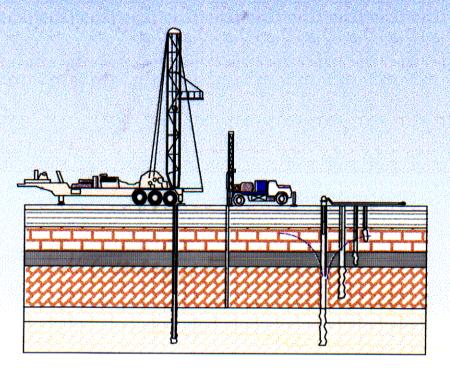
ROMP 5 CECIL WEBB MONITOR WELL SITE CHARLOTTE COUNTY, FLORIDA

VOLUMES THREE AND FOUR

MONITOR WELL CONSTRUCTION AND AQUIFER PERFORMANCE TESTING





Geohydrologic Data Section Resource Data Department Southwest Florida Water Management District September 1997

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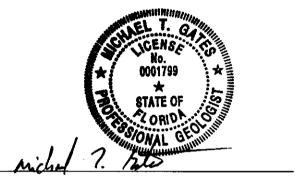
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The geological evaluations and interpretations contained in the ROMP 5 Monitor Well Construction and Aquifer Performance Testing Report have been prepared by or approved by a Certified Professional Geologist in the State of Florida, in accordance with Chapter 492, Florida Statutes.



Michael T. Gates Professional Geologist License No. PG 0001799

Date: <u>9-23-1997</u>

ROMP 5 CECIL WEBB MONITOR WELL SITE CHARLOTTE COUNTY, FLORIDA

VOLUMES THREE AND FOUR

MONITOR WELL CONSTRUCTION AND AQUIFER PERFORMANCE TESTING

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> > September 1997

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1.0 INTRODUCTION

The ROMP 5 (WRAP S-2) Cecil Webb well site is one of six Regional Observation and Monitor-Well Program (ROMP) well sites constructed for the Southern District Water Resource Assessment Project (SDWRAP). The SDWRAP is a long-term study of the ground-water systems in DeSoto County, Hardee County, and portions of Charlotte, Polk, and Sarasota Counties (Figure 1).

The ROMP 5 Well Site was obtained by the Southwest Florida Water Management District (SWFWMD) in December 1992 for construction of a multiple well monitor site. Drilling, testing, and monitor well construction at ROMP 5 was planned in several phases. The data collected during these phases is presented as a four volume report: Volume One - Core Drilling and Testing, Volume Two - Exploratory Drilling and Testing, Volumes Three and Four - Monitor Well Construction and Aquifer Performance Testing.

The first phase, exploratory coring from land surface to 1,304 feet below land surface (bls), began June 1993 and was completed in December 1993. The next phase of work, deep exploratory drilling (below 1,304 ft bls) and testing and monitor well construction was initiated in February 1995. The exploratory drilling and testing was completed in June 1996 and monitor well construction was completed in September 1996. The last phase of work at ROMP 5, aquifer performance testing, began in January 1997 and was completed in April 1997. This report, Volumes Three and Four - Monitor Well Construction and Aquifer Performance Testing, presents the well construction information and the hydraulic data collected during the aquifer performance tests.

2.0 SITE LOCATION

The ROMP 5 (WRAP S-2) Cecil Webb well site is located in Charlotte County, on the south side of Highway 74 (Figure 2). ROMP 5 is located within the Cecil M. Webb Wildlife Management Area in the northwest quarter of the northwest quarter of Section 3, Township 41 South, Range 25 East at latitude 26° 56' 44", longitude 81° 48' 29" (Figure 3). Land surface elevation at the well site is 40 ft above the National Geodetic Vertical Datum of 1929 (NGVD).

3.0 MONITOR WELL CONSTRUCTION

Drilling and construction of six permanent monitor wells at the ROMP 5 Cecil Webb Monitor Well Site began in March 1996 and was completed in July 1996. All permanent monitor wells were drilled by the District contractor, Diversified Drilling, Inc., using a Speedstar 25 drilling rig. Mud- rotary and reverse-air methods of drilling were utilized to construct the monitor wells.

Permanent monitor wells constructed include: a 12-inch diameter surficial aquifer monitor well (MW-1), an 8-inch diameter upper permeable zone intermediate aquifer system monitor well (MW-2), a 12-inch diameter lower permeable zone intermediate aquifer system monitor well (MW-3), a 12-inch diameter Suwannee Limestone/Upper Floridan aquifer monitor well (MW-4), a 4-inch diameter surficial aquifer permanent observation well (MW-5), and a 6-inch diameter Avon Park Formation/Upper Floridan aquifer monitor well (MW-6). The Avon Park well construction was begun with the SWFWMD owned SS 40 drilling rig in 1995, and was later modified by the District contractor, Diversified Drilling, Inc in 1996.

Two temporary observation wells were previously constructed at the ROMP 5 site by the District-owned CME 75 drilling rig. The upper permeable zone intermediate aquifer system observation well and the Suwannee/Upper Floridan observation well, are presented in Figures 4 and 5, respectively. Well construction details for the monitor wells are presented in Table 1. Figure 6 presents a diagram of the hydrogeology of the ROMP 5 well site.

3.1 Surficial Aquifer Monitor Well

A 22-inch diameter borehole was drilled from land surface to 85 feet bls using the mud-rotary drilling method. Following drilling to 85 feet bls, clean water was flushed through the drill rods to clean the mudded hole and the drill rods were removed. Eighty feet of 12-inch diameter schedule 40 poly-vinyl chloride (PVC) .020 well screen (85 to 5 feet bls) and seven feet of 12-inch diameter schedule 40 PVC casing (5 feet bls to 2 feet above land surface) (als) was installed to the bottom of the borehole. A 6-20 grain size silica sand pack was installed in the annulus from 85 feet bls to 2.5 feet bls. Portland cement was installed from 2.5 feet bls to land surface. The well was developed using a mechanical surging device and airlifted until the water appeared clear. The well was capped with a 12-inch diameter PVC cap and an

18-inch locking steel cover was constructed around the well. Figure 7 presents the as-built diagram for the surficial aquifer monitor well (MW-1).

3.2 Upper Permeable Zone Intermediate Aquifer System Monitor Well

A 17.5-inch diameter borehole was drilled from land surface to 60 feet bls using the mud-rotary drilling method. Sixty-one feet of 12-inch diameter welded steel casing was installed to the bottom of the borehole. The casing was pressure grouted in place using the casing method of grouting (formerly known as the Haliburton method) (Driscoll, 1986). An 11.5-inch drill bit was installed into the 12-inch casing and mud-rotary drilling resumed from 60 feet bls to 230 feet bls. After flushing the hole with clean water, 100 feet of schedule 40 PVC .020-inch slotted well screen (230 to 130 feet bls) and 133 feet of schedule 40 PVC casing (130 feet bls to 3 feet als) was installed to the bottom of the borehole. A 6-20 grain sand pack was installed in the annulus from 230 feet bls to 126 feet bls. Bentonite pellets were installed from 126 feet bls to 118 feet bls to form a grout seal above the sand. Portland cement grout slurry was installed from 118 feet bls to land surface using the tremie method of grouting. The well was developed by airlifting. An eight-inch PVC cap was installed on the casing and an 18-inch diameter locking steel cover was constructed around the well. Figure 8 presents the as-built diagram for the upper permeable zone intermediate aquifer monitor well (MW-2).

3.3 Lower Permeable Zone Intermediate Aquifer System Monitor Well

The potentiometric surface of the lower permeable zone of the intermediate aquifer system is above land surface at ROMP 5. The mud-rotary method of drilling was used to keep the well from flowing while drilling and constructing the well. A 23.5-inch diameter borehole was drilled from land surface to 65 feet bls using the mud-rotary drilling method. Sixty-five feet of 18-inch diameter welded steel casing was installed to the bottom of the borehole. The casing was pressure grouted in place using the casing method of grouting. Following grouting, a 17.5-inch bit was installed into the 18-inch casing and mud-rotary drilling resumed from 65 feet bls to 440 feet bls. Twelve-inch diameter welded steel casing was installed from 440 feet bls to 0.5 feet als. The 12-inch casing was pressure grouted in place using the casing method of grouting. Following grouting, an 11.5-inch drill bit was installed into the 12-inch casing and drilling resumed from 440 feet bls to 565 feet bls using the mud-rotary method. The reverse-air method of drilling was used for drilling from 565 feet bls to 600 feet bls. The well was developed using the airlifting method until all drilling mud was flushed from the well. Head levels in the well rose to approximately 10 feet als

after the drilling mud was flushed from the well. A 12-inch x 8-inch diameter steel tee was installed on top of the 12-inch steel casing to stop the flow of water from the well. Figure 9 presents the as-built diagram for the Lower Permeable Zone Intermediate Aquifer System monitor well (MW-3).

3.4 Suwannee Limestone/Upper Floridan Aquifer Monitor Well

The potentiometric surface of the Upper Floridan Aquifer is above land surface at ROMP 5. The mudrotary method of drilling was used to keep the well from flowing while constructing the well. A 23.5-inch diameter borehole was drilled from land surface to 65 feet bls using the mud-rotary drilling method. Sixtyfive feet of 18-inch diameter welded steel casing was installed to the bottom of the borehole. The casing was pressure grouted in place using the casing method of grouting. A 17.5-inch bit was installed into the 18-inch casing and mud-rotary drilling resumed from 65 feet bls to 720 feet bls. Twelve-inch diameter welded steel casing was installed from 720 feet bls to 2 feet als. The 12-inch casing was pressure grouted in place using the casing method of grouting. An 11.5-inch drill bit was installed into the 12-inch casing and drilling resumed from 720 feet bls to 780 feet bls using the mud-rotary method. The reverse-air method of drilling was used for drilling from 780 feet bls to 810 feet bls. Thick sequences of quartz sand encountered at 810 feet bls necessitated the use of drilling mud to continue drilling. The mud-rotary method was used again for drilling from 810 feet bls to 970 feet bls. The well was developed using the airlifting method until all drilling mud and sand was flushed from the well. Head levels in the well rose to approximately 10 feet als after removing the drilling mud from the well. A 12-inch x 8-inch diameter steel tee was installed on top of the 12-inch steel casing to stop the flow of water from the well. Figure 10 presents the as-built diagram for the Suwannee Limestone/Upper Floridan Aquifer monitor well (MW-4).

3.5 Permanent Surficial Aquifer Observation Well

A 12.25-inch diameter borehole was drilled from land surface to 85 feet bls using the mud-rotary method. The drilling mud was flushed from the hole and 80 feet of 4-inch diameter Tri-Lock® schedule 40 PVC 0.010-inch slot well screen (85 feet bls to 5 feet bls) and 7 feet of 4-inch diameter Tri-Lock® schedule 40 PVC casing (5 feet bls to 2 feet als) was installed into the borehole. A 150 gallon mixture of hexaphos® and water was poured into the well to breakdown the remaining drilling mud in the borehole. A 6-20 grain-size silica sand pack was installed from 85 feet bls to 4 feet bls in the annulus of the well. Bentonite chips were installed above the sand from 4 feet bls to 2 feet bls to form a seal. Portland cement was installed from 2 feet bls to land surface. The well was developed using the airlifting method. A 12-inch diameter locking steel cover was installed around the well. Figure 11 presents the as-built diagram for the permanent surficial observation well (MW-5).

3.6 Avon Park/Upper Floridan Aquifer Monitor Well

The Avon Park well was previously constructed by the District owned Speedstar SS-40 drilling rig in July 1995. The well consisted of 18-inch steel casing from land surface to 180 feet bls, 12-inch steel casing from 180 feet bls to 1,080 feet bls, and an 11-inch open hole interval of 1,080 feet bls to 1, 650 feet bls.

The District contractor (Diversified Drilling, Inc.) set-up on the Avon Park well and drilled a 5.675-inch diameter borehole from the previous total depth of 1,650 feet bls to 1,776 feet bls. Drilling was terminated at 1,176 feet bls. Ground-water samples collected from this depth were near sea-water concentrations (see **Volume II - Exploratory Drilling and Testing**). Following all testing activities, the borehole was tremie grouted from 1,776 feet bls to 1,716 feet bls. Limestone gravel was installed in the borehole from 1,716 feet bls to 1,645 feet bls. Portland cement was tremie grouted from 1,645 feet bls to 1,465 feet bls and gravel was installed again from 1,465 feet bls to 1,445 feet bls. The borehole was then tremie grouted from 1,465 to 1,400 feet bls, the bottom of the open hole interval. Thirteen-hundred fifty-three feet of 6-inch schedule 40 PVC (1,350 feet bls to 3 feet als) was installed into the well. A 6-inch x 11-inch cement basket was attached to the bottom of the 6-inch PVC prior to installation. A bentonite seal was installed in the annular space, above the cement basket from 1,350 feet bls to 1,330 feet bls prior to grouting. The annular space was then tremie grouted from 1,330 feet bls to land surface. Development of the well was achieved by allowing the well to flow during the tremie grouting procedure. The 6-inch casing was equipped with a 6-inch valve above land surface. Figure 12 presents the as-built diagram for the Avon Park/Upper Floridan Aquifer monitor well (MW-6).

4.0 AQUIFER PERFORMANCE TESTING

Aquifer performance tests (APT's) were conducted on all permanent wells, except the Avon Park/Upper Floridan monitor well (MW-6), from January 1997 to April 1997 at the ROMP 5 wellsite. The APT's were conducted to determine the hydraulic characteristics (hydraulic conductivity, transmissivity, storativity) of the water bearing units in the vicinity of ROMP 5. The data collected from the APT's is

used in the development of computer ground-water models that simulate the flow system in the SDWRAP. Table 2 presents the hydraulic values for each aquifer tested.

4.1 Surficial Aquifer System

The surficial aquifer system APT was conducted from January 13, 1997 to January 16, 1997. Background water levels were collected in the surficial aquifer system from December 13, 1996 to January 31, 1997. Figure 13 presents a hydrograph of the surficial aquifer at ROMP 5. A step-test was conducted on the surficial aquifer on 1-6-97 and the IAS Upper Permeable Zone APT was conducted from 1-6-97 to 1-8-97. The water level changes in the surficial aquifer during these events can be seen on the hydrograph in figure 13.

The 12-inch diameter surficial aquifer monitor well (MW-1) was pumped with a 1.5 horsepower (HP) electrical submersible pump at 65 gallons per minute (gpm) for 64.5 hours. The discharge water was pumped approximately 1000 feet away from the well through a 2-inch diameter discharge hose. During the drawdown and recovery phase of the APT, water levels were measured in the 12-inch surficial pumped well (MW-1), the 4-inch surficial observation well (OB) located 45 feet from the pumped well, and the 8-inch diameter upper intermediate aquifer well. The water level measurements were recorded using pressure transducers and an In-Situ® data logger. Five hundred minutes into the drawdown phase of the APT heavy rain occurred which caused water levels in the surficial aquifer to rise. This rain event is noted on the drawdown curves of both the surficial pumped well and OB well (Figure 14). The data effected by the rain event was not used in the determination of the hydraulic values.

