayou test injection site, other proposed injection sites, and Tampa Bay area municipal well fields.

### Previous Investigations

The geology and hydrology of Pinellas County have been the subjects of several investigations. Chen (1965) described the lithology penetrated from 500 to 5,000 ft below land surface by an oil test hole in Pinellas County as part of his regional stratigraphic analysis of the Paleocene and Eocene rocks of Florida. Heath and Smith (1954) and Black, Crow and Eidsness (1970) analyzed the upper carbonate rock section to depths seldom exceeding 400 ft, mostly from a water-supply point of view. Black, Crow and Eidsness (1974) investigated the potential for storing stormwater runoff and recovering it from saline zones within the carbonate rocks for the city of St. Petersburg and the Florida Department of Natural Resources. As part of their investigation, a test hole was drilled to a depth of 3,504 ft. They concluded from their investigation that most of the transmissive zones capable of accepting large volumes of stormwater runoff were less than 1,270 ft below land surface. In addition to other tests, two injection tests, each lasting 1 day, were run on a zone between 1,180 and 1,270 ft. Black, Crow and Eidsness (1974) reported a transmissibility of 107,000  $\text{ft}^2/\text{d}$  for the test-injection zone. Greenleaf and Telesca (1975) described the well construction at the South Cross Bayou test-injection site. Rosenschein and Hickey (1977) discussed the vertical distribution of permeable zones within the carbonate strata underlying the Pinellas peninsula and their potential use for storing treated sewage effluent and stormwater. Hickey (1977) presented hydrogeologic data collected at the McKay Creek injection test site.

### Regional Hydrogeologic Setting

The Tampa Bay area, including the South Cross Bayou test site, is underlain by carbonate strata to a depth of about 10,000 ft below land surface (Applin, 1951), with a surficial cover of sand, marl, and clay. The upper 1,300 ft of the carbonate strata has a number of very permeable zones, which together, constitute one of the most productive aquifers in the world--the Floridan aquifer (Parker, 1955). The transmissivity of the aquifer where it is tapped for water supplies--east and north of Tampa Bay--is estimated to range from about 32,000  $\text{ft}^2/\text{d}$  to more than 270,000  $\text{ft}^2/\text{d}$  (Rosenschein and Hickey, 1977). The permeable zones within the aquifer are thought to be separated by carbonate strata of relatively low permeability (Rosenschein and Hickey, 1977). In general, the flow of portable ground water in the Floridan aquifer is westward toward the Gulf of Mexico and Tampa Bay.

The upper part of the carbonate strata in the Tampa Bay area generally is overlain by less than 200 ft of surficial sand, marl, and clay. The clay commonly forms the basal strata of these surficial deposits and, in northwest Hillsborough County, is in part a weathered residue of the underlying carbonate rock. There, according to Sinclair (1974, p. 24-26), the clay has a vertical hydraulic conductivity of less than 0.003  $\text{ft}/\text{d}$ .

The surficial sand in the study area is less than 35 ft thick. During dry weather it is generally saturated to within 5 to 10 ft of the land surface. During wet weather, the water table in the sand is at or near land surface. In the northwest Hillsborough County area, the sand has a horizontal hydraulic conductivity of about 13 ft/d and a vertical hydraulic conductivity ranging from 0.36 to 13 ft/d (Sinclair, 1974, p. 13).

Summary of South Cross Bayou Test Site Data

|  |  |
|--|--|
| Depth of exploratory hole                | 3,280 ft   |
| Injection test well                      | cased to 961 ft; open hole to 1,080 ft   |
| Observation wells                        | 1 within injection zone<br>1 below injection zone<br>7 above injection zone  |
| Lithology                                | 0 to 125 ft, sand, clay and limestone;<br>125 to 3,280 ft, limestone and dolomite;<br>below 1,260 ft, gypsum is also present                           |
| Cored intervals                          | 670 to 719 ft<br>910 to 920 ft   |
| Vertical intrinsic permeability of cores | $2.37 \times 10^{-10}$ to $6.12 \times 10^{-10}$ cm <sup>2</sup>   |
| Effective porosity of cores              | 0.1 to 30 percent  |
| Compressibility of cores                 | $3.1 \times 10^{-7}$ to $1.6 \times 10^{-6}$ in <sup>2</sup> /lb   |
| Hydraulic tests                          | 1 withdrawal test at 5,000 gal/min<br>1 injection test at 4,350 gal/min  |
| Chloride concentrations                  | 31 to 35 ft, 25 mg/L;<br>90 to 94 ft, 52 mg/L;<br>200 to 250 ft, 450 mg/L;<br>370 to 2,100 ft, 1,900 mg/L;<br>2,100 to 3,280 ft, 25,000 to 31,000 mg/L |

## WELL CONSTRUCTION

One exploratory hole, a test injection well, and nine observation wells were drilled between January 1973 and October 1975 at the South Cross Bayou test site (table 1). The exploratory hole and the test injection well are 856 ft apart. Of the nine observation wells, four are within the exploratory hole and three are within 140 ft of it. All three remaining observation wells are within 106 ft of the test injection well. Greenleaf and Telesca (1975) describe in detail the construction history of the wells.

### Exploratory Hole

An exploratory hole (well E1) was drilled to a depth of 3,280 ft below land surface for provisional identification of permeable and semi-permeable strata at the South Cross Bayou test site. Location of this well and other wells at the site are shown on figure 2. Conventional and air-reverse rotary drilling methods were used to drill well E1. The upper 450 ft of hole was drilled with conventional rotary mud circulation because experience indicated that this section of carbonates had the potential for collapse when drilled with the air-reverse method. After placing a 16-in casing to 374 ft and cementing the annulus to land surface, drilling continued to 2,176 ft using the air-reverse method. An 8-in casing was installed to 1,863 ft and cemented back to 1,620 ft; well E1 was then drilled to 3,280 ft.

### Observation Wells in the Exploratory Hole

Four observation wells (B1, B2, B3, and B4) were constructed in the exploratory hole (well E1) from 463 ft to 1,224 ft below land surface (fig. 3). The exploratory hole was plugged back with gravel and a cap of cement from 3,280 ft to 1,600 ft before these wells were constructed. Well B1 has a 2-in casing attached to a packer placed at 1,150 ft and monitors a perforated interval in the 8-in casing from 1,210 to 1,224 ft. Well B2 has an 8-in casing and monitors a perforated interval in the 8-in casing above the packer open to the interval from 1,025 to 1,055 ft. Wells B3 and B4 have 2-in casings and are screened and gravel packed from 780 to 815 ft and 463 to 520 ft. All of the wells are separated by cement in the annulus of the 8-in casing. Figure 3 and table 1 show the construction of these wells.

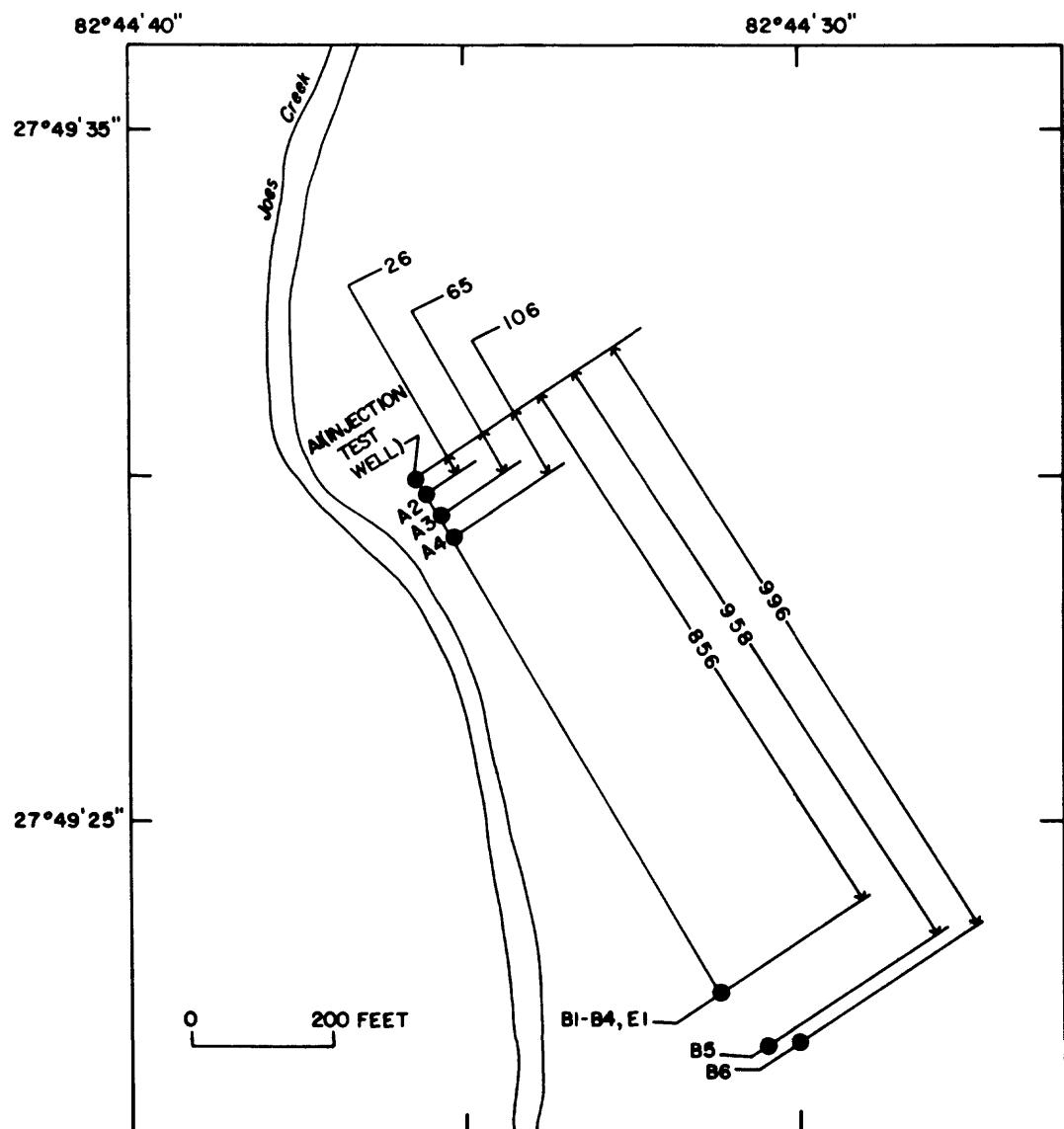


Figure 2.--Exploratory hole and wells at the test site.

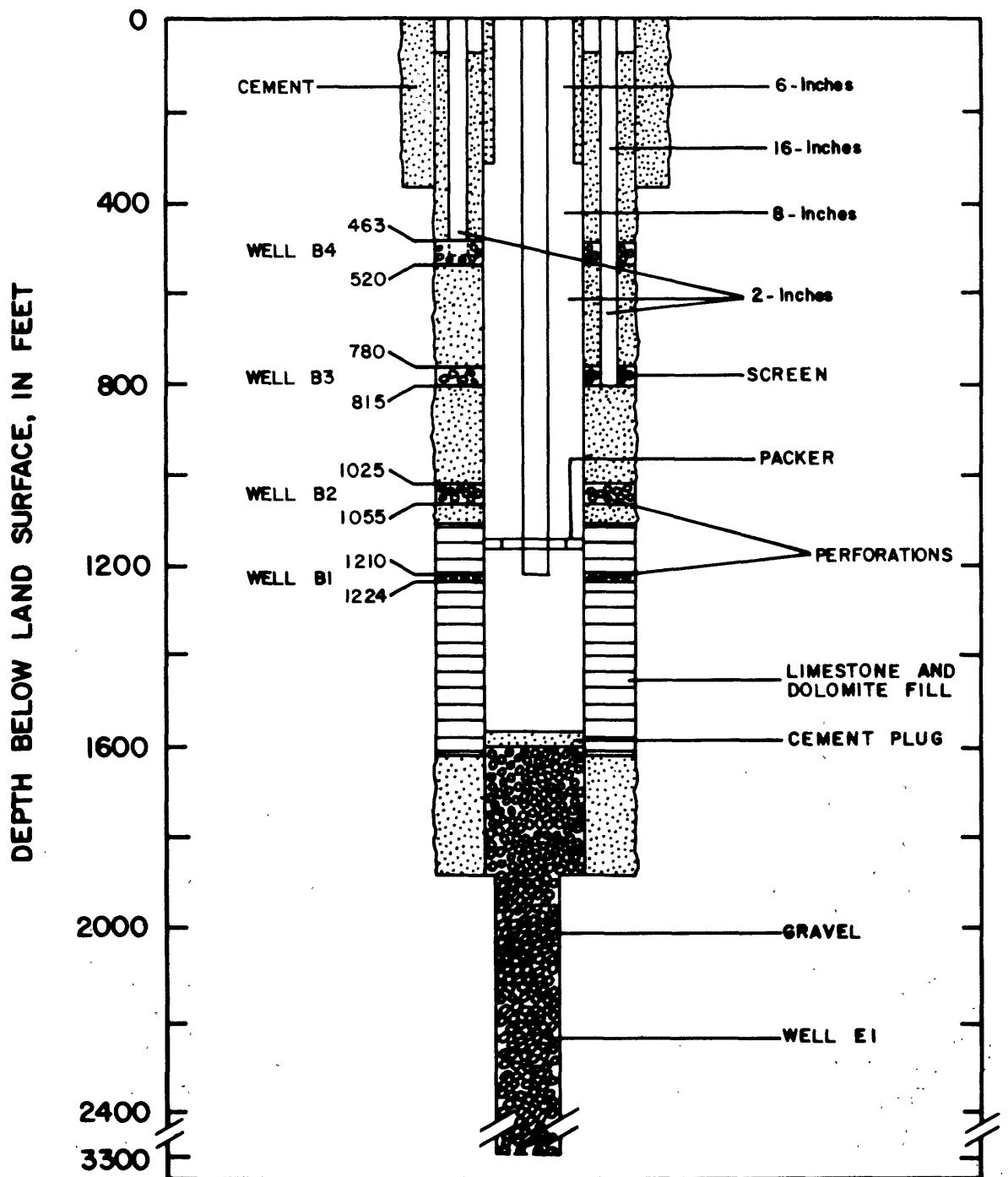


Figure 3.--Construction of wells B1, B2, B3, B4, and El.

### Observation Wells near the Exploratory Hole

The two observation wells, B5 and B6 (fig. 4), were constructed near the exploratory hole. Well B5 is 102 ft from the exploratory hole (fig. 2) and has a 2-in casing and a well point set from 90 to 94 ft. Well B6 is 140 ft from the exploratory hole (fig. 2) and has a 2-in casing and a well point set from 31 to 35 ft.

### Test Injection Well and Nearby Observation Wells

The test injection well (well A1 on fig. 5) is 856 ft distant from wells B1-B4 (fig. 3). A 36-in casing was set at 380 ft and the annulus cemented back to land surface. Then, a 24-in casing was set at 961 ft and the annulus cemented back to 500 ft. The well is an open hole from 961 to 1,080 ft.

The injection well was drilled with conventional rotary mud circulation from land surface to 988 ft. Mud circulation was lost between 762 and 802 ft. This interval was cemented and drilling continued with mud. The mud level in A1 dropped at the depths 903, 945, 947, and 960 ft but immediately recovered. Mud circulation was again lost between 975 and 988 ft.

Cores were taken in two strata during the drilling of well A1. Descriptions and laboratory analyses of these cores are presented later in this report.

Observation wells, A2, A3, and A4 (fig. 2), are 26 ft, 65 ft, and 106 ft from well A1, the injection test well. They have 6-in casings which are cemented to land surface. A2 is open from 746 to 800 ft, A3 from 473 to 521 ft, and A4 from 200 to 250 ft. Figure 5 shows the construction of these wells.

### HYDROGEOLOGIC DATA

Hydrogeologic data collected at the South Cross Bayou injection test site include descriptions and laboratory analyses of drill cuttings and cores, withdrawal and injection test results, water-level hydrographs, geophysical logs, and water-quality analyses.

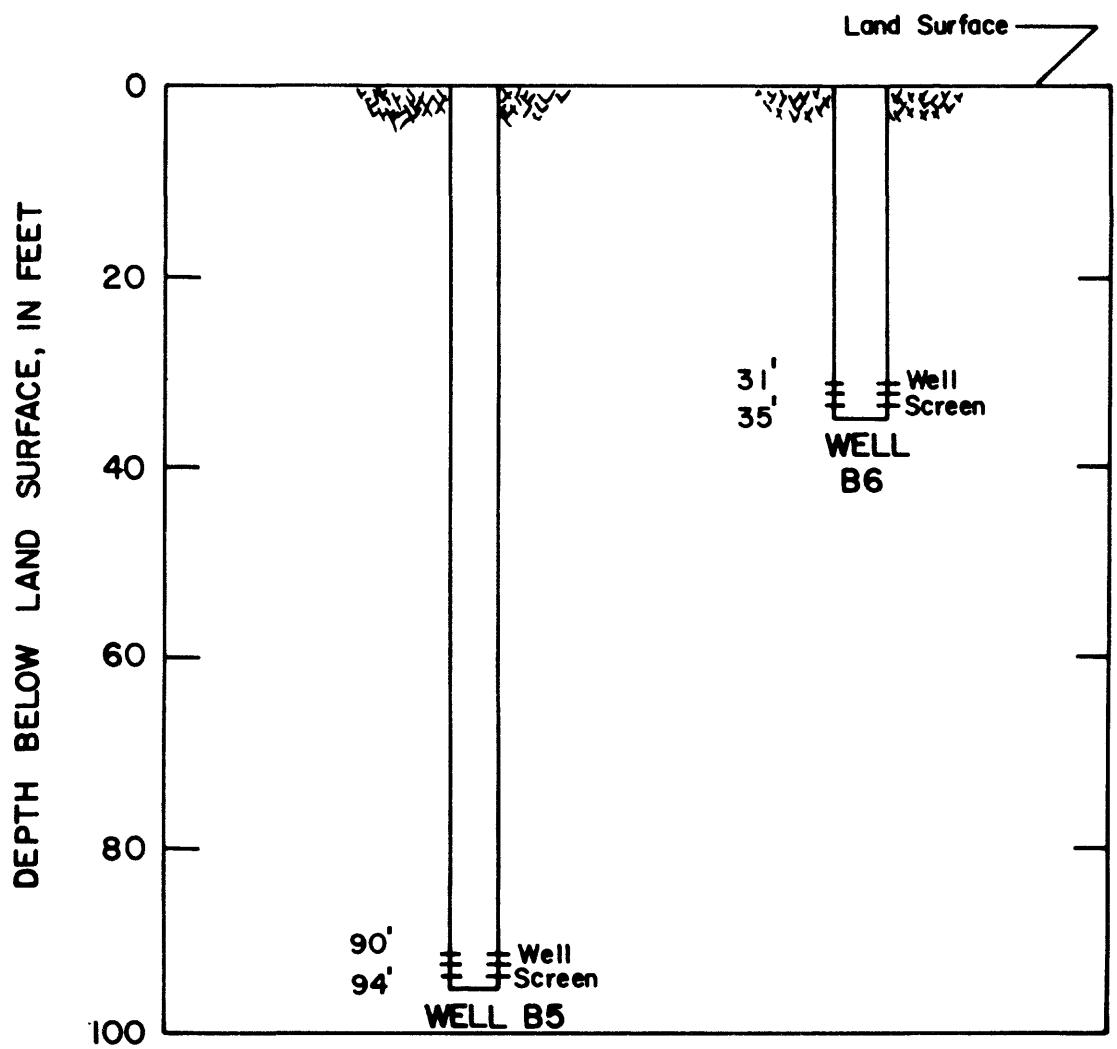


Figure 4.--Construction of wells B5 and B6.

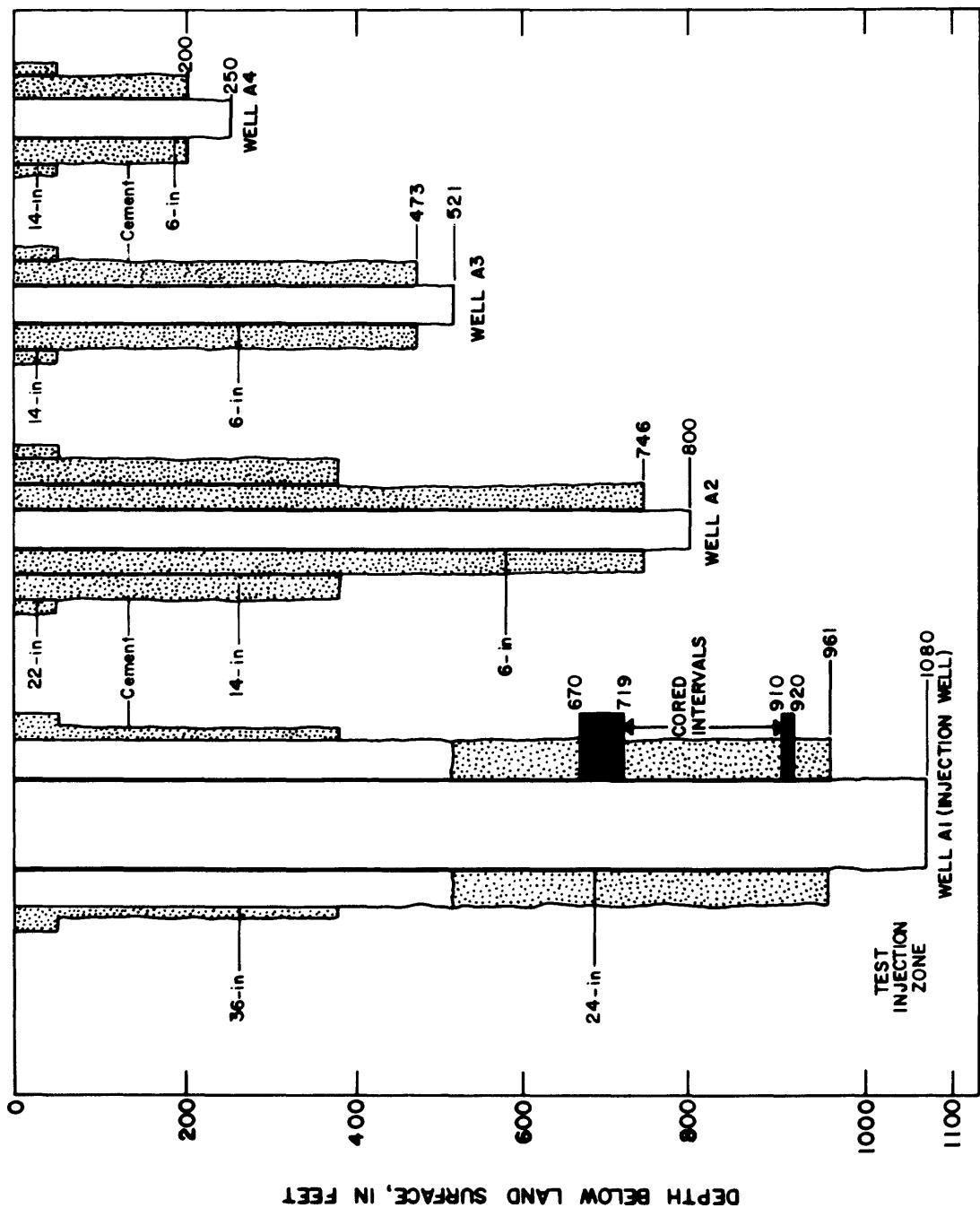


Figure 5.--Construction of wells A1, A2, A3, and A4.

## Drill Cuttings and Cores

Drill cuttings were collected every 10 ft from each hole drilled at the South Cross Bayou site. These cuttings were sent to the Florida State Bureau of Geology in Tallahassee, Florida, as required by state law. Descriptions of the cuttings from well El are given in table 2. A graphic lithologic log of well El and depths at which cores were obtained from well Al is shown in figure 6. The mineralogy of drill cuttings and cores from selected depths is given in table 3.

Cores of two strata were taken during the drilling of well Al from 670 to 719 ft below land surface (9 ft of core recovered) and 910 to 920 ft (3 ft of core recovered). Core descriptions are given in table 4. Laboratory analyses were performed by Core Laboratories, Inc., Dallas, Texas, and the U.S. Geological Survey Hydrologic Laboratory, Lakewood, Colorado. Analyses included air and water vertical intrinsic permeability, porosity, interval transit time, and compressibility. These measurements are presented in tables 5, 6, and 7.

## Hydraulic Testing

### Short-term Withdrawal and Injection Tests

Short-term withdrawal and injection tests were performed in well Al and water-level drawdown and buildup were measured in wells Al and B3. The procedure involved pumping Al for 2 hours at one rate, allowing 2 hours for the water levels to recover, then starting the next step test at a higher pumping rate. The purpose of these tests was to determine if Darcy's law is applicable for radial flow in the test injection zone and to determine total well losses (Jacob, 1947) and casing losses in well Al. Table 8 lists the water-level measurements made in well B3 during these tests and table 9 lists the measurements in well Al.

Short-term withdrawal tests were performed on wells El and A4. During the test, well El was uncased from 1,853 to 3,280 ft. Discharge and water-level data for these tests are given in tables 10 and 11.

Water levels, instead of drawdowns, are given in this report for tests which exceed 1 hour because several environmental factors cause natural fluctuations at the South Cross Bayou test site. These factors, which have to be accounted for in computing the drawdowns, include tidal changes in the Gulf of Mexico, periodic dilation of the rock column caused by earth tides, barometric pressure changes, and regional trends in groundwater levels.

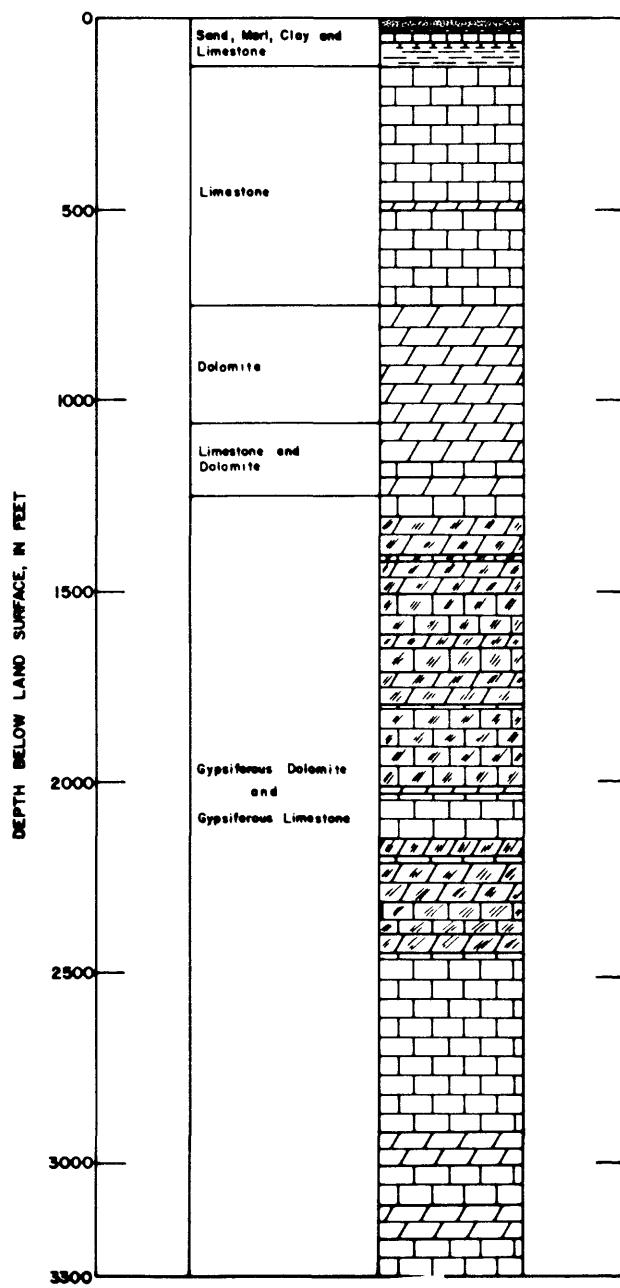


Figure 6.--Lithologic log of well E1.

### Withdrawal Test

Well A1, the test-injection well, was pumped at a rate of 5,000 gal/min for 33 hours from October 16 to October 18, 1974. Water levels were measured during the test in wells A1, A2, A3, A4, B1, B2, B3, B4, and B5. The measurements are listed in tables 12 through 14.

### Injection Test

From October 30 to November 3, 1974, a total of 96.33 hours, water from Joe's Creek (fig. 1) was injected into well A1 at an average rate of 4,350 gal/min. The injected water ranged in chloride concentration from 92 to 2,400 mg/L and was 820 mg/L near the end of the test. Prior to the test, well-head pressure in well A1 was 5.6 lb/in<sup>2</sup>, and at test end it was 9.1 lb/in<sup>2</sup>. Bottomhole pressure in well A1 is shown in table 15. Water levels in wells A2-A4 and B1-B4 are shown in table 16.

On November 8, 1974, well A1 was allowed to backflow. Backflow lasted 11 minutes and was estimated between 9,000 and 17,000 gal--a backflow volume less than the 21,650-gal casing volume of A1. Chloride concentration of the backflow water ranged from 810 to 850 mg/L. Nine minutes after backflow ceased, water from Joe's Creek again was injected into A1, this time for 1 hr at a rate of about 2,000 gal/min. The well was immediately allowed to backflow. Significant backflow lasted for about 10 minutes--a small stream of water (less than 1 gal/min) flowed for an additional 53 minutes. Total backflow volume cannot be estimated, but it likely exceeded the casing volume of well A1 because hydrogen sulfide, a common constituent in ground water in the test area, was smelled just before major backflow ceased. From 8 to 63 minutes after start of backflow, chloride concentration ranged from 5,600 to 9,410 mg/L. After backflow ceased, 19,000 gal of water was withdrawn from well A1. Chloride concentration after withdrawing that volume was 19,000 mg/L.