The data collected from the surficial APT was analyzed using Waterloo Hydrogeologic Inc., AquiferTest® software. The drawdown curve of the 4-inch surficial OB well (MW-5) was analyzed using the *Neuman Method (Unconfined)* and the *Cooper & Jacob Method (with Jacob correction for unconfined conditions)*. The recovery curve for MW-5 was analyzed using the *Theis & Jacob Recovery Test Method (with Jacob correction for unconfined conditions)*. The following are the averaged values for the three methods:

Transmissivity (T) = 2.78×10^3 feet²/day Horizontal hydraulic conductivity (K_h) = 3.27×10^1 feet/day

The drawdown and recovery curves analyzed by the Neuman, Cooper Jacob, and Theis & Jacob methods are presented in Figures 15, 16, and 17, respectively. The water level measurements collected by the data logger for the surficial APT are presented in Appendix A.

4.2 Upper Permeable Zone Intermediate Aquifer System

The APT for the upper permeable zone of the intermediate aquifer system was conducted from January 6, 1997 to January 8, 1997. Background water levels were recorded from December 31, 1996 to January 13, 1997 in the surficial monitor well, and lower permeable zone IAS monitor well. Equipment failure prevented the collection of water level data in the upper permeable zone (IAS) well (prior to drawdown), and in the lower permeable zone (IAS) well (during recovery). Figure 18 presents a hydrograph of the available water levels collected from December 31, 1996 to January 13, 1997. The 8-inch diameter upper permeable IAS monitor well (MW-2) (Figure 8) was pumped with a 10 HP electrical submersible pump at 237 gpm for 37.5 hours. The discharge water was pumped approximately 1,000 feet away through two 2-inch diameter discharge hoses.

Water level changes were recorded in all on-site monitor wells during the drawdown and recovery phases of the APT. The water levels measurements were recorded using pressure transducers and an In-Situ® data logger. During the pumping phase of the test maximum drawdown in the pumped well was 40 feet. Maximum drawdown in the observation well was 16 feet. The drawdown and recovery curves of the 8-inch diameter upper permeable zone IAS pumped well and the 2-inch diameter upper permeable zone IAS observation well (located 93 feet from the pumped well) are shown in Figure 19.

The data collected from the upper permeable zone APT was analyzed using Waterloo Hydrogeologic Inc., AquiferTest® software. The drawdown curve of the 2-inch temporary upper permeable zone IAS OB well was analyzed using the *Cooper & Jacob Time Drawdown Method* and the *Hantush Method (leaky, no aquitard storage)*. The recovery curve of the 2-inch OB well was analyzed using the *Theis & Jacob Recovery Test Method (confined)*. The following are the averaged values for the three methods:

Transmissivity (T) = 1.39×10^3 feet²/day Horizontal hydraulic conductivity (K_b) = 1.39×10^1 feet/day Storativity (S) = 2.12×10^{-3} The drawdown and recovery curves analyzed by the Cooper & Jacob, Hantush, and Theis & Jacob methods are presented in Figures 20, 21, and 22, respectively. The water level measurements collected by the data logger for the upper permeable zone IAS APT are presented in Appendix B.

4.3 Lower Permeable Zone Intermediate Aquifer System

The APT for the lower permeable zone of the IAS was conducted from April 2, 1997 to April 3, 1997. Background water levels were recorded in all on-site monitor wells from March 27, 1997 to April 7, 1997. Figure 23 presents hydrographs of the upper permeable zone (IAS), lower permeable zone (IAS), Suwannee, and Avon Park monitor wells from March 27, 1997 to April 7, 1997. The 12-inch diameter lower permeable zone IAS monitor well (MW-3) was pumped with a 30 HP right-angle drive, diesel turbine pump at 930 gpm for 21 hours. The discharge water was pumped 600 feet away through a 6-inch diameter discharge hose .

During the APT, water level changes were recorded in all wells using pressure transducers and an In-Situ® data logger. Maximum drawdown in the pumped well was 19 feet at 930 gpm. No observation well was constructed at this site for the lower permeable zone. Figure 24 presents the drawdown and recovery curves of the 12-inch lower permeable zone pumped well. During the drawdown phase, the water levels in the 12-inch Suwannee/Upper Floridan monitor well (MW-4) declined approximately 1.5 feet. During the recovery phase of the test the water level in the 12-inch Suwannee well rose to the pre-pumping level (Figure 23). These water level changes indicate a hydraulic connection between the lower permeable zone of the IAS and the Upper Floridan aquifer.

The data collected from the upper permeable zone IAS APT was analyzed using Waterloo Hydrogeologic, Inc., AquiferTest® software. The recovery curve of the 12-inch pumped well was analyzed using the *Theis & Jacob Recovery Test Method (confined)*. No observation well was available at this site for the APT. The approximate hydraulic values for the Upper Permeable of the IAS at ROMP 5 are:

Transmissivity (T) = 2.97×10^3 feet²/day Horizontal hydraulic conductivity (K_h) = 1.98×10^1 feet/day

The recovery curve analyzed by the Theis & Jacob method is presented in Figure 25. The water level measurements collected by the data logger for the lower permeable zone IAS APT are presented in Appendix C.

4.4 Suwannee/Upper Floridan Aquifer

The Suwannee/Upper Florida aquifer APT was conducted from April 9, 1997 to April 10, 1997. Background water levels were collected in all on-site monitor wells from April 4, 1997 to April 17, 1997. Figure 26 presents hydrographs of the monitor wells. The 12-inch Suwannee/Upper Floridan aquifer well (MW-4) was pumped with a 30 HP right-angle drive diesel turbine pump at 349 gpm for 24 hours. The discharge water was pumped 600 feet away through a 6-inch diameter discharge hose.

An In-Situ® data logger and water level transducers recorded water level changes in all on-site monitor wells during the APT. Maximum drawdown in the pumped well was 61 feet while pumping at 349 gpm. The maximum drawdown in the Suwannee/Upper Floridan aquifer OB well (located 130 feet from pumped well) was 8.5 feet. Figure 27 presents the drawdown and recovery curves of the Suwannee/Upper Floridan pumped and observation wells. During the drawdown phase of the test, the water level in the 12-inch lower permeable zone IAS monitor well declined approximately 0.7 feet. During the recovery phase, the water levels in this well returned to the pre-pumping level (Figure 26).

The data collected from the Suwannee/Upper Floridan aquifer APT was analyzed using Waterloo Hydrogeologic, Inc., AquiferTest® software. The drawdown curve of the 2-inch Suwannee/Upper Floridan OB well was analyzed using the *Cooper & Jacob Time Drawdown Method* and the *Hantush Method (leaky, no aquitard storage)*. The recovery curve was analyzed using the *Theis & Jacob Recovery Test Method (confined)*. The following values represent the average of the three methods:

Transmissivity (T) = 2.61×10^3 feet²/day Horizontal hydraulic conductivity (K_h) = 1.04×10^1 feet/day Storativity (S) = 4.08×10^{-1}

The drawdown and recovery curves analyzed by the Cooper & Jacob Time Drawdown, Hantush, and Theis & Jacob methods are presented in Figures 28, 29, and 30, respectively. The water level measurements collected by the data logger for the Suwannee/Upper Floridan aquifer APT are presented in Appendix D.

5.0 SUMMARY

Six permanent monitor wells were constructed during phase three (March 1996 to July 1996) of the hydrogeologic investigation at the ROMP 5 Cecil Webb monitor well site. The monitor wells were constructed to collect long-term water level and water quality information from the surficial aquifer system, upper and lower permeable zones of the intermediate aquifer system, the Suwannee permeable zone of Upper Floridan aquifer, and the Avon Park permeable zone of the Upper Floridan aquifer. The ROMP 5 permanent monitor wells will be equipped with continuous water level recorders. The record of the monitor well water levels will be compiled and maintained by the District's Hydrologic Data Section.

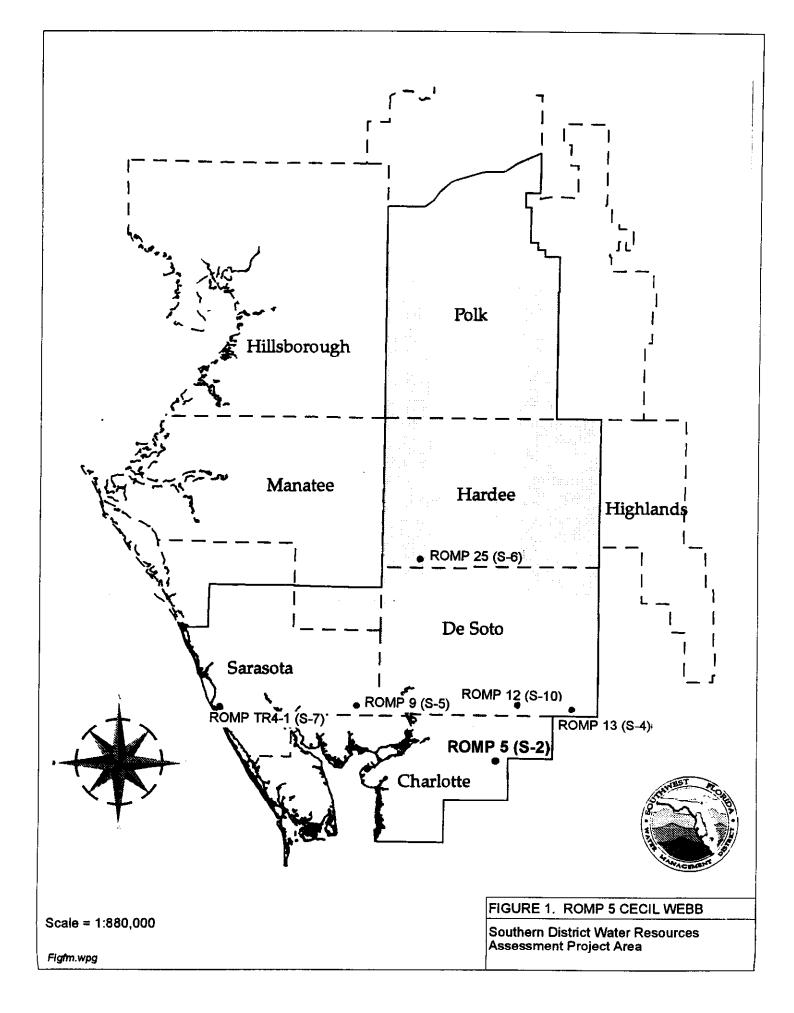
The fourth and final phase of the ROMP 5 investigation, aquifer performance testing, was conducted from January 1997 to April 1997. Aquifer performance tests were conducted on the surficial aquifer system, upper and lower permeable zones of the intermediate aquifer system, and the Suwannee permeable zone of the Upper Floridan aquifer. The APT results indicate the 85 feet thick surficial aquifer system is fairly productive with a transmissivity (T) value of 2,780 feet²/day or 20,794 gallons/day/foot. The APT results of the 100 feet thick upper permeable zone of the IAS indicate this zone is less productive than the surficial aquifer with a transmissivity (T) value of 1,390 feet²/day or 10,397 gallons/day/foot. The APT conducted on the 150 feet thick lower permeable zone of the IAS showed it is in hydraulic connection with the underlying Suwannee permeable zone of the Upper Floridan aquifer. This test was conducted without an observation well so the hydraulic values are less reliable than the other APT's conducted at the site. The transmissivity (T) of the lower permeable zone of the IAS is approximately 2,970 feet²/day or 22,216 gallons/day/foot. The APT conducted on the 250 feet thick Suwannee permeable zone of the Upper Floridan aquifer indicates that this zone is comparatively low for other zones of the Upper Floridan aquifer. Transmissivity of the Suwannee permeable zone of the Zone of the Zone of the Upper Floridan aquifer.

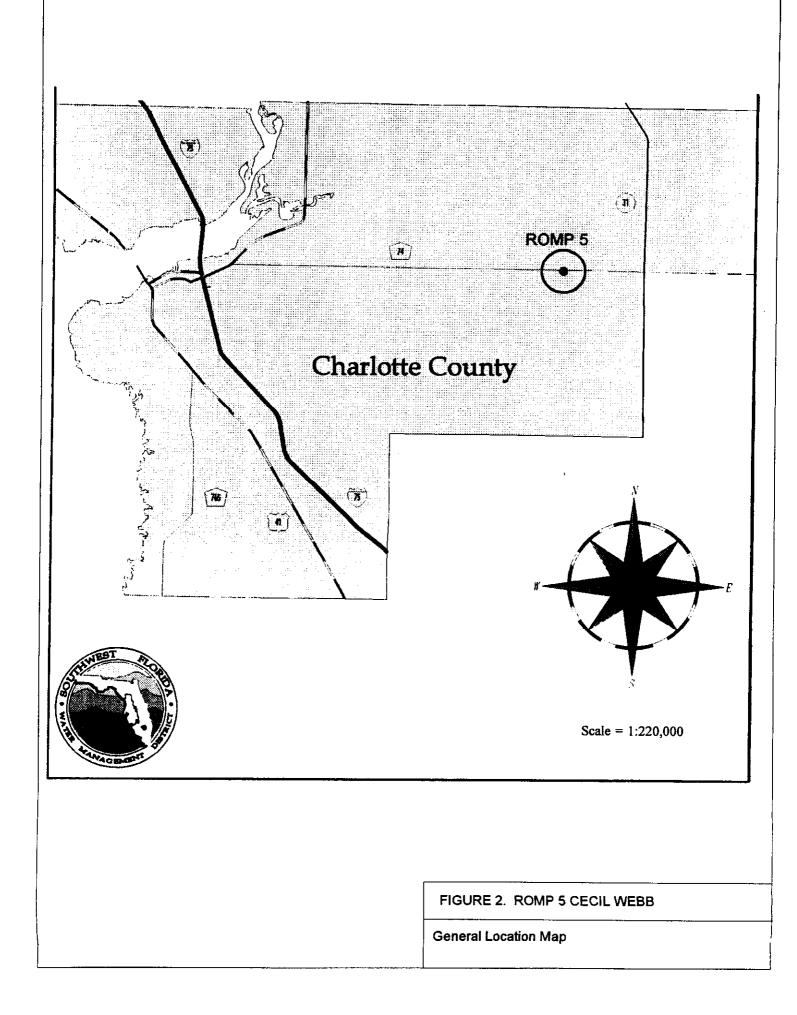
This report completes the hydrogeologic investigation performed at ROMP 5 from June 1993 to April 1997. The data collected from the ROMP 5 investigation will be used in the District's Southern District Water Resources Project.

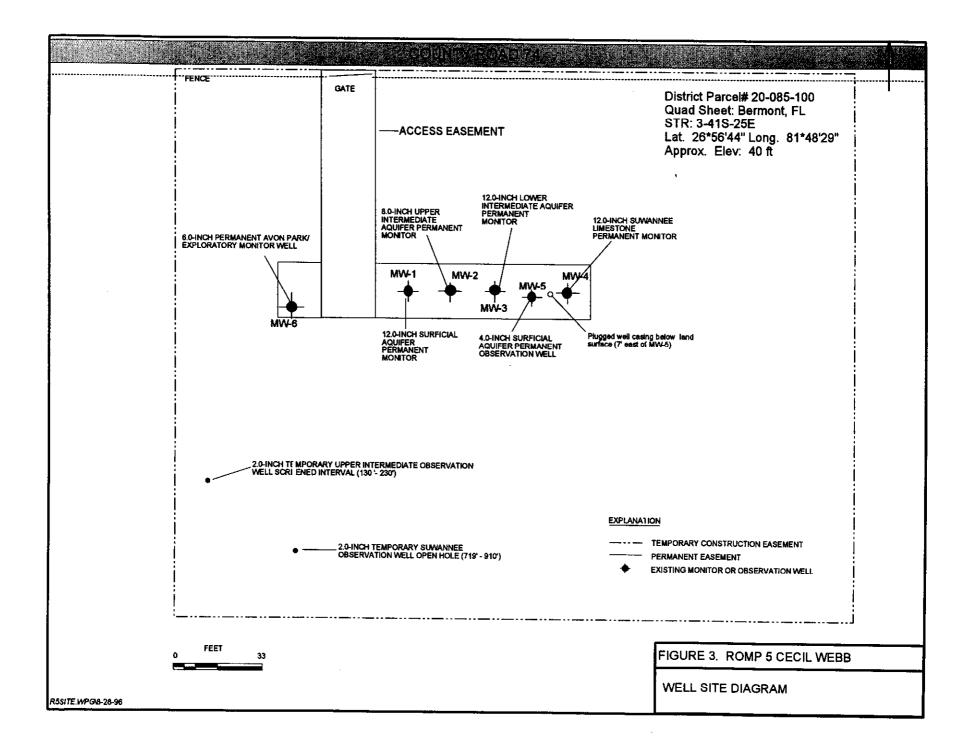
6.0 <u>REFERENCES</u>

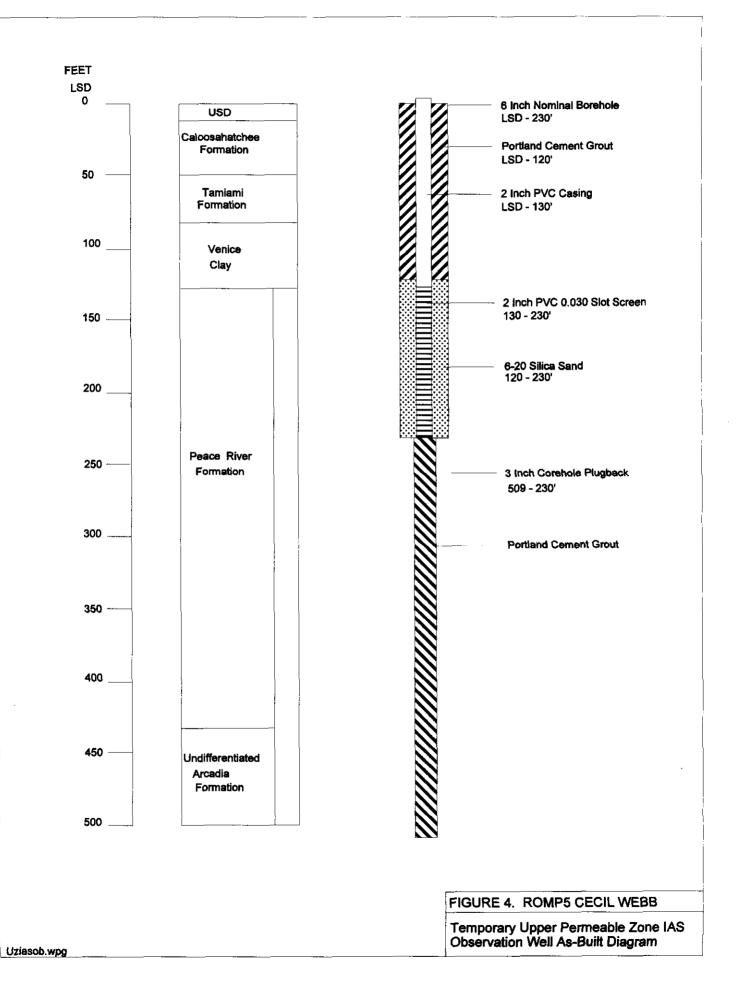
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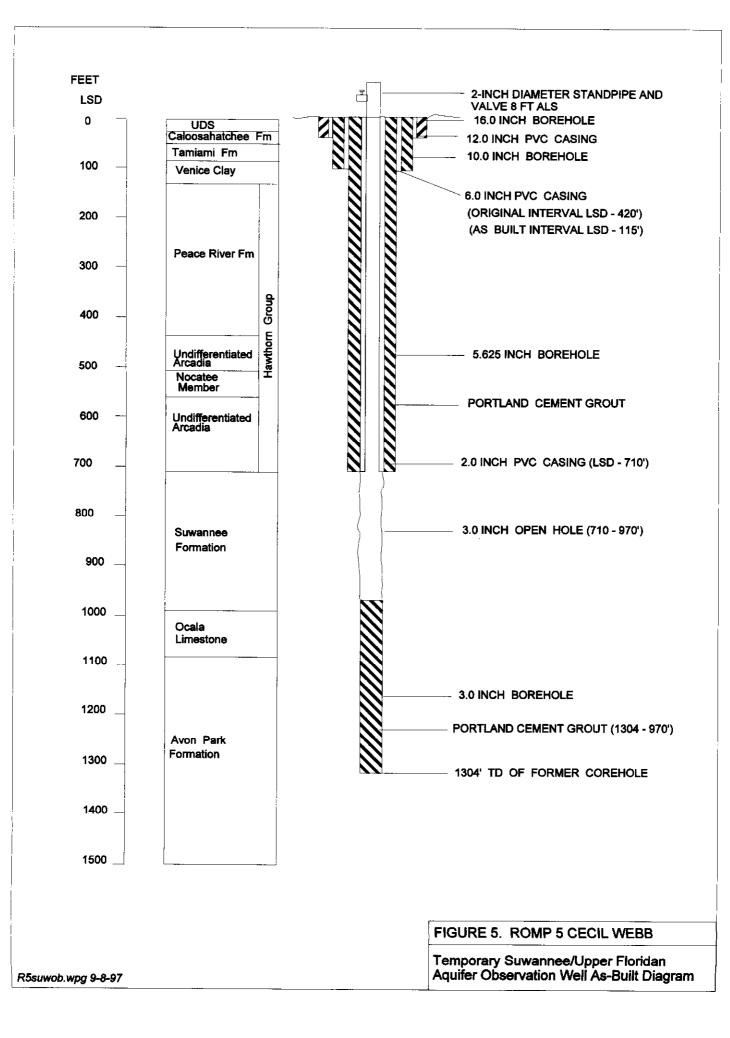
FIGURES