Water-level hydrographs that cover the time spans of the withdrawal and injection tests for wells A2, A3, A4, B1, B2, B3, and B4 are shown on figures 7 and 8. Water levels in A2 changed substantially during and after the injection test (fig. 7).

### Geophysical Logs

Geophysical logs were run in the test wells at the South Cross Bayou test site while the wells were being drilled. Tables 17, 18, and 19 are a summary of all of the geophysical logs run at the test site. Caliper and flowmeter logs for well A1 are shown on figure 9. A graphic lithologic log with caliper, resistivity, flowmeter, and a temperature profile

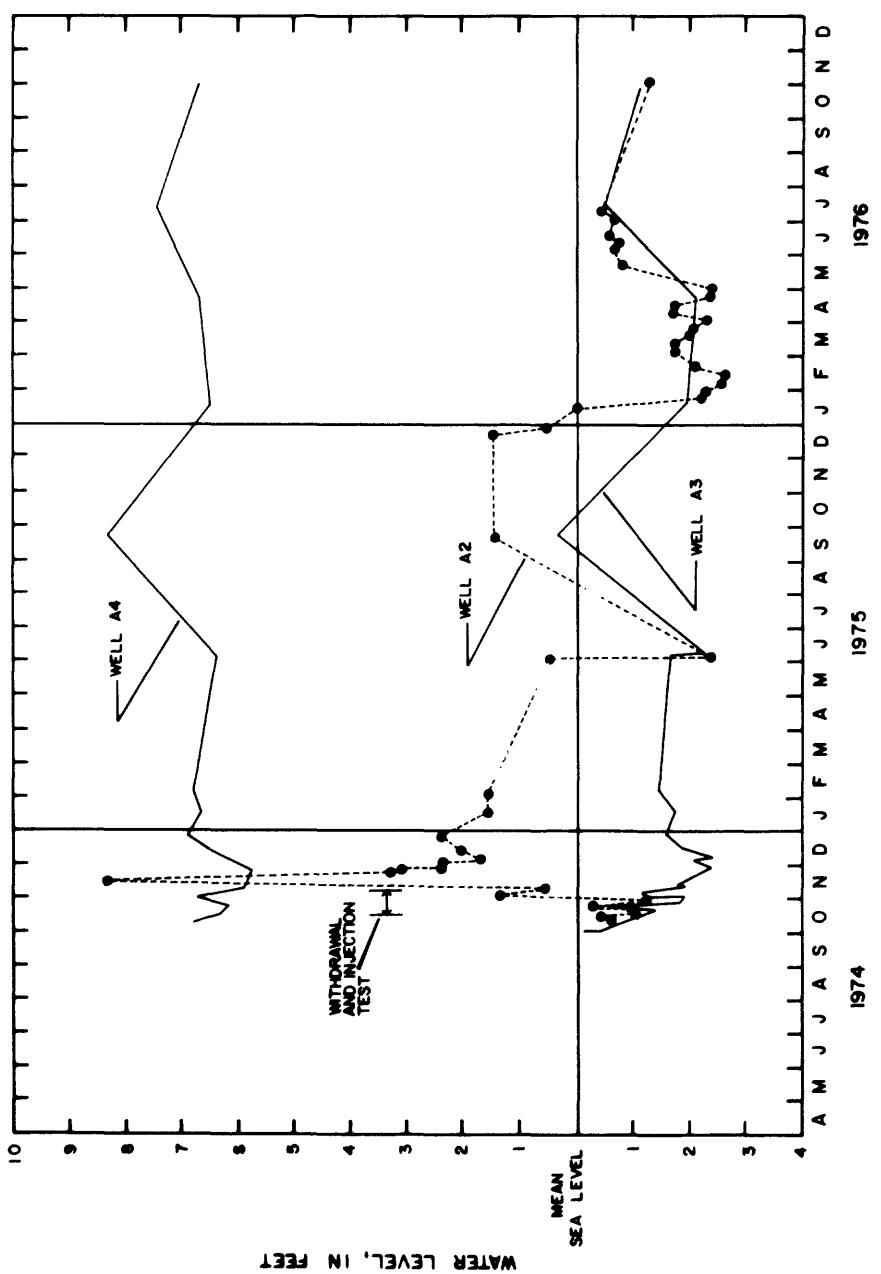


Figure 7.--Hydrographs of water levels in wells A2, A3, and A4, 1974-76.

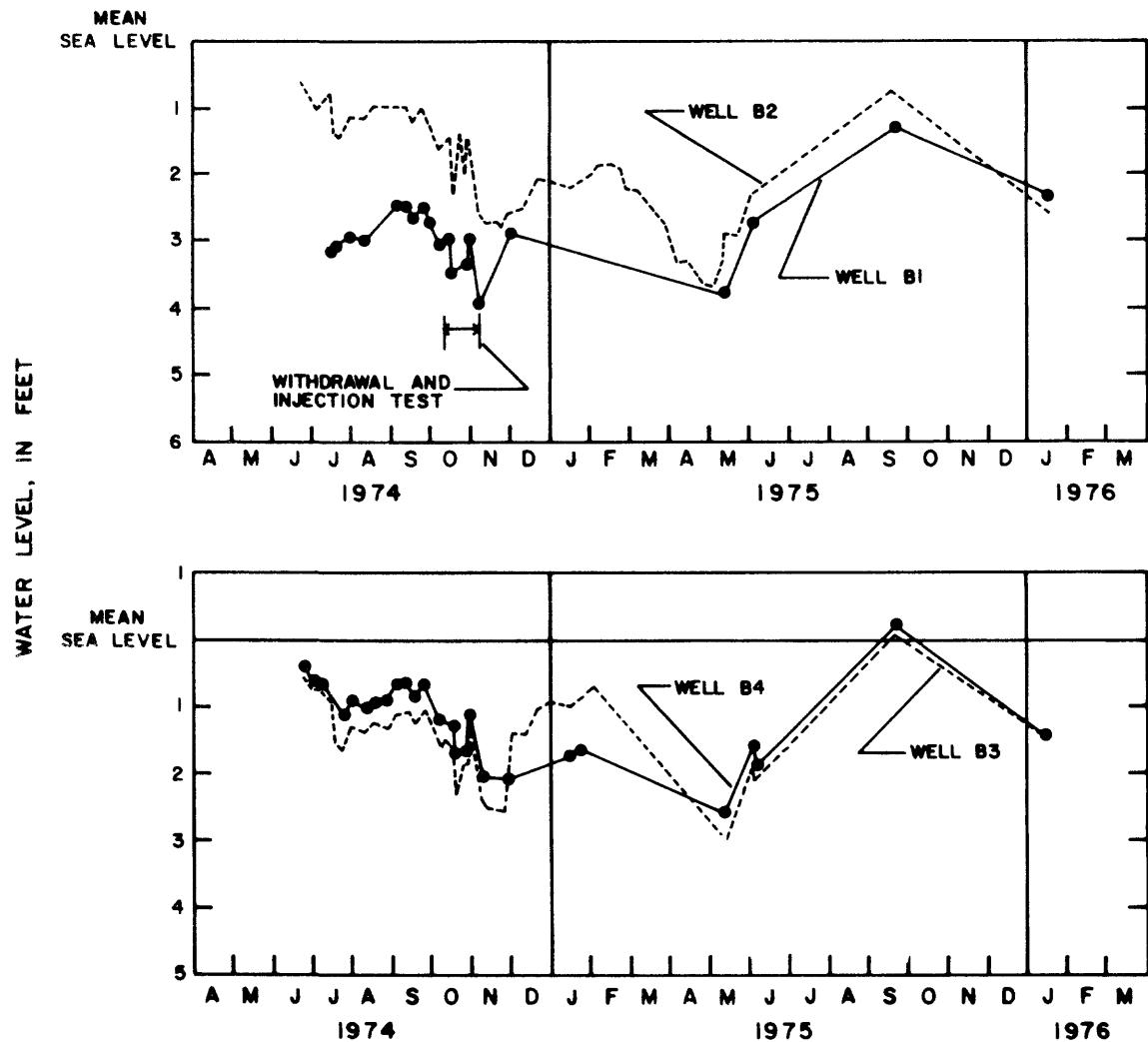


Figure 8.--Hydrographs of water levels in wells B1, B2, B3, and B4, 1974-76.

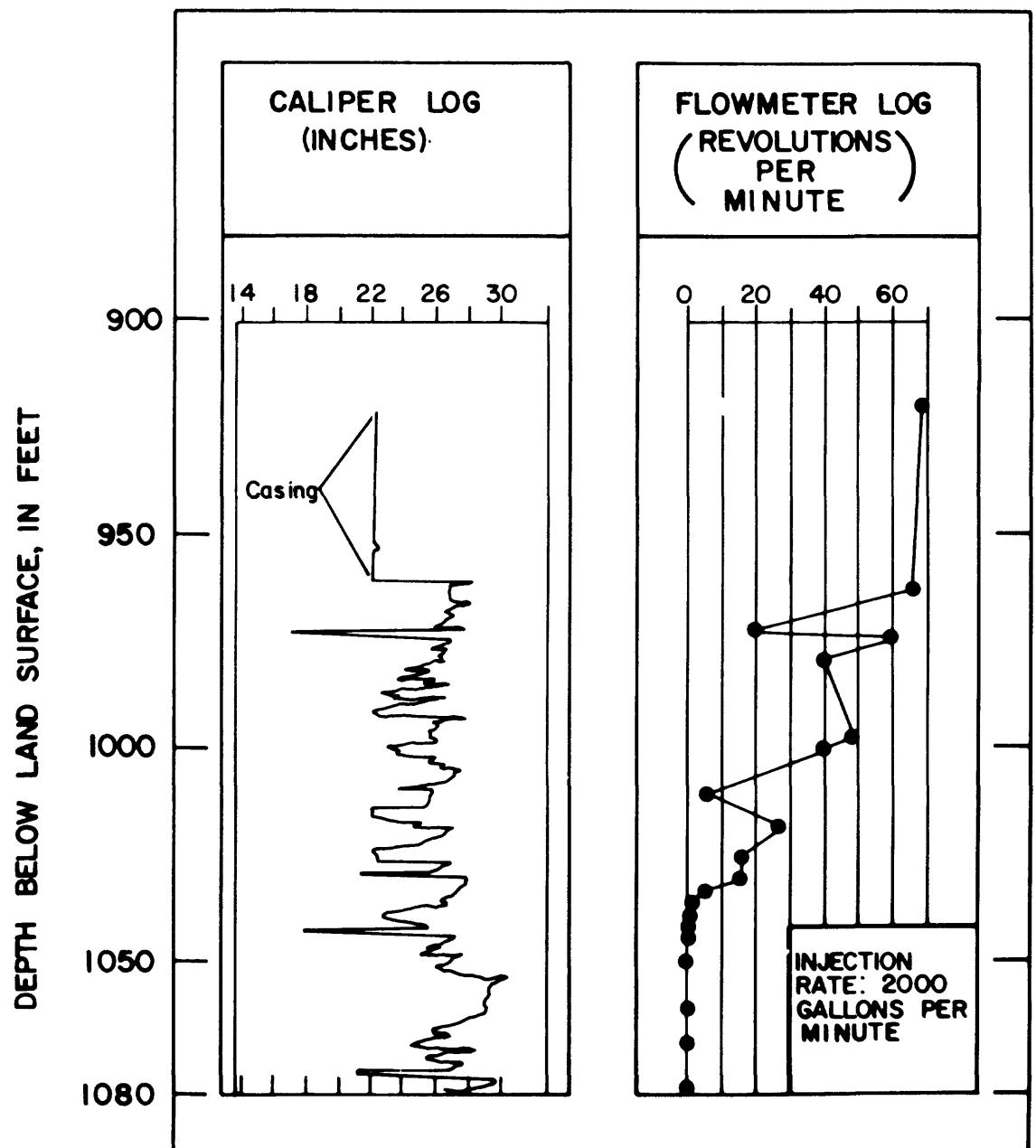


Figure 9.--Caliper and flowmeter logs of well Al.

during pumping for the upper part of well E1 are shown on figure 10. A lithologic log with caliper, static and pumping temperature profiles for the lower part of well E1 are shown on figure 11. The scale for the temperature logs in figure 11 is "counts per second" because a calibration curve correlating counts per second to temperature was not available. These logs are useful, nevertheless, for indicating where inflow is occurring within the borehole. Normal and lateral resistivity logs for well A2 are shown in figure 12.

#### Water-Quality Analyses

Water samples were collected for chemical analysis from well E1 (exploratory hole) during drilling, from all wells after their completion, and during and after the injection test. Table 20 shows the specific conductance and chloride concentration of water from well E1 as the well was deepened during drilling. Table 21 shows the temperature, specific conductance, and chloride concentration of water from wells A1, A2, A3, B1, B2, B3, and B4, before, during, and after the injection test. Analyses of water from well A1, after the injection test, include analyses of backflow samples, pumped samples, and point samples. Tables 22 through 24 give the chemical analyses of water from wells at the site.

Before the injection test, chloride concentration of the native formation water from wells at the site increased with depth. For example, water from test well A1 had a chloride concentration of 20,000 mg/L in the interval 961-1,080 ft (table 1) (table 21). Water samples from well A4, uncased from 200-250 ft, and A3, uncased from 463-571 ft, had chloride concentrations of 450 mg/L and 19,000 mg/L (table 21). Therefore, the uppermost position of water with 19,000 mg/L chloride concentration must be between 250 and 463 ft (table 1). Based on a lateral resistivity log of well A2 (fig. 12), the uppermost position of water with 19,000 mg/L chloride concentration is estimated to be about 370 ft.

The following water-quality sampling procedures were used at the wells. All water samples were pumped from wells using either centrifugal or turbine pumps. Before collecting the initial pumped water sample, the total volume within each well was removed at least once. Specific gravity, specific conductance, and temperature of the discharging water were then measured. Initial water samples were collected at the South Cross Bayou test site after the specific gravity or specific conductance and temperature of the water became constant. All other samples were collected after the total volume within each well was removed.

Freshwater was introduced into each test hole during drilling and construction. After placement of cement in wells B1-B4, freshwater was introduced to wash cement from the work pipe. A substantial volume of

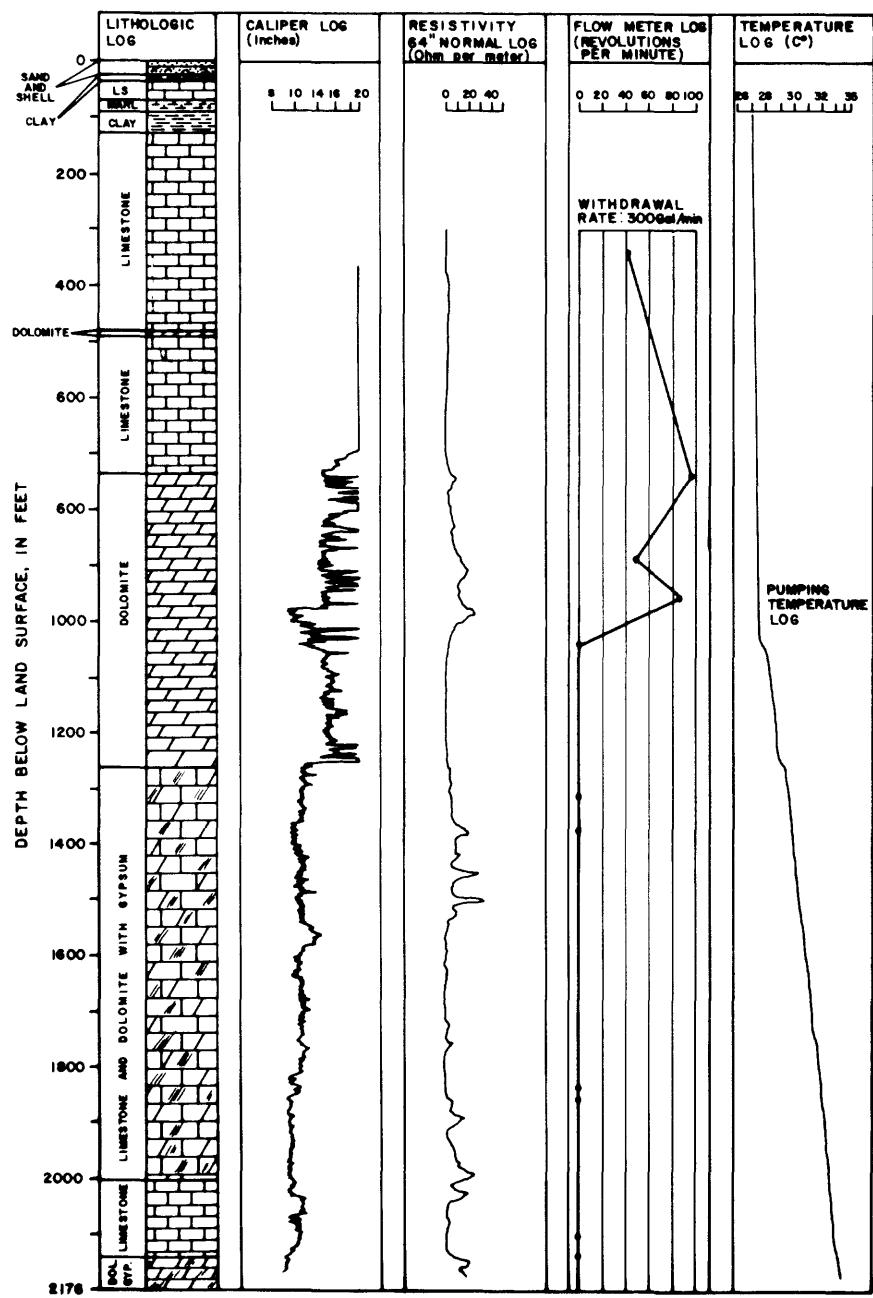


Figure 10.--Lithologic and geophysical logs of well El, from land surface to 2,176 feet.

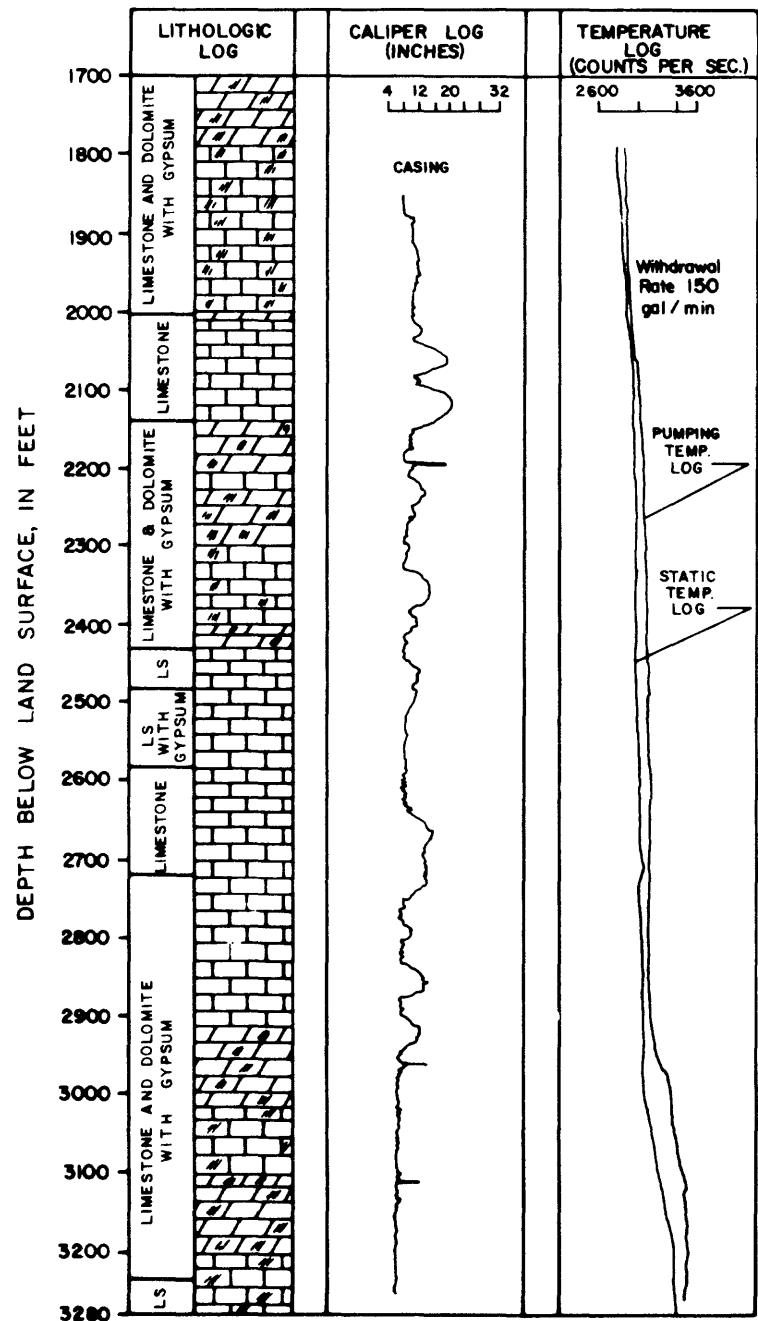


Figure 11.--Lithologic and geophysical logs of well E1 from 1,700 to 3,280 feet.

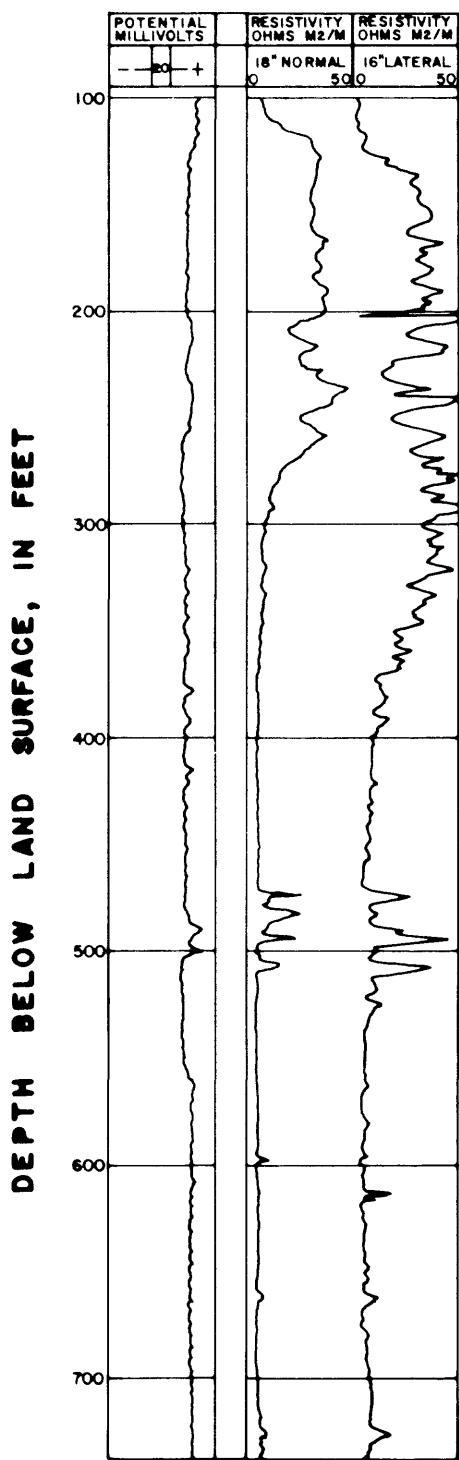


Figure 12.--Normal and lateral resistivity logs of well A2.

freshwater was introduced into well A1 during drilling when loss of circulation occurred from 762 to 802 ft and 975 to 988 ft. The disposition of this water and to what extent it mixed with the native saline waters is unknown.

#### QUALITY OF WATER FROM WELLS NEAR THE TEST INJECTION SITE

Wells within about a 1-mi radius of the test injection site were sampled and analyzed to provide water-quality background data prior to anticipated long-term injection at the test site. Locations of the wells sampled are shown on figure 13; reported construction data are given in table 25; and the chemical analyses of water from these wells are given in tables 26 and 27. Chloride concentration of water from the wells near the test site ranged between 9.8 to 290 mg/L. Reported depth of these wells ranged from 25 to 302 ft.

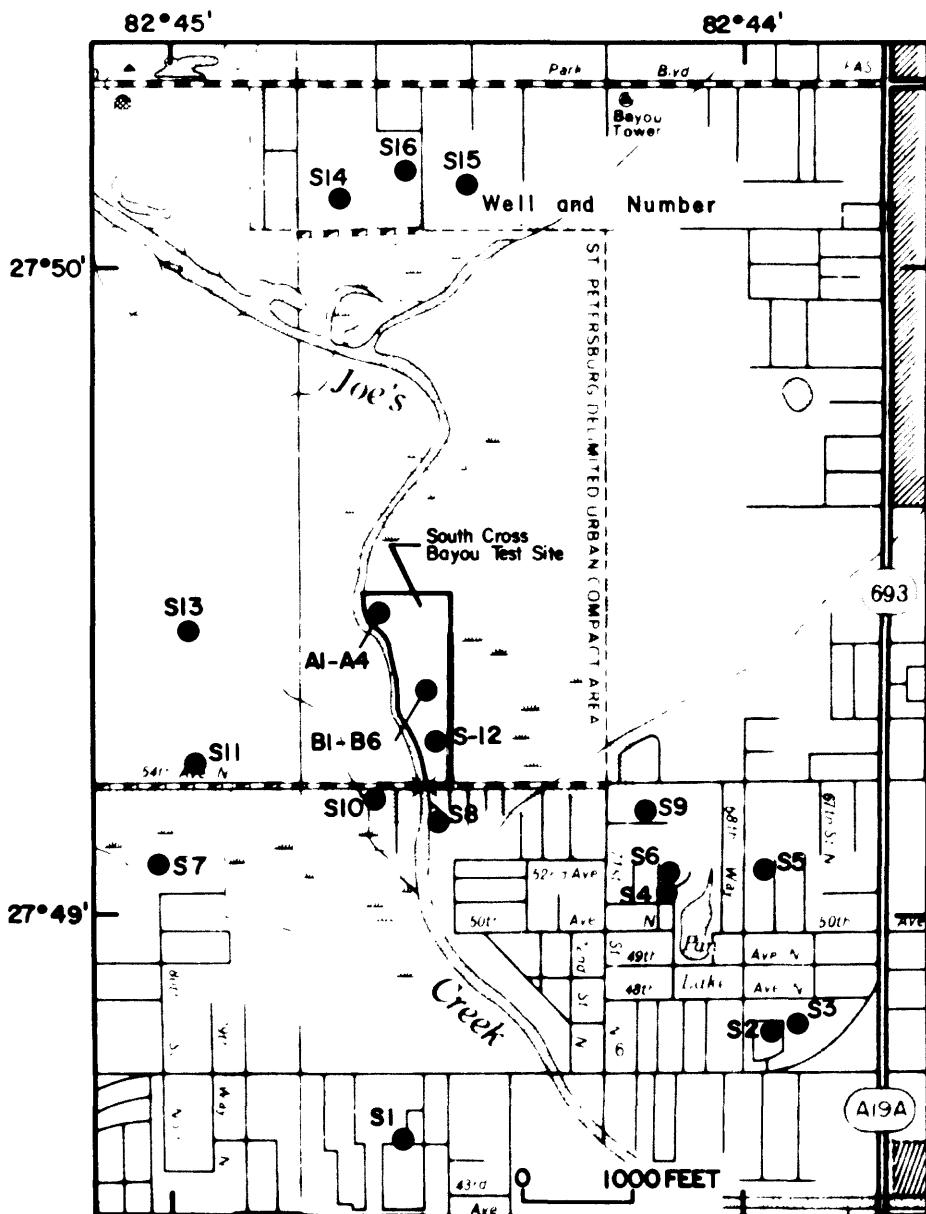


Figure 13.--Location of selected wells near the South Cross Bayou test site.