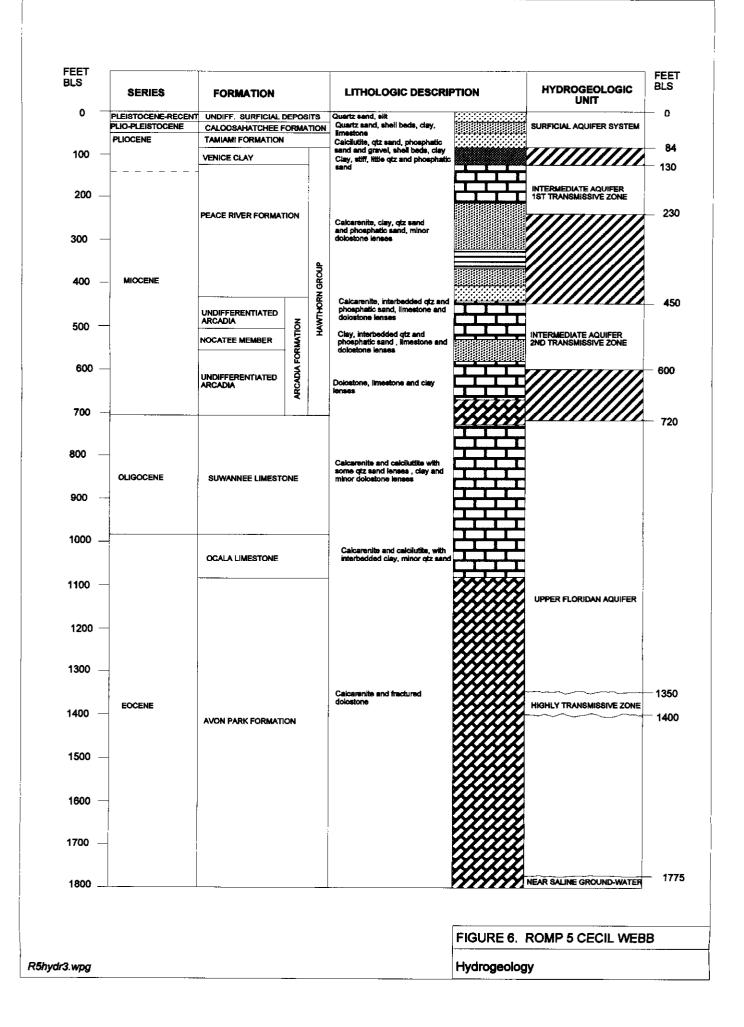


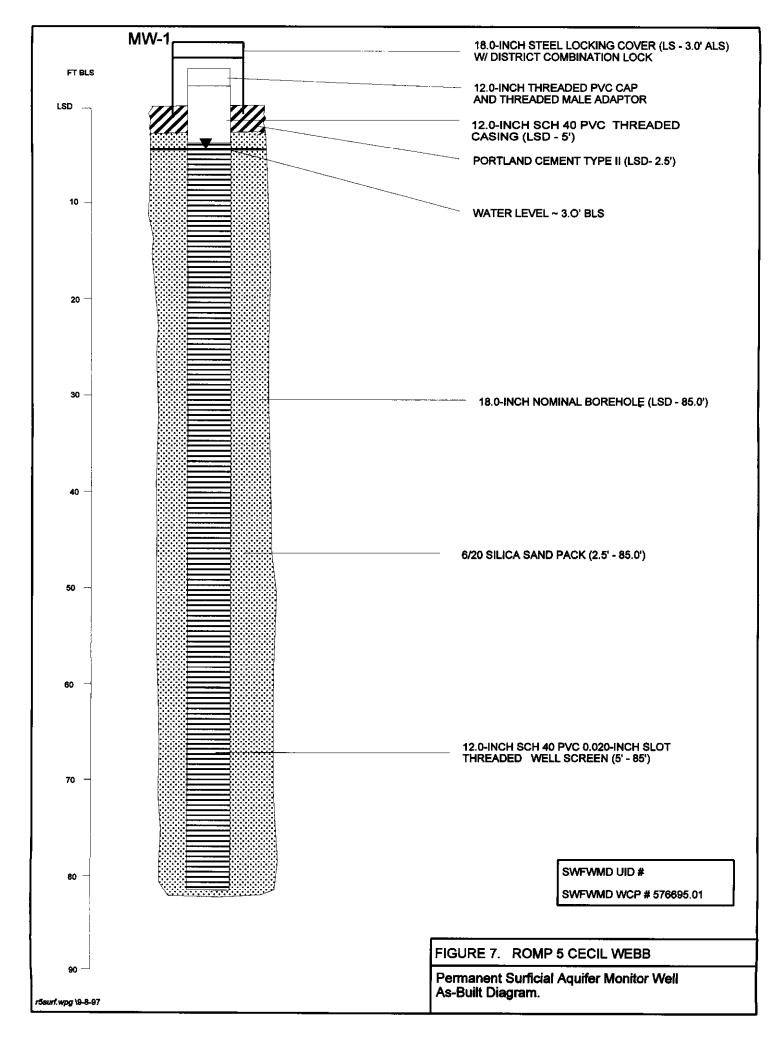


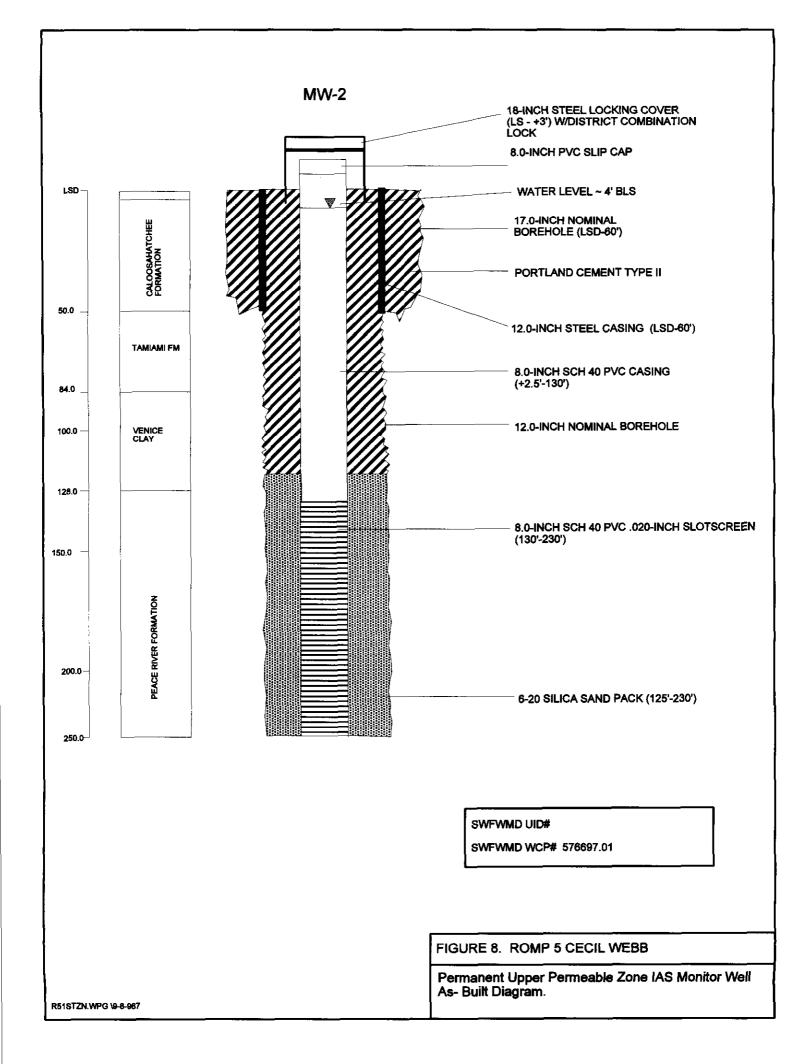


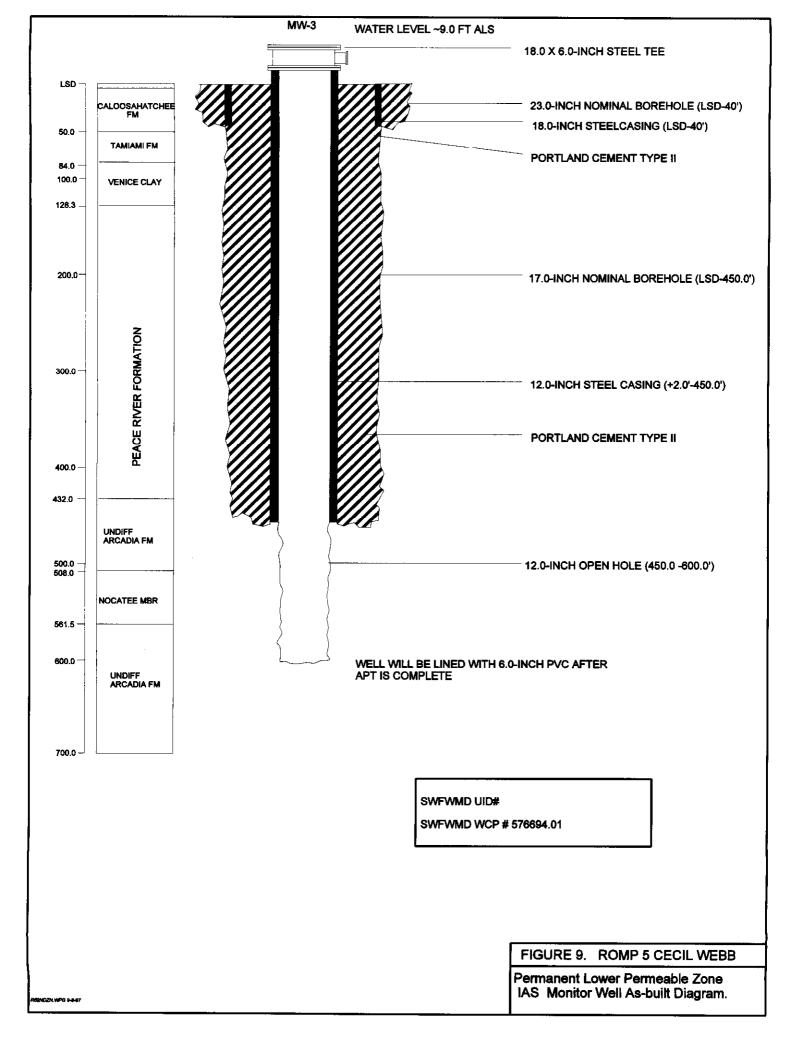


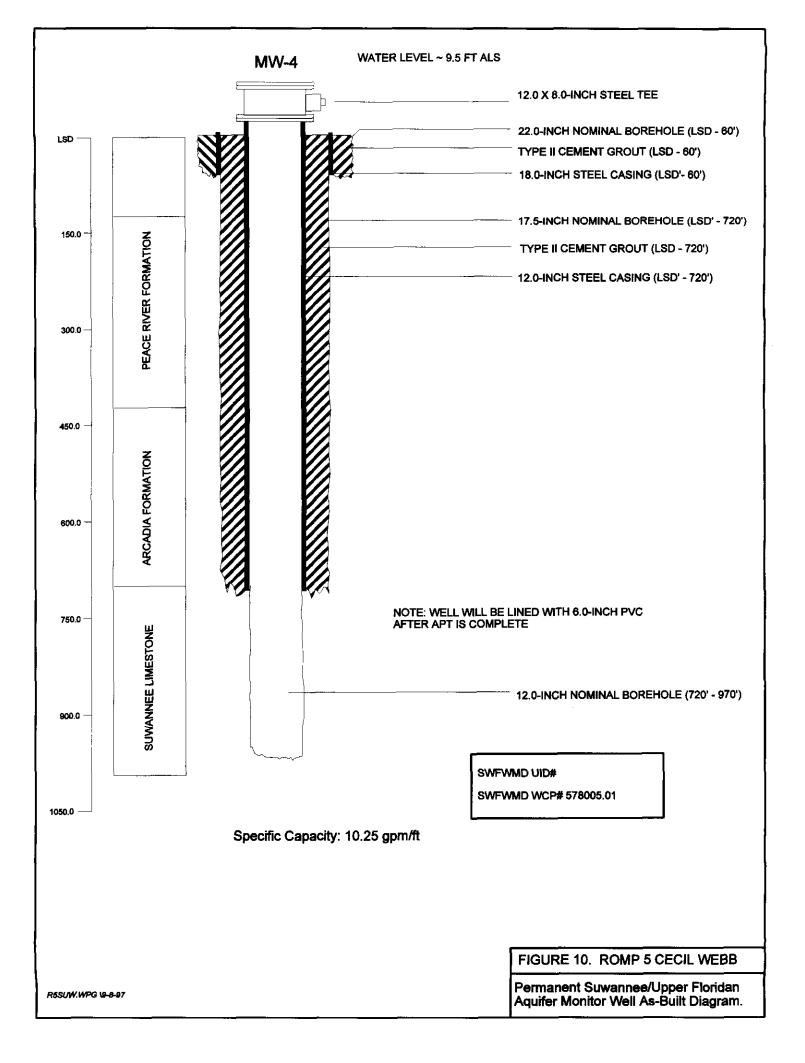


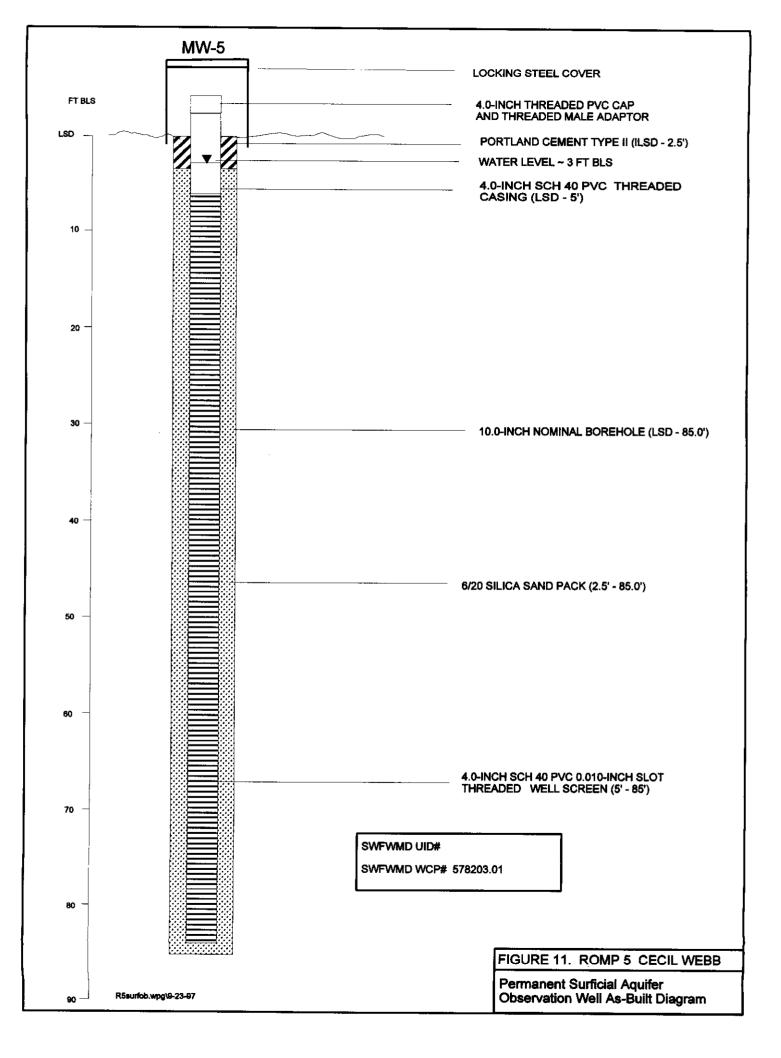


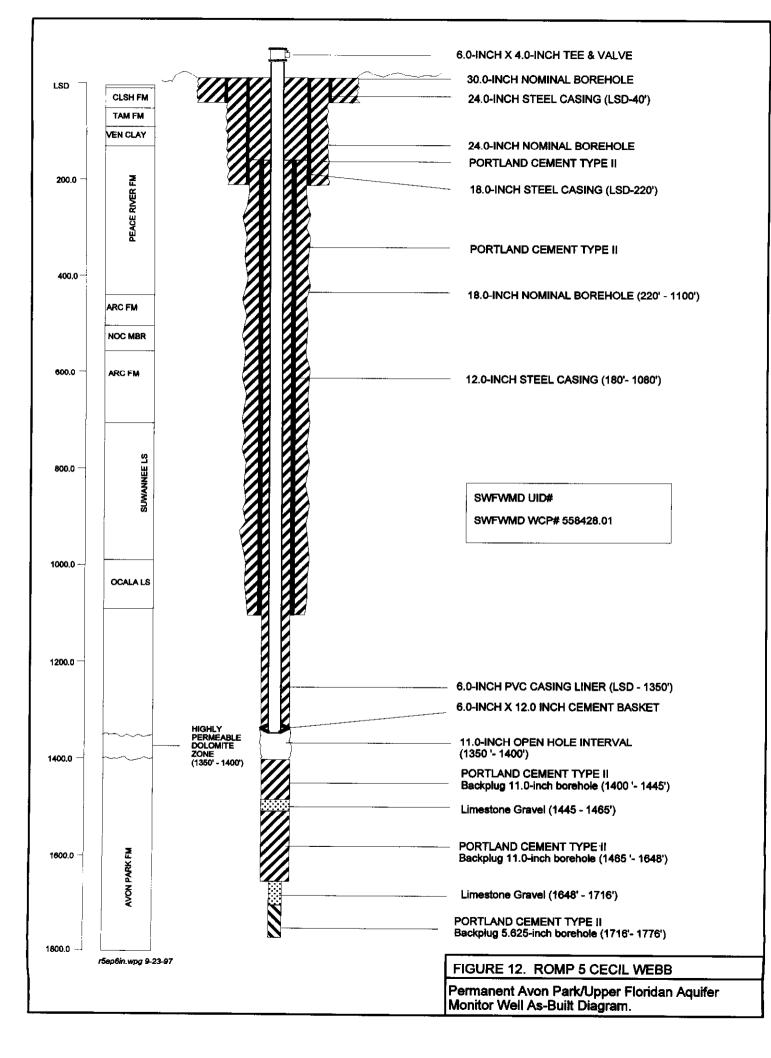


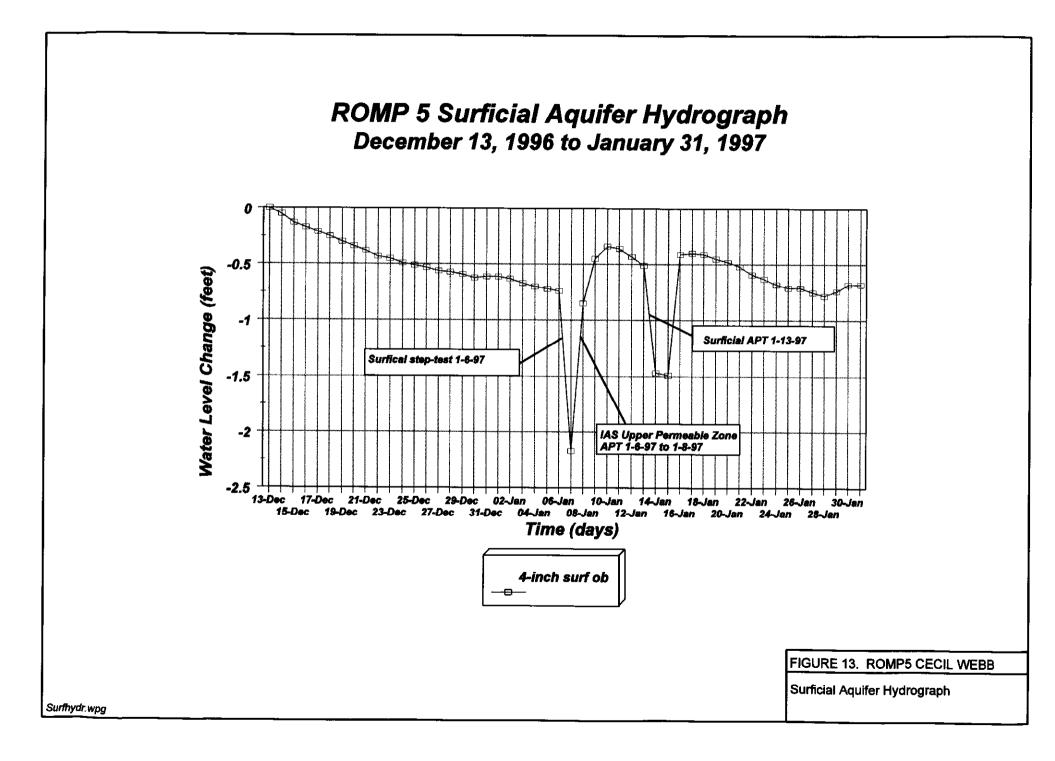


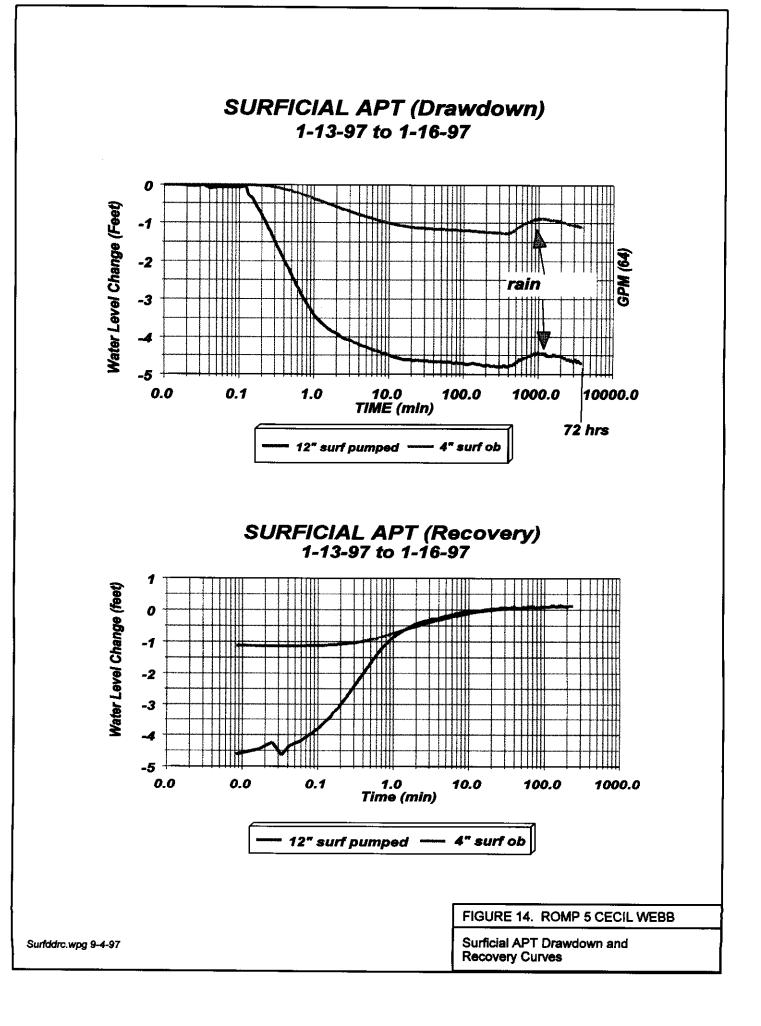


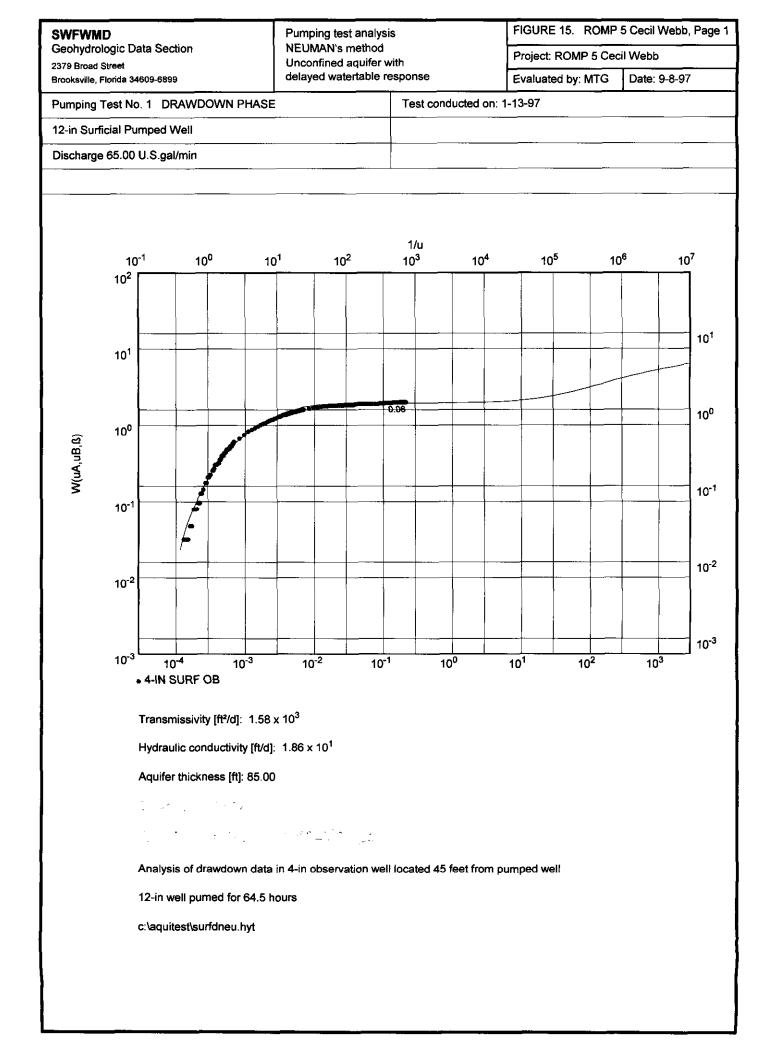


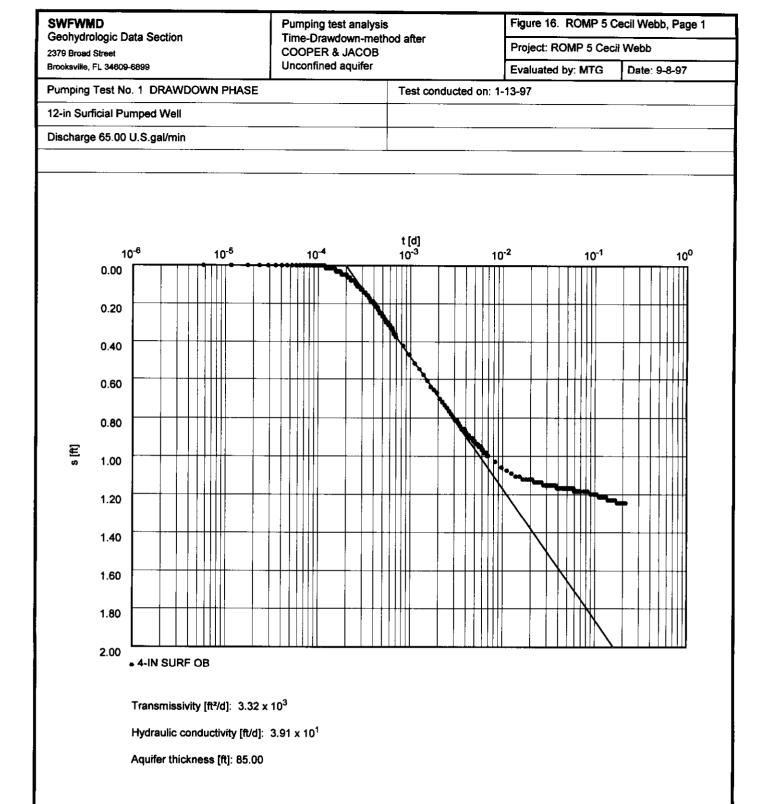






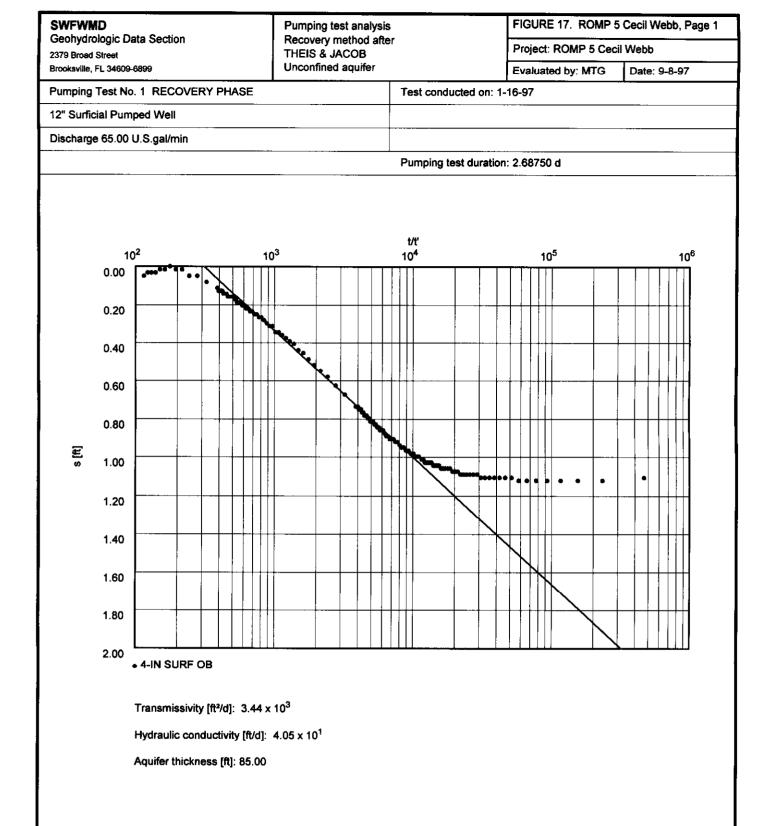






Analysis of drawdown data in 4-inch surficial observation well located 45 feet from pumped well 12-inch well pumped for 64.5 hours

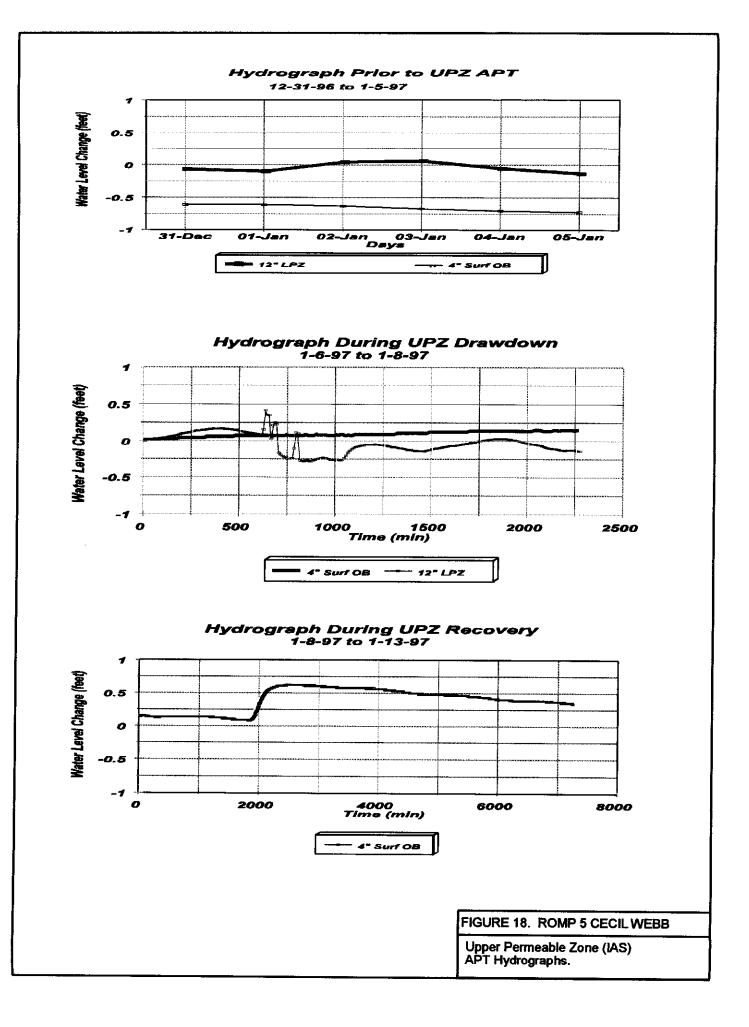
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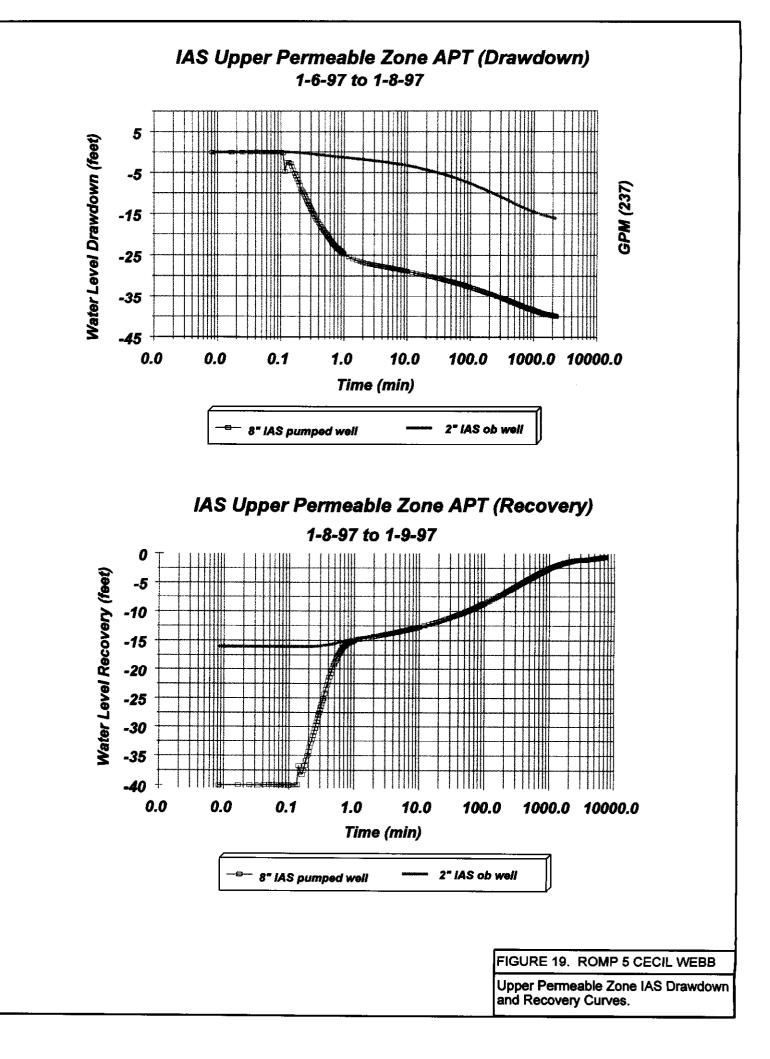


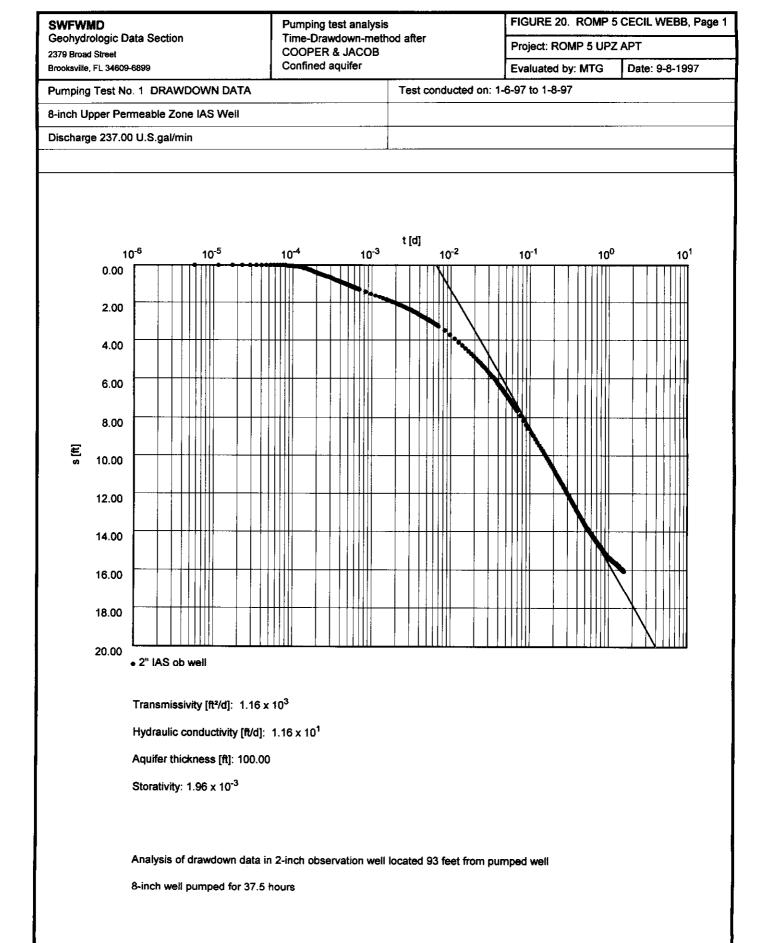
Analysis of recovery data in 4-in surficial observation well located 45 feet from pumped well