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Table 1.--Record of wells for South Cross Bayou test injection site

| Well number | Latitude<br>Longitude | Name of well          | Land-surface altitude<br>(ft above mean sea level) | Total depth<br>(ft below land surface) | Open interval<br>(ft below land surface) | Casing diameter<br>(in) | Distance from injection well Al (ft) |
|-------------|-----------------------|-----------------------|--|--|--|-------------------------|--------------------------------------|
| A1          | 274929N0824435.01     | Test injection well   | 8.0  | 1,080                                  | 961-1,080                                | 24                      | ---                                  |
| A2          | 274929N0824435.02     | Injection monitor 800 | 8.1  | 800                                    | 746-                                     | 800                     | 6                                    |
| A3          | 274929N0824435.03     | Injection monitor 521 | 7.7  | 521                                    | 463-                                     | 521                     | 6                                    |
| A4          | 274929N0824435.04     | Injection monitor 250 | 7.8  | 250                                    | 200-                                     | 250                     | 106                                  |
| B1          | 274922N0824431.04     | Monitor 1224          | 8.3  | 1,224                                  | 1,210-1,224                              | 2                       | 856                                  |
| B2          | 274922N0824431.03     | Monitor 1055          | 8.3  | 1,035                                  | 1,025-1,035                              | 8                       | 856                                  |
| B3          | 274922N0824431.02     | Monitor 815           | 8.3  | 815                                    | 780-                                     | 815                     | 2                                    |
| B4          | 274922N0824431.01     | Monitor 520           | 8.3  | 520                                    | 463-                                     | 520                     | 2                                    |
| B5          | 274921N0824430.02     | Monitor 94            | 8  | 94                                     | 90-                                      | 94                      | 2                                    |
| B6          | 274921N0824430.01     | Monitor 35            | 8  | 35                                     | 31-                                      | 35                      | 2                                    |
| E1          | 274922N0824431.00     | Exploratory hole      | 8.3  | 3,280                                  | ---                                      | -                       | 856                                  |

Table 2.--Lithologic log of well El

|  | <u>Thickness<br/>(ft)</u> | <u>Depth<br/>(ft)</u> |
|--|---------------------------|-----------------------|
| Sand, fine to coarse; some pebbles; some lignite                               | 15                        | 15                    |
| Shells; some sand; clay  | 10                        | 25                    |
| Clay, gray-brown; sandy; shells and fossils; conglomeratic; trace phosphate    | 10                        | 35                    |
| Limestone, cream, chalky, some vugs, fossiliferous; sand; some clay; phosphate | 30                        | 65                    |
| Clay, pale green; some limestone   | 5                         | 70                    |
| Marl, pale green, sandy, silty; some clay; trace phosphate                     | 15                        | 85                    |
| Limestone, cream, chalky, fossiliferous  | 5                         | 90                    |
| Clay, dark green, calcareous; sand   | 5                         | 95                    |
| Sand, medium grained; clay, calcareous   | 5                         | 100                   |
| Clay, gray, calcareous; sand; pebbles; trace phosphate                         | 25                        | 125                   |
| Limestone, cream, chalky, some vugs, fossiliferous; sand; trace phosphate      | 60                        | 185                   |
| No sample  | 5                         | 190                   |
| Limestone, cream-gray, dense; chert  | 5                         | 195                   |
| Limestone, cream, fossiliferous; much sand                                     | 20                        | 215                   |
| Limestone, cream-gray, some vugs   | 30                        | 245                   |
| Limestone, cream, chalky, sand; trace phosphate                                | 10                        | 255                   |
| Limestone, cream, some vugs, fossiliferous; trace chert; trace phosphate       | 30                        | 285                   |
| Limestone, cream; sand; fossiliferous; chert; phosphate                        | 45                        | 330                   |

Table 2.--Lithologic log of well El - continued

|  | <u>Thickness<br/>(ft)</u> | <u>Depth<br/>(ft)</u> |
|--|---------------------------|-----------------------|
| Limestone, cream-buff, chalky, vugular, fossiliferous; some coquinoid                                  | 60                        | 390                   |
| Limestone, cream-buff, chalky, granular, fossiliferous   | 90                        | 480                   |
| Dolomite, yellow-brown, crystalline  | 10                        | 490                   |
| Limestone, cream-buff, chalky, granular, very fossiliferous; much black chert                          | 5                         | 495                   |
| Limestone, cream-buff, chalky, soft, fossiliferous   | 40                        | 535                   |
| Limestone, cream-buff, granular, very fossiliferous  | 20                        | 555                   |
| Limestone, cream-buff, granular, very fossiliferous; sand  | 105                       | 660                   |
| Limestone, granular, some vugs, oolitic, very fossiliferous  | 75                        | 735                   |
| Dolomite, yellow-brown, crystalline, vugular, very porous, trace of <u>Dictyoconus</u> at 745; chert   | 310                       | 1045                  |
| Dolomite, yellow, gray, crystalline, some vugular, some very porous; some limestone, cream; some chert | 10                        | 1055                  |
| Dolomite, cream-brown, sucrosic, vugular, dolomitic, some fossils; some chert                          | 65                        | 1120                  |
| Dolomite, brown, chalky, vugular, some crystalline, some fossils; trace limestone                      | 65                        | 1185                  |
| Dolomite, granular, sucrosic, oolitic; some limestone, cream; trace lignite                            | 65                        | 1250                  |
| Limestone, cream, chalky, granular   | 10                        | 1260                  |
| Limestone, vugular, dolomitic; chert, dark brown-black; some dolomite; trace of gypsum                 | 20                        | 1280                  |

Table 2.--Lithologic log of well El - continued

|  | <u>Thickness</u><br><u>(ft)</u> | <u>Depth</u><br><u>(ft)</u> |
|--|---------------------------------|-----------------------------|
| Dolomite, vugular, dolomitic; chert, dark brown-black  | 10                              | 1290                        |
| Dolomite, vugular, dolomitic limestone, some chert, dark brown-black; gypsum, anhydrite              | 60                              | 1350                        |
| Dolomite, cream-brown, platy; limestone, finely crystalline; gypsum                                  | 50                              | 1400                        |
| Limestone, cream, vugular; some dolomite; chert; gypsum  | 30                              | 1430                        |
| Dolomite, cream-brown, vugular, platy; some limestone, cream, some black streaks; chert; some gypsum | 70                              | 1500                        |
| Limestone, cream, vugular, dolomitic, fossiliferous; gypsum  | 30                              | 1530                        |
| Limestone, cream, vugular, fossiliferous; some dolomite; much gypsum and anhydrite                   | 20                              | 1550                        |
| Limestone, white, chalky, vugular, fossiliferous; gypsum   | 20                              | 1570                        |
| Limestone, white, chalky, less vugular, fossiliferous; some dolomite, cream brown                    | 25                              | 1595                        |
| Dolomite, cream-buff, vugular, fossiliferous; some limestone; chert; gypsum                          | 40                              | 1635                        |
| Limestone, cream-brown to yellow-brown, sandy, granular; gypsum                                      | 65                              | 1700                        |
| Dolomite, yellow-cream, chalky, vugular; chert; much gypsum and anhydrite                            | 90                              | 1790                        |
| Limestone, cream-buff, chalky, dolomitic; gypsum   | 60                              | 1850                        |
| Limestone, cream, chalky, vugular, dolomitic; chert; gypsum  | 40                              | 1890                        |
| Limestone, cream, chalky, slightly dolomitic; gypsum   | 60                              | 1950                        |

Table 2.--Lithologic log of well El - continued

|  | <u>Thickness<br/>(ft)</u> | <u>Depth<br/>(ft)</u> |
|--|---------------------------|-----------------------|
| Limestone, cream-tan, vugular, dolomitic; dolomite, brown, crystalline; chert; considerable gypsum and anhydrite | 50                        | 2000                  |
| Dolomite, gray-brown to yellow-brown, coarsely crystalline; chert  | 10                        | 2010                  |
| Limestone, cream, granular, nodular, coarsely crystalline, very fossiliferous (coquina), <u>Dictyoconus</u>      | 75                        | 2085                  |
| Dolomite, yellow-brown, some vugs, crystalline; chert  | 5                         | 2090                  |
| Limestone, cream, granular, finely crystalline, slightly fossiliferous; some dolomite, yellow-brown              | 50                        | 2140                  |
| Dolomite, yellow-brown, vugular, crystalline; chert, gypsum  | 10                        | 2150                  |
| Dolomite, cream-brown, granular; limestone; gypsum   | 25                        | 2175                  |
| No sample  | 3                         | 2178                  |
| Dolomite, cream-brown, granular, coarsely crystalline; limestone; some gypsum                                    | 7                         | 2185                  |
| Dolomite, yellow-brown, coarsely crystalline; trace gypsum   | 15                        | 2200                  |
| Dolomite, dark-brown   | 10                        | 2210                  |
| Limestone, cream-white, very fossiliferous; dolomite, light-brown, crystalline                                   | 20                        | 2230                  |
| Dolomite, light yellow-brown, finely crystalline; limestone; gypsum  | 20                        | 2250                  |
| Dolomite, light yellow-brown, finely crystalline; limestone; gypsum; iron mineral                                | 10                        | 2260                  |

Table 2.--Lithologic log of well El - continued

|  | <u>Thickness</u><br><u>(ft)</u> | <u>Depth</u><br><u>(ft)</u> |
|--|---------------------------------|-----------------------------|
| Dolomite, light yellow-brown, finely crystalline; limestone, finely granular or oolitic, fossiliferous; trace gypsum | 5                               | 2265                        |
| Dolomite, yellow-brown, finely to coarsely crystalline; gypsum   | 10                              | 2275                        |
| Dolomite, yellow-brown, finely to coarsely crystalline; some limestone, brown, dolomitic, fossiliferous; gypsum      | 25                              | 2300                        |
| Limestone, cream to yellow, granular, fossiliferous; some dolomite, gypsum   | 35                              | 2335                        |
| Limestone, cream-gray, very fossiliferous ( <u>Dictyoconus</u> ?)  | 5                               | 2340                        |
| Poor recovery-limestone, dolomite, gypsum, sand, iron mineral  | 60                              | 2400                        |
| Dolomite, gray-brown, crystalline; some limestone; some gypsum; much of iron mineral                                 | 20                              | 2420                        |
| Dolomite; limestone; much chert  | 10                              | 2430                        |
| Limestone; much chert; iron mineral  | 10                              | 2440                        |
| Limestone, cream, chalky, granular, fossiliferous; chert; much of iron mineral; caving                               | 45                              | 2485                        |
| Limestone, cream, chalky, granular, fossiliferous; some dolomite, yellow-brown; gypsum; iron mineral                 | 65                              | 2550                        |
| Limestone, cream, fossiliferous; some dolomite; some gypsum; possible contamination                                  | 35                              | 2585                        |
| Limestone, cream-white, granular, fossiliferous; much chert  | 15                              | 2600                        |
| Limestone, cream-white, granular, fossiliferous; much chert  | 95                              | 2695                        |
| No samples   | 5                               | 2700                        |

Table 2.--Lithologic log of well E1 - continued

|   | <u>Thickness<br/>(ft)</u> | <u>Depth<br/>(ft)</u> |
|---|---------------------------|-----------------------|
| Limestone, cream-buff, chalky, granular, fossiliferous  | 15                        | 2715                  |
| No sample   | 5                         | 2720                  |
| Limestone, cream-buff, chalky, granular, fossiliferous; trace gypsum  | 30                        | 2750                  |
| Limestone, cream, granular, fossiliferous; some dolomite, crystalline; trace gypsum                                       | 10                        | 2760                  |
| Limestone, cream granular, micro-oolitic?, fossiliferous; little gypsum   | 20                        | 2780                  |
| Limestone, cream, granular; some dolomite, coarsely crystalline; little gypsum  | 70                        | 2850                  |
| Limestone, cream, chalky, granular, crystalline, fossiliferous; some dolomite, yellow, coarsely crystalline; trace gypsum | 40                        | 2890                  |
| Limestone, cream, very finely crystalline; little dolomite  | 30                        | 2920                  |
| Dolomite, yellow to clear, coarsely crystalline; some limestone; some gypsum  | 30                        | 2950                  |
| Dolomite, yellow-brown, very coarsely crystalline; some gypsum  | 30                        | 2980                  |
| Dolomite, yellow-brown, coarsely crystalline; chert; some gypsum  | 15                        | 2995                  |
| Dolomite, yellow-brown, coarsely crystalline; some limestone, cream-white, chalky, granular, fossiliferous                | 10                        | 3005                  |
| Dolomite, yellow-brown, coarsely crystalline; gypsum  | 5                         | 3010                  |
| Limestone, cream-white, chalky, granular, fossiliferous; dolomite, gray, finely crystalline; gypsum                       | 85                        | 3095                  |

Table 2.--Lithologic log of well E1 - continued

|   | <u>Thickness<br/>(ft)</u> | <u>Depth<br/>(ft)</u> |
|---|---------------------------|-----------------------|
| Dolomite, gray-brown, finely crystalline;<br>little gypsum  | 5                         | 3100                  |
| Dolomite, gray-brown, finely crystalline;<br>some chert; little gypsum                            | 15                        | 3115                  |
| Dolomite, gray-brown, finely crystalline;<br>some limestone, cream, fossiliferous; some<br>gypsum | 35                        | 3150                  |
| Dolomite, gray-brown, crystalline; limestone,<br>cream, fossiliferous; chert; trace gypsum        | 50                        | 3200                  |
| Limestone, cream-white, granular; some<br>dolomite; trace gypsum                                  | 35                        | 3235                  |
| Limestone, cream-white, granular; possibly<br>micro-oolitic; some dolomite                        | 15                        | 3250                  |
| Limestone, yellow-brown, granular, very fine<br>grained; dolomite; iron mineral                   | 30                        | 3280                  |

Table 3.--X-ray diffraction analyses of selected lithologic samples from wells E1 and A1

[Analyses, in percent based on peak height, performed by USGS Hydrologic Laboratory, Lakewood, Colorado.]

| Well | Depth<br>(ft) | Quartz | Calcite | Dolomite | Aragonite | Siderite | Total<br>clay<br>minerals | Total |
|------|---------------|--------|---------|----------|-----------|----------|---------------------------|-------|
| E1   | 35            | 16     | 0       | 0        | 33        | 0        | 29                        | 78    |
| E1   | 50            | 20     | 0       | 59       | 0         | 0        | 7                         | 86    |
| E1   | 155           | 2      | 97      | 1        | 0         | 0        | 0                         | 100   |
| E1   | 355           | 2      | 97      | 1        | 0         | 0        | 0                         | 100   |
| E1   | 530           | 0      | 92      | 0        | 0         | 0        | 0                         | 92    |
| A1   | 712           | 0      | 83      | 14       | 0         | 0        | 0                         | 97    |
| A1   | 716           | 9      | 98      | 2        | 0         | 0        | 0                         | 100   |
| E1   | 760           | 1      | 20      | 79       | 0         | 0        | 0                         | 100   |
| A1   | 915           | 0      | 0       | 99       | 0         | 0        | 0                         | 99    |
| E1   | 1010          | 0      | 6       | 85       | 0         | 0        | 0                         | 91    |
| E1   | 1100          | 0      | 0       | 100      | 0         | 0        | 0                         | 100   |
| E1   | 1200          | 2      | 5       | 93       | 0         | 0        | 0                         | 100   |

Table 4.--Description of cores from well A1

| Lithology  | Depth of cored interval (ft) | Core recovery (ft) | Largest core segment (in) |
|--|------------------------------|--------------------|---------------------------|
| No core recovered  | 670-710                      | 0                  |                           |
| Limestone, cream to light brown, granular, some vugs, some vertical and horizontal fractures, fossiliferous  | 710-719                      | 9                  | 6                         |
| Limestone, white, very soft, no fossils  | 910-911                      | 1                  | crushed                   |
| Dolomite, brown-gray, micro-crystalline, some pin point and large vugs, some fractures which are mainly vertical and found in lower part of recovered core, no fossils | 911-920                      | 2                  | 4                         |

Table 5.--Vertical intrinsic permeability of cores from well A1

[Analyses performed by Core Laboratories, Inc., Dallas, Texas. Nitrogen gas intrinsic permeabilities corrected for Klinkenberg effect (Klinkenberg, 1941) by Core Laboratories. Kinematic viscosity of the formation and distilled water used in the tests were 0.960 centistokes and 0.955 centistokes, respectively. Kinematic viscosity of the nitrogen gas was 15.391 centistokes. Temperature of all of the fluids was 75°F (23.9°C). Intrinsic permeability may be converted to hydraulic conductivity as shown in Lohman and others (1972, p. 10).]

| Depth of core (ft) | Nitrogen gas intrinsic permeability ( $\text{cm}^2$ ) | Water intrinsic permeability      |                                   |
|--------------------|---|-----------------------------------|-----------------------------------|
|                    |   | Formation water ( $\text{cm}^2$ ) | Distilled water ( $\text{cm}^2$ ) |
| 710-713            | $6.12 \times 10^{-10}$                                | $3.16 \times 10^{-10}$            | $3.85 \times 10^{-10}$            |
| 710-713            | $2.37 \times 10^{-10}$                                |                                   |                                   |

Table 6.--Porosity of cores from well Al

[Porosity determined by the U.S. Geological Survey Hydrologic Laboratory, Lakewood, Colorado, and Core Laboratories, Inc., Dallas, Texas.]

| Depth of core<br>(feet) | Total porosity<br>(percent) | Effective porosity<br>(percent) |
|-------------------------|-----------------------------|---------------------------------|
| 710-713                 | --                          | 30                              |
| 710-713                 | --                          | 28                              |
| 710-713                 | 34                          | 31                              |
| 715-717                 | 22                          | 19                              |
| 914-916                 | 3                           | 0.1                             |

Table 7.--Compressibility of cores from well Al

[Analyses performed by Core Laboratories, Inc., Dallas, Texas. Core Laboratories calculated pore volume compressibility which is change in pore volume divided by average pore volume divided by initial bulk volume divided by pressure change. Compressibility was calculated from the Core Laboratory results by multiplying pore volume compressibility by average pore volume divided by initial bulk volume. Average pore volume was calculated over a selected range of pressures. Initial bulk volume was measured at the first pressure in the selected range.]

| Depth<br>of<br>core<br>(ft) | Average pore volume<br>Initial bulk volume<br>(percent) | Pressure<br>(lb/in <sup>2</sup> ) |          | Compressibility<br>(in <sup>2</sup> /lb) |
|-----------------------------|---|-----------------------------------|----------|--|
|                             |   | External                          | Internal |  |
|                             |   |                                   |          |  |

Hydraulic loading of core samples  
(Corrected to uniaxial loading by Core Laboratories)

|         |      |      |      |                      |
|---------|------|------|------|----------------------|
| 710-713 | 30.7 | 2000 | 1800 | $1.6 \times 10^{-6}$ |
|         |      | 2000 | 1371 |                      |
| 710-713 | 28.0 | 2000 | 1800 | $3.1 \times 10^{-7}$ |
|         |      | 2000 | 1371 |                      |

Table 8.--Water-level drawdown and buildup in well B3 during short-term withdrawal and injection tests in well A1

| Date     | Elapsed time (min) | Well A1            |                             | Well B3                        |
|----------|--------------------|--------------------|-----------------------------|--------------------------------|
|          |                    | A) withdrawal rate | B) injection rate (gal/min) | A) drawdown<br>B) buildup (ft) |
| 7-22-74  | 90                 | A) 820             |                             | A) 0.05                        |
| 7-23-74  | 90                 |                    | 1480                        | .12                            |
| 7-23-74  | 90                 |                    | 2340                        | .18                            |
| 7-24-74  | 90                 |                    | 2710                        | .20                            |
| 7-25-74  | 90                 |                    | 2840                        | .22                            |
| 10-16-74 | 90                 |                    | 5000                        | .40                            |
|          |                    | B) 1140            |                             | B) .06                         |
| 10-28-74 | 90                 |                    | 2050                        | .17                            |
| 10-30-74 | 90                 |                    | 3400                        | .29                            |
| 10-30-74 | 90                 |                    | 4600                        | .38                            |

Table 9.--Water-level drawdown and buildup in well A1 during short-term withdrawal and injection tests in well A1

[Buildup was measured in the casing at 38 and 958 feet below land surface. Casing depth is 961 feet.]

| Date     | Elapsed time (min) | Well A1            |                             | Well A1   |
|----------|--------------------|--------------------|-----------------------------|---|
|          |                    | A) withdrawal rate | B) injection rate (gal/min) | A) drawdown<br>B) buildup at 38 feet<br>C) buildup at 958 feet (ft) |
| 7-23-74  | 90                 | A) 1480            |                             | A) 1.03   |
| 10-16-74 | 90                 |                    | 5000                        | 5.22  |
|          |                    | B) 1140            |                             | B) C) 1.1   |
| 10-29-74 | 90                 |                    | 2050                        | 2.2 1.7   |
| 10-29-74 | 18                 |                    |                             |   |
| 10-30-74 | 90                 |                    | 3400                        | 3.8 2.9   |
| 10-30-74 | 90                 |                    | 4600                        | 4.9 3.3   |

Table 10.--Water levels in well E1 during short-term well E1 withdrawal test

[Depth interval, 1,863 to 3,280 feet; test began March 25, 1974 at 2240 hours and ended March 26, 1974 at 0608 hours. Discharge of well E1 ranged from 150 to 175 gallons per minute for first hour of test. Average discharge for rest of the test was 145 gallons per minute and ranged from 140 to 149 gallons per minute.]

| Time<br>(hr) | Water level<br>(ft below<br>measuring<br>point) | Time<br>(hr) | Water level<br>(ft below<br>measuring<br>point) |
|--------------|---|--------------|---|
| 3-25-74      |   | 2350         | 52.53   |
| 1121         | 31.85   | 2400         | 52.63   |
| 1125         | 31.84   | 3-26-74      |   |
| 1130         | 31.85   | 0010         | 52.75   |
| 1135         | 31.86   | 0020         | 52.80   |
| 1140         | 31.85   | 0030         | 52.95   |
| 1144         | 31.86   | 0040         | 53.07   |
| 1733         | 31.63   | 0050         | 53.21   |
| 1742         | 31.62   | 0055         | 53.32   |
| 1748         | 31.63   | 0102         | 53.43   |
| 2232         | 31.66   | 0110         | 53.55   |
| 2237         | 31.66   | 0120         | 53.54   |
| 2240         | 31.66   | 0121         | 53.54   |
| 2242         | 43.71   | 0130         | 53.57   |
| 2243         | 45.19   | 0142         | 53.73   |
| 2244         | 46.12   | 0150         | 53.71   |
| 2245         | 47.26   | 0200         | 53.64   |
| 2247         | 47.54   | 0203         | 53.70   |
| 2248         | 47.77   | 0218         | 53.85   |
| 2252         | 47.81   | 0221         | 53.84   |
| 2256         | 47.51   | 0240         | 53.70   |
| 2257         | 47.51   | 0258         | 53.76   |
| 2300         | 47.57   | 0323         | 53.85   |
| 2305         | 47.68   | 0340         | 53.91   |
| 2310         | 48.02   | 0400         | 53.98   |
| 2315         | 49.17   | 0419         | 53.99   |
| 2320         | 51.02   | 0444         | 54.09   |
| 2325         | 51.60   | 0504         | 54.12   |
| 2331         | 52.32   | 0544         | 54.24   |
| 2335         | 52.57   | 0609         | 54.31   |
| 2340         | 52.67   | 0611         | 54.21   |

Table 11.--Water levels in well A4 during short-term well A4 withdrawal test

[Test began January 16, 1976 at 1345 hours and ended January 16, 1976 at 1515 hours. Discharge of well A4 was 105 gallons per minute.]

| Time<br>(hr) | Water level<br>(ft above (+)<br>and below (-)<br>mean sea level) | Time<br>(hr) | Water level<br>(ft above (+)<br>and below (-)<br>mean sea level) |
|--------------|--|--------------|--|
| 1-16-76      |  | 1445         | -17.23   |
| 1230         | 6.57   | 1455         | -17.22   |
| 1380         | 6.52   | 1505         | -17.24   |
| 1338         | 6.56   | 1515         | -17.24   |
| 1342         | 6.59   | 1516         | 1.37   |
| 1346         | -8.23  | 1517         | 3.21   |
| 1347         | -16.53   | 1518         | 4.10   |
| 1349         | -16.59   | 1519         | 4.70   |
| 1350         | -16.70   | 1520         | 5.07   |
| 1351         | -16.77   | 1521         | 5.26   |
| 1352         | -16.81   | 1522         | 5.45   |
| 1353         | -16.81   | 1523         | 5.59   |
| 1354         | -16.85   | 1524         | 5.72   |
| 1355         | -16.91   | 1525         | 5.82   |
| 1357         | -16.91   | 1527         | 5.97   |
| 1400         | -16.92   | 1529         | 6.07   |
| 1401         | -16.95   | 1531         | 6.15   |
| 1403         | -16.99   | 1533         | 6.21   |
| 1405         | -17.01   | 1535         | 6.25   |
| 1410         | -17.06   | 1540         | 6.33   |
| 1415         | -17.06   | 1545         | 6.37   |
| 1420         | -17.23   | 1550         | 6.40   |
| 1425         | -17.21   | 1555         | 6.42   |
| 1430         | -17.22   | 1605         | 6.45   |
| 1435         | -17.22   | 1615         | 6.47   |

Table 12.--Water levels in well Al during well Al withdrawal test

[Test began October 16, 1974 at 2338 hours and ended October 18, 1974 at 0838 hours. Discharge of well Al was 5,000 gallons per minute.]

| Time<br>(hr) | Water level<br>(ft below<br>mean sea level) | Time<br>(hr) | Water level<br>(ft below<br>mean sea level) |
|--------------|---|--------------|---|
| 10-16-74     |   | 0638         | 6.24  |
| 2130         | 1.66  | 0738         | 6.35  |
| 2200         | 1.65  | 0838         | 6.44  |
| 2300         | 1.63  | 0938         | 6.44  |
| 2330         | 1.63  | 1038         | 6.37  |
| 2338         | 1.63  | 1138         | 6.30  |
| 2393         | 2.98  | 1238         | 6.24  |
| 2344         | 6.50  | 1338         | 6.31  |
| 10-17-74     |   | 1438         | 6.24  |
| 0004         | 5.96  | 1538         | 6.25  |
| 0007         | 6.20  | 1638         | 6.23  |
| 0015         | 6.05  | 1738         | 6.25  |
| 0018         | 6.06  | 1838         | 6.30  |
| 0031         | 5.86  | 1938         | 6.30  |
| 0038         | 5.81  | 2038         | 6.31  |
| 0048         | 6.10  | 2138         | 6.31  |
| 0058         | 6.17  | 2238         | 6.29  |
| 0098         | 6.21  | 2338         | 6.26  |
| 0138         | 6.21  | 10-18-74     |   |
| 0158         | 6.07  | 0038         | 6.26  |
| 0218         | 6.16  | 0138         | 6.23  |
| 0238         | 6.19  | 0238         | 6.16  |
| 0258         | 6.07  | 0338         | 6.15  |
| 0328         | 6.10  | 0438         | 6.15  |
| 0338         | 6.14  | 0538         | 6.23  |
| 0438         | 6.17  | 0638         | 6.23  |
| 0508         | 6.22  | 0738         | 6.24  |
| 0538         | 6.19  | 0838         | 6.26  |

Table 13.--Water levels in wells A2, A3, A4, B1, B2, B3, and B4 during well A1 withdrawal test

[Test began October 16, 1974 at 2338 hours and ended October 18, 1974 at 0838 hours. Discharge of well A1 was 5,000 gallons per minute. Levels shown are in feet below mean sea level.]

| Date     | Time<br>(hr) | Well A2 | Well A3 | Well A4 | Well B1 | Well B2 | Well B3 | Well B4 |
|----------|--------------|---------|---------|---------|---------|---------|---------|---------|
| 10-16-77 | 2200         | 0.53    | 1.00    | 6.87    | 2.97    | 1.51    | 1.52    | 1.20    |
|          | 2215         | .53     | 1.00    | 6.87    | 2.97    | 1.50    | 1.52    | 1.19    |
|          | 2230         | .52     | 1.00    | 6.87    | 2.97    | 1.50    | 1.51    | 1.19    |
|          | 2245         | .51     | .99     | 6.88    | 2.97    | 1.49    | 1.51    | 1.19    |
|          | 2230         | .51     | .99     | 6.88    | 2.96    | 1.48    | 1.51    | 1.18    |
|          | 2315         | .50     | .98     | 6.89    | 2.96    | 1.49    | 1.50    | 1.17    |
|          | 2330         | .49     | .98     | 6.89    | 2.96    | 1.48    | 1.50    | 1.16    |
|          | 2338         | .48     | .96     | 6.90    | 2.95    | 1.46    | 1.48    | 1.16    |
|          | 2339         | .55     | .97     | 6.91    | 2.95    | 1.62    | 1.56    | 1.16    |
|          | 2340         | .70     | 1.02    | 6.91    | 2.95    | 1.69    | 1.63    | 1.18    |
|          | 2341         | .77     | 1.03    | 6.91    | 2.95    | 1.70    | 1.69    | 1.19    |
|          | 2342         | .80     | 1.05    | 6.91    | 2.95    | 1.72    | 1.73    | 1.21    |
|          | 2343         | .81     | 1.08    | 6.91    | 2.95    | 1.74    | 1.75    | 1.23    |
|          | 2344         | .82     | 1.10    | 6.90    | 2.96    | 1.74    | 1.76    | 1.24    |
|          | 2345         | .83     | 1.12    | 6.90    | 2.96    | 1.75    | 1.76    | 1.26    |
|          | 2346         | .84     | 1.12    | 6.90    | 2.96    | 1.76    | 1.78    | 1.27    |
|          | 2347         | .84     | 1.14    | 6.89    | 2.97    | 1.76    | 1.78    | 1.28    |
|          | 2348         | .85     | 1.16    | 6.89    | 2.97    | 1.77    | 1.80    | 1.29    |
|          | 2353         | .87     | 1.20    | 6.86    | 2.99    | 1.78    | 1.81    | 1.34    |
|          | 2358         | .88     | 1.22    | 6.84    | 3.01    | 1.80    | 1.82    | 1.37    |
| 10-17-74 | 0003         | .89     | 1.24    | 6.82    | 3.03    | 1.80    | 1.83    | 1.39    |
|          | 0008         | .90     | 1.26    | 6.81    | 3.04    | 1.82    | 1.84    | 1.40    |
|          | 0013         | .91     | 1.27    | 6.80    | 3.05    | 1.82    | 1.85    | 1.41    |
|          | 0018         | .92     | 1.28    | 6.78    | 3.07    | 1.82    | 1.86    | 1.43    |
|          | 0023         | .92     | 1.28    | 6.77    | 3.08    | 1.83    | 1.86    | 1.43    |
|          | 0028         | .92     | 1.28    | 6.76    | 3.09    | 1.83    | 1.86    | 1.44    |
|          | 0038         | .92     | 1.29    | 6.75    | 3.10    | 1.83    | 1.86    | 1.44    |

Table 13.--Water levels in wells A2, A3, A4, B1, B2, B3, and B4 during well A1 withdrawal test - continued

| Date     | Time<br>(hr) | Well A2 | Well A3 | Well A4 | Well B1 | Well B2 | Well B3 | Well B4 |
|----------|--------------|---------|---------|---------|---------|---------|---------|---------|
| 10-17-74 | 0048         | 0.94    | 1.31    | 6.73    | 3.11    | 1.85    | 1.87    | 1.46    |
|          | 0058         | .94     | 1.32    | 6.72    | 3.12    | 1.86    | 1.88    | 1.47    |
| 0108     | .95          | 1.33    | 6.71    | 3.13    | 1.86    | 1.89    | 1.47    |         |
| 0118     | .96          | 1.33    | 6.70    | 3.14    | 1.86    | 1.89    | 1.48    |         |
| 0128     | .96          | 1.34    | 6.70    | 3.15    | 1.87    | 1.90    | 1.48    |         |
| 0138     | .96          | 1.34    | 6.69    | 3.15    | 1.87    | 1.90    | 1.48    |         |
| 0148     | .96          | 1.35    | 6.68    | 3.16    | 1.88    | 1.91    | 1.49    |         |
| 0158     | .97          | 1.35    | 6.67    | 3.16    | 1.88    | 1.90    | 1.49    |         |
| 0208     | 1.00         | 1.35    | 6.66    | 3.17    | 1.88    | 1.91    | 1.50    |         |
| 0218     | 1.00         | 1.35    | 6.67    | 3.17    | 1.89    | 1.91    | 1.50    |         |
| 0228     | 1.00         | 1.35    | 6.67    | 3.18    | 1.89    | 1.92    | 1.51    |         |
| 0238     | 1.00         | 1.36    | 6.67    | 3.18    | 1.90    | 1.92    | 1.51    |         |
| 0248     | 1.01         | 1.36    | 6.66    | 3.19    | 1.90    | 1.92    | 1.51    |         |
| 0258     | 1.01         | 1.36    | 6.66    | 3.19    | 1.90    | 1.92    | 1.51    |         |
| 0323     | 1.01         | 1.38    | 6.65    | 3.19    | 1.90    | 1.93    | 1.51    |         |
| 0348     | 1.02         | 1.38    | 6.64    | 3.19    | 1.90    | 1.94    | 1.52    |         |
| 0413     | 1.03         | 1.39    | 6.63    | 3.21    | 1.92    | 1.95    | 1.53    |         |
| 0438     | 1.05         | 1.41    | 6.62    | 3.22    | 1.94    | 1.97    | 1.54    |         |
| 0503     | 1.07         | 1.43    | 6.60    | 3.23    | 1.96    | 1.99    | 1.56    |         |
| 0528     | 1.10         | 1.45    | 6.58    | 3.25    | 1.98    | 2.02    | 1.58    |         |
| 0553     | 1.12         | 1.48    | 6.55    | 3.27    | 2.00    | 2.03    | 1.61    |         |
| 0618     | 1.12         | 1.51    | 6.53    | 3.30    | 2.03    | 2.08    | 1.63    |         |
| 0708     | 1.18         | 1.57    | 6.47    | 3.35    | 2.08    | 2.11    | 1.70    |         |
| 0758     | 1.24         | 1.62    | 6.42    | 3.41    | 2.14    | 2.17    | 1.75    |         |
| 0848     | 1.25         | 1.67    | 6.36    | 3.46    | 2.23    | 2.21    | 1.80    |         |
| 0938     | 1.35         | 1.72    | 6.31    | 3.52    | 2.25    | 2.24    | 1.85    |         |
| 1028     | 1.37         | 1.73    | 6.27    | 3.55    | 2.27    | 2.27    | 1.88    |         |
| 1118     | 1.38         | 1.74    | 6.25    | 3.57    | 2.28    | 2.28    | 1.89    |         |

Table 13.--Water levels in wells A2, A3, A4, B1, B2, B3, and B4 during well A1 withdrawal test - continued

| Date     | Time<br>(hr) | Well A2 | Well A3 | Well A4 | Well B1 | Well B2 | Well B3 | Well B4 |
|----------|--------------|---------|---------|---------|---------|---------|---------|---------|
| 10-17-74 | 1208         | 1.37    | 1.74    | 6.22    | 3.56    | 2.26    | 2.27    | 1.87    |
|          | 1258         | 1.33    | 1.72    | 6.29    | 3.54    | 2.23    | 2.24    | 1.85    |
|          | 1348         | 1.31    | 1.71    | 6.31    | 3.52    | 2.23    | 2.23    | 1.84    |
|          | 1438         | 1.29    | 1.68    | 6.32    | 3.50    | 2.20    | 2.22    | 1.82    |
|          | 1528         | 1.28    | 1.68    | 6.32    | 3.50    | 2.20    | 2.20    | 1.80    |
|          | 1618         | 1.29    | 1.67    | 6.32    | 3.47    | 2.20    | 2.20    | 1.81    |
|          | 1758         | 1.30    | 1.67    | 6.36    | 3.48    | 2.22    | 2.21    | 1.81    |
|          | 1938         | 1.33    | 1.70    | 6.32    | 3.52    | 2.24    | 2.25    | 1.85    |
|          | 2118         | 1.36    | 1.73    | 6.29    | 3.56    | 2.28    | 2.27    | 1.87    |
|          | 2258         | 1.35    | 1.74    | 6.27    | 3.56    | 2.27    | 2.27    | 1.87    |
|          | 0038         | 1.31    | 1.70    | 6.35    | 3.53    | 2.23    | 2.22    | 1.83    |
|          | 0218         | 1.28    | 1.65    | 6.35    | 3.49    | 2.20    | 2.20    | 1.80    |
| 10-18-74 | 0358         | 1.27    | 1.64    | 6.36    | 3.47    | 2.20    | 2.19    | 1.79    |
|          | 0538         | 1.29    | 1.66    | 6.37    | 3.48    | 2.22    | 2.22    | 1.80    |
|          | 0718         | 1.36    | 1.72    | 6.31    | 3.53    | 2.29    | 2.29    | 1.87    |
|          | 0838         | 1.44    | 1.79    | 6.22    | 3.58    | 2.39    | 2.36    | 1.93    |

Table 14.--Water levels in well B5 during well A1 withdrawal test

[Test began October 16, 1974 at 2338 hours and ended October 18, 1974 at 0838 hours. Discharge of well A1 was 5,000 gallons per minute.]

| Time<br>(hr) | Water level<br>(ft below<br>measuring<br>point) | Time<br>(hr) | Water level<br>(ft below<br>measuring<br>point) |
|--------------|---|--------------|---|
| 10-16-74     |   |              |   |
| 2200         | 5.48  | 1030         | 5.53  |
| 2215         | 5.49  | 1200         | 5.56  |
| 2230         | 5.49  | 1221         | 5.55  |
| 2245         | 5.48  | 1245         | 5.55  |
| 2300         | 5.49  | 1330         | 5.55  |
| 2315         | 5.49  | 1430         | 5.54  |
| 2330         | 5.48  | 1530         | 5.51  |
| 2338         | 5.49  | 1630         | 5.49  |
| 2340         | 5.48  | 1725         | 5.52  |
| 2341         | 5.50  | 1935         | 5.52  |
| 2342         | 5.50  | 2035         | 5.53  |
| 2343         | 5.49  | 2304         | 5.52  |
| 2344         | 5.49  | 10-18-74     |   |
| 2345         | 5.49  | 0020         | 5.49  |
| 2346         | 5.49  | 0106         | 5.48  |
| 2347         | 5.49  | 0238         | 5.47  |
| 2350         | 5.49  | 0321         | 5.48  |
| 2355         | 5.48  | 0436         | 5.48  |
| 2400         | 5.48  | 0547         | 5.49  |
| 10-17-74     |   | 0644         | 5.51  |
| 0005         | 5.48  | 0730         | 5.51  |
| 0010         | 5.46  | 0827         | 5.52  |
| 0035         | 5.46  | 0910         | 5.53  |
| 0043         | 5.41  | 0955         | 5.53  |
| 0216         | 5.41  | 1030         | 5.54  |
| 0344         | 5.43  | 1058         | 5.55  |
| 0445         | 5.45  | 1130         | 5.55  |
| 0525         | 5.45  | 1248         | 5.55  |
| 0708         | 5.49  | 1507         | 5.53  |
| 0838         | 5.51  |              |   |

Table 15.--Bottom-hole pressure in well A1 during well A1 injection test

[Test began October 30, 1974 at 1547 hours and ended November 3, 1974 at 1607 hours. Average rate of injection in well A1 was 4,350 gallons per minute. Pressure measured at a depth of 958 feet in casing.]

| Time<br>(hr) | Bottom-hole<br>pressure (ft<br>of water above<br>mean sea level) | Time<br>(hr) | Bottom-hole<br>pressure (ft<br>of water above<br>mean sea level) |
|--------------|--|--------------|--|
| 10-30-74     |  | 1907         | 24.40  |
| 1505         | 20.83  | 1927         | 24.68  |
| 1515         | 20.83  | 1947         | 24.90  |
| 1534         | 20.73  | 2007         | 24.96  |
| 1545         | 20.72  | 2027         | 25.02  |
| 1546         | 20.73  | 2047         | 25.07  |
| 1547         | 20.78  | 2107         | 25.13  |
| 1548         | 24.12  | 2127         | 25.22  |
| 1549         | 24.18  | 2147         | 25.24  |
| 1550         | 24.18  | 2207         | 25.29  |
| 1552         | 24.18  | 2227         | 25.28  |
| 1553         | 24.16  | 2247         | 25.35  |
| 1554         | 24.12  | 2347         | 25.46  |
| 1555         | 24.12  | 10-31-74     |  |
| 1556         | 24.11  | 0007         | 25.46  |
| 1557         | 24.01  | 0027         | 25.40  |
| 1559         | 24.07  | 0047         | 25.40  |
| 1601         | 24.01  | 0107         | 25.35  |
| 1603         | 24.01  | 0127         | 25.29  |
| 1605         | 24.01  | 0147         | 25.24  |
| 1607         | 23.07  | 0237         | 25.02  |
| 1612         | 23.96  | 0327         | 24.79  |
| 1617         | 24.81  | 0417         | 24.68  |
| 1622         | 23.99  | 0507         | 24.59  |
| 1627         | 23.99  | 0647         | 22.62  |
| 1637         | 24.01  | 0737         | 22.59  |
| 1647         | 24.04  | 0827         | 22.62  |
| 1657         | 24.01  | 1007         | 22.96  |
| 1707         | 23.96  | 1147         | 23.90  |
| 1717         | 23.96  | 1300         | 23.90  |
| 1727         | 23.96  | 1400         | 23.85  |
| 1747         | 23.96  | 1500         | 25.57  |
| 1807         | 23.90  | 1600         | 25.24  |
| 1827         | 23.90  | 1700         | 25.13  |
| 1847         | 24.35  | 1800         | 25.13  |

Table 15.--Bottom-hole pressure in well A1 during well A1  
injection test - continued

| Time<br>(hr) | Bottom-hole<br>pressure (ft<br>of water above<br>mean sea level) | Time<br>(hr) | Bottom-hole<br>pressure (ft<br>of water above<br>mean sea level) |
|--------------|--|--------------|--|
| 1900         | 25.13  | 0700         | 25.63  |
| 2000         | 25.79  | 0800         | 24.96  |
| 2100         | 26.13  | 0900         | 24.12  |
| 2200         | 26.24  | 1000         | 24.24  |
| 2300         | 26.63  | 1100         | 23.78  |
| 2400         | 26.80  | 1200         | 25.40  |
| 11-1-74      |  | 1300         | 26.35  |
| 0100         | 26.74  | 1400         | 26.52  |
| 0200         | 26.46  | 1500         | 26.63  |
| 0300         | 26.24  | 1600         | 26.57  |
| 0400         | 26.13  | 1700         | 26.52  |
| 0500         | 25.74  | 1800         | 26.24  |
| 0600         | 25.47  | 1900         | 26.02  |
| 0700         | 25.29  | 2000         | 26.13  |
| 0800         | 25.29  | 2100         | 26.57  |
| 0900         | 25.24  | 2200         | 26.80  |
| 1000         | 25.40  | 2300         | 26.90  |
| 1100         | 26.91  | 2400         | 27.07  |
| 1200         | 26.80  | 11-3-74      |  |
| 1300         | 26.85  | 0100         | 27.13  |
| 1400         | 26.80  | 0200         | 26.91  |
| 1500         | 26.81  | 0300         | 27.02  |
| 1600         | 26.68  | 0400         | 26.85  |
| 1700         | 26.46  | 0500         | 26.52  |
| 1800         | 26.24  | 0600         | 26.18  |
| 2000         | 26.68  | 0700         | 26.02  |
| 2100         | 26.91  | 0800         | 25.85  |
| 2300         | 27.02  | 0900         | 25.85  |
| 2400         | 25.07  | 1000         | 25.85  |
| 11-2-74      |  | 1100         | 25.85  |
| 0107         | 26.57  | 1200         | 26.07  |
| 0200         | 26.57  | 1300         | 26.74  |
| 0300         | 26.46  | 1400         | 27.24  |
| 0400         | 26.35  | 1500         | 27.41  |
| 0500         | 26.02  | 1600         | 27.41  |
| 0600         | 25.79  | 1607         | 27.35  |

Table 16.—Water levels in wells A<sub>2</sub>, A<sub>3</sub>, A<sub>4</sub>, B<sub>1</sub>, B<sub>2</sub>, B<sub>3</sub> and B<sub>4</sub> during well A<sub>1</sub> injection test[Test began October 30, 1974 at 1547 hours and ended November 3, 1974 at 1607 hours. Average rate of injection in well A<sub>1</sub> was 4,350 gallons per minute.]

| Date     | Time<br>(hr) | Well A <sub>2</sub>  |   |   | Well A <sub>3</sub>                         |   |   | Well A <sub>4</sub>                         |   |   | Well B <sub>1</sub>                         |   |   | Well B <sub>2</sub>                         |   |   | Well B <sub>3</sub>                         |   |   | Well B <sub>4</sub> |  |  |
|----------|--------------|--|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---------------------|--|--|
|          |              | water level<br>(ft above (+)<br>and below (-)<br>mean sea level) | water level<br>(ft below<br>mean sea level) | water level<br>(ft below<br>mean sea level) | water level<br>(ft above<br>mean sea level) | water level<br>(ft below<br>mean sea level) | water level<br>(ft below<br>mean sea level) | water level<br>(ft above<br>mean sea level) | water level<br>(ft below<br>mean sea level) |                     |  |  |
| 10-30-74 | 1400         | -1.18  | 1.89  | 6.40  | 3.27  | 1.93  | 1.89  | 1.62  | 3.27  | 1.93  | 1.89  | 1.62  | 1.62  | 1.62  | 1.62  | 1.62  | 1.62  | 1.62  | 1.62  |                     |  |  |
|          | 1415         | -1.18  | 1.90  | 6.38  | 3.29  | 1.94  | 1.90  | 1.63  | 3.29  | 1.94  | 1.90  | 1.63  | 1.63  | 1.63  | 1.63  | 1.63  | 1.63  | 1.63  | 1.63  |                     |  |  |
|          | 1430         | -1.19  | 1.91  | 6.36  | 3.30  | 1.95  | 1.90  | 1.64  | 3.30  | 1.95  | 1.90  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  |                     |  |  |
|          | 1445         | -1.20  | 1.91  | 6.34  | 3.31  | 1.96  | 1.91  | 1.64  | 3.31  | 1.96  | 1.91  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  |                     |  |  |
|          | 1500         | -1.20  | 1.92  | 6.33  | 3.32  | 1.96  | 1.92  | 1.64  | 3.32  | 1.96  | 1.92  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  |                     |  |  |
|          | 1515         | -1.25  | 1.92  | 6.31  | 3.32  | 1.96  | 1.92  | 1.64  | 3.32  | 1.96  | 1.92  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  |                     |  |  |
|          | 1530         | -1.25  | 1.93  | 6.29  | 3.33  | 1.96  | 1.92  | 1.64  | 3.33  | 1.96  | 1.92  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  |                     |  |  |
|          | 1545         | -1.26  | 1.94  | 6.28  | 3.33  | 1.96  | 1.92  | 1.64  | 3.33  | 1.96  | 1.92  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  |                     |  |  |
|          | 1547         | -1.26  | 1.94  | 6.27  | 3.33  | 1.96  | 1.92  | 1.64  | 3.33  | 1.96  | 1.92  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  |                     |  |  |
|          | 1548         | -1.25  | 1.94  | 6.26  | 3.33  | 1.96  | 1.92  | 1.64  | 3.33  | 1.96  | 1.92  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  |                     |  |  |
|          | 1549         | -1.15  | 1.90  | 6.26  | 3.33  | 1.83  | 1.80  | 1.64  | 3.33  | 1.83  | 1.80  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  |                     |  |  |
|          | 1550         | -1.00  | 1.85  | 6.26  | 3.33  | 1.79  | 1.73  | 1.64  | 3.33  | 1.79  | 1.73  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  |                     |  |  |
|          | 1551         | - .99  | 1.83  | 6.26  | 3.32  | 1.75  | 1.70  | 1.64  | 3.32  | 1.75  | 1.70  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  |                     |  |  |
|          | 1552         | - .98  | 1.82  | 6.27  | 3.32  | 1.72  | 1.68  | 1.64  | 3.32  | 1.72  | 1.68  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  |                     |  |  |
|          | 1553         | - .96  | 1.81  | 6.27  | 3.32  | 1.72  | 1.68  | 1.64  | 3.32  | 1.72  | 1.68  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  |                     |  |  |
|          | 1554         | - .96  | 1.80  | 6.27  | 3.32  | 1.71  | 1.67  | 1.64  | 3.32  | 1.71  | 1.67  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  |                     |  |  |
|          | 1555         | - .95  | 1.79  | 6.27  | 3.32  | 1.70  | 1.66  | 1.64  | 3.32  | 1.70  | 1.66  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  |                     |  |  |
|          | 1556         | - .95  | 1.78  | 6.27  | 3.31  | 1.70  | 1.66  | 1.64  | 3.31  | 1.70  | 1.66  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  |                     |  |  |
|          | 1557         | - .94  | 1.76  | 6.28  | 3.31  | 1.69  | 1.65  | 1.64  | 3.31  | 1.69  | 1.65  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  |                     |  |  |
|          | 1602         | - .92  | 1.73  | 6.29  | 3.29  | 1.68  | 1.63  | 1.64  | 3.29  | 1.68  | 1.63  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  |                     |  |  |
|          | 1607         | - .90  | 1.71  | 6.31  | 3.27  | 1.67  | 1.62  | 1.64  | 3.27  | 1.67  | 1.62  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  |                     |  |  |
|          | 1612         | - .89  | 1.69  | 6.33  | 3.26  | 1.66  | 1.61  | 1.64  | 3.26  | 1.66  | 1.61  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  |                     |  |  |
|          | 1617         | - .89  | 1.68  | 6.34  | 3.25  | 1.65  | 1.60  | 1.64  | 3.25  | 1.65  | 1.60  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  |                     |  |  |
|          | 1622         | - .88  | 1.67  | 6.36  | 3.23  | 1.64  | 1.59  | 1.64  | 3.23  | 1.64  | 1.59  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  |                     |  |  |
|          | 1627         | - .87  | 1.66  | 6.37  | 3.22  | 1.64  | 1.58  | 1.64  | 3.22  | 1.64  | 1.58  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  |                     |  |  |
|          | 1632         | - .87  | 1.65  | 6.39  | 3.22  | 1.63  | 1.58  | 1.64  | 3.22  | 1.63  | 1.58  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  |                     |  |  |
|          | 1637         | - .86  | --  | 6.40  | 3.21  | 1.63  | 1.57  | 1.64  | 3.21  | 1.63  | 1.57  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  |                     |  |  |
|          | 1647         | - .85  | 1.63  | 6.43  | 3.19  | 1.62  | 1.57  | 1.64  | 3.19  | 1.62  | 1.57  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  | 1.64  |                     |  |  |

Table 16.--Water levels in wells A2, A3, A4, B1, B2, B3 and B4 during well A1 injection test - continued

| Date | Time<br>(hr) | Well A2<br>water level<br>(ft above (+)<br>and below (-)<br>mean sea level) | Well A3<br>water level<br>(ft below<br>mean sea level) | Well A4<br>water level<br>(ft above<br>mean sea level) | Well B1<br>water level<br>(ft below<br>mean sea level) | Well B2<br>water level<br>(ft below<br>mean sea level) | Well B3<br>water level<br>(ft below<br>mean sea level) | Well B4<br>water level<br>(ft below<br>mean sea level) |
|------|--------------|---|--|--|--|--|--|--|
| 48   | 10-30-74     | 1657  | -0.84  | 1.62   | 6.46   | 3.18   | 1.61   | 1.37   |
|      | 1707         | -.84  | 1.61   | 6.48   | 3.17   | 1.61   | 1.36   |  |
|      | 1717         | -.83  | 1.60   | 6.50   | 3.16   | 1.60   | 1.35   |  |
|      | 1727         | -.82  | 1.59   | 6.52   | 3.15   | 1.60   | 1.34   |  |
|      | 1817         | -.80  | 1.56   | 6.57   | 3.14   | 1.58   | 1.33   |  |
|      | 1907         | -.76  | 1.54   | 6.60   | 3.13   | 1.58   | 1.31   |  |
|      | 1957         | -.72  | 1.52   | 6.63   | 3.11   | 1.55   | 1.29   |  |
|      | 2047         | -.68  | 1.49   | 6.65   | 3.09   | 1.53   | 1.27   |  |
|      | 2137         | -.64  | 1.46   | 6.69   | 3.06   | 1.50   | 1.24   |  |
|      | 2227         | -.60  | 1.43   | 6.73   | 3.03   | 1.46   | 1.21   |  |
|      | 2317         | -.58  | 1.40   | 6.77   | 3.00   | 1.44   | 1.18   |  |
|      | 0007         | -.56  | 1.39   | 6.79   | 2.97   | 1.42   | 1.14   |  |
|      | 0147         | -.53  | 1.38   | 6.82   | 2.94   | 1.42   | 1.12   |  |
|      | 0327         | -.53  | 1.39   | 6.82   | 2.95   | 1.46   | 1.14   |  |
|      | 0507         | -.57  | 1.45   | 6.77   | 3.01   | 1.54   | 1.21   |  |
|      | 0647         | -.74  | 1.62   | 6.66   | 3.13   | 1.71   | 1.36   |  |
|      | 0827         | -.74  | 1.69   | 6.53   | 3.22   | 1.76   | 1.42   |  |
|      | 1647         | -.36  | 1.48   | 6.60   | 3.08   | 1.54   | 1.24   |  |
| 48   | 11- 1-74     | 0107  | +.02   | 1.28   | 6.87   | 2.94   | 1.41   | 1.11   |
|      |              | 0927  | -.04   | 1.55   | 6.49   | 3.22   | 1.68   | 1.39   |
|      |              | 1747  | +.25   | 1.46   | 6.56   | 3.11   | 1.61   | 1.30   |
|      | 11- 2-74     | 0207  | +.59   | 1.29   | 6.77   | 3.01   | 1.99   | 1.15   |
|      |              | 1027  | +.42   | 1.61   | 6.43   | 3.32   | 1.89   | 1.49   |
| 48   | 11- 3-74     | 1847  | +.82   | 1.40   | 6.61   | 3.16   | 1.65   | 1.32   |
|      |              | 0307  | +1.16  | 1.20   | 6.80   | 3.03   | 1.52   | 1.15   |
|      |              | 1607  | +1.31  | 1.24   | 6.70   | 3.12   | 1.60   | 1.43   |

Table 17.--Summary of geophysical logs of well El

[Logs are on file in the U.S. Geological Survey Southwest Florida Sub-district Office, Tampa, Florida.]

| Date    | Log   | Depth interval (ft) | Logged by                    |
|---------|---|---------------------|------------------------------|
| 2/ 6/73 | Caliper   | 0- 430              | U.S.G.S., Tampa              |
| 2/ 6/73 | Single point resistance and spontaneous potential           | 0- 430              | U.S.G.S., Tampa              |
| 2/ 6/73 | Specific conductance  | 0- 430              | U.S.G.S., Tampa              |
| 2/ 6/73 | Gamma   | 0- 430              | U.S.G.S., Tampa              |
| 5/11/73 | Caliper   | 260-2160            | U.S.G.S., Lakewood, Colorado |
| 5/11/73 | Long and short normal resistivity and spontaneous potential | 374-2160            | U.S.G.S., Lakewood, Colorado |
| 5/11/73 | Flowmeter   | 0-2160              | U.S.G.S., Lakewood, Colorado |
| 5/11/73 | Gamma   | 0-2160              | U.S.G.S., Lakewood, Colorado |
| 5/11/73 | Gamma-Gamma   | 1200-2160           | U.S.G.S., Lakewood, Colorado |
| 5/11/73 | Neutron   | 0-2160              | U.S.G.S., Lakewood, Colorado |
| 5/11/73 | Temperature - pumping                                       | 50-2160             | U.S.G.S., Lakewood, Colorado |
| 3/25/74 | Caliper   | 1884-3260           | U.S.G.S., Tampa              |
| 3/26/74 | Temperature - static  | 1600-3260           | U.S.G.S., Tampa              |
| 3/26/74 | Temperature - pumping                                       | 1700-3260           | U.S.G.S., Tampa              |
| 3/26/74 | Single point resistance spontaneous potential               | 1780-3260           | U.S.G.S., Tampa              |
| 6/11/74 | Cement bond   | 100-1590            | Schlumberger <sup>1/</sup>   |

1/ The use of brand names in this report is for identification purposes only and does not imply endorsement by the U.S. Geological Survey.