12-in well pumped for 64.5 hrs

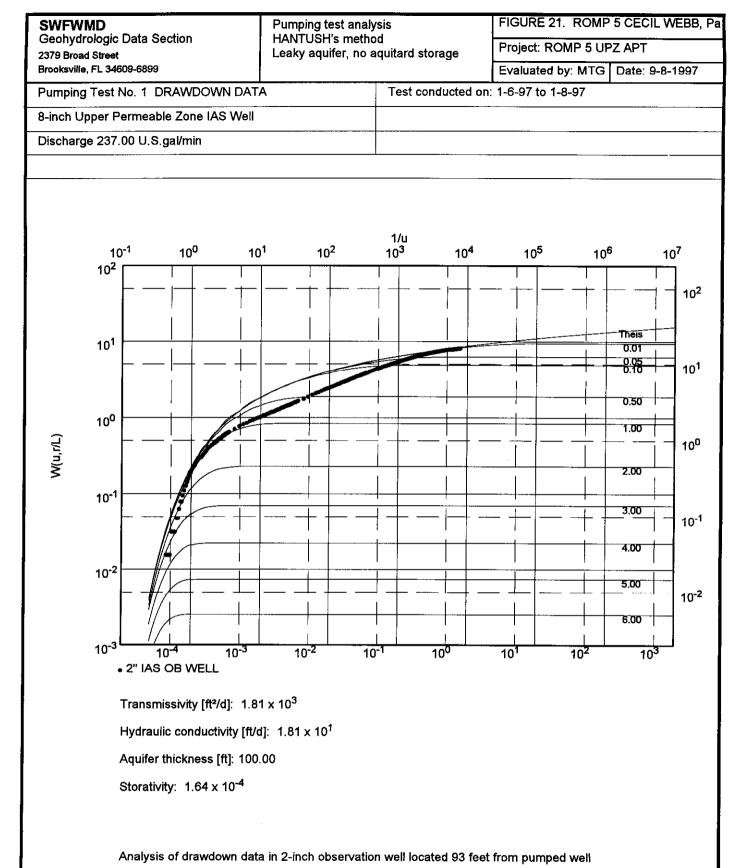
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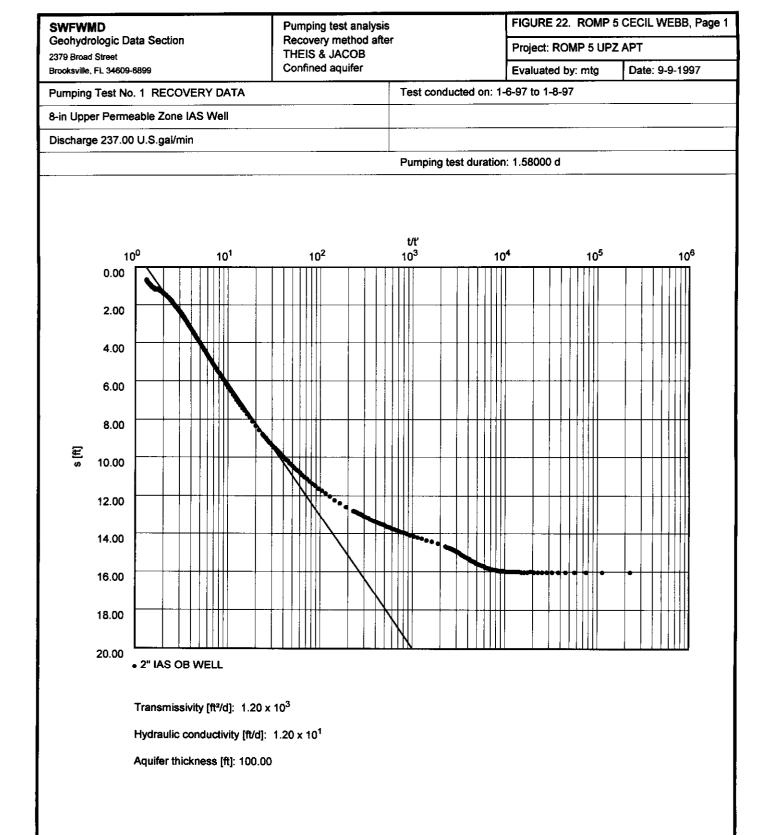


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8-inch well pumped for 37.5 hours

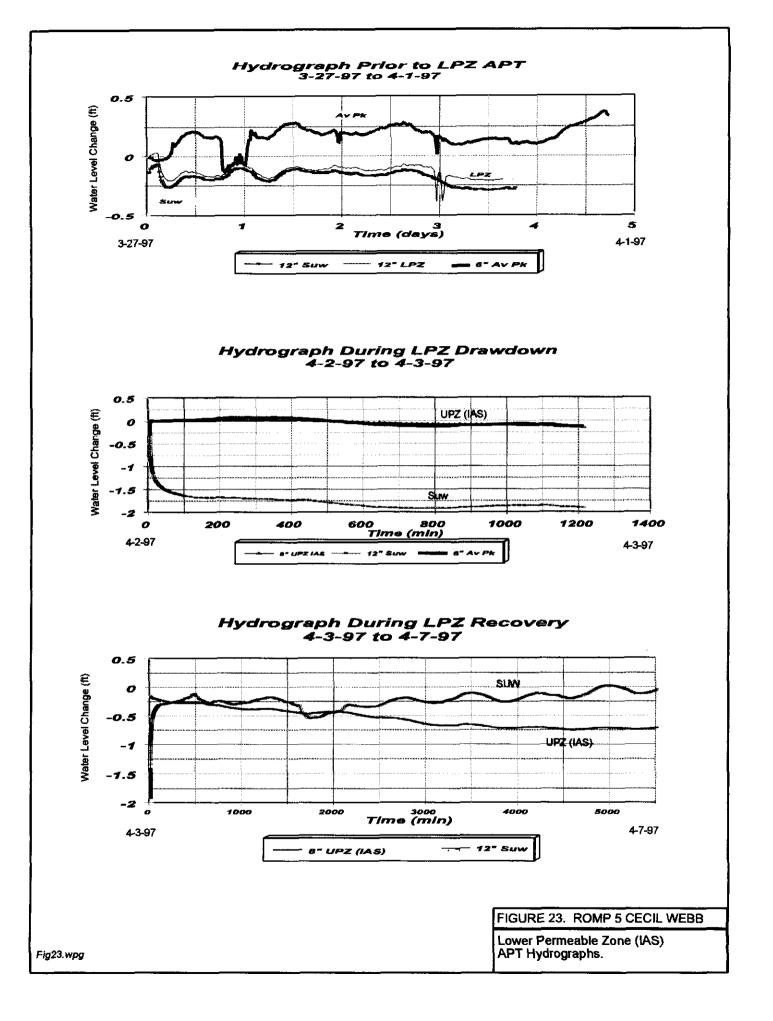
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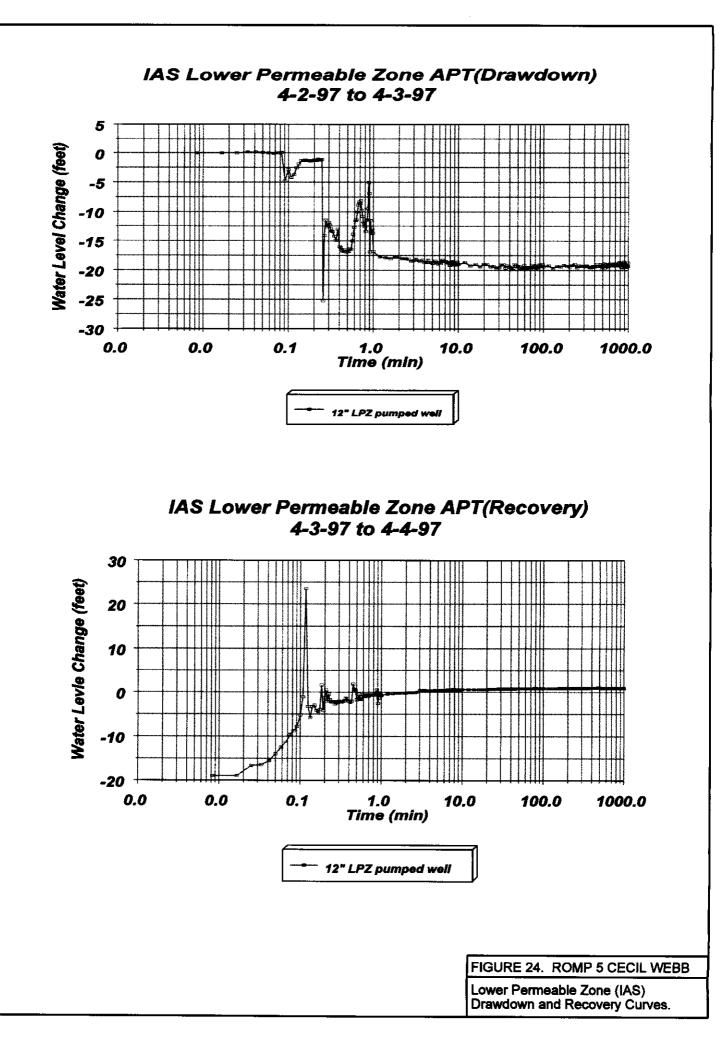


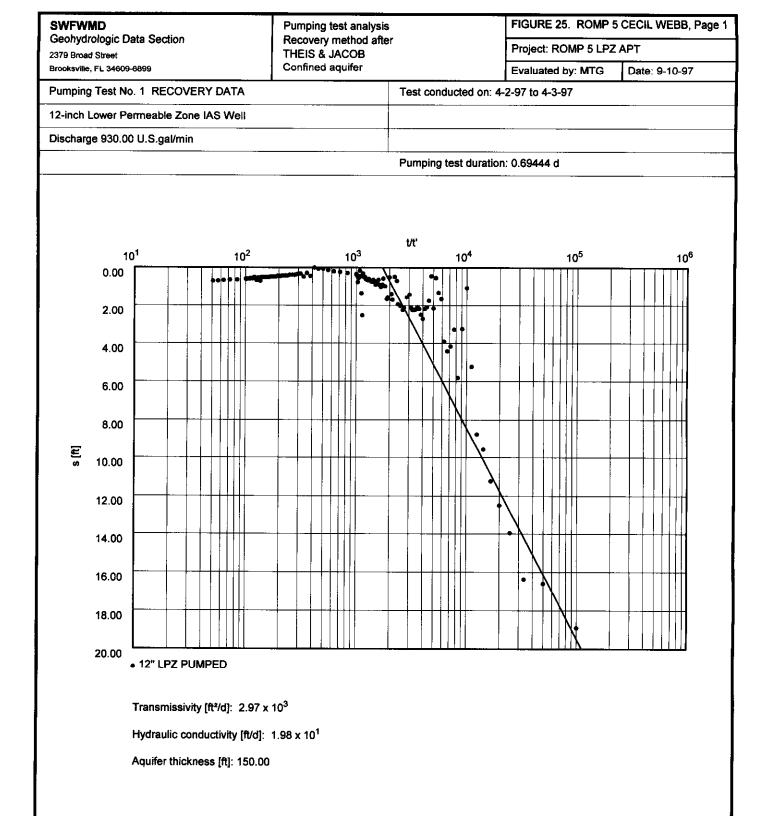
Analysis of recovery data in 2-in observation well located 93 feet from pumped well

8-in well pumped for 37.5 hours

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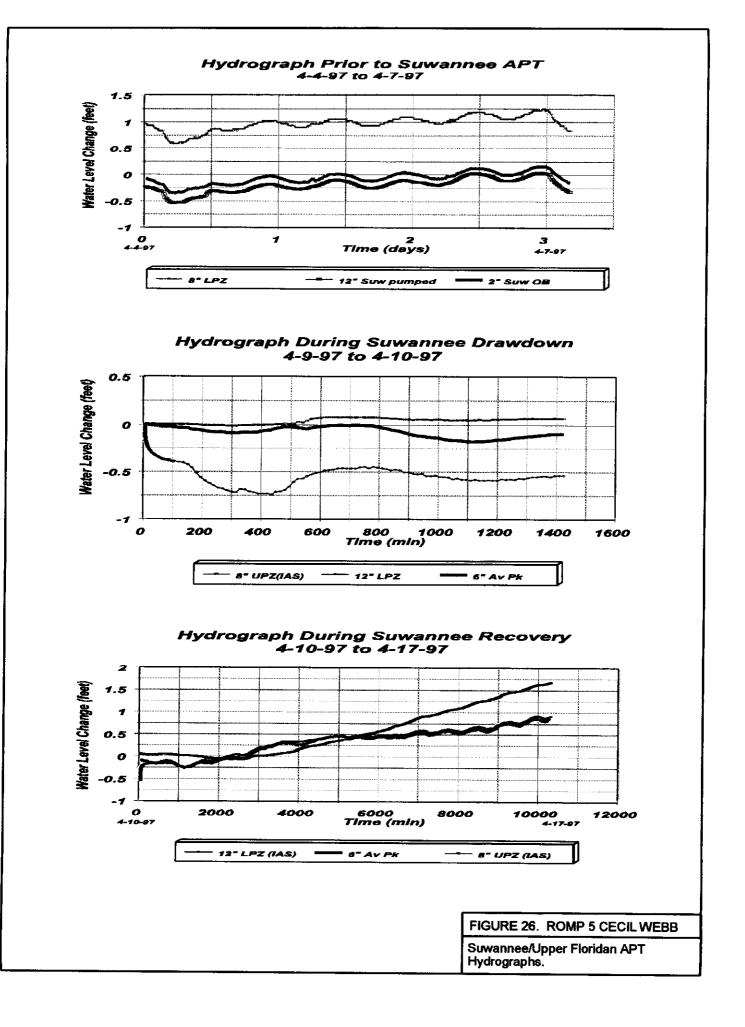