Table 18.--Summary of geophysical logs of well Al

[Logs are on file in the U.S. Geological Survey Southwest Florida Sub-district Office, Tampa, Florida.]

| Date     | Log                     | Depth interval (ft) | Logged by       |
|----------|-------------------------|---------------------|-----------------|
| 6/11/74  | Cement bond             | 370- 970            | Schlumberger    |
| 10/24/74 | Temperature - static    | 940-1080            | U.S.G.S., Tampa |
| 10/28/74 | Temperature - injection | 960-1080            | U.S.G.S., Tampa |
| 10/28/74 | Flowmeter               | 940-1080            | U.S.G.S., Tampa |
| 12/23/74 | Temperature - static    | 40-1080             | U.S.G.S., Tampa |
| 1/23/75  | Caliper                 | 920-1080            | U.S.G.S., Tampa |
| 4/ 9/75  | Temperature - static    | 0-1080              | U.S.G.S., Tampa |
| 8/ 8/75  | Temperature - static    | 80-1070             | U.S.G.S., Tampa |
| 10/ 1/75 | Temperature - static    | 200-1060            | U.S.G.S., Tampa |

Table 19.--Summary of geophysical logs of wells A2, A3 and A4

[Logs are on file in the U.S. Geological Survey Southwest Florida Sub-district Office, Tampa, Florida.]

| Well | Date     | Log                                  | Depth interval (ft) | Logged by   |
|------|----------|--------------------------------------|---------------------|-------------|
| A2   | 9/21/74  | Microseismogram                      | 50-103              | Welex, Inc. |
| A2   | 9/22/74  | Lateral and short normal resistivity | 100-743             | Welex, Inc. |
| A2   | 9/22/74  | Caliper                              | 50-602              | Welex, Inc. |
| A2   | 9/22/74  | Acoustic velocity                    | 50-602              | Welex, Inc. |
| A2   | 11/20/74 | Cement bond                          | 100-750             | Welex, Inc. |
| A3   | 11/20/74 | Cement bond                          | 50-508              | Welex, Inc. |
| A4   | 11/20/74 | Cement bond                          | 50-200              | Welex, Inc. |

Table 20.—Specific conductance and chloride concentration of water from exploratory well E1

| DATE              | TIME | DEPTH<br>OF<br>SAMPLE<br>INTER-<br>VAL<br>(FT) | DEPTH<br>TO TOP<br>OF<br>SAMPLE<br>INTER-<br>VAL<br>(FT) | SPE-<br>CIFIC<br>COND-<br>DUCT-<br>ANCE<br>(CL) | DIS-<br>SOLVENT<br>CHLO-<br>RIDE<br>(MG/L) | EXPLORATORY HOLE (LAT 27 49 ?? LONG 082 44 31)               |             |                 |
|-------------------|------|--|--|---|--|--|-------------|-----------------|
|                   |      |  |  |   |  | DEPTH<br>TO BOT-<br>OM OF<br>SAMPLE<br>INTER-<br>VAL<br>(FT) | VAL<br>(FT) | MICRO-<br>MHOES |
| <b>FEB • 1973</b> |      |  |  |   |  |  |             |                 |
| 14•••             | 1830 | 374  | 490  | 44400   | 16000                                      |  |             |                 |
| 15•••             | 0900 | 374  | 500  | 45800   | 17000                                      |  |             |                 |
| 15•••             | 1000 | 374  | 520  | 45200   | 16000                                      |  |             |                 |
| 15•••             | 1045 | 374  | 540  | 45200   | 17000                                      |  |             |                 |
| 15•••             | 1100 | 374  | 560  | 45000   | 16000                                      |  |             |                 |
| 15•••             | 1430 | 374  | 580  | 45800   | 17000                                      |  |             |                 |
| 15•••             | 1500 | 374  | 585  | 46600   | 17000                                      |  |             |                 |
| 15•••             | 1545 | 374  | 600  | 45200   | 17000                                      |  |             |                 |
| 16•••             | 0900 | 374  | 620  | 46000   | 17000                                      |  |             |                 |
| 16•••             | 1030 | 374  | 640  | 46200   | 17000                                      |  |             |                 |
| 16•••             | 1103 | 374  | 660  | 47000   | 17000                                      |  |             |                 |
| 16•••             | 1230 | 374  | 680  | 47000   | 17000                                      |  |             |                 |
| 16•••             | 1350 | 374  | 700  | 48000   | 18000                                      |  |             |                 |
| 16•••             | 1510 | 374  | 720  | 48000   | 17000                                      |  |             |                 |
| 16•••             | 1645 | 374  | 740  | 48000   | 18000                                      |  |             |                 |
| 18•••             | 1200 | 374  | 760  | 50000   | 19000                                      |  |             |                 |
| 21•••             | 0950 | 374  | 780  | 51000   | 19000                                      |  |             |                 |
| <b>MAR</b>        |      |  |  |   |  |  |             |                 |
| 03•••             | 0905 | 374  | 800  | 50000   | 19000                                      |  |             |                 |
| 04•••             | 1155 | 374  | 820  | 50000   | 18000                                      |  |             |                 |
| 07•••             | --   | 374  | 840  | 51000   | 20000                                      |  |             |                 |
| 12•••             | --   | 374  | 860  | 52000   | 19000                                      |  |             |                 |
| 14•••             | --   | 374  | 900  | 51000   | 19000                                      |  |             |                 |
| 14•••             | --   | 374  | 920  | 48000   | 18000                                      |  |             |                 |
| 15•••             | --   | 374  | 940  | 52000   | 20000                                      |  |             |                 |
| 16•••             | --   | 374  | 960  | 52000   | 20000                                      |  |             |                 |
| <b>APR</b>        |      |  |  |   |  |  |             |                 |
| 10•••             | 0700 | 374  | 1000   | 52000   | 19000                                      |  |             |                 |
| 10•••             | 0715 | 374  | 1020   | 52000   | 19000                                      |  |             |                 |
| 10•••             | 0730 | 374  | 1040   | 53000   | 19000                                      |  |             |                 |
| 10•••             | 0745 | 374  | 1060   | 53000   | 19000                                      |  |             |                 |
| 10•••             | 0800 | 374  | 1080   | 53000   | 19000                                      |  |             |                 |
| 10•••             | 0815 | 374  | 1100   | 53000   | 19000                                      |  |             |                 |
| 11•••             | 0820 | 374  | 1120   | 52000   | 19000                                      |  |             |                 |
| 11•••             | 0830 | 374  | 1140   | 52500   | 19000                                      |  |             |                 |
| 11•••             | 0845 | 374  | 1160   | 52500   | 19000                                      |  |             |                 |

Table 20.--Specific conductance and chloride concentration of water from exploratory well El - continued

| WELL NUMBER F1 |              | EXPLORATORY HOLE (LAT 27 49 22 LONG 082 44 31)           |   |  |   |   |   |
|----------------|--------------|--|---|--|---|---|---|
| DATE           | TIME<br>(FT) | DEPTH<br>TO TOP<br>OF<br>SAMPLE<br>INTER-<br>VAL<br>(FT) | DEPTH<br>TO BOTTOM<br>OF<br>SAMPLE<br>INTER-<br>VAL<br>(FT) | SPEC-<br>IFIC<br>COND.<br>DUCT-<br>ANCE<br>(MICRO-<br>MHOES) | SPEC-<br>IFIC<br>COND.<br>DUCT-<br>ANCE<br>(CL)<br>(MG/L) | DIS-<br>SOLVED<br>CHLOR-<br>IDE<br>(CL) | DIS-<br>SOLVED<br>CHLOR-<br>IDE<br>(MG/L) |
| APR 1973       |              |  |   |  |   |   |   |
| 11...0         | 0900         | 374  | 1180  | 52500  | 19000   | 52500                                   | 19000                                     |
| 11...0         | 0930         | 374  | 1220  | 52500  | 19000   | 52500                                   | 19000                                     |
| 11...5         | 0945         | 374  | 1240  | 52500  | 19000   | 52500                                   | 19000                                     |
| 11...0         | 1000         | 374  | 1260  | 53000  | 19000   | 53000                                   | 19000                                     |
| 11...5         | 1015         | 374  | 1280  | 53000  | 19000   | 53000                                   | 19000                                     |
| 12...0         | 1030         | 374  | 1300  | 53000  | 19000   | 53000                                   | 19000                                     |
| 12...5         | 1045         | 374  | 1320  | 53000  | 19000   | 53000                                   | 19000                                     |
| 12...0         | 1100         | 374  | 1340  | 53000  | 19000   | 53000                                   | 19000                                     |
| 12...5         | 1115         | 374  | 1360  | 53000  | 19000   | 53000                                   | 19000                                     |
| 12...0         | 1130         | 374  | 1380  | 53000  | 19000   | 53000                                   | 19000                                     |
| 13...0         | 1145         | 374  | 1400  | 53000  | 19000   | 53000                                   | 19000                                     |
| 13...5         | 1200         | 374  | 1420  | 53000  | 19000   | 53000                                   | 19000                                     |
| 13...0         | 1215         | 374  | 1440  | 53000  | 19000   | 53000                                   | 19000                                     |
| 15...0         | 1300         | 374  | 1460  | 53500  | 19000   | 53500                                   | 19000                                     |
| 15...5         | 1315         | 374  | 1480  | 53500  | 19000   | 53500                                   | 19000                                     |
| 15...0         | 1330         | 374  | 1500  | 53500  | 19000   | 53500                                   | 19000                                     |
| 16...0         | --           | 374  | 1540  | 53000  | 20000   | 53000                                   | 20000                                     |
| 16...5         | 1000         | 374  | 1560  | 51500  | 20000   | 51500                                   | 20000                                     |
| 17...0         | --           | 374  | 1580  | 56000  | 20000   | 56000                                   | 20000                                     |
| 18...0         | --           | 374  | 1600  | 55000  | 20000   | 55000                                   | 20000                                     |
| 18...5         | 0800         | 374  | 1620  | 57000  | 20000   | 57000                                   | 20000                                     |
| 18...0         | 0900         | 374  | 1640  | 57000  | 20000   | 58000                                   | 20000                                     |
| 19...0         | 1000         | 374  | 1660  | 57000  | 20000   | 58000                                   | 20000                                     |
| 23...0         | --           | 374  | 1680  | 58000  | 20000   | 58000                                   | 20000                                     |
| 23...5         | 0900         | 374  | 1700  | 58000  | 20000   | 59000                                   | 21000                                     |
| 24...0         | --           | 374  | 1720  | 58000  | 20000   | 58000                                   | 20000                                     |
| 24...5         | 1300         | 374  | 1740  | 58000  | 20000   | 57000                                   | 20000                                     |
| 24...0         | 1400         | 374  | 1760  | 58000  | 20000   | 58000                                   | 20000                                     |
| 24...5         | 1500         | 374  | 1780  | 58000  | 20000   | 58000                                   | 20000                                     |
| 25...0         | --           | 374  | 1800  | 58000  | 20000   | 59000                                   | 21000                                     |
| 25...5         | 1100         | 374  | 1820  | 59000  | 21000   | 59000                                   | 21000                                     |
| 25...0         | 1200         | 374  | 1840  | 57000  | 20000   | 57000                                   | 20000                                     |
| 25...5         | 1300         | 374  | 1860  | 57000  | 20000   | 58000                                   | 20000                                     |
| 26...0         | --           | 374  | 1880  | 58000  | 20000   | 58000                                   | 20000                                     |
| 27...0         | --           | 374  | 1900  | 58000  | 20000   | 58000                                   | 20000                                     |
| 27...5         | 0900         | 374  | 1920  | 58000  | 20000   | 58000                                   | 20000                                     |
| 27...0         | 1000         | 374  | 1940  | 58000  | 20000   | 58000                                   | 20000                                     |

Table 20.—Specific conductance and chloride concentration of water from exploratory well E1 - continued

| DATE           | TIME | DEPTH<br>TO TOP<br>OF<br>SAMPLE<br>INTER-<br>VAL<br>(FT) | DEPTH<br>TO BOT-<br>OM OF<br>SAMPLE<br>INTER-<br>VAL<br>(FT) | SPECI-<br>CIFIC<br>COND-<br>DUCT-<br>ANCE<br>(MICRO-<br>MHOES) | DIS-<br>SOLVED<br>CHLO-<br>RIDE<br>(CL)<br>(MG/L) |
|----------------|------|--|--|--|---|
|                |      |  |  |  | EXPLORATORY HOLE (LAT 27 49 22 LONG 082 44 31)    |
| MAY 1 1973     |      |  |  |  |   |
| 01... 0900     | 374  | 1980   | 59000  | 20000  |   |
| 01... 0900     | 374  | 2000   | 58000  | 20000  |   |
| 01... 1000     | 374  | 2020   | 59000  | 20000  |   |
| 02... 0700     | 374  | 2040   | 58000  | 20000  |   |
| 02... 0730     | 374  | 2060   | 57000  | 20000  |   |
| 02... 0800     | 374  | 2080   | 55000  | 20000  |   |
| 02... 0830     | 374  | 2100   | 60000  | 23000  |   |
| 02... 0900     | 374  | 2120   | 60000  | 22000  |   |
| 02... 1000     | 374  | 2140   | 55000  | 21000  |   |
| 02... 1030     | 374  | 2160   | 55000  | 21000  |   |
| 02... 1100     | 374  | 2178   | 55000  | 20000  |   |
| JUL 11... 1345 | 1863 | 2178   | 58000  | 24600  |   |
| AUG 08... 0900 | 1863 | 2200   | 66000  | 25000  |   |
| 08... 0930     | 1863 | 2220   | 66000  | 25000  |   |
| 08... 0900     | 1863 | 2240   | 65000  | 24000  |   |
| 08... 0930     | 1863 | 2260   | 73000  | 27000  |   |
| 08... 1000     | 1863 | 2280   | 73000  | 27000  |   |
| 08... 1030     | 1863 | 2300   | 73000  | 27000  |   |
| 08... 1100     | 1863 | 2320   | 75000  | 27000  |   |
| 08... 1130     | 1863 | 2340   | 75000  | 27000  |   |
| 08... 1200     | 1863 | 2360   | 75000  | 27000  |   |
| 08... 1230     | 1863 | 2380   | 75000  | 27000  |   |
| 08... 1300     | 1863 | 2400   | 75000  | 28000  |   |
| 08... 1313     | 1863 | 2420   | 76000  | 28000  |   |
| 08... 1330     | 1863 | 2440   | 76000  | 28000  |   |
| 08... 0830     | 1863 | 2460   | 76000  | 28000  |   |
| 14... 0900     | 1863 | 2480   | 75000  | 28000  |   |
| 14... 0930     | 1863 | 2500   | 75000  | 28000  |   |
| 14... 1000     | 1863 | 2520   | 68000  | 28000  |   |
| 15... 1030     | 1863 | 2540   | 69000  | 28000  |   |
| 15... 1100     | 1863 | 2560   | 68000  | 26000  |   |
| 15... 1130     | 1863 | 2580   | 71000  | 28000  |   |
| 15... 1150     | 1863 | 2600   | 71000  | 28000  |   |
| 15... 1150     | 1863 | 2620   | 71000  | 28000  |   |
| 15... 1150     | 1863 | 2640   | 71000  | 28000  |   |

Table 20.—Specific conductance and chloride concentration of water from exploratory well El - continued

| DATE<br>(FT) | TIME<br>(FT) | WELL NUMBER F1  |  | EXPLORATORY HOLE (LAT 27 49 22 LONG 082 44 31) |  |   |   |   |   |
|--------------|--------------|---|--|--|--|---|---|---|---|
|              |              | DEPTH<br>TO TOP<br>OF<br>SAMPLE<br>TUBE—<br>VAL<br>(FT) | DEPTH<br>TO BOTTOM<br>OF<br>SAMPLE<br>TUBE—<br>VAL<br>(FT) | SPECIFIC<br>COND.<br>DUCT-<br>ANCE<br>(CL)     | SPECIFIC<br>COND.<br>DUCT-<br>ANCE<br>(MG/L) | DIS-<br>SOLVED<br>CHLO-<br>RIDE<br>(MG/L) | DIS-<br>SOLVED<br>CHLO-<br>RIDE<br>(MG/L) | DIS-<br>SOLVED<br>CHLO-<br>RIDE<br>(MG/L) | DIS-<br>SOLVED<br>CHLO-<br>RIDE<br>(MG/L) |
| AUG • 1973   |              | 1863  | 2660   | 71000  | 28000  |   |   |   |   |
| 15•••        | 1130         | 1863  | 2680   | 71000  | 28000  |   |   |   |   |
| 15•••        | 1200         | 1863  | 2700   | 71000  | 28000  |   |   |   |   |
| 15•••        | 1230         | 1863  | 2720   | 69000  | 27000  |   |   |   |   |
| 15•••        | 1300         | 1863  | 2740   | 69000  | 27000  |   |   |   |   |
| 15•••        | 1330         | 1863  | 2760   | 70000  | 27000  |   |   |   |   |
| 15•••        | 1400         | 1863  | 2780   | 70000  | 27000  |   |   |   |   |
| 15•••        | 1430         | 1863  | 2800   | —  | 31000  |   |   |   |   |
| 15•••        | 1500         | 1863  | 2820   | 70000  | 28000  |   |   |   |   |
| 15•••        | 1530         | 1863  | 2840   | 74000  | 28000  |   |   |   |   |
| 21•••        | 0800         | 1863  | 2860   | 70000  | 27000  |   |   |   |   |
| 21•••        | 0900         | 1863  | 2880   | 70000  | 27000  |   |   |   |   |
| 21•••        | 1000         | 1863  | 2900   | 70000  | 26000  |   |   |   |   |
| 21•••        | 1030         | 1863  | 2920   | 70000  | 28000  |   |   |   |   |
| 21•••        | 1100         | 1863  | 2940   | 69000  | 29000  |   |   |   |   |
| 21•••        | 1130         | 1863  | 2960   | 72000  | 27000  |   |   |   |   |
| 21•••        | 1200         | 1863  | 2980   | 70000  | 31000  |   |   |   |   |
| 21•••        | 1300         | 1863  | 2980   | 70000  | 31000  |   |   |   |   |
| SEP          |              |   |  |  |  |   |   |   |   |
| 20•••        | 0400         | 1863  | 3000   | 72500  | 28000  |   |   |   |   |
| 20•••        | 0430         | 1863  | 3020   | 72500  | 28000  |   |   |   |   |
| 20•••        | 0900         | 1863  | 3040   | 72500  | 28000  |   |   |   |   |
| 20•••        | 0930         | 1863  | 3060   | 72500  | 29000  |   |   |   |   |
| 20•••        | 1000         | 1863  | 3080   | 72500  | 29000  |   |   |   |   |
| 20•••        | 1030         | 1863  | 3100   | 72500  | 29000  |   |   |   |   |
| 20•••        | 1100         | 1863  | 3120   | 72500  | 28000  |   |   |   |   |
| 20•••        | 1130         | 1863  | 3140   | 72000  | 30000  |   |   |   |   |
| OCT          |              |   |  |  |  |   |   |   |   |
| 18•••        | 0800         | 1863  | 3160   | 70000  | 28000  |   |   |   |   |
| 18•••        | 0900         | 1863  | 3180   | 70000  | 28000  |   |   |   |   |
| 18•••        | 1000         | 1863  | 3200   | 71000  | 28000  |   |   |   |   |
| 18•••        | 1100         | 1863  | 3220   | 71000  | 28000  |   |   |   |   |
| 18•••        | 1200         | 1863  | 3240   | 71000  | 28000  |   |   |   |   |
| 18•••        | 1300         | 1863  | 3260   | 72000  | 28000  |   |   |   |   |
| JAN • 1974   |              |   |  |  |  |   |   |   |   |
| 09•••        | 1425         | 1863  | 3280   | 49000  | 19000  |   |   |   |   |
| 09•••        | 1440         | 1863  | 3280   | 66000  | 26000  |   |   |   |   |
| 09•••        | 1451         | 1863  | 3280   | 68000  | 27000  |   |   |   |   |

Table 20.—Specific conductance and chloride concentration of water from exploratory well E1 - continued

| DATE       | TIME | DEPTH<br>TO TOP<br>OF<br>SAMPLE<br>INTER-<br>VAL<br>(FT) | DEPTH<br>TO BOT-<br>OM OF<br>SAMPLE<br>INTER-<br>VAL<br>(FT) | SPECI-<br>CIFIC<br>COND-<br>DUCT-<br>ANCE<br>(MHO-<br>MHS) | DIS-<br>SOLVED<br>CHLO-<br>RIDE<br>(CL)<br>(MG/L) |
|------------|------|--|--|--|---|
|            |      |  |  | WELL NUMBER E1   | EXPLORATORY HOLE (LAT 27 49 22 LONG 082 44 31)    |
| JAN 9....  | 1974 | 1502   | 1863   | 3280   | 61000 23000                                       |
| 09.....    |      | 1515   | 1863   | 3280   | 62000 24000                                       |
| 09.....    |      | 1531   | 1863   | 3280   | 68000 27000                                       |
| 09.....    |      | 1547   | 1863   | 3280   | 70000 29000                                       |
| 09.....    |      | 1602   | 1863   | 3280   | 71000 29000                                       |
| 09.....    |      | 1620   | 1863   | 3280   | 70000 28000                                       |
| 09.....    |      | 1633   | 1863   | 3280   | 71000 29000                                       |
| 09.....    |      | 1645   | 1863   | 3280   | 70000 28000                                       |
| MAR 20.... |      | 1700   | 1863   | 3280   | 70100 28000                                       |

Table 21.--Temperature, specific conductance and chloride concentration of water from selected wells at the test site

| DATE   | TIME | TEMPERATURE |            | DEPTH<br>TO<br>TOP<br>OF<br>SAMPLE<br>INTERVAL<br>(FT) | TEMPER-<br>ATURE<br>VAL-<br>(FT) | SPF =<br>CIFIC<br>COND-<br>DUCT-<br>ANCE<br>(MICRO-<br>MHO'S) | DIS-<br>SOLVED<br>CHLO-<br>RIDE<br>(CL)<br>(MG/L) |
|--|------|-------------|------------|--|----------------------------------|---|---|
|  |      | TO<br>20°F  | TO<br>60°F |  |                                  |   |   |
| SO CROSSING WELL (LAT 27°49'29" LONG 082°44'35.01) |      |             |            |  |                                  |   |   |
| OCT 8 1974   |      |             |            |  |                                  |   |   |
| 17.....  | 0040 | 961         | 1080       | 28.0   | --                               | --  | --  |
| 17.....  | 0240 | 961         | 1080       | 27.0   | --                               | --  | --  |
| 17.....  | 0440 | 961         | 1080       | 28.0   | --                               | --  | --  |
| 17.....  | 0640 | 961         | 1080       | 28.0   | --                               | --  | --  |
| 17.....  | 0840 | 961         | 1080       | 28.0   | --                               | --  | --  |
| 17.....  | 1040 | 961         | 1080       | 28.0   | --                               | --  | --  |
| 17.....  | 1240 | 961         | 1080       | 28.5   | --                               | --  | --  |
| 17.....  | 1400 | 961         | 1080       | 28.0   | 50600                            | 20000   |   |
| 17.....  | 1440 | 961         | 1080       | 27.0   | --                               | --  | --  |
| 17.....  | 1640 | 961         | 1080       | 28.5   | --                               | --  | --  |
| 17.....  | 1840 | 961         | 1080       | 27.0   | --                               | --  | --  |
| 17.....  | 2040 | 961         | 1080       | 27.3   | --                               | --  | --  |
| 17.....  | 2240 | 961         | 1080       | 27.0   | --                               | --  | --  |
| 18.....  | 0240 | 961         | 1080       | 28.0   | --                               | --  | --  |
| 18.....  | 0540 | 961         | 1080       | 28.0   | --                               | --  | --  |
| 18.....  | 0840 | 961         | 1080       | --   | 1960                             | 420   |   |
| 18.....  | 1916 | 961         | 1080       | --   | 2050                             | 440   |   |
| 29.....  | 2916 | 961         | 1080       | --   | 1750                             | 390   |   |
| 29.....  | 1750 | 961         | 1080       | --   | 1040                             | 190   |   |
| 30.....  | 0920 | 961         | 1080       | --   | 3980                             | 1100  |   |
| 30.....  | 0955 | 961         | 1080       | --   | 2000                             | 450   |   |
| 30.....  | 1152 | 961         | 1080       | --   | 1750                             | 390   |   |
| 30.....  | 1303 | 961         | 1080       | --   | 1990                             | 460   |   |
| 30.....  | 1647 | 961         | 1080       | 25.0   | 1240                             | 250   |   |
| 30.....  | 2247 | 961         | 1080       | 26.5   | 3740                             | 980   |   |
| 30.....  | 1747 | 961         | 1080       | 24.8   | 1010                             | 190   |   |
| 30.....  | 1847 | 961         | 1080       | 25.8   | 1460                             | 260   |   |
| 30.....  | 1947 | 961         | 1080       | 27.5   | 2210                             | 520   |   |
| 30.....  | 2047 | 961         | 1080       | 27.0   | 2170                             | 510   |   |
| 30.....  | 2147 | 961         | 1080       | 26.5   | 2250                             | 500   |   |
| 30.....  | 2247 | 961         | 1080       | 26.5   | 3740                             | 980   |   |
| 30.....  | 2347 | 961         | 1080       | 26.1   | 3530                             | 900   |   |
| 31.....  | 0047 | 961         | 1080       | 26.5   | 2800                             | 670   |   |
| 31.....  | 0147 | 961         | 1080       | 25.5   | 2510                             | 620   |   |
| 31.....  | 0247 | 961         | 1080       | 24.5   | 2160                             | 490   |   |
| 31.....  | 0347 | 951         | 1080       | 24.0   | 1600                             | 340   |   |
| 31.....  | 0447 | 951         | 1080       | 23.0   | 1170                             | 220   |   |

Table 21.--Temperature, specific conductance and chloride concentration of water from selected wells at the test site - continued

| WELL NUMBER AND DATE | DEPTH TO TOP OF SAMPLE INTERVAL (FT) | DEPTH TO BOTTOM OF SAMPLE INTERVAL (FT) | TEMPERATURE (DEG C.) | SPECIFIC CONDUCTANCE (MICRO-MHOES) | DISCHARGE RATE (CL/MHOES) |
|----------------------|--------------------------------------|---|----------------------|------------------------------------|---------------------------|
| OCT. 1974            | 0547                                 | 961                                     | 1080                 | 23.0                               | 935                       |
| 31... 0645           | 961                                  | 1080                                    | 22.8                 | 848                                |                           |
| 31... 0745           | 961                                  | 1080                                    | 22.8                 | 820                                |                           |
| 31... 10245          | 961                                  | 1080                                    | 22.8                 | 735                                |                           |
| 31... 0945           | 961                                  | 1080                                    | 25.5                 | 705                                |                           |
| 31... 1130           | 961                                  | 1080                                    | 27.5                 | 1970                               |                           |
| 31... 1245           | 961                                  | 1080                                    | 27.0                 | 2130                               |                           |
| 31... 1330           | 961                                  | 1080                                    | 27.8                 | 2330                               |                           |
| 31... 1430           | 961                                  | 1080                                    | 27.8                 | 2500                               |                           |
| 31... 1600           | 961                                  | 1080                                    | 26.2                 | 1480                               |                           |
| 31... 1700           | 961                                  | 1080                                    | 26.0                 | 1240                               |                           |
| 31... 1800           | 961                                  | 1080                                    | 25.5                 | 1150                               |                           |
| 31... 1960           | 961                                  | 1080                                    | 26.0                 | 1360                               |                           |
| 31... 2000           | 961                                  | 1080                                    | 27.2                 | 2030                               |                           |
| 31... 2100           | 961                                  | 1080                                    | 26.7                 | 2180                               |                           |
| 31... 2200           | 961                                  | 1080                                    | 26.5                 | 3100                               |                           |
| 31... 2300           | 961                                  | 1080                                    | 25.6                 | 6600                               |                           |
| NOV.                 | 00001                                | 961                                     | 1080                 | —                                  | 1900                      |
| 01... 0100           | 961                                  | 1080                                    | 26.0                 | 6200                               |                           |
| 01... 0200           | 961                                  | 1080                                    | 25.8                 | 4840                               |                           |
| 01... 0300           | 961                                  | 1080                                    | 25.3                 | 4400                               |                           |
| 01... 0400           | 961                                  | 1080                                    | 24.3                 | 1200                               |                           |
| 01... 0500           | 961                                  | 1080                                    | 24.0                 | 3490                               |                           |
| 01... 0500           | 961                                  | 1090                                    | 23.0                 | 2590                               |                           |
| 01... 0700           | 961                                  | 1080                                    | 23.0                 | 1870                               |                           |
| 01... 0800           | 961                                  | 1080                                    | 23.0                 | 300                                |                           |
| 01... 0900           | 961                                  | 1080                                    | 23.0                 | 1210                               |                           |
| 01... 1000           | 961                                  | 1080                                    | 23.0                 | 260                                |                           |
| 01... 1100           | 961                                  | 1080                                    | 23.0                 | 1050                               |                           |
| 01... 1200           | 961                                  | 1080                                    | 23.0                 | 200                                |                           |
| 01... 1300           | 961                                  | 1080                                    | 27.5                 | 930                                |                           |
| 01... 1400           | 961                                  | 1080                                    | 27.5                 | 170                                |                           |
| 01... 1500           | 961                                  | 1080                                    | 27.7                 | 2880                               |                           |
| 01... 1600           | 961                                  | 1080                                    | 27.0                 | 2370                               |                           |
| 01... 1700           | 961                                  | 1080                                    | 26.0                 | 590                                |                           |
| 01... 1800           | 961                                  | 1080                                    | 25.6                 | 400                                |                           |
| 01... 1900           | 961                                  | 1080                                    | 25.6                 | 320                                |                           |

Table 21.—Temperature, specific conductance and chloride concentration of water from selected wells at the test site—continued

| DATE        | TIME | DEPTH<br>TO<br>TOP<br>OF<br>SAMPLE<br>INTER-<br>VAL<br>(FT) | DEPTH<br>TO AN-<br>TOM OF<br>SAMPLE<br>INTER-<br>VAL<br>(FT) | SPECI-<br>CIFIC<br>COND-<br>DUCT-<br>ANCE<br>(CL) | DIS-<br>SOLVED<br>CHLOR-<br>IDE<br>(MG/L) | SPE-<br>CIFIC<br>COND-<br>DUCT-<br>ANCE<br>(MICRO-<br>Mhos) |                                  |
|-------------|------|---|--|---|---|---|----------------------------------|
|             |      |   |  |   |   |   | (LAT 27 49 29 LONG 082 44 35.01) |
| NOV 9, 1974 |      |   |  |   |   |   |                                  |
| 01....      | 1900 | 961   | 1080   | 25.2  | 1210                                      | 250   |                                  |
| 01....      | 2000 | 961   | 1080   | 26.6  | 2050                                      | 480   |                                  |
| 01....      | 2100 | 961   | 1080   | 27.0  | 2350                                      | 540   |                                  |
| 01....      | 2200 | 961   | 1080   | 26.2  | 2700                                      | 670   |                                  |
| 01....      | 2300 | 961   | 1080   | 26.4  | 5800                                      | 1600  |                                  |
| 02....      | 0001 | 961   | 1080   | 26.0  | 7200                                      | 2200  |                                  |
| 02....      | 0100 | 961   | 1080   | 26.1  | 7600                                      | 2400  |                                  |
| 02....      | 0200 | 961   | 1080   | 26.0  | 5600                                      | 1600  |                                  |
| 02....      | 0300 | 961   | 1080   | 25.5  | 4700                                      | 1400  |                                  |
| 02....      | 0400 | 961   | 1080   | 25.0  | 4090                                      | 1200  |                                  |
| 02....      | 0500 | 961   | 1080   | 24.2  | 3320                                      | 920   |                                  |
| 02....      | 0600 | 961   | 1080   | 25.6  | 2500                                      | 650   |                                  |
| 02....      | 0700 | 961   | 1080   | 23.3  | 1630                                      | 380   |                                  |
| 02....      | 0800 | 961   | 1080   | 23.3  | 1420                                      | 340   |                                  |
| 02....      | 0900 | 961   | 1080   | 23.5  | 1240                                      | 260   |                                  |
| 02....      | 1000 | 961   | 1080   | 23.5  | 1090                                      | 230   |                                  |
| 02....      | 1100 | 961   | 1080   | 23.5  | 920                                       | 170   |                                  |
| 02....      | 1200 | 961   | 1080   | 25.5  | 1320                                      | 280   |                                  |
| 02....      | 1300 | 961   | 1080   | 28.0  | 3410                                      | 900   |                                  |
| 02....      | 1400 | 961   | 1080   | 28.0  | 2600                                      | 590   |                                  |
| 02....      | 1500 | 961   | 1080   | 27.5  | 2700                                      | 630   |                                  |
| 02....      | 1600 | 961   | 1080   | 27.5  | 2610                                      | 660   |                                  |
| 02....      | 1700 | 961   | 1080   | 27.0  | 2400                                      | 640   |                                  |
| 02....      | 1800 | 961   | 1080   | 26.0  | 1930                                      | 440   |                                  |
| 02....      | 1900 | 961   | 1080   | 25.2  | 1310                                      | 280   |                                  |
| 02....      | 2000 | 961   | 1080   | 25.2  | 1630                                      | 360   |                                  |
| 02....      | 2100 | 961   | 1080   | 26.5  | 2300                                      | 540   |                                  |
| 02....      | 2200 | 961   | 1080   | 26.5  | 2470                                      | 590   |                                  |
| 02....      | 2300 | 961   | 1080   | 26.0  | 4610                                      | 1300  |                                  |
| 03....      | 0001 | 961   | 1080   | 26.5  | 8000                                      | 2400  |                                  |
| 03....      | 0100 | 961   | 1080   | 26.5  | 7750                                      | 2200  |                                  |
| 03....      | 0200 | 961   | 1080   | 26.2  | 7700                                      | 2300  |                                  |
| 03....      | 0300 | 961   | 1080   | 25.8  | 6200                                      | 1700  |                                  |
| 03....      | 0400 | 961   | 1080   | 25.3  | 4950                                      | 1400  |                                  |
| 03....      | 0500 | 961   | 1080   | 24.5  | 4600                                      | 1300  |                                  |
| 03....      | 0600 | 961   | 1080   | 24.0  | 3650                                      | 980   |                                  |
| 03....      | 0700 | 961   | 1080   | 23.5  | 2480                                      | 620   |                                  |

Table 21.--Temperature, specific conductance and chloride concentration of water from selected wells at the test site - continued

| WELL   | NUMBER | DATE       | TIME | DEPTH<br>TO TOP<br>OF<br>SAMPLE<br>INTER-<br>VAL<br>(FT) | TO RWT-<br>OM OF<br>SAMPLE<br>INTER-<br>VAL<br>(FT) | TEMPER-<br>ATURE<br>(DEG C) | SPEC-<br>IFIC<br>COND-<br>DUCT-<br>ANCE<br>(MICRO-<br>MHOES) | DIS-<br>SOLVED<br>CHLO-<br>RIDE<br>(CL)<br>(MG/L) |
|--|--------|------------|------|--|---|-----------------------------|--|---|
| SO CROSS INJ WELL (LAT 27 49 29 LONG 082 44 35.01) |        |            |      |  |   |                             |  |   |
|  |        | NOV 1 1974 |      |  |   |                             |  |   |
|  | 03***  | 0400       | 961  | 1080   | 23.0  | 1980                        | 460  |   |
|  | 03***  | 0900       | 961  | 1080   | 23.3  | 1500                        | 330  |   |
|  | 03***  | 1000       | 961  | 1080   | 23.9  | 1310                        | 270  |   |
|  | 03***  | 1100       | 961  | 1080   | 24.3  | 1070                        | 200  |   |
|  | 03***  | 1200       | 961  | 1080   | 24.8  | 965                         | 170  |   |
|  | 03***  | 1300       | 961  | 1080   | 27.8  | 2940                        | 720  |   |
|  | 03***  | 1400       | 961  | 1080   | 28.3  | 3900                        | 1000   |   |
|  | 03***  | 1500       | 961  | 1080   | 27.5  | 3130                        | 760  |   |
|  | 03***  | 1600       | 961  | 1080   | 27.3  | 3300                        | 820  |   |
|  | 08***  | 1457       | 961  | 1080   | 26.3  | 3110                        | 850  |   |
|  | 08***  | 1500       | 961  | 1080   | 26.3  | 3110                        | 810  |   |
|  | 08***  | 1503       | 961  | 1080   | 26.3  | 3150                        | 840  |   |
|  | 08***  | 1620       | 961  | 1080   | 24.5  | 16900                       | 5600   |   |
|  | 08***  | 1625       | 961  | 1080   | --  | 17100                       | 5800   |   |
|  | 08***  | 1643       | 961  | 1080   | --  | 27000                       | 9400   |   |
|  | 08***  | 1715       | 961  | 1080   | --  | 17800                       | 6400   |   |
|  | 11***  | 1100       | 961  | 1080   | 25.5  | 18300                       | 6000   |   |
| DEC  |        |            |      |  |   |                             |  |   |
|  | 05***  | 1000       |      |  | --  | 50000                       | --   |   |
|  | 05***  | 1034       | 961  | 1080   | 24.2  | 21800                       | 7900   |   |
|  | 05***  | 1100       | 961  | 1080   | --  | 51000                       | --   |   |
|  | 05***  | 1200       | 961  | 1080   | 25.9  | 50000                       | 19000  |   |
|  | 05***  | 1245       | 961  | 1080   | 25.9  | 52000                       | 20000  |   |
|  | 05***  | 1315       | 961  | 1080   | 25.9  | 52000                       | 18000  |   |
|  | 05***  | 1330       | 1050 | 1050   | 25.8  | 54000                       | 19000  |   |
|  | 20***  | 1000       | 200  | 200  | --  | 50000                       | 19000  |   |
|  | 20***  | 1100       | 977  | 977  | --  | 51000                       | 19000  |   |
|  | 20***  | 1200       | 990  | 990  | --  | 50000                       | 19000  |   |

Table 21.—Temperature, specific conductance and chloride concentration of water from selected wells at the test site—continued

| WELL NUMBER A2 | DATE | TIME<br>(FT) | DEPTH<br>TO TOP<br>OF<br>SAMPLE<br>INTER-<br>VAL<br>(FT) | DEPTH<br>TO HOT-<br>WATER<br>SAMPLE<br>INTER-<br>VAL<br>(FT) | TEMPER-<br>ATURE<br>(DEG C.) | SOUTH CROSS INJ MON 801 (LAT 27 49 29 LONG 082 44 35.0?)             |  |  |  |  |  |
|----------------|------|--------------|--|--|------------------------------|--|--|--|--|--|--|
|                |      |              |  |  |                              | DIS-<br>CIFIC<br>COND-<br>DUCT-<br>ANCE<br>(MCPD-<br>MHO5)<br>(MG/L) | SPE-<br>CIFIC<br>COND-<br>DUCT-<br>ANCE<br>(MCPD-<br>MHO5)<br>(MG/L) | SPE-<br>CIFIC<br>COND-<br>DUCT-<br>ANCE<br>(MCPD-<br>MHO5)<br>(MG/L) | SPE-<br>CIFIC<br>COND-<br>DUCT-<br>ANCE<br>(MCPD-<br>MHO5)<br>(MG/L) | SPE-<br>CIFIC<br>COND-<br>DUCT-<br>ANCE<br>(MCPD-<br>MHO5)<br>(MG/L) | SPE-<br>CIFIC<br>COND-<br>DUCT-<br>ANCE<br>(MCPD-<br>MHO5)<br>(MG/L) |
| OCT • 1974     |      |              | 746  | 800  | 27.5                         | 25100  | 8800   | 52000  | 19000  | 52000  | 19000  |
| 23***          | 1006 |              | 746  | 800  | 28.0                         | —  | —  | —  | —  | —  | —  |
| 23***          | 1210 |              | 746  | 800  | —                            | 50100  | 19000  | 50100  | 19000  | 50100  | 19000  |
| 23***          | 2400 |              | 746  | 800  | —                            | —  | —  | —  | —  | —  | —  |
| NOV            |      |              |  |  |                              |  |  |  |  |  |  |
| 08***          | 1215 |              | 746  | 800  | 27.5                         | 25100  | 8800   | 52000  | 19000  | 52000  | 19000  |
| 08***          | 1312 |              | 746  | 800  | 27.8                         | 25700  | 9000   | 52700  | 19000  | 52700  | 19000  |
| 08***          | 1416 |              | 746  | 800  | 27.9                         | 29800  | 9300   | 529800   | 19300  | 529800   | 19300  |
| 08***          | 1526 |              | 746  | 800  | 27.9                         | 26500  | 9200   | 526500   | 19200  | 526500   | 19200  |
| 08***          | 1603 |              | 746  | 800  | 27.9                         | 26500  | 9300   | 526500   | 19300  | 526500   | 19300  |
| 08***          | 1643 |              | 746  | 800  | 27.6                         | 26500  | 9300   | 526500   | 19300  | 526500   | 19300  |
| 10***          | 1245 |              | 746  | 800  | —                            | 29800  | 11000  | —  | —  | —  | —  |
| 11***          | 1143 |              | 746  | 800  | 27.5                         | 29700  | 10000  | —  | —  | —  | —  |
| 11***          | 1200 |              | 746  | 800  | 28.0                         | 29900  | 11000  | —  | —  | —  | —  |
| 11***          | 1215 |              | 746  | 800  | 27.5                         | 29800  | 10000  | —  | —  | —  | —  |
| 11***          | 1230 |              | 746  | 800  | 26.0                         | 29800  | 10000  | —  | —  | —  | —  |
| 11***          | 1347 |              | 746  | 800  | 27.5                         | 30300  | 11000  | —  | —  | —  | —  |
| 11***          | 1437 |              | 746  | 800  | 27.5                         | 30800  | 11000  | —  | —  | —  | —  |
| 12***          | 1120 |              | 746  | 800  | 26.0                         | 30900  | 11000  | —  | —  | —  | —  |
| 12***          | 1125 |              | 746  | 800  | 26.0                         | 35400  | 13000  | —  | —  | —  | —  |
| 12***          | 1240 |              | 746  | 800  | 28.0                         | 31500  | 11000  | —  | —  | —  | —  |
| 12***          | 1500 |              | 746  | 800  | 28.0                         | 32100  | 11000  | —  | —  | —  | —  |
| 12***          | 1600 |              | 746  | 800  | 28.0                         | 32200  | 12000  | —  | —  | —  | —  |
| 18***          | 1200 |              | 746  | 800  | 27.8                         | 34900  | 13000  | —  | —  | —  | —  |
| 18***          | 1300 |              | 746  | 800  | 27.8                         | 35200  | 12000  | —  | —  | —  | —  |
| 18***          | 1400 |              | 746  | 800  | 27.8                         | 37500  | 14000  | —  | —  | —  | —  |
| 18***          | 1500 |              | 746  | 800  | 28.0                         | 35500  | 13000  | —  | —  | —  | —  |
| 19***          | 1030 |              | 746  | 800  | 27.8                         | 36200  | 12000  | —  | —  | —  | —  |
| 19***          | 1130 |              | 746  | 800  | 28.0                         | 36000  | 13000  | —  | —  | —  | —  |
| 20***          | 1235 |              | 746  | 800  | 27.9                         | 36900  | 14000  | —  | —  | —  | —  |
| 20***          | 1500 |              | 746  | 800  | 27.8                         | 37500  | 14000  | —  | —  | —  | —  |
| 21***          | 1200 |              | 746  | 800  | 27.8                         | 37500  | 14000  | —  | —  | —  | —  |
| 21***          | 1500 |              | 746  | 800  | 27.8                         | 37500  | 14000  | —  | —  | —  | —  |
| 22***          | 0930 |              | 746  | 800  | 27.8                         | 37300  | 14000  | —  | —  | —  | —  |
| 22***          | 1130 |              | 746  | 800  | 27.8                         | 37800  | 13000  | —  | —  | —  | —  |
| 25***          | 1245 |              | 746  | 800  | 27.9                         | 38400  | 14000  | —  | —  | —  | —  |
| 25***          | 1415 |              | 746  | 800  | 27.9                         | 38200  | 14000  | —  | —  | —  | —  |
| 25***          | 1530 |              | 746  | 800  | 27.9                         | 38900  | 15000  | —  | —  | —  | —  |

Table 21.--Temperature, specific conductance and chloride concentration of water from selected wells at the test site - continued

| DATE                  | TIME | DEPTH<br>TO TOP<br>OF<br>SAMPLE<br>INTER-<br>VAL<br>(FT) | DEPTH<br>TO ROT-<br>TOM OF<br>SAMPLE<br>INTER-<br>VAL<br>(FT) | TEMPER-<br>ATURE<br>(DEG C) | SOUTH CROSS INJ MON 800 (LAT 27 49 29 LONG 082 44 35.02) |   |   |  |
|-----------------------|------|--|---|-----------------------------|--|---|---|--|
|                       |      |  |   |                             | SPCIFIC<br>COND-<br>DUCT-<br>ANCE<br>(MICRO-<br>MHOS)    | DIS-<br>CHLO-<br>RIDE<br>(CL)<br>(MG/L) | DIS-<br>SOLVED<br>CHLO-<br>RIDE<br>(CL)<br>(MG/L) |  |
| <b>WELL NUMBER A2</b> |      |  |   |                             |  |   |   |  |
| NOV • 1974            |      |  |   |                             |  |   |   |  |
| 26•••                 | 0955 | 746  | 800   | 27.8                        | 38800  | 14000                                   |   |  |
| 26•••                 | 1155 | 746  | 800   | 27.8                        | 38900  | 15000                                   |   |  |
| 26•••                 | 1415 | 746  | 800   | 27.8                        | 39500  | 15000                                   |   |  |
| 26•••                 | 1520 | 746  | 800   | 27.8                        | 39100  | 15000                                   |   |  |
| 27•••                 | 1010 | 746  | 800   | 27.9                        | 39100  | 15000                                   |   |  |
| 27•••                 | 1155 | 746  | 800   | 27.9                        | 39700  | 14000                                   |   |  |
| 27•••                 | 1400 | 746  | 800   | 27.9                        | 37500  | 14000                                   |   |  |
| 27•••                 | 1430 | 746  | 800   | 27.9                        | 40100  | 15000                                   |   |  |
| 27•••                 | 1500 | 746  | 800   | 27.9                        | 39700  | 14000                                   |   |  |
| DEC                   |      |  |   |                             |  |   |   |  |
| 02•••                 | 1405 | 746  | 800   | 27.7                        | 40200  | 16000                                   |   |  |
| 02•••                 | 1445 | 746  | 800   | 27.7                        | 49200  | 18000                                   |   |  |
| 03•••                 | 1300 | 746  | 800   | 27.7                        | 40200  | 15000                                   |   |  |
| 03•••                 | 1445 | 746  | 800   | 27.7                        | 40300  | 16000                                   |   |  |
| 20•••                 | 0900 | 746  | 800   | 25.3                        | 42200  | 16000                                   |   |  |
| 26•••                 | 1000 | 746  | 800   | 27.4                        | 43200  | 17000                                   |   |  |
| FEB • 1975            |      |  |   |                             |  |   |   |  |
| 04•••                 | 1323 | 746  | 800   | 27.6                        | 44500  | 16000                                   |   |  |
| 04•••                 | 1440 | 746  | 800   | 27.7                        | 44300  | 17000                                   |   |  |
| 04•••                 | 1615 | 746  | 800   | 27.7                        | 44800  | 18000                                   |   |  |
| MAY                   |      |  |   |                             |  |   |   |  |
| 14•••                 | 2045 | 746  | 800   | --                          | 52000  | 19000                                   |   |  |
| JUN                   |      |  |   |                             |  |   |   |  |
| 04•••                 | 1240 | 746  | 800   | 27.6                        | 47000  | 18000                                   |   |  |
| JAN • 1976            |      |  |   |                             |  |   |   |  |
| 20•••                 | 1200 | 746  | 800   | 27.5                        | 52000  | 18000                                   |   |  |
| APR                   |      |  |   |                             |  |   |   |  |
| 20•••                 | 1350 | 746  | 800   | --                          | 49200  | 19000                                   |   |  |

Table 21.—Temperature, specific conductance and chloride concentration of water from selected wells at the test site - continued

| WELL NUMBER | DATE          | TIME | DEPTH<br>TO TOP<br>OF<br>SAMPLE      | DEPTH<br>TO ROT-<br>TOM OF<br>SAMPLE | TEMPER-<br>ATURE<br>VAL<br>(FT) | TEMPFR-<br>ATURE<br>VAL<br>(DEG C) | SPEC-<br>CIFIC<br>COND-<br>DUCT-<br>ANCE<br>(MG/L) | DIS-<br>CIFIC<br>COND-<br>DUCT-<br>ANCE<br>(CL)<br>(MG/L) | SOUTH CROSS INJ MON 521 (LAT 27 49 29 LONG 082 44 35.03)  |   |   |  |       |  |
|-------------|---------------|------|--------------------------------------|--------------------------------------|---------------------------------|------------------------------------|--|---|---|---|---|--|-------|--|
|             |               |      |                                      |                                      |                                 |                                    |  |   | DEPTH<br>TO ROT-<br>TOM OF<br>SAMPLE                      | INTERP-<br>VAL<br>(FT)                                    | TEMPFR-<br>ATURE<br>VAL<br>(DEG C)                        | SPEC-<br>CIFIC<br>COND-<br>DUCT-<br>ANCE<br>(CL)<br>(MG/L) |       |  |
| WELL NUMBER | DATE          | TIME | DEPTH<br>TO ROT-<br>TOM OF<br>SAMPLE | DEPTH<br>TO ROT-<br>TOM OF<br>SAMPLE | TEMPER-<br>ATURE<br>VAL<br>(FT) | TEMPFR-<br>ATURE<br>VAL<br>(DEG C) | SPEC-<br>CIFIC<br>COND-<br>DUCT-<br>ANCE<br>(MG/L) | DIS-<br>CIFIC<br>COND-<br>DUCT-<br>ANCE<br>(CL)<br>(MG/L) | DIS-<br>CIFIC<br>COND-<br>DUCT-<br>ANCE<br>(CL)<br>(MG/L) | DIS-<br>CIFIC<br>COND-<br>DUCT-<br>ANCE<br>(CL)<br>(MG/L) | DIS-<br>CIFIC<br>COND-<br>DUCT-<br>ANCE<br>(CL)<br>(MG/L) | DIS-<br>CIFIC<br>COND-<br>DUCT-<br>ANCE<br>(CL)<br>(MG/L)  |       |  |
| 43          | OCT. 23, 1974 | 1004 | 473                                  | 521                                  | --                              | --                                 | 52000  | 18000   | 49300   | 19000   | 49800   | 19000  | 51000 |  |
|             | 23, 1974      | 1240 | 473                                  | 521                                  | 26.5                            | 26.5                               | 51000  | 20000   | 49900   | 19000   | 50000   | 19000  | 51000 |  |
|             | NOV. 11, 1974 | 1339 | 473                                  | 521                                  | 25.0                            | 25.0                               | 49800  | 19000   | 51000   | 20000   | 49900   | 19000  | 50000 |  |
|             | 11, 1974      | 1345 | 473                                  | 521                                  | 26.0                            | 26.0                               | 51000  | 20000   | 49900   | 19000   | 50000   | 19000  | 51000 |  |
|             | 11, 1974      | 1422 | 473                                  | 521                                  | 26.5                            | 26.5                               | 51000  | 20000   | 49900   | 19000   | 50000   | 19000  | 51000 |  |
|             | 11, 1974      | 1503 | 473                                  | 521                                  | 26.3                            | 26.3                               | 51000  | 19000   | 49900   | 19000   | 50000   | 19000  | 51000 |  |
|             | 12, 1974      | 1055 | 473                                  | 521                                  | 26.0                            | 26.0                               | 51000  | 19000   | 49900   | 19000   | 50000   | 19000  | 51000 |  |
|             | 12, 1974      | 1250 | 473                                  | 521                                  | 26.5                            | 26.5                               | 49900  | 19000   | 49800   | 20000   | 49900   | 19000  | 50000 |  |
|             | 12, 1974      | 1500 | 473                                  | 521                                  | 26.5                            | 26.5                               | 49800  | 19000   | 49900   | 20000   | 49900   | 19000  | 50000 |  |
|             | 12, 1974      | 1500 | 473                                  | 521                                  | 26.5                            | 26.5                               | 49800  | 19000   | 49900   | 20000   | 49900   | 19000  | 50000 |  |
|             | 19, 1974      | 1450 | 473                                  | 521                                  | 26.5                            | 26.5                               | 51000  | 19000   | 49900   | 20000   | 49900   | 19000  | 50000 |  |
|             | 19, 1974      | 1245 | 473                                  | 521                                  | 26.1                            | 26.1                               | 49900  | 19000   | 49800   | 20000   | 49900   | 19000  | 50000 |  |
|             | 20, 1974      | 1505 | 473                                  | 521                                  | 26.1                            | 26.1                               | 49800  | 20000   | 49900   | 20000   | 49900   | 20000  | 50000 |  |
|             | 21, 1974      | 1205 | 473                                  | 521                                  | 25.7                            | 25.7                               | 49800  | 20000   | 49900   | 20000   | 49900   | 20000  | 50000 |  |
|             | 21, 1974      | 1405 | 473                                  | 521                                  | 25.7                            | 25.7                               | 49900  | 20000   | 49900   | 20000   | 49900   | 19000  | 50000 |  |
|             | 21, 1974      | 1505 | 473                                  | 521                                  | 25.9                            | 25.9                               | 49900  | 19000   | 49800   | 19000   | 49900   | 19000  | 50000 |  |
|             | 22, 1974      | 0935 | 473                                  | 521                                  | 25.7                            | 25.7                               | 49800  | 19000   | 49900   | 19000   | 49900   | 19000  | 50000 |  |
|             | 22, 1974      | 1135 | 473                                  | 521                                  | 25.8                            | 25.8                               | 50000  | 19000   | 49900   | 19000   | 49900   | 19000  | 50000 |  |
|             | JUNE, 1975    | 1345 | 473                                  | 521                                  | 26.4                            | 26.4                               | 49100  | 19000   | 49100   | 19000   | 49100   | 19000  | 49100 |  |
|             | JAN., 1976    | 1200 | 473                                  | 521                                  | 26.3                            | 26.3                               | 52000  | 18000   | 52000   | 18000   | 52000   | 18000  | 52000 |  |
|             | APR., 1976    | 1210 | 473                                  | 521                                  | 26.0                            | 26.0                               | 50000  | 19000   | 50000   | 19000   | 50000   | 19000  | 50000 |  |

Table 21.--Temperature, specific conductance and chloride concentration of water from selected wells at the test site - continued

| DATE           | TIME | DEPTH<br>TO TOP<br>OF<br>SAMPLE | DEPTH<br>TO BOT-<br>OM OF<br>SAMPLE | TEMPER-<br>INTFR-<br>VAL.<br>(FT) | TEMPER-<br>ATUR-<br>E<br>(DEG C) | SPE-<br>CIFIC<br>COND-<br>DUCT-<br>ANCE<br>(MICRO-<br>MHOS) | DIS-<br>SOLVED<br>CHLO-<br>RIDE<br>(CL)<br>(MG/L) |
|----------------|------|---------------------------------|-------------------------------------|-----------------------------------|----------------------------------|---|---|
| WELL NUMBER A4 |      |                                 |                                     |                                   |                                  |   |   |
| OCT., 1974     |      |                                 |                                     |                                   |                                  |   |   |
| 23... 1975     | 1200 | 200                             | 250                                 | --                                | 5400                             | 440   |   |
| 23... 1975     | 1305 | 200                             | 250                                 | 25.5                              | 1700                             | 450   |   |
| JUNE, 1975     |      |                                 |                                     |                                   |                                  |   |   |
| 04... 1975     | 1445 | 200                             | 250                                 | 24.4                              | 1910                             | 470   |   |
| SEP.           |      |                                 |                                     |                                   |                                  |   |   |
| 15... 1976     | 1600 | 200                             | 250                                 | --                                | 1580                             | 390   |   |
| JAN., 1976     |      |                                 |                                     |                                   |                                  |   |   |
| 16... 1976     | 1430 | 200                             | 250                                 | 24.2                              | 1990                             | 480   |   |
| APR.           |      |                                 |                                     |                                   |                                  |   |   |
| 20... 1976     | 1100 | 200                             | 250                                 | 24.0                              | 2020                             | 540   |   |

Table 21.—Temperature, specific conductance and chloride concentration of water from selected wells at the test site—continued

| DATE           | TIME | DEPTH<br>TO TOP<br>OF<br>SAMPLE<br>INTER-<br>VAL<br>(FT) | DEPTH<br>TOM OF<br>SAMPLE<br>INTER-<br>VAL<br>(FT) | TEMPER-<br>ATURE<br>(DEG C) | SPECI-<br>CIFIC<br>CONDUC-<br>TANCE<br>ANCFC<br>(CL)<br>(MG/L) | DIS-<br>SOLVED<br>CHLO-<br>RIDE<br>(MG/L)             |
|----------------|------|--|--|-----------------------------|--|---|
|                |      |  |  |                             | WELL NUMBER B1   | SOUTH CROSS MON 1224 (LAT 27 49 22 LONG 082 44 31.04) |
| JULY, 1974     |      |  |  |                             |  |   |
| 16....         | 1630 | 1210   | 1224   | 26.0                        | 53700  | 21000   |
| DEC.           |      |  |  |                             |  |   |
| 02....         | 1535 | 1210   | 1224   | --                          | 53000  | 20000   |
| JUNE, 1975     |      |  |  |                             |  |   |
| 05....         | 1530 | 1210   | 1224   | 25.3                        | 54000  | 20000   |
| JAN., 1976     |      |  |  |                             |  |   |
| 16....         | 1215 | 1210   | 1224   | --                          | 52000  | 20000   |
| 16....         | 1324 | 1210   | 1224   | --                          | 52000  | 19000   |
| APR.           |      |  |  |                             |  |   |
| 20....         | 1300 | 1210   | 1224   | 25.0                        | 53500  | 20000   |
| WELL NUMBER B2 |      |  |  |                             |  |   |
| JULY, 1974     |      |  |  |                             |  |   |
| 17....         | 1225 | 1025   | 1055   | 27.5                        | 52600  | 20000   |
| AUG.           |      |  |  |                             |  |   |
| 23....         | 1115 | 1025   | 1055   | --                          | 52500  | 20000   |
| DFC.           |      |  |  |                             |  |   |
| 03....         | 1345 | 1025   | 1055   | --                          | 52000  | 18000   |
| JUNE, 1975     |      |  |  |                             |  |   |
| 06....         | 1320 | 1025   | 1055   | --                          | 53000  | 20000   |
| JAN., 1976     |      |  |  |                             |  |   |
| 22....         | 1100 | 1025   | 1055   | 26.3                        | 55000  | 21000   |
| APR.           |      |  |  |                             |  |   |
| 21....         | 1507 | 1025   | 1055   | --                          | 51000  | 20000   |

Table 21.—Temperature, specific conductance and chloride concentration of water from selected wells at the test site—continued

| DATE   | TIME | DEPTH<br>TO TOP<br>OF<br>SAMPLE<br>INTER-<br>VAL<br>(FT) | DEPTH<br>TO BOT-<br>OM OF<br>SAMPLE<br>INTER-<br>VAL<br>(FT) | SPF—<br>CIFIC<br>COND-<br>DUCT-<br>ANCE<br>(CL)<br>(MG/L) | NIS-<br>SOLVED<br>CHLO-<br>RIDE<br>(MICRO-<br>MOS) |
|--|------|--|--|---|--|
| <b>WELL NUMBER R3</b>                                    |      |  |  |   |  |
| SOUTH CROSS MONITOR R15 (LAT 27 49 22 LONG 082 44 31.02) |      |  |  |   |  |
| JULY * 1974  |      |  |  |   |  |
| 17••• 1350   |      | 780  | 815  | 28.5  | 52300 20000  |
| AUG.*  |      |  |  | --  | 53000 20000  |
| 23••• 1230   |      | 780  | 815  | --  |  |
| MAY * 1975   | 1230 |  |  |   |  |
| 14••• 2045   |      |  |  |   |  |
| JUNE   |      | 780  | 815  | 26.5  | 52000 19000  |
| 05••• 1235   |      | 780  | 815  | 24.9  | 52000 19000  |
| APR••• 1976  |      |  |  |   |  |
| 20••• 1245   |      | 780  | 815  | 25.0  | 51000 20000  |
| <b>WELL NUMBER R4</b>                                    |      |  |  |   |  |
| SOUTH CROSS MONITOR 520 (LAT 27 49 22 LONG 082 44 31.01) |      |  |  |   |  |
| JULY * 1974  |      |  |  |   |  |
| 17••• 1425   |      | 463  | 520  | 27.0  | 49900 19000  |
| AUG.*  |      |  |  | --  | 50000 19000  |
| 23••• 1140   |      | 463  | 520  | --  |  |
| DFC.   |      |  |  |   |  |
| 02••• 1215   |      | 463  | 520  | --  | 49100 19000  |
| JUNE * 1975  | 1215 |  |  |   |  |
| 05••• 0940   |      | 463  | 520  | 26.0  | 49800 18000  |
| APR••• 1976  |      |  |  | --  |  |
| 20••• 1410   |      | 463  | 520  | --  | 49200 18000  |
| <b>WELL NUMBER R5</b>                                    |      |  |  |   |  |
| SOUTH CROSS RAVINE 94 (LAT 27 49 21 LONG 082 44 30.02)   |      |  |  |   |  |
| JULY * 1976  |      |  |  |   |  |
| 29••• 1310   |      | 90   | 94   | --  | 780 52   |
| <b>WELL NUMBER R6</b>                                    |      |  |  |   |  |
| SOUTH CROSS RAVINE 95 (LAT 27 49 21 LONG 082 44 30.01)   |      |  |  |   |  |
| JULY * 1976  |      |  |  |   |  |
| 29••• 1325   |      | 31   | 35   | --  | 580 25   |