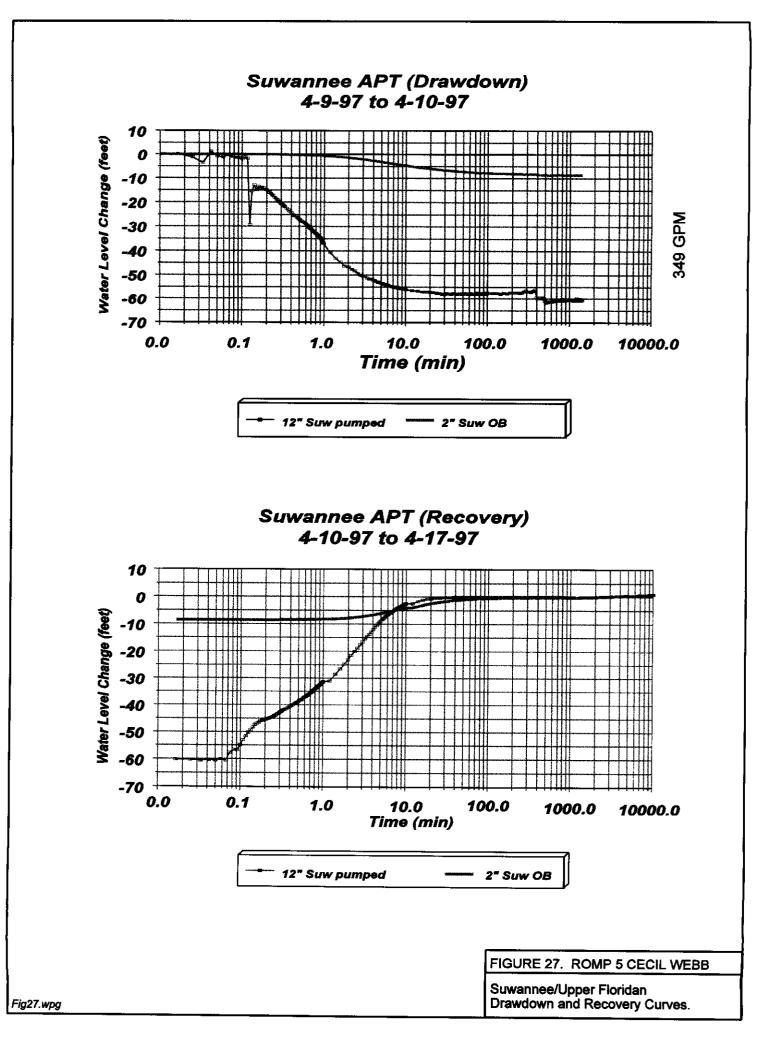


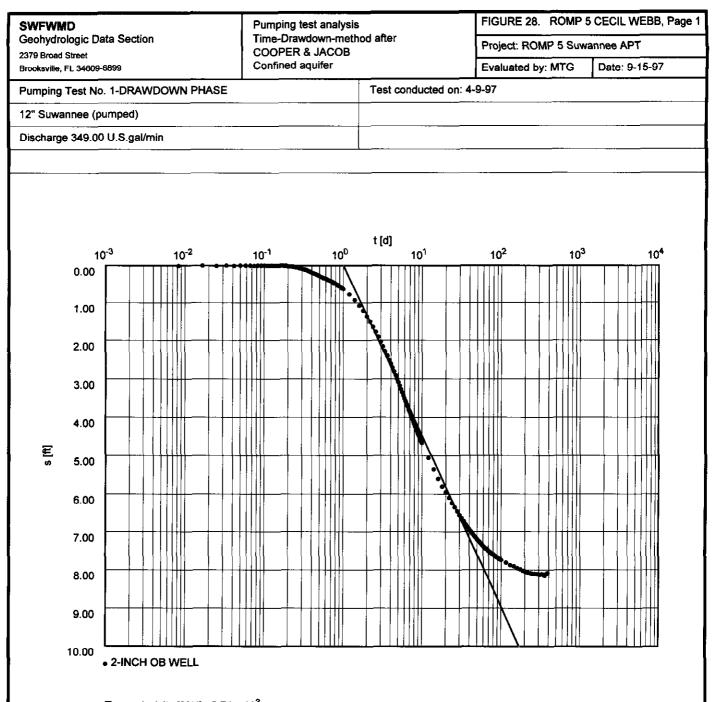


Analysis of 12-inch pumped well - no observation well available

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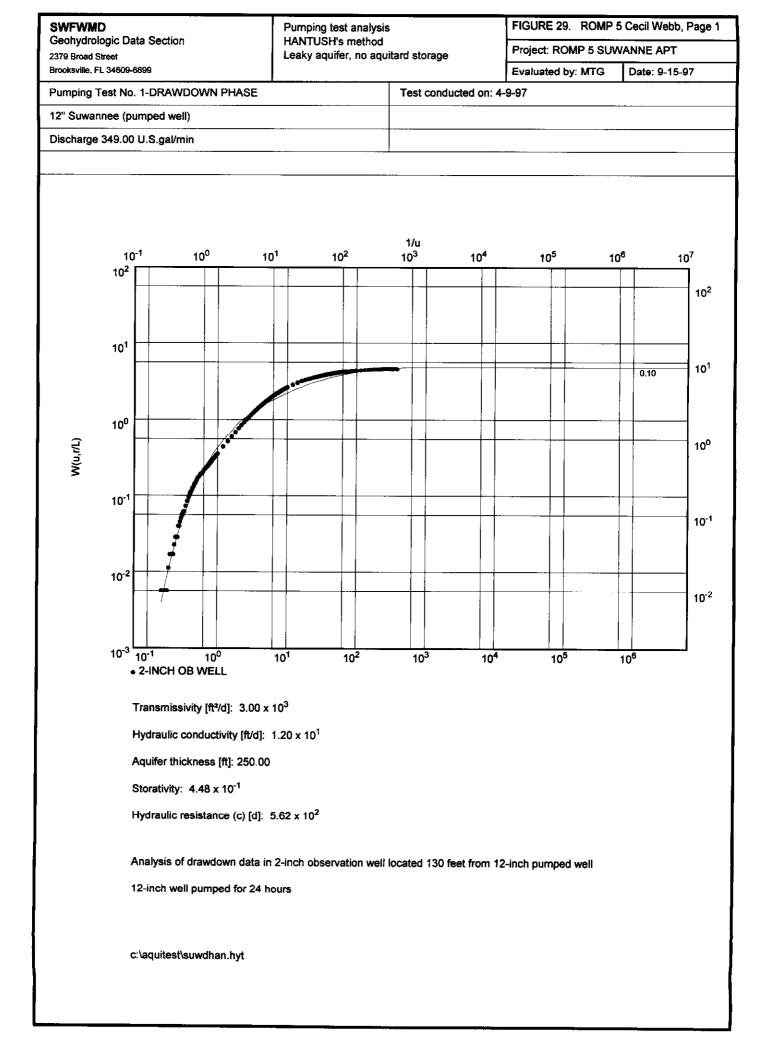


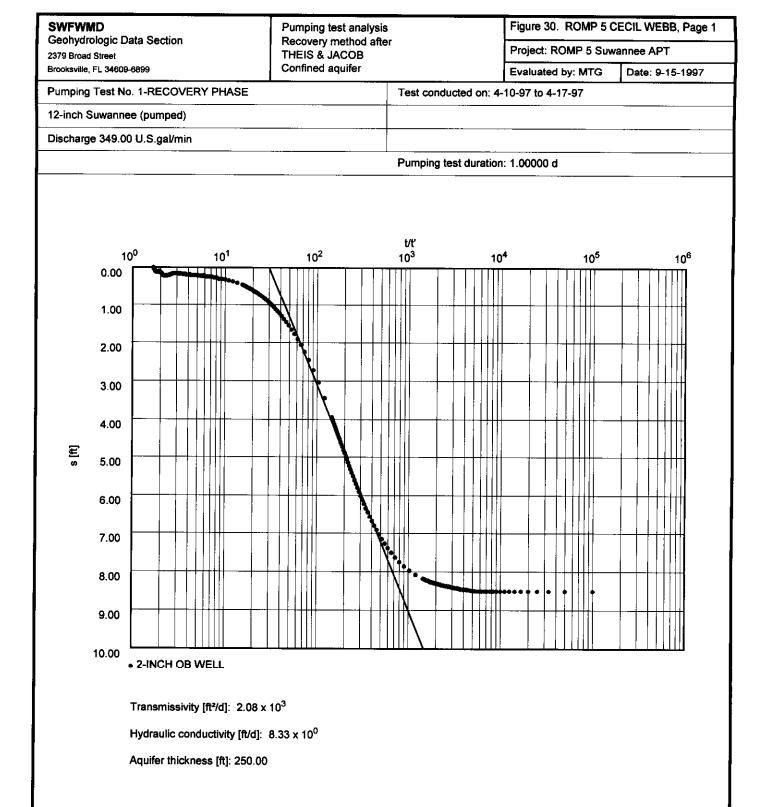


Transmissivity [ft²/d]: 2.74×10^3 Hydraulic conductivity [ft/d]: 1.09×10^1

Aquifer thickness [ft]: 250.00

Storativity: 3.67 x 10⁻¹





Analysis of recovery data in 2-inch ob well located 130 feet from pumped well

12-inch well pumped for 24 hours

c:\aquitest\suwrt&j.hyt

TABLES

Table 1. Well Construction Details

Well No.	Formation Monitored	Aquifer Monitored	Casing Interval	Monitored Interval
MVV-1	UDS, Caloosahatchee, Tamiami Fm.	Surficial	12" PVC Casing (+2.5 - 5')	12" PVC Screen (5' -85')
MW-2	Peace River Fm.	Upper Permeable Zone Intermediate Aquifer System	8" PVC Casing (+2.5' - 130')	8" PVC Screen (130' - 230')
MW-3	Undifferentiated Arcaida Fm, Nocatee Fm.	Lower Permeable Zone Intermediate Aquifer System	12" Steel Casing (+2.5 - 450')	12" Open Hole (450' - 600')
MW-4	Suwannee Limestone	Upper Floridan Aquifer	12" Steel Casing (+2.5' - 720')	12" Open Hole (720' - 970')
MW-5	UDS, Caloosahatchee, Tamiami Fm	Surficial	4" PVC Casing (+2.5' - 5')	4" PVC Screen (5' 85')
MW-6	Avon Park Fm.	Upper Floridan Aquifer	6" PVC Casing (+3.0' - 1,350')	11" Open Hole (1,350-1,400')
Temporary	Peace River Fm	Upper Permeable Zone Intermediate Aquifer System	2" PVC Casing (+3' - 130')	2" PVC Screen (130' - 230')
Temporary	Suwannee Limestone	Upper Floridan Aquifer	2"PVC Casing (+4 - 710')	3" Open Hole (710' - 970')

Table 2. Aquifer Hydraulic Values

Aquifer Tested	Well Analyzed	Test Phase	Method	Transmissivity (T) (Feet²/day)	Hydraulic Conductivity (K _h) (Feet/day)	Storativtiy (S)
	4" OB	Drawdown	Neuman	1.58 x 10 ³	1.86 x 10 ¹	N/A
Surficial	4" OB	Drawdown	Cooper & Jacob	3.32 x 10 ³	3.91 x 10 ¹	N/A
	4" OB	Recovery	Theis & Jacob	3.44 × 10 ³	4.05 x 10 ¹	N/A
			Average	2.78 x 10 ³	3.27 x 10 ¹	NA
	2" OB	Drawdown	Cooper & Jacob	1:16 x 10 ³	1.16 x 10 ¹	1.96 x 10 ⁻³
Upper Permeable Zone	2" OB	Drawdown	Hantush	1,81 x 10 ³	1.81 x 10 ¹	1.64 x 10 ⁻⁴
Intermediate Aquifer System	2" OB	Recovery	Theis & Jacob	1.20 x 10 ³	1.20 x 10 ¹	NA
			Average	139 x 10'	1.39 x 10 ¹	212340
Lower Permeable Zone	12" Pumped	Recovery	Theis & Jacob	2.97 x 10 ³	1.98 x 10 ¹	N/A
Intermediate Aquifer System			• · · · · · · · · · · · · · · · · · · ·	■ • • • • • • • • • • • • • • • • • • •		Consequences and a second s
	2" OB	Brawdown	Cooper & Jacob	2.74 x 10 ³	1.09 x 10 ¹	3.67 x 10 ⁻¹
Suwannee	2" OB	Drawdown	Hantush	3.00 x 10 ³	1.20 x 10 ¹	4.48 x 10 ⁻¹
Upper Floridan	2" OB	Recovery	Theis & Jacob	2.08 × 10 ³	8.33 x 10 ⁰	N/A
			Average	2.61 × 10 ²	1.04 x 10 ¹	4.08 x 10 ⁻¹

apttbl.wpd

APPENDIX A

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Data Logger Water Level Measurements for Surficial APT.

SE2000
Environmental Logger
01/13 18:55
Unit# 577 Test 2
Setups: INPUT 1 INPUT 2 INPUT 3
Type Level (F) Level (F) Level (F)
Mode Surface Surface Surface
Reference 0.000 0.000 0.000
PSI at Ref. 15.318 22.862 8.661
SG 1.000 1.000 1.000
Linearity 0.036 0.014 0.073
Scale factor 99.651 49.817 14.905
Offset -0.083 -0.107 0.009
Delay mSEC 50.000 50.000 50.000
Step 0 01/13 16:39:11 SURFD-A.WB2

	0.025	-0.031	0.000	0.000	0.000	-4
	0.033	0.000	0.000	0.000	0.008	-4
	0.042	-0.094	0.000	0.000	0.017	-4
	0.050	-0.062	0.000	0.000	0.025	-4
	0.058	-0.062	0.000	0.000	0.033	-4
	0.067	-0.062	0.000	0.000	0.042	-4
	0.075	-0.062	0.000	-0.004	0.050	-4
	0.083	-0.062	0.000	0.000	0.058	-4
	0.092	-0.062	0.000	0.000	0.067	-4
	0.100	-0.062	0.000	0.000	0.075	-4
	0.108	-0.062	0.000	0.000	0.083	-3
	0.117	-0.031	0.000	0.000	0.092	-3
	0.125	-0.062	0.000	0.000	0.100	-3
	0.133	-0.282	0.000	-0.004	0.108	-3
	0.142	-0.313	0.000	0.000	0.117	-3
	0.150	-0.345	0.000	0.000	0.125	-3
	0.158	-0.439	0.000	0.000	0.133	-3.
	0.167	-0.533	0.000	0.000	0.142	-3.
	0.175	-0.596	-0.015	0.000	0.150	-3
	0.183	-0.658	-0.015	-0.004	0.158	-3.
	0.192	-0.721	-0.015	-0.004	0.167	-3.
l	0.200	-0.784	-0.015	-0.004	0.175	-3.
	0.208	-0.878	-0.015	0.000	0.183	-3
	0.217	-0.909	-0.015	0.000	0.192	-3.
	0.225	-0.972	-0.031	0.000	0.200	-3.
	0.233	-1.035	-0.031	0.000	0.208	-2
	0.242	-1.097	-0.031	-0.004	0.217	-2.
	0.250	-1.160	-0.031	-0.004	0.225	-2.
	0.258	-1.192	-0.047	0.000	0.233	-2.
Ì.	0.267	-1.254	-0.047	0.000	0.242	-2.
	0.275	-1.317	-0.047	0.000	0.250	-2.
	0.283	-1.380	-0.047	0.000	0.258	-2.
ļ	0.292	-1.411	-0.047	0.000	0.267	-2 .
	0.300	-1.474	-0.062	-0.004	0.275	-2 .
	0.308	-1.505	-0.062	0.000	0.283	-2.
	0.317	-1.568	-0.062	0.000	0.292	-2.