Table 22.—Chemical analyses of water from selected wells at the test site

| DEPTH<br>TO TOP<br>OF<br>SAMPLE<br>INTER-<br>VAL<br>(FT)         | DEPTH<br>TO BOTTOM<br>OF<br>SAMPLE<br>INTER-<br>VAL<br>(FT)  | SPEC-<br>IFIC<br>CON-<br>DUCT-<br>ANCE<br>(MICRO-<br>MHO/S) | ALKALI-<br>NITY<br>PH<br>(UNITS) | RICAR-<br>BONATE<br>AS<br>(HC03)<br>(MG/L) | CAR-<br>BONATE<br>(CO3)<br>(MG/L) | TOTAL<br>SULFIDE<br>(S)<br>(MG/L) | SOLVED<br>CHLORIDE<br>(CL)<br>(MG/L) |                                |
|--|--|---|----------------------------------|--|-----------------------------------|-----------------------------------|--------------------------------------|--------------------------------|
| TIME<br>DATE   | WELL<br>NUMBER A1  | SO CROSS INJ WELL (LAT 27 49 29 LONG 082 44 35.01)          |                                  |  |                                   |                                   |                                      |                                |
| OCT 17... 1974<br>DEC 05... 1974<br>05... 1974<br>05... 1974     | 961<br>961<br>961<br>1050                                    | 1030<br>1030<br>1080<br>1050                                | 29.0<br>24.2<br>25.9<br>25.8     | 50600<br>21400<br>50000<br>54000           | 7.5<br>7.4<br>7.4<br>7.3          | 186<br>210<br>200<br>232          | 0<br>0<br>0<br>0                     | 1.1<br>20000<br>--<br>--<br>-- |
| WELL NUMBER A2   | SOUTHERN CROSS INJ WELL 800 (LAT 27 49 29 LONG 082 44 35.02) |   |                                  |  |                                   |                                   |                                      |                                |
| OCT 23... 1974<br>Nov 18... 1974<br>18... 1974<br>DEC 03... 1974 | 746<br>746<br>746<br>746                                     | 816<br>810<br>860<br>800                                    | --<br>27.8<br>35500<br>27.7      | 50100<br>34400<br>35500<br>40200           | 7.2<br>--<br>--<br>--             | 157<br>145<br>145<br>176          | 191<br>225<br>225<br>214             | 0<br>--<br>--<br>--            |
| WELL NUMBER A3   | SOUTHERN CROSS INJ WELL 521 (LAT 27 49 29 LONG 082 44 35.03) |   |                                  |  |                                   |                                   |                                      |                                |
| OCT 23... 1974<br>23... 1974                                     | 1240<br>1240   | 473<br>473  | 521<br>521                       | 26.5<br>26.5                               | 49300<br>49300                    | 7.1<br>1.4                        | 224<br>0                             | --<br>--                       |
| WELL NUMBER A4   | SOUTH CROSS INJ 250 (LAT 27 49 29 LONG 082 44 35.04)         |   |                                  |  |                                   |                                   |                                      |                                |
| OCT 23... 1974<br>23... 1974                                     | 260<br>260   | 250<br>250  | 1700<br>1700                     | 7.4<br>7.4                                 | 130<br>159                        | 0<br>0                            | --<br>450                            |                                |

Table 22.--Chemical analyses of water from selected wells at the test site - continued

|  | DIS-              | DIS-               | DIS-              | DIS-             | DIS-             | DIS-               |
|--|-------------------|--------------------|-------------------|------------------|------------------|--------------------|
|  | SOLVED<br>SOLVENT | SOLVED<br>FLUORIDE | SOLVED<br>CALCIUM | SOLVED<br>SODIUM | SOLVED<br>SILICA | SOLVED<br>SOLVENTS |
|  | (MG/L)            | (MG/L)             | (MG/L)            | (MG/L)           | (MG/L)           | (MG/L)             |
| WELL NUMBER A1   |                   |                    |                   |                  |                  |                    |
| OCT 1974   | 1.1               | 910                | 1600              | 400              | 11               | 38100              |
| DEC 1974   | 1.1               | 910                | 1600              | 400              | 11               | 36300              |
| JAN 1975   | 1.1               | 910                | 1600              | 400              | 11               | 36300              |
| FEB 1975   | 1.1               | 910                | 1600              | 400              | 11               | 36300              |
| MAR 1975   | 1.1               | 910                | 1600              | 400              | 11               | 36300              |
| JULY 1975  | 1.1               | 910                | 1600              | 400              | 11               | 36300              |
| SOUTH CROSS INJ WELL (LAT 27 49 29 LONG 082 44 35.01)    |                   |                    |                   |                  |                  |                    |
| OCT 1974   | 1.1               | 910                | 1600              | 400              | 11               | 38100              |
| DEC 1974   | 1.1               | 910                | 1600              | 400              | 11               | 36300              |
| JAN 1975   | 1.1               | 910                | 1600              | 400              | 11               | 36300              |
| FEB 1975   | 1.1               | 910                | 1600              | 400              | 11               | 36300              |
| MAR 1975   | 1.1               | 910                | 1600              | 400              | 11               | 36300              |
| JULY 1975  | 1.1               | 910                | 1600              | 400              | 11               | 36300              |
| SOUTH CROSS INJ MON 800 (LAT 27 49 29 LONG 082 44 35.02) |                   |                    |                   |                  |                  |                    |
| OCT 1974   | 1.1               | 910                | 1600              | 400              | 11               | 36100              |
| DEC 1974   | 1.1               | 910                | 1600              | 400              | 11               | 36100              |
| JAN 1975   | 1.1               | 910                | 1600              | 400              | 11               | 36100              |
| FEB 1975   | 1.1               | 910                | 1600              | 400              | 11               | 36100              |
| MAR 1975   | 1.1               | 910                | 1600              | 400              | 11               | 36100              |
| JULY 1975  | 1.1               | 910                | 1600              | 400              | 11               | 36100              |
| SOUTH CROSS INJ MON 521 (LAT 27 49 29 LONG 082 44 35.03) |                   |                    |                   |                  |                  |                    |
| OCT 1974   | 1.1               | 910                | 1600              | 400              | 11               | 35800              |
| DEC 1974   | 1.1               | 910                | 1600              | 400              | 11               | 35800              |
| JAN 1975   | 1.1               | 910                | 1600              | 400              | 11               | 35800              |
| FEB 1975   | 1.1               | 910                | 1600              | 400              | 11               | 35800              |
| MAR 1975   | 1.1               | 910                | 1600              | 400              | 11               | 35800              |
| JULY 1975  | 1.1               | 910                | 1600              | 400              | 11               | 35800              |
| SOUTH CROSS INJ 250 (LAT 27 49 29 LONG 082 44 35.04)     |                   |                    |                   |                  |                  |                    |
| OCT 1974   | 1.1               | 910                | 1600              | 400              | 11               | 35900              |
| DEC 1974   | 1.1               | 910                | 1600              | 400              | 11               | 35900              |
| JAN 1975   | 1.1               | 910                | 1600              | 400              | 11               | 35900              |
| FEB 1975   | 1.1               | 910                | 1600              | 400              | 11               | 35900              |
| MAR 1975   | 1.1               | 910                | 1600              | 400              | 11               | 35900              |
| JULY 1975  | 1.1               | 910                | 1600              | 400              | 11               | 35900              |

Table 22.—Chemical analyses of water from selected wells at the test site—continued

Table 22.--Chemical analyses of water from selected wells at the test site - continued

| DATE<br>(SO <sub>4</sub> )<br>(Mg/L) | WELL NUMBER<br>B1 | SOUTH CROSS MONITOR 1224* (LAT 27 49 22 LONG 082 44 31.04) |   |  |  |  |  | DIS-<br>SOLVED<br>SOLID<br>(RESI-<br>DUE AT<br>TEMP.)<br>(MG/L) | DIS-<br>SOLVED<br>SOLID<br>(SUM OF<br>CONSTI-<br>TUENTS)<br>(MG/L) |
|--------------------------------------|-------------------|--|---|--|--|--|--|---|--|
|                                      |                   | DIS-<br>SOLVED<br>SOLID<br>CAL-<br>CIUM<br>(Ca)<br>(Mg/L)  | DIS-<br>SOLVED<br>SOLID<br>SODIUM<br>(Na)<br>(Mg/L) | DIS-<br>SOLVED<br>PO-<br>TAS-<br>SIUM<br>(K)<br>(Mg/L) | DIS-<br>SOLVED<br>SOLID<br>SILICA<br>(SiO <sub>2</sub> )<br>(Mg/L) | DIS-<br>SOLVED<br>SOLID<br>SILICA<br>(SiO <sub>2</sub> )<br>(Mg/L) | DIS-<br>SOLVED<br>SOLID<br>SILICA<br>(SiO <sub>2</sub> )<br>(Mg/L) |   |  |
| JUL * 1974<br>16... 3800             | 1.1 1300          | 1100   | 12000   | 9.5  | 10   | 39800  | 39400  | 1.026   |  |
|                                      | * WELL NUMBER B2  | SOUTH CROSS MONITOR 1224* (LAT 27 49 22 LONG 082 44 31.03) |   |  |  |  |  |   |  |
| JUL * 1974<br>17... 3200             | •7 850            | 990  | 11000   | 460  | 1.8  | 37500  | 36600  | 1.025   |  |
|                                      | * WELL NUMBER B3  | SOUTH CROSS MONITOR 815 (LAT 27 49 22 LONG 082 44 31.02)   |   |  |  |  |  |   |  |
| JUL * 1974<br>17... 6200             | •8 880            | 1<00   | 12000   | 420  | 7.1  | 37600  | 40800  | 1.025   |  |
|                                      | * WELL NUMBER B4  | SOUTH CROSS MONITOR 520 (LAT 27 49 22 LONG 082 44 31.01)   |   |  |  |  |  |   |  |
| JUL * 1974<br>17... 3000             | •6 1000           | 920  | 11000   | 430  | 7.5  | 35500  | 35400  | 1.024   |  |
|                                      | * WELL NUMBER E1  | EXPLORATORY HOLE (LAT 27 49 22 LONG 082 44 31)             |   |  |  |  |  |   |  |
| FEB * 1973<br>14... 2700             | 1.0 1400          | 890  | 8700  | 240  | 14   | --   | --   | --  | --   |
| JUL 11... 4800                       | 5.8 1500          | 1200   | 14000   | 440  | 13   | --   | 46800  | 1.033   |  |
| MAK * 1974<br>20... 5100             | 5.4 1600          | 1300   | 16000   | 700  | 14   | 54500  | 52900  | 1.040   |  |

Table 23.--Concentrations of trace elements in water from selected wells at the test site

| TIME<br>DATE    | DEPTH<br>TO TOP<br>OF<br>SAMPLE<br>INTER-<br>VAL<br>(FT) | DEPTH<br>TO BOT-<br>TOM OF<br>SAMPLE<br>INTER-<br>VAL<br>(FT) | DIS-<br>SOLVED<br>ARSENIC<br>(AS)<br>(UG/L) | DIS-<br>SOLVED<br>Boron<br>(B)<br>(UG/L) | DIS-<br>SOLVED<br>CAD-<br>MIUM<br>(CD)<br>(UG/L) | DIS-<br>SOLVED<br>CHRO-<br>MIUM<br>(CR)<br>(UG/L) | HEXA-<br>VALENT<br>CHRO-<br>MIUM<br>(CO)<br>(UG/L) | DIS-<br>SOLVED<br>COBALT<br>(CO)<br>(UG/L) | DIS-<br>SOLVED<br>COPPER<br>(CU)<br>(UG/L) | DIS-<br>SOLVED<br>IRON<br>(FE)<br>(UG/L) |
|-----------------|--|---|---|--|--|---|--|--|--|--|
|                 |  |   | WELL<br>NUMBER A1                           | WELL<br>NUMBER A2                        | WELL<br>NUMBER A3                                | WELL<br>NUMBER A4                                 | WELL<br>NUMBER A5                                  | WELL<br>NUMBER A6                          | WELL<br>NUMBER A7                          | WELL<br>NUMBER A8                        |
| OCT. 17... 1974 | 1400   | 961   | 1080  | 0  | 4200   | 1   | 0  | 0  | 0  | 220                                      |
| OCT. 23... 1974 | 2400   | 746   | 800   | 3  | 1900   | 4   | 1  | 0  | 0  | 160                                      |
| OCT. 23... 1974 | 1240   | 473   | 521   | 1  | 2300   | --  | 1  | 0  | 3  | 170                                      |
| OCT. 23... 1974 | 1305   | 200   | 250   | 0  | 50   | 8   | 1  | 0  | 7  | 10                                       |

Table 23.—Concentrations of trace elements in water from selected wells at the test site - continued

|  | DIS-SOLVED<br>MANGANESE<br>(Mn)<br>(PPB) | DIS-SOLVED<br>MOLYBDENUM<br>(Mo)<br>(UG/L) | DIS-SOLVED<br>NICKEL<br>(Ni)<br>(UG/L) | DIS-SOLVED<br>SODIUM<br>(NaF)<br>(UG/L) | DIS-SOLVED<br>VANADIUM<br>(V)<br>(UG/L) | DIS-SOLVED<br>ZINC<br>(Zn)<br>(UG/L) | DIS-SOLVED<br>LITHIUM<br>(Li)<br>(UG/L) | DIS-SOLVED<br>MERCURY<br>(Hg)<br>(UG/L) |
|--|--|--|--|---|---|--------------------------------------|---|---|
| WELL NUMBER A1   |  |  |  |   |   |                                      |   |   |
| OCT.. 1974<br>17...                                      | ?  | 120  | 2                                      | 0                                       | 27000                                   | 500                                  | 90                                      | 0                                       |
| WELL NUMBER A2   |  |  |  |   |   |                                      |   |   |
| SOUTH CROSS INJ MON 800 (LAT 27 49 29 LONG 082 44 35.01) |  |  |  |   |   |                                      |   |   |
| OCT.. 1974<br>23...                                      | 0  | 110  | 90                                     | 29                                      | 32000                                   | 250                                  | 60                                      | 10                                      |
| WELL NUMBER A3   |  |  |  |   |   |                                      |   |   |
| SOUTH CROSS INJ MON 521 (LAT 27 49 29 LONG 082 44 35.02) |  |  |  |   |   |                                      |   |   |
| OCT.. 1974<br>23...                                      | 0  | 93   | 8                                      | --                                      | 38000                                   | 250                                  | 90                                      | 7                                       |
| WELL NUMBER A4   |  |  |  |   |   |                                      |   |   |
| SOUTH CROSS INJ 250 (LAT 27 49 29 LONG 082 44 35.04)     |  |  |  |   |   |                                      |   |   |
| OCT.. 1974<br>23...                                      | 0  | 780  | 1                                      | --                                      | 5000                                    | 8.7                                  | 500                                     | 10                                      |
|  |  |  |  |   |   |                                      | 25                                      | 0                                       |

Table 23.—Concentrations of trace elements in water from selected wells at the test site—continued

| DATE   | TIME | DEPTH<br>TO TOP<br>OF<br>SAMPLE<br>INTER-<br>VAL<br>(FT) | DEPTH<br>TO 20 FT<br>OF<br>TOM OF<br>SAMPLE<br>INTER-<br>VAL<br>(FT) | DIS-<br>SOLVED                                  |                                    | DIS-<br>SOLVED                   |                               | DIS-<br>SOLVED                           |                          |
|--|------|--|--|---|------------------------------------|----------------------------------|-------------------------------|--|--------------------------|
|  |      |  |  | DIS-<br>SAMPLE<br>INTER-<br>VAL<br>(AS)<br>(FT) | SOLVED<br>APATNIC<br>(A)<br>(UG/L) | SOLVED<br>BOPON<br>(R)<br>(UG/L) | CAD-<br>MUM<br>(CD)<br>(UG/L) | VALENT<br>CHRO-<br>MUM<br>(CR)<br>(UG/L) | COPPFR<br>(CU)<br>(UG/L) |
| wFLL NUMBER H1                                 |      |  |  |   |                                    |                                  |                               |  |                          |
| JULY, 1974<br>16...                            | 1630 | 1210   | 1224   | 0   | 4500                               | 2                                | 1                             | 0  | 0                        |
| JULY, 1974<br>17...                            | 1225 | 1025   | 1055   | 0   | 2500                               | 2                                | 0                             | --                                       | 6                        |
| wFLL NUMBER R2                                 |      |  |  |   |                                    |                                  |                               |  |                          |
| JULY, 1974<br>17...                            | 1350 | 780  | 815  | 0   | 4700                               | 0                                | 0                             | 2  | 0                        |
| wFLL NUMBER B3                                 |      |  |  |   |                                    |                                  |                               |  |                          |
| JULY, 1974<br>17...                            | 1425 | 463  | 520  | 0   | 3300                               | 2                                | 0                             | 4  | 30                       |
| wFLL NUMBER R4                                 |      |  |  |   |                                    |                                  |                               |  |                          |
| JULY, 1974<br>17...                            | 1700 | 1863   | 3280   | 5   | 15000                              | 0                                | 0                             | 9  | 0                        |
| WELL NUMBER E1                                 |      |  |  |   |                                    |                                  |                               |  |                          |
| FER., 1973<br>14...                            | 1830 | 374  | 490  | 20  | --                                 | 0                                | 50                            | 0  | 40                       |
| JULY   |      |  |  |   |                                    |                                  |                               |  | 1100                     |
| 11...  | 1345 | 1863   | 2178   | 0   | --                                 | 0                                | --                            | 0  | 260                      |
| MAR., 1974<br>20...                            |      |  |  |   |                                    |                                  |                               |  | 260                      |
| EXPLORATORY HOLE (LAT 27 49 22 LONG 082 44 31) |      |  |  |   |                                    |                                  |                               |  |                          |

Table 23. --Concentrations of trace elements in water from selected wells at the test site - continued

|  | DIS-      | DIS-       | DIS-      | DIS-     | DIS-     | DIS-     | DIS-     |
|--|-----------|------------|-----------|----------|----------|----------|----------|
|  | SOLVED    | SOLVED     | SOLVED    | SOLVED   | SOLVED   | SOLVED   | SOLVED   |
|  | MANGANESE | MOLYBDENUM | STRONTIUM | VANADIUM | ZINC     | ALUMINUM | SOLVENT  |
| DATE   | (P.B.)    | (M.M.)     | (N.O.)    | (S.R.)   | (T.N.)   | (L.I.)   | MERCURY  |
|  | (U.G/L.)  | (U.G/L.)   | (U.G/L.)  | (U.G/L.) | (U.G/L.) | (U.G/L.) | (HG)     |
|  |           |            |           |          |          |          | (U.G/L.) |
| WELL NUMBER P1                                 |           |            |           |          |          |          |          |
| JULY 1974<br>16***                             | 10        | 200        | 3         | 4        | 29000    | 670      | 3500     |
|  |           |            |           |          |          | 0        | 420      |
|  |           |            |           |          |          |          | .3       |
| WELL NUMBER 92                                 |           |            |           |          |          |          |          |
| JULY 1974<br>17***                             | 7         | 100        | 5         | 12       | 17000    | 760      | 34000    |
|  |           |            |           |          |          | 30       | 150      |
|  |           |            |           |          |          |          | .1       |
| WELL NUMBER H3                                 |           |            |           |          |          |          |          |
| JULY 1974<br>17***                             | 5         | 120        | 2         | 0        | 33000    | 730      | 4600     |
|  |           |            |           |          |          | 10       | 140      |
|  |           |            |           |          |          |          | .0       |
| WELL NUMBER P4                                 |           |            |           |          |          |          |          |
| JULY 1974<br>17***                             | 7         | 150        | 9         | 22       | 23000    | 670      | 1600     |
|  |           |            |           |          |          | 50       | 150      |
|  |           |            |           |          |          |          | .1       |
| WELL NUMBER E1                                 |           |            |           |          |          |          |          |
| FEB. 1973<br>14***                             | 1         | 60         | 15        | 1        | 34000    | 280      | 40       |
| JULY<br>11***                                  | 0         | 40         | 0         | 0        | 30000    | 360      | 0        |
| MAR. 1974<br>20***                             | 2         | 100        | 0         | 2        | 33000    | 400      | 30       |
|  |           |            |           |          |          |          | 20       |
|  |           |            |           |          |          |          | 4        |
|  |           |            |           |          |          |          | 1.7      |
| EXPLORATORY HOLE (LAT 27 49 22 LONG 082 44 31) |           |            |           |          |          |          |          |

Table 24.--Concentrations of nitrogen and phosphorus in water from selected wells at the test site

| DATE   | TIME | DEPTH<br>TO TOP<br>OF<br>SAMPLE<br>INTER-<br>VAL<br>(FT) | DEPTH<br>TO BOT-<br>OM OF<br>SAMPLE<br>INTER-<br>VAL<br>(FT) | TOTAL<br>NITRO-<br>GEN<br>(N)<br>(MG/L) | TOTAL<br>ORGANIC<br>NITRO-<br>GEN<br>(N)<br>(MG/L) | TOTAL<br>AMMONIA<br>NITRO-<br>GEN<br>(N)<br>(MG/L) | TOTAL<br>NITRATE<br>(N)<br>(MG/L) | TOTAL<br>NITRATE<br>(N)<br>(MG/L) | TOTAL<br>PHOS-<br>PHORUS<br>(P)<br>(MG/L) | TOTAL<br>ORTHOPHOS-<br>PHORUS<br>(P)<br>(MG/L) |
|--|------|--|--|---|--|--|-----------------------------------|-----------------------------------|---|--|
|  |      |  |  |   |  |  |                                   |                                   |   |  |
| SO CROSS INJ WELL (LAT 27 49 29 LONG 082 44 35.01)       |      |  |  |   |  |  |                                   |                                   |   |  |
| OCT 17... 1974   | 1400 | 961  | 1080   | .65                                     | .17  | .48  | .00                               | .00                               | .03                                       | .03  |
| SOUTH CROSS INJ MON 800 (LAT 27 49 29 LONG 082 44 35.02) |      |  |  |   |  |  |                                   |                                   |   |  |
| OCT 23... 1974   | 1210 | 746  | 800  | .65                                     | .12  | .53  | .00                               | .00                               | .07                                       | .02  |
| SOUTH CROSS INJ MON 521 (LAT 27 49 29 LONG 082 44 35.03) |      |  |  |   |  |  |                                   |                                   |   |  |
| OCT 23... 1974   | 1240 | 473  | 521  | 1.0                                     | .27  | .73  | .00                               | .00                               | .08                                       | .03  |
| SOUTH CROSS INJ 250 (LAT 27 49 29 LONG 082 44 35.04)     |      |  |  |   |  |  |                                   |                                   |   |  |
| OCT 23... 1974   | 1305 | 200  | 250  | .62                                     | .08  | .54  | .00                               | .00                               | .03                                       | .01  |

Table 24.--Concentrations of nitrogen and phosphorus in water from selected wells at the test site - continued

| DATE   | TIME | WELL NUMBER | DEPTH<br>TO HOLE<br>OF<br>SAMPLE | INTER-<br>VAL<br>(FT) | TOTAL<br>NITRO-<br>GEN<br>(MG/L) | TOTAL<br>AMMONIACAL<br>NITRO-<br>GEN<br>(MG/L) | TOTAL<br>NITRITE<br>(N)<br>(MG/L) | TOTAL<br>NITRATE<br>(N)<br>(MG/L) | TOTAL<br>NITRATE<br>(N)<br>(MG/L) | TOTAL<br>PHOS-<br>PHORUS<br>(P)<br>(MG/L) | TOTAL<br>PHOS-<br>PHORUS<br>(P)<br>(MG/L) |
|--|------|-------------|----------------------------------|-----------------------|----------------------------------|--|-----------------------------------|-----------------------------------|-----------------------------------|---|---|
|  |      |             |                                  |                       |                                  |  |                                   |                                   |                                   |   |   |
| SOUTH CROSS MUN 1<24° (LAT 27 49 22 LONG 082 44 31.04)   |      |             |                                  |                       |                                  |  |                                   |                                   |                                   |   |   |
| JUL 16... 1974   | 1030 | 1210        | 1214                             |                       | .11                              |  | .00                               | .00                               | .13                               | .00                                       |   |
| SOUTH CROSS MUN 105° (LAT 27 49 22 LONG 082 44 31.03)    |      |             |                                  |                       |                                  |  |                                   |                                   |                                   |   |   |
| JUL 17... 1974   | 1225 | 1025        | 1055                             |                       | .47                              | .02  | .45                               | .00                               | .01                               | .00                                       |   |
| SOUTH CROSS MONITOR 815 (LAT 27 49 22 LONG 082 44 31.02) |      |             |                                  |                       |                                  |  |                                   |                                   |                                   |   |   |
| JUL 17... 1974   | 1350 | 780         | 815                              |                       | .72                              | .30  | .42                               | .00                               | .02                               | .02                                       |   |
| SOUTH CROSS MONITOR 520 (LAT 27 49 22 LONG 082 44 31.01) |      |             |                                  |                       |                                  |  |                                   |                                   |                                   |   |   |
| FEB 14... 1973   | 1830 | 374         | 490                              |                       | --                               | --   | --                                | .00                               | .00                               | .35                                       | --  |
| JUL 11... 1974   | 1345 | 1863        | 2118                             |                       | 4.2                              | .48  | .08                               | .00                               | .04                               | .04                                       |   |
| MAR 20... 1974   | 1700 | 1863        | 3280                             |                       | 7.2                              | 2.5  | 4.7                               | .01                               | .08                               | --  | --  |
| EXPLOATORY HOLE (LAT 27 49 22 LONG 082 44 31)            |      |             |                                  |                       |                                  |  |                                   |                                   |                                   |   |   |
| WELL NUMBER E1   |      |             |                                  |                       |                                  |  |                                   |                                   |                                   |   |   |
| JUL 17... 1974   | 463  | 520         | .31                              |                       | .31                              |  | .00                               | .00                               | .04                               | .03                                       |   |

Table 25.—Record of wells near the South Cross Bayou test site

| Well number | Latitude<br>Longitude | Name or owner       | Land surface altitude<br>(ft above mean sea level) | Reported total depth<br>(ft below land surface) | Reported casing depth<br>(ft below land surface) | Casing diameter<br>(in) | Distance from injection well Al (ft) |
|-------------|-----------------------|---------------------|--|---|--|-------------------------|--------------------------------------|
| S1          | 274840N0824433.01     | Isle of Palms       | 20   | 187   | --   | 2                       | 4950                                 |
| S2          | 274850N0824355.01     | E1 Rey Trailer Park | 17   | 35  | --   | 1.5                     | 5330                                 |
| S3          | 274852N0824353.01     | E1 Rey Trailer Park | 17   | 90  | --   | 2                       | 5450                                 |
| S4          | 274904N0824406.01     | Kubanka             | 17   | 100   | --   | 2                       | 3770                                 |
| S5          | 274906N0824359.01     | Stevens             | 17   | 198   | 135  | 2                       | 4290                                 |
| S6          | 274906N0824406.01     | Boluzar             | 16   | 56  | --   | 2                       | 3650                                 |
| S7          | 274907N0824505.01     | Paradise Shores     | 10   | 240   | --   | 4                       | 3120                                 |
| S8          | 274910N0824433.01     | E. T. Johns         | 5  | 60  | --   | 2                       | 2080                                 |
| S9          | 274912N0834410.01     | Mitchell            | 15   | 150   | --   | -                       | 3120                                 |
| S10         | 274913N0824439.01     | Beleroze            | 10   | 25  | --   | 1-1/4                   | 1820                                 |
| S11         | 274916N0824458.01     | Five Towns          | 10   | 300   | --   | -                       | 2210                                 |
| S12         | 274918N0824431.01     | Spangler            | 10   | 100   | --   | 2                       | 1430                                 |
| S13         | 274925N0824458.01     | Five Towns          | 8  | 302   | 127  | 6                       | 1700                                 |
| S14         | 275007N0824441.01     | Showard             | 11   | 60  | --   | 1-1/4                   | 3770                                 |
| S15         | 275008N0824429.01     | Butler              | 10   | 146   | 105  | 3                       | 3900                                 |
| S16         | 275010N0824433.01     | Butler              | 12   | 98  | 90   | 2                       | 4030                                 |

Table 26.—Chemical analyses of water from selected wells near the test site

| DATE  | TIME       | TOTAL<br>DEPTH<br>OF<br>WELL<br>(FT) | TEMPER-<br>ATURE<br>(°F G C) | PH<br>(MICRO-<br>MHOES) | ALKALI-<br>NITY<br>AS<br>(UNITS) | ACIDIC-<br>RONATE<br>(HCN3)<br>(MG/L) | CARBONATE<br>(CO3)<br>(MG/L) | TOTAL<br>SULFIDE<br>(S)<br>(MG/L) | DIS-                                     |
|---|------------|--------------------------------------|------------------------------|-------------------------|----------------------------------|---------------------------------------|------------------------------|-----------------------------------|--|
|   |            |                                      |                              |                         |                                  |                                       |                              |                                   | DIS-<br>SOLVENT<br>CHLOR-<br>IDE<br>(CL) |
| WELL NUMBER S1  |            |                                      |                              |                         |                                  |                                       |                              |                                   |  |
| MAR.. 1973<br>01... 1505<br>SEP.. 1975<br>02... 1340  | 147<br>187 | --<br>--                             | 1180<br>979                  | --<br>--                | --<br>--                         | --<br>--                              | --<br>--                     | --<br>--                          | 210<br>130                               |
| WELL NUMBER S2  |            |                                      |                              |                         |                                  |                                       |                              |                                   |  |
| MAR.. 1973<br>01... 1445                              | 35         | --                                   | 236                          | --                      | --                               | --                                    | --                           | --                                | 54                                       |
| WELL NUMBER S3  |            |                                      |                              |                         |                                  |                                       |                              |                                   |  |
| MAR.. 1973<br>01... 1440<br>SEP.. 1975<br>02... 1300  | 90         | --                                   | 760                          | --                      | --                               | --                                    | --                           | --                                | 110                                      |
| WELL NUMBER S4  |            |                                      |                              |                         |                                  |                                       |                              |                                   |  |
| MAR.. 1973<br>01... 1240<br>SEP.. 1975<br>02... 1130  | 100        | --                                   | 725                          | --                      | --                               | --                                    | --                           | --                                | 52                                       |
| WELL NUMBER S5  |            |                                      |                              |                         |                                  |                                       |                              |                                   |  |
| JULY.. 1974<br>17... 1521<br>AUG.. 1975<br>20... 1310 | 198        | 26.5                                 | 1330                         | 6.5                     | 215                              | 262                                   | 0                            | --                                | 290                                      |
| STEVEN'S (LAT 27 49 06 LONG 082 43 59.01)             |            |                                      |                              |                         |                                  |                                       |                              |                                   |  |

Table 26.--Chemical analyses of water from selected wells near the test site - continued

| DATE                                     | MAP.<br>SOLVED<br>FLUOR.<br>SULFATE<br>( $\text{SO}_4$ )<br>( $\text{Mg/L}$ ) | WELL<br>SOLVED<br>SOLVENT<br>FLUOR.<br>RIDGE<br>( $\text{F}$ )<br>( $\text{mg/L}$ )                      | WELL<br>DIS-<br>SOLVED<br>SOLVENT<br>CAI -<br>CLUM<br>( $\text{Ca}$ )<br>( $\text{mg/L}$ )               | WELL<br>DIS-<br>SOLVED<br>NE -<br>SOLVED<br>SILICA<br>( $\text{K}$ )<br>( $\text{mg/L}$ )                | WELL<br>DIS-<br>SOLVED<br>PO-<br>SOLVED<br>SILICA<br>( $\text{K}$ )<br>( $\text{mg/L}$ )                 | WELL<br>DIS-<br>SOLVED<br>RESI-<br>SOLID<br>DUF AT<br>( $\text{SiO}_2$ )<br>( $\text{mg/L}$ )            | WELL<br>DIS-<br>SOLVED<br>SOLIDS<br>(SUM OF<br>SOLIDS<br>AT<br>( $\text{mg/L}$ )<br>( $\text{mg/L}$ )    | DENSITY<br>( $\text{GM}/\text{ML}$ )   |
|--|---|--|--|--|--|--|--|--|
| MAR. 1973<br>01.00<br>SFP. 1975<br>02.00 | --<br>--<br>4.4   | --<br>--<br>--   | --<br>--<br>35   | --<br>--<br>--   | --<br>--<br>--   | --<br>--<br>--   | --<br>--<br>--   | --   |
| JULY 1974<br>01.00<br>SFP. 1975<br>02.00 | 1.473<br>1.075<br>1.04  | WELL NUMBER S1<br>WELL NUMBER S2<br>WELL NUMBER S3<br>WELL NUMBER S4<br>WELL NUMBER S5<br>WELL NUMBER S6 | WELL NUMBER S1<br>WELL NUMBER S2<br>WELL NUMBER S3<br>WELL NUMBER S4<br>WELL NUMBER S5<br>WELL NUMBER S6 | WELL NUMBER S1<br>WELL NUMBER S2<br>WELL NUMBER S3<br>WELL NUMBER S4<br>WELL NUMBER S5<br>WELL NUMBER S6 | WELL NUMBER S1<br>WELL NUMBER S2<br>WELL NUMBER S3<br>WELL NUMBER S4<br>WELL NUMBER S5<br>WELL NUMBER S6 | WELL NUMBER S1<br>WELL NUMBER S2<br>WELL NUMBER S3<br>WELL NUMBER S4<br>WELL NUMBER S5<br>WELL NUMBER S6 | WELL NUMBER S1<br>WELL NUMBER S2<br>WELL NUMBER S3<br>WELL NUMBER S4<br>WELL NUMBER S5<br>WELL NUMBER S6 | WELL NUMBER S1<br>WELL NUMBER S2<br>WELL NUMBER S3<br>WELL NUMBER S4<br>WELL NUMBER S5<br>WELL NUMBER S6 |
| MAP. 1973<br>01.00<br>SFP. 1975<br>02.00 | --<br>--<br>1.1   | WELL NUMBER S1<br>WELL NUMBER S2<br>WELL NUMBER S3<br>WELL NUMBER S4<br>WELL NUMBER S5<br>WELL NUMBER S6 | WELL NUMBER S1<br>WELL NUMBER S2<br>WELL NUMBER S3<br>WELL NUMBER S4<br>WELL NUMBER S5<br>WELL NUMBER S6 | WELL NUMBER S1<br>WELL NUMBER S2<br>WELL NUMBER S3<br>WELL NUMBER S4<br>WELL NUMBER S5<br>WELL NUMBER S6 | WELL NUMBER S1<br>WELL NUMBER S2<br>WELL NUMBER S3<br>WELL NUMBER S4<br>WELL NUMBER S5<br>WELL NUMBER S6 | WELL NUMBER S1<br>WELL NUMBER S2<br>WELL NUMBER S3<br>WELL NUMBER S4<br>WELL NUMBER S5<br>WELL NUMBER S6 | WELL NUMBER S1<br>WELL NUMBER S2<br>WELL NUMBER S3<br>WELL NUMBER S4<br>WELL NUMBER S5<br>WELL NUMBER S6 | WELL NUMBER S1<br>WELL NUMBER S2<br>WELL NUMBER S3<br>WELL NUMBER S4<br>WELL NUMBER S5<br>WELL NUMBER S6 |
| JULY 1974<br>1.700<br>AUG. 1975<br>20.00 | 25<br>1.2   | WELL NUMBER S1<br>WELL NUMBER S2<br>WELL NUMBER S3<br>WELL NUMBER S4<br>WELL NUMBER S5<br>WELL NUMBER S6 | WELL NUMBER S1<br>WELL NUMBER S2<br>WELL NUMBER S3<br>WELL NUMBER S4<br>WELL NUMBER S5<br>WELL NUMBER S6 | WELL NUMBER S1<br>WELL NUMBER S2<br>WELL NUMBER S3<br>WELL NUMBER S4<br>WELL NUMBER S5<br>WELL NUMBER S6 | WELL NUMBER S1<br>WELL NUMBER S2<br>WELL NUMBER S3<br>WELL NUMBER S4<br>WELL NUMBER S5<br>WELL NUMBER S6 | WELL NUMBER S1<br>WELL NUMBER S2<br>WELL NUMBER S3<br>WELL NUMBER S4<br>WELL NUMBER S5<br>WELL NUMBER S6 | WELL NUMBER S1<br>WELL NUMBER S2<br>WELL NUMBER S3<br>WELL NUMBER S4<br>WELL NUMBER S5<br>WELL NUMBER S6 | WELL NUMBER S1<br>WELL NUMBER S2<br>WELL NUMBER S3<br>WELL NUMBER S4<br>WELL NUMBER S5<br>WELL NUMBER S6 |

Table 26.—Chemical analyses of water from selected wells near the test site—continued

|                 |            |             | TOTAL<br>SOLDF. | CATIONIC<br>CONC.<br>OF<br>DUCT-<br>ANCE<br>(MICRO-<br>MHS) | PH<br>(UNITS) | ALKALI-<br>LITY<br>AS<br>CACO <sub>3</sub><br>(MG/L) | HICAP-<br>BONATE<br>(HCO <sub>3</sub> )<br>(MG/L) | CAR-<br>BONATE<br>(CO <sub>3</sub> )<br>(MG/L) | TOTAL<br>SULF.<br>FIDE.<br>(S)<br>(MG/L) | DIS-<br>SOLVF.<br>CHLO-<br>RIDE.<br>(CL)<br>(MG/L) |
|-----------------|------------|-------------|-----------------|---|---------------|--|---|--|--|--|
| WELL NUMBER 56  |            |             |                 |   |               |  |   |  |  |  |
| MAR. • 1973     | 01. • 1975 | AUG. • 1975 | 20. • 1975      | 56  | --            | 720  | --  | --   | --                                       | 56   |
| 08. • 1973      | 1145       | 240         | --              | 56  | --            | 718  | --  | --   | --                                       | 55   |
| SEP. • 1975     | 1325       | 25.3        | --              | 56  | --            | 718  | --  | --   | --                                       | 55   |
| WELL NUMBER 57  |            |             |                 |   |               |  |   |  |  |  |
| MAR. • 1973     | 08. • 1975 | AUG. • 1975 | 20. • 1975      | 240   | --            | 1250   | 7.9   | 217  | 264                                      | 240  |
| 01. • 1973      | 1400       | 240         | --              | 240   | --            | 1220   | --  | --   | --                                       | 240  |
| WELL NUMBER 58  |            |             |                 |   |               |  |   |  |  |  |
| MAR. • 1973     | 01. • 1973 | AUG. • 1975 | 20. • 1975      | 60  | --            | 650  | --  | --   | --                                       | 27   |
| 01. • 1973      | 1400       | 25.7        | --              | 60  | --            | 650  | --  | --   | --                                       | 27   |
| WELL NUMBER 59  |            |             |                 |   |               |  |   |  |  |  |
| MAR. • 1973     | 08. • 1975 | AUG. • 1975 | 20. • 1975      | 150   | --            | 560  | 7.6   | 269  | 328                                      | 22   |
| 01. • 1973      | 1345       | 150         | --              | 150   | 25.7          | 555  | --  | --   | --                                       | 21   |
| WELL NUMBER 510 |            |             |                 |   |               |  |   |  |  |  |
| MAR. • 1973     | 01. • 1973 | AUG. • 1975 | 20. • 1975      | 25  | --            | 540  | --  | --   | --                                       | 16   |
| 01. • 1973      | 1340       | 25          | --              | 25  | 26.1          | 646  | --  | --   | --                                       | 33   |
| WELL NUMBER 511 |            |             |                 |   |               |  |   |  |  |  |
| MAR. • 1973     | 01. • 1973 | AUG. • 1975 | 20. • 1975      | 25  | --            | 540  | --  | --   | --                                       | 16   |
| 01. • 1973      | 1340       | 25          | --              | 25  | 26.1          | 646  | --  | --   | --                                       | 33   |

Table 26.--Chemical analyses of water from selected wells near the test site - continued

| DATE             | WELL NUMBER | WELL NAME   |   | DIS-  |                                    | DIS-   |   | DIS-   |  | DIS-   |  |
|------------------|-------------|---|---|---|------------------------------------|--|---|--|--|--|--|
|                  |             | SOLVED<br>FLUO-<br>RIDE<br>(SO <sub>4</sub> )<br>(MG/L) | SOLVED<br>CAL-<br>CLIM<br>(F)<br>(MG/L) | SOLVED<br>KAG-<br>SIL-<br>TUM<br>(CA)<br>(MG/L) | SOLVED<br>SODIUM<br>(NA)<br>(MG/L) | SOLVED<br>PO-<br>TAS-<br>SIUM<br>(K)<br>(MG/L) | SOLVED<br>SILICA<br>(SiO <sub>2</sub> )<br>(MG/L) | SOLVED<br>RESI-<br>DUE AT<br>CONSTI-<br>TUENTS<br>(MG/L) | SOLVED<br>SOLIDS<br>(SUM OF<br>SILICA<br>(SiO <sub>2</sub> )<br>(MG/L) | SOLVED<br>SOLIDS<br>(SUM OF<br>CONSTI-<br>TUENTS<br>(MG/L) | SOLVED<br>SOLIDS<br>(SUM OF<br>CONSTI-<br>TUENTS<br>(MG/L) |
| WELL NAME: S6    |             |   |   |   |                                    |  |   |  |  |  |  |
| MAR•• 1973       | --          | --  | --                                      | --  | --                                 | --   | --  | --   | --   | --   | --   |
| APR•• 1975       | 1.02        | --  | --                                      | --  | 30                                 | --   | --  | --   | --   | --   | 0.998  |
| WELL NUMBER: S7  |             |   |   |   |                                    |  |   |  |  |  |  |
| MAR•• 1973       | 16          | •4  | 120                                     | 35  | 49                                 | 11   | 37  | 902  | 641  | 1.001  |  |
| SEP•• 1975       | 34          | --  | --                                      | --  | 48                                 | --   | --  | --   | --   | 0.998  |  |
| WELL NUMBER: S8  |             |   |   |   |                                    |  |   |  |  |  |  |
| MAR•• 1973       | --          | --  | --                                      | --  | --                                 | --   | --  | --   | --   | --   | --   |
| WELL NUMBER: S9  |             |   |   |   |                                    |  |   |  |  |  |  |
| MAR•• 1973       | 4.00        | •3  | 70                                      | 16  | 20                                 | 3.8  | 42  | 346  | 736  | 1.001  |  |
| APR•• 1975       | 25          | --  | --                                      | --  | 20                                 | --   | --  | --   | --   | 0.998  |  |
| WELL NUMBER: S10 |             |   |   |   |                                    |  |   |  |  |  |  |
| MAR•• 1973       | --          | --  | --                                      | --  | --                                 | --   | --  | --   | --   | --   | --   |
| APR•• 1975       | 25          | --  | --                                      | --  | 17                                 | --   | --  | --   | --   | 0.998  |  |

Table 26.—Chemical analyses of water from selected wells near the test site—continued

| DATE                    | TIME | WELL<br>(F) | TEMPER-<br>ATURE<br>(DEG. C.) | DUCT-<br>ANCE<br>(MICRONS) | CONC-<br>ENTRATION<br>(MG/L) | SPEC-<br>IFIC<br>COND. |                                  | ALKALI-<br>LITY<br>AS<br>(UNITS) | BICAR-<br>BOONATE<br>(HCO <sub>3</sub> )<br>(MG/L) | CARBONATE<br>(CO <sub>3</sub> )<br>(MG/L) | TOTAL<br>SULFATE<br>(S)<br>(MG/L) | DIS-<br>SOLVENT<br>CHLO-<br>RIDE<br>(CL) |  |
|-------------------------|------|-------------|-------------------------------|----------------------------|------------------------------|------------------------|----------------------------------|----------------------------------|--|---|-----------------------------------|--|--|
|                         |      |             |                               |                            |                              | pH                     | ALKALI-<br>LITY<br>AS<br>(UNITS) |                                  |  |   |                                   |  |  |
| WELL NUMBER S11         |      |             |                               |                            |                              |                        |                                  |                                  |  |   |                                   |  |  |
| MAR. 1973<br>02... 1120 | 300  |             | —                             | 1040                       | 7.6                          | 207                    | 252                              | 0                                | 4.6  | 180                                       |                                   |  |  |
| AUG. 1975<br>20... 1435 | 300  | 24.2        | 1100                          | —                          | —                            | —                      | —                                | —                                | —  | —   | 190                               |  |  |
| WELL NUMBER S12         |      |             |                               |                            |                              |                        |                                  |                                  |  |   |                                   |  |  |
| MAR. 1973<br>03... 1020 | 100  |             | —                             | 660                        | 7.7                          | 315                    | 394                              | 0                                | 1.3  | 37  |                                   |  |  |
| AUG. 1975<br>20... 1245 | 100  | 24.3        | 672                           | —                          | —                            | —                      | —                                | —                                | —  | —   | 35                                |  |  |
| WELL NUMBER S13         |      |             |                               |                            |                              |                        |                                  |                                  |  |   |                                   |  |  |
| AUG. 1975<br>20... 1450 | 302  | 24.4        | 3610                          | —                          | —                            | —                      | —                                | —                                | —  | —   | 970                               |  |  |
| WELL NUMBER S14         |      |             |                               |                            |                              |                        |                                  |                                  |  |   |                                   |  |  |
| MAR. 1973<br>01... 1140 | 60   |             | —                             | 530                        | —                            | —                      | —                                | —                                | —  | —   | 9.8                               |  |  |
| AUG. 1975<br>20... 1545 | 60   | 25.4        | 528                           | —                          | —                            | —                      | —                                | —                                | —  | —   | 11                                |  |  |
| WELL NUMBER S15         |      |             |                               |                            |                              |                        |                                  |                                  |  |   |                                   |  |  |
| MAR. 1973<br>08... 0900 | 146  |             | —                             | 1150                       | 7.6                          | 210                    | 256                              | 0                                | 5.1  | 210                                       |                                   |  |  |
| SEP. 1975<br>02... 1200 | 146  | —           | 1160                          | —                          | —                            | —                      | —                                | —                                | —  | —   | 210                               |  |  |

Table 26.—Chemical analyses of water from selected wells near the test site—continued

| DATE  | TIME<br>SOL VF D<br>FLIC-<br>P TCE<br>(SCN)<br>(MG/L) | DIS-<br>SOL VF D<br>FLIC-<br>P TCE<br>(+)<br>(MG/L) | DIS-<br>SOL VF D<br>NE-<br>STUM<br>(CA)<br>(MG/L) | DIS-<br>SOL VF D<br>NE-<br>STUM<br>(NA)<br>(MG/L) | DIS-<br>SOL VF D<br>NE-<br>STUM<br>(K)<br>(MG/L) | DIS-<br>SOL VF D<br>NE-<br>STUM<br>(SiO2)<br>(MG/L) | DIS-<br>SOL VF D<br>NE-<br>STUM<br>(Mg/C)<br>(MG/L) | DIS-<br>SOL VF D<br>NE-<br>STUM<br>(AT)<br>(MG/L) | DIS-<br>SOL VF D<br>NE-<br>STUM<br>(20 C) |
|---|---|---|---|---|--|---|---|---|---|
|   |   |   |   |   |  |   |   |   |   |
| WELL NUMBER S11                             |   |   |   |   |  |   |   |   |   |
| MAR.. 1973<br>08...<br>AUG.. 1975<br>20.... | 32<br>•4<br>75<br>--                                  | •4<br>110<br>--<br>--                               | 32<br>--<br>--<br>--                              | 41<br>40<br>--<br>--                              | 10<br>--<br>--<br>--                             | 39<br>--<br>--<br>--                                | 786<br>--<br>--<br>--                               | 571<br>--<br>--<br>--                             | 1.000<br>0.998                            |
| WELL NUMBER S12                             |   |   |   |   |  |   |   |   |   |
| MAR.. 1973<br>08...<br>AUG.. 1975<br>20.... | •3<br>•3<br>1.3<br>--                                 | •3<br>100<br>--<br>--                               | 10<br>--<br>--<br>--                              | 28<br>28<br>--<br>--                              | •9<br>--<br>--<br>--                             | 22<br>--<br>--<br>--                                | 404<br>--<br>--<br>--                               | 389<br>--<br>--<br>--                             | --  |
| WELL NUMBER S13                             |   |   |   |   |  |   |   |   |   |
| AUG.. 1975<br>20....                        | H2<br>--  | --<br>--  | --<br>--  | --<br>--  | 320<br>--  | --<br>--  | --<br>--  | --<br>--  | 0.999                                     |
| WELL NUMBER S14                             |   |   |   |   |  |   |   |   |   |
| MAR.. 1973<br>01...<br>AUG.. 1975<br>20.... | 36<br>--<br>75<br>1.3                                 | --<br>--<br>--<br>--                                | --<br>--<br>--<br>--                              | --<br>--<br>7.7<br>--                             | --<br>--<br>--<br>--                             | --<br>--<br>--<br>--                                | --<br>--<br>--<br>--                                | --<br>--<br>--<br>--                              | --  |
| WELL NUMBER S15                             |   |   |   |   |  |   |   |   |   |
| MAR.. 1973<br>01...<br>SEP.. 1975<br>02...  | 36<br>--<br>75<br>2.3                                 | •4<br>--<br>--<br>--                                | 110<br>--<br>--<br>--                             | 32<br>--<br>--<br>--                              | 47<br>--<br>46<br>--                             | 7.8<br>--<br>--<br>--                               | 38<br>--<br>--<br>--                                | 590<br>--<br>--<br>--                             | 610<br>1.000<br>0.999                     |
| WELL NUMBER S16                             |   |   |   |   |  |   |   |   |   |
| FIVE TOWNS (LAT 27 49 16 LONG 082 44 58.01) |   |   |   |   |  |   |   |   |   |
| SPANGER (LAT 27 49 18 LONG 082 44 31.01)    |   |   |   |   |  |   |   |   |   |
| FIVE TOWNS (LAT 27 49 25 LONG 082 44 58.01) |   |   |   |   |  |   |   |   |   |
| SHOWARD (LAT 27 50 07 LONG 082 44 41.01)    |   |   |   |   |  |   |   |   |   |
| HUTLER (LAT 27 50 08 LONG 082 44 29.01)     |   |   |   |   |  |   |   |   |   |

Table 26.--Chemical analyses of water from selected wells near the test site - continued

| DATE            | TIME | WELL<br>(FT) | DEPTH<br>OF<br>WELL<br>(FT) | TEMPER-<br>ATURE<br>(DEG C) | DUCT-<br>ANCE<br>(MICRO-<br>MHOES) | PH<br>(UNITS) | ALKA-<br>LINITY<br>AS<br>(MG/L) | PICA-<br>RONATE<br>(HC03)<br>(MG/L) | CAR-<br>BONATE<br>(CO3)<br>(MG/L) | TOTAL<br>SUL-<br>FIDE<br>(MG/L)        |                   |                                 | DIS-<br>SOLVED<br>CHLO-<br>RINE<br>(CL)<br>(MG/L) |
|-----------------|------|--------------|-----------------------------|-----------------------------|------------------------------------|---------------|---------------------------------|-------------------------------------|-----------------------------------|--|-------------------|---------------------------------|---|
|                 |      |              |                             |                             |                                    |               |                                 |                                     |                                   | SPE-<br>CIFIC<br>CON-<br>DUCT-<br>ANCE | (MICRO-<br>MHOES) | TOTAL<br>SUL-<br>FIDE<br>(MG/L) |   |
| WELL NUMBER S16 |      |              |                             |                             |                                    |               |                                 |                                     |                                   |  |                   |                                 |   |
| FEB. 26... 1973 |      | 1235         | 98                          | --                          | 660                                | --            | --                              | --                                  | --                                |  |                   | 19                              |   |
| SEP. 02... 1975 |      | 1220         | 98                          | --                          | --                                 | --            | --                              | --                                  | --                                |  |                   | 13                              |   |

Table 26.--Chemical analyses of water from selected wells near the test site - continued

|             | WELL NUMBER S16 | PUTLER (LAT 27 50 10 LONG 082 44 33.01) | DIS-   | SOLVED | DIS- | SOLVED | DIS-   | SOLVED | DIS-   | SOLVED  | DIS-    | SOLVED  |
|-------------|-----------------|---|--------|--------|------|--------|--------|--------|--------|---------|---------|---------|
|             |                 |   | SOLVED | SOLVED | MAG- | POT-   | SOLVED | SOLVED | RESI-  | SOLIDS  | SOLIDS  | DENSITY |
|             |                 |   | (MG/L) | (MG/L) | NE-  | TAS-   | SILICA | SILICA | DUF AT | (SUM OF | (GM/ML) | (GM/ML) |
| FFH... 1973 | --              | --                                      | --     | --     | --   | --     | --     | --     | --     | --      | --      | --      |
| 26... 1975  | --              | --                                      | --     | --     | --   | --     | --     | --     | --     | --      | --      | --      |
| SEP... 1975 | 1.1             | --                                      | --     | --     | --   | 8.4    | --     | --     | --     | --      | --      | 0.998   |
| OCT... 1975 | --              | --                                      | --     | --     | --   | --     | --     | --     | --     | --      | --      | --      |

Table 27.--Concentrations of nitrogen, phosphorus, coliform, and streptococci in water from selected wells near the test site

| DATE           | TIME | WELL | NUMBER | WELL NUMBER 51                                |  |  |  | WELL NUMBER 55                            |   |  |  | WELL NUMBER 59   |  |   |   | WELL NUMBER 54 |  |  |  | WELL NUMBER 59 |  |  |  |
|----------------|------|------|--------|---|--|--|--|---|---|--|--|--|--|---|---|----------------|--|--|--|----------------|--|--|--|
|                |      |      |        | TOTAL<br>NITRUE<br>OF<br>GEN<br>(N)<br>(MG/L) | TOTAL<br>ORGANIC<br>NITRUE<br>GEN<br>(N)<br>(MG/L) | TOTAL<br>AMMONIA<br>NITRUE<br>GEN<br>(N)<br>(MG/L) | TOTAL<br>NITRATE<br>NITRUE<br>GEN<br>(N)<br>(MG/L) | TOTAL<br>PHOS-<br>PHORUS<br>(P)<br>(MG/L) | TOTAL<br>PHOS-<br>PHORUS<br>(P)<br>(MG/L) | TOTAL<br>URINE<br>PHOS-<br>PHORUS<br>(P)<br>(MG/L) | TOTAL<br>URINE<br>PHOS-<br>PHORUS<br>(P)<br>(MG/L) | TOTAL<br>COLI-<br>FORM<br>(COL-<br>ONIES<br>PER<br>100 mL) | TOTAL<br>COLI-<br>FORM<br>(COL-<br>ONIES<br>PER<br>100 mL) | TOTAL<br>STREPTO-<br>TOCOCCEI<br>(COL-<br>ONIES<br>PER<br>100 mL) | TOTAL<br>STREPTO-<br>TOCOCCEI<br>(COL-<br>ONIES<br>PER<br>100 mL) |                |  |  |  |                |  |  |  |
| JUN 13... 1974 | 0900 | 187  |        | --  | --   | --   | --   | --  | --  | --   | --   | <1   | <1   | <1  | <1  |                |  |  |  |                |  |  |  |
| JUL 08... 1974 | 0845 | 198  |        | --  | --   | --   | --   | --  | --  | --   | --   | <1   | <1   | <1  | <1  |                |  |  |  |                |  |  |  |
| JUL 17... 1974 | 1521 | 198  |        | •73   | •29  | •44  | •00  | •00                                       | •03                                       | •03  | •03  | --   | --   | --  | --  |                |  |  |  |                |  |  |  |
| JUN 08... 1973 | 1145 | 240  |        | •45   | •45  | •40  | •00  | •00                                       | ---                                       | 4•0  | 0  | 0  | 0  | 0   | 0   |                |  |  |  |                |  |  |  |
|                |      |      |        |   |  |  |  |   |   |  |  |  |  |   |   |                |  |  |  |                |  |  |  |
| MAR 03... 1973 | 0955 | 150  |        | •99   | •51  | •44  | •00  | •00                                       | ---                                       | 5•1  | 0  | 0  | 0  | 0   | 0   |                |  |  |  |                |  |  |  |
| JUN 13... 1974 | 0840 | 150  |        | --  | --   | --   | --   | --  | --  | --   | --   | <1   | <1   | <1  | <1  |                |  |  |  |                |  |  |  |
| JUN 13... 1973 | 1120 | 300  |        | •70   | •02  | •68  | •00  | •00                                       | ---                                       | 5•0  | 13   | 0  | 0  | 0   | 0   |                |  |  |  |                |  |  |  |
| JUN 13... 1974 | 0835 | 300  |        | --  | --   | --   | --   | --  | --  | --   | --   | <1   | <1   | <1  | <1  |                |  |  |  |                |  |  |  |

Table 27. -Concentrations of nitrogen, phosphorus, coliform, and streptococci in water from selected wells near the test site - continued

| DATE            | TIME | WELL | DEPTH<br>OF<br>WELL<br>(FT) | TOTAL<br>NITRO-<br>GEN<br>(N)<br>(MG/L) | TOTAL<br>ORGANIC<br>NITRO-<br>GEN<br>(N)<br>(MG/L) | TOTAL<br>AMMONIA<br>NITRO-<br>GEN<br>(N)<br>(MG/L) | TOTAL<br>NITRATE<br>(N)<br>(MG/L) | TOTAL<br>NITRATE<br>(N)<br>(MG/L) | TOTAL<br>PHOS-<br>PHORUS<br>(P)<br>(MG/L) | TOTAL<br>PHOS-<br>PHORUS<br>(P)<br>(MG/L) | IMMEDIATE  |  | STREP-<br>TOCCCI<br>(COL-<br>ONIES<br>PER<br>100<br>ML) |
|-----------------|------|------|-----------------------------|---|--|--|-----------------------------------|-----------------------------------|---|---|--|--|---|
|                 |      |      |                             |   |  |  |                                   |                                   |   |   | FECAL<br>COLI-<br>FORM<br>(COL.<br>PER<br>100<br>ML) | FECAL<br>COLI-<br>FORM<br>(COL.<br>PER<br>100<br>ML) |   |
| WELL NUMBER S12 |      |      |                             |   |  |  |                                   |                                   |   |   |  |  |   |
| MAR 08... 1973  | 1020 | 100  | .54                         | .16                                     | .39  | .00  | .00                               | --                                | --  | 2.8                                       | 0  | 0  | --  |
| JUN 13... 1974  | 0825 | 100  | --                          | --                                      | --   | --   | --                                | --                                | --  | <1  | <1   | <1   | <1  |
| WELL NUMBER S15 |      |      |                             |   |  |  |                                   |                                   |   |   |  |  |   |
| MAR 08... 1973  | 0900 | 146  | .89                         | .41                                     | .48  | .00  | .00                               | --                                | 4.8                                       | 0   | 0  | 0  | --  |
| JUN 13... 1974  | 0825 | 146  | --                          | --                                      | --   | --   | --                                | --                                | --  | <1  | <1   | <1   | <1  |
| WELL NUMBER S16 |      |      |                             |   |  |  |                                   |                                   |   |   |  |  |   |
| JUN 13... 1974  | 0815 | 98   | --                          | --                                      | --   | --   | --                                | --                                | --  | <1  | <1   | <1   | 81  |

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