65000
SE2000
Environmental Logger
01/16 09:36
Unit# 577 Test 2
Setups: INPUT 1 INPUT 2 INPUT 3
Type Level (F) Level (F) Level (F)
Mode Surface Surface Surface
Reference 0.000 0.000 0.000
PSI at Ref. 15.318 22.862 8.661
SG 1.000 1.000 1.000
Linearity 0.036 0.014 0.073
Scale factor 99.651 49.817 14.905
Offset -0.083 -0.107 0.009
Delay mSEC 50.000 50.000 50.000
Step 1 01/16 09:00:10

SORFICIAL	RECOVERI	FRASE	
A sasa			
0.000	-4.705	-1.129	0.594
0.008	-4.611	-1.113	0.594
0.017	-4.454	-1.129	0.594
0.025	-4.234	-1.129	0.594
0.033	-4.642	-1.129	0.594
0.042	-4.360	-1.129	0.594
0.050	-4.266	-1.129	0.594
0.058	-4.203	-1.129	0.594
0.067	-4.109	-1.129	0.594
0.075	-4.015	-1.113	0.594
0.083	-3.952	-1.113	0.594
0.092	-3.858	-1.113	0.594
0.100	-3.795	-1.113	0.594
0.108	-3.732	-1.113	0.594
0.117	-3.638	-1.113	0.594
0.125	-3.576	-1.113	0.594
0.133	-3.513	-1.097	0.594
0.142	-3.450	-1.097	0.594
0.150	-3.387	-1.097	D.594
0.158	-3.293	-1.097	0.594
0.167	-3.231	-1.097	0.594
0.175	-3.168	-1.097	0.594
0.183	-3.136	-1.082	0.594
0.192	-3.074	-1.082	0.594
0.200	-3.011	-1.082	0.594
0.208	-2.948	-1.066	0.594
0.217	-2.885	-1.066	0.594
0.225	-2.854	-1.066	0.594
0.233	-2.791	-1.066	0.594
0.242	-2.760	-1.066	0.594
0.250	-2.697	-1.050	0.594
0.258	-2.635	-1.050	0.594
0.267	-2.603	-1.050	0.594
0.275	-2.540	-1.050	0.594
0.283	-2.509	-1.035	0.594
0.292	-2.478	-1.035	0.594

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Bistory		10012	inpin 3	Elected		inter 2
			St Ligner Parm	Time (min)		
0.325	-1.599	-0.078	0.000	0.300	2 4 4 5	1.025
0.333	-1.662	-0.078	0.000	0.300 0.308	-2.415 -2.384	-1.03 5 -1.035
0.350	-1.725	-0.078	0.000	0.317	-2.352	-1.035
0.367	-1.819	-0.094	0.000	0.325	-2.321	-1.019
0.383	-1.882	-0.109	0.000	0.333	-2.258	-1.019
0.400	-1.976	-0.109	0.000	0.350	-2.195	-1.003
0.417	-2.039	-0.125	0.000	0.367	-2.133	-1.003
0.433	-2.101	-0.125	0.000	0.383	-2.070	-0.988
0.450	-2.164	-0.141	-0.004	0.400	-2.007	-0.988
0.467	-2.227	-0.141	0.000	0.417	-1.944	-0.972
0.483	-2.321	-0.156	0.000	0.433	-1.882	-0.972
0.500	-2.352	-0.156	0.000	0.450	-1.819	-0.956
0.517	-2.415	-0.172	0.000	0.467	-1.788	-0.956
0.533	-2.478	-0.188	0.000	0.483	-1.725	-0. 9 41
0.550	-2.509	-0.188	0.000	0.500	-1.662	-0.925
0.567	-2.572	-0.188	0.000	0.517	-1.631	-0.925
0.583	-2.635	-0.203	0.000	0.533	-1.568	-0.909
0.600	-2.666	-0.203	0.000	0.550	-1.537	-0.909
0.617	-2.697	-0.219	0.000	0.567	-1.505	-0.909
0.633	-2.760	-0.219	0.000	0.583	-1.443	-0.894
0.650	-2.791	-0.235	0.000	0.600	-1.411	-0.894
0.667	-2.854	-0.250	0.000	0.617	-1.380	-0.878
0.683 0.700	-2.885	-0.250	0.000	0.633	-1.348	-0.862
0.700	-2.917 -2.948	-0.250 -0.266	0.000 0.000	0.650	-1.317	-0.862
0.717	-2.940	-0.266	0.000	0.667	-1.286	-0.862
0.750	-3.011	-0.282	0.000	0.683 0.700	-1.254	-0.846
0.767	-3.042	-0.282	0.000	0.700	-1.223 -1.192	-0.846 -0.831
0.783	-3.074	-0.298	0.000	0.733	-1.152	-0.831
0.800	-3.105	-0.298	0.000	0.750	-1.129	-0.815
0.817	-3.136	-0.298	0.000	0.767	-1.129	-0.815
0.833	-3.168	-0.313	0.000	0.783	-1.097	-0.815
0.850	-3.199	-0.313	0.000	0.800	-1.066	-0.799
0.867	-3.199	-0.313	0.000	0.817	-1.066	-0.799
0.883	-3.231	-0.329	0.000	0.833	-1.035	-0.784
0.900	-3.262	-0.329	0.000	0.850	-1.003	-0.784
0.917	-3.293	-0.329	-0.004	0.867	-0.972	-0.784
0.933	-3.325	-0.345	0.000	0.883	-0.972	-0.768
0.950	-3.356	-0.360	0.000	0.900	-0. 94 1	-0.768
0.967	-3.356	-0.360	0.000	0.917	-0.941	-0.752
0.983	-3.387	-0.360	0.000	0.933	-0.909	-0.752
1.000	-3.419	-0.376	0.000	0.950	-0.909	-0.752
1.200	-3.576	-0.423	0.000	0.967	-0.878	-0.737
1.400	-3.701	-0.470	0.000	0.983	-0.878	-0.737
1.600	-3.795	-0.517	0.000	1.000	-0.846	-0.737
1.800	-3.858	-0.548	0.000	1.200	-0.721	-0.674
2.000	-3.889	-0.580	0.000	1.400	-0.627	-0.627
2.200 2.400	-3.952 -4.015	-0.611 -0.643	0.000	1.600	-0.564	-0.580
2.400	-4.015	-0.643 -0.658	0.000 0.000	1.800	-0.501	-0.548
2.800	-4.078	-0.638	0.000	2.000	-0.439	-0.517
3.000	-4.078	-0.705	0.000	2.200 2.400	-0.407 -0.376	-0.486 -0.454
				2.700	0.070	-0.734

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SURFICIAL	DRAWDOWN	PHASE		SURFICIAL	RECOVERY	PHASE
		観察会を感	te lipin 3	Elapsed	inoit S	A BOOM
Stand Grade	and the second		B Upger Perm	Tupe (min)	nt for the set	
			ZOWERKS			
3.200	-4.109	-0.721	0.000	2.600	-0.345	-0.439
3.400	-4.140	-0.737	0.000	2.800	-0.345	-0.407
3.600	-4.172	-0.752	0.000	3.000	-0.313	-0.392
3.800 4.000	-4.172	-0.768	0.000	3.200	-0.282	-0.376
4.000	-4.203 -4.234	-0.784 -0.799	0.000 0.000	3.400	-0.282	-0.360
4.400	-4.234	-0.799	0.000	3.600 3.800	-0.282	-0.345
4.600	-4.266	-0.815	0.000	4.000	-0.282 -0.250	-0.345 -0.313
4.800	-4.266	-0.831	0.000	4.200	-0.250	-0.313
5.000	-4.266	-0.846	0.000	4.400	-0.219	-0.298
5.200	-4.297	-0.862	0.000	4.600	-0.219	-0.282
5.400	-4.297	-0.862	0.000	4.800	-0.188	-0.266
5.600	-4.328	-0.862	0.000	5.000	-0.188	-0.266
5.800	-4.328	-0.878	0.000	5.200	-0.188	-0.250
6.000	-4.328	-0.894	0.000	5.400	-0.188	-0.250
6.200	-4.360	-0.894	0.000	5.600	-0.156	-0.235
6.400	-4.360	-0.909	0.000	5.800	-0.156	-0.235
6.600	-4.360	-0.909	0.000	6.000	-0.156	-0.219
6.800	-4.391	-0.909	0.000	6.200	-0.156	-0.219
7.000	-4.391	-0.925	0.000	6.400	-0.125	-0.203
7.200	-4.391	-0.925	0.000	6.600	-0.125	-0.203
7.400	-4.391	-0.941	0.000	6.800	-0.125	-0.188
7.600	-4.423	-0.941	0.000	7.000	-0.125	-0.188
7.800	-4.423	-0. 94 1	0.000	7.200	-0.125	-0.188
8.000	-4.423	-0.956	0.000	7.400	-0.094	-0.172
8.200	-4.454	-0.956	0.000	7.600	-0.094	-0.156
8.400	-4.423	-0.956	0.000	7.800	-0.094	-0.156
8.600	-4.454	-0.972	0.000	8.000	-0.094	-0.156
8.800	-4.454	-0.972	0.000	8.200	-0.094	-0.156
9.000	-4.454	-0.988	0.000	8.400	-0.062	-0.156
9.200	-4.454	-0.988	0.000	8.600	-0.062	-0.141
9.400	-4.454 -4.454	-0.988	0.000	8.800	-0.062	-0.141
9.600 9.800	-4.434 -4.485	-0.988	0.000	9.000	-0.062	-0.141
9.000 10.000	-4.485 -4.485	-1.003 -1.003	0.000 0.000	9.200	-0.062	-0.125
12.000	-4.548	-1.005	0.000	9.400 9.600	-0.062 -0.062	-0.125
14.000	-4.579	-1.066	0.000	9.800	-0.031	-0.125 -0.125
16.000	-4.611	-1.082	0.004	10.000	-0.031	-0.125
18.000	-4.611	-1.097	0.000	12.000	-0.062	-0.078
20.000	-4.611	-1.113	0.000	14.000	-0.031	-0.047
22.000	-4.642	-1.113	0.004	16.000	0.000	-0.047
24.000	-4.611	-1.129	0.004	18.000	0.000	-0.015
26.000	-4.642	-1.129	0.004	20.000	0.031	-0.015
28.000	-4.642	-1.129	0.004	22.000	0.031	0.000
30.000	-4.642	-1.129	0.004	24.000	0.031	0.015
32.000	-4.642	-1.144	0.004	26.000	0.062	0.015
34.000	-4.642	-1.144	0.009	28.000	0.062	0.031
36.000	-4.674	-1.144	0.009	30.000	0.062	0.031
38.000	-4.642	-1.144	0.009	32.000	0.062	0.031
40.000	-4.674	-1.160	0.009	34.000	0.062	0.047
42.000	-4.642	-1.160	0.009	36.000	0.062	0.047
44.000	-4.674	-1.160	0.009	38.000	0.094	0.047

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SURFICIAL	DRAWDOWN	PHASE	
	i i i i i i i i i i i i i i i i i i i	han2	Thora 3
			C Lapper Parro
			Conductors 1
46.000	-4.674	-1.160	0.009
48.000	-4.642	-1.160	0.004
50.000	-4.674	-1.160	0.009
52.000	-4.674	-1.160	0.004
54.000	-4.674	-1.160	0.009
56.000	-4.674	-1.176	0.004
58.000	-4.674	-1.176	0.004
60.000	-4.674	-1.176	0.004
62.000	-4.674	-1.176	0.004
64.000	-4.674	-1.176	0.004
66.000	-4.674	-1.176	0.004
68.000	-4.674	-1.176	0.000
70.000	-4.674	-1.176	0.004
72.000	-4.705		
72.000	-4.705	-1.176	0.004
76.000		-1.176	0.000
	-4.705	-1.176	0.004
78.000	-4.705	-1.176	0.004
80.000	-4.674	-1.176	0.000
82.000	-4.674	-1.176	0.004
84.000	-4.705	-1.176	0.004
86.000	-4.705	-1.192	0.004
88.000	-4.705	-1.192	0.004
90.000	-4.705	-1.192	0.004
92.000	-4.705	-1.192	0.004
94.000	-4.705	-1.192	0.004
96.000	-4.705	-1.192	0.004
98.000	-4.705	-1.192	0.004
100.000	-4.705	-1.192	0.004
110.000	-4.736	-1.192	0.004
120.000	-4.736	-1.192	0.004
130.000	-4.705	-1.207	0.004
140.000	-4.705	-1.207	0.004
150.000 160.000	-4.736 -4.736	-1.207	0.004
170.000		-1.223	0.009
180.000	-4.736	-1.223	0.009 0.009
190.000	-4.768 -4.768	-1.223	
200.000		-1.223	0.009
210.000	-4.768	-1.239	0.009
220.000	-4.736 -4.768	-1.239	0.009 0.014
230.000		-1.239	
	-4.768	-1.239	0.014
240.000 250.000	-4.799	-1.239	0.018
	-4.768	-1.254	0.014
260.000 270.000	-4.768 -4.799	-1.254 -1.254	0.018 0.018
280.000	-4.799 -4.799	-1.254 -1.254	0.018
290.000	-4.799	-1.254 -1.254	0.018
300.000	-4.799	-1.254 -1.254	0.023
310.000	-4.799	-1.254	0.023
320.000	-4.799	-1.254	0.018
330.000	-4.799	-1.270	0.018
340.000	-4.799	-1.270	0.018
			0.010

SURFICIAL RECOVERY PHASE

Elected Trips (min)	Diske (P Lossi Pano Sole (45)
40.000	0.094	0.047	0.599
42.000	0.062	0.047	0.603
44.000	0.062	0.047	0.603
46.000	0.062	0.062	0.599
48.000	0.062	0.062	0.603
50.000	0.062	0.062	0.603
52.000	0.094	0.062	0.603
54.000	0.094	0.062	0.603
56.000	0.062	0.062	0.603
58.000	0.094	0.062	0.603
60.000	0.094	0.078	0.608
62.000	0.094	0.078	0.603
64.000	0.094	0.078	0.603
66.000	0.094	0.078	0.608
68.000	0.094	0.078	0.608
70.000	0.094	0.078	0.608
72.000	0.094	0.078	0.608
74.000	0.094	0.078	0.608
76.000	0.125	0.078	0.608
78.000	0.031	0.078	0.613
80.000	0.062	0.078	0.608
82.000	0.062	0.094	0.613
84.000	0.062	0.078	0.613
86.000	0.094	0.094	0.613
88.000	0.062	0.094	0.613
90.000	0.062	0.094	0.618
92.000	0.062	0.094	0.618
94.000	0.062	0.094	0.618
96.000	0.094	0.094	0.618
98.000	0.094	0.094	0.618
100.000	0.094	0.094	0.622
110.000	0.094	0.094	0.627
120.000	0.094	0.109	0.632
130.000	0.156	0.109	0.632
140.000	0.094	0.109	0.641
150.000	0.094	0.109	0.641
160.000	0.156	0.109	0.641
170.000	0.125	0.109	0.646
180.000	0.125	0.109	0.655
190.000	0.094	0.109	0.655
200.000	0.094	0.109	0.655
210.000	0.125	0.125	0.660
220.000	0.125	0.125	0.665
230.000	0.125	0.125	0.665
240.000	0.125	0.125	0.665

SURFICIAL	DRAWDOWN	N PHASE	
		Hinget 2	input 3
Time (mil)	e a sundar		2 Linger Perm
			Zone (AS)
350.000	-4.736	-1.254	0.018
360.000	-4.799	-1.270	0.023
370.000	-4.799	-1.270	0.023
380.000	-4.799	-1.270	0.023
390,000	-4.799	-1.270	0.023
400.000	-4.799	-1.270	0.028
410.000	-4.768	-1.254	0.037
420.000	-4.768	-1.254	0.037
430.000	-4.768	-1.239	0.037
440.000	-4.736	-1.223	0.042
450.000	-4.768	-1.223	0.042
460.000	-4.768	-1.223	0.042
470,000	-4.736	-1.192	0.051
480.000	-4.705	-1.192	
490.000	-4.705		0.056
490.000 500.000		-1.176	0.056
500.000 510.000	-4.705	-1.160	0.056
	-4.705	-1.144	0.056
520.000	-4.674	-1.129	0.061
530.000	-4.674	-1.113	0.066
540.000	-4.642	-1.097	0.070
550.000	-4.642	-1.097	0.070
560.000	-4.579	-1.082	0.070
570.000	-4.642	-1.066	0.075
580.000	-4.611	-1.066	0.075
590.000	-4.611	-1.050	0.070
600.000	-4.611	-1.050	0.080
610.000	-4.579	-1.035	0.075
620.000	-4.579	-1.035	0.080
630.000	-4.579	-1.019	0.080
640.000	-4.579	-1.019	0.080
650.000	-4.579	-1.019	0.084
660.000	-4.579	-1.003	0.089
670.000	-4.548	-1.003	0.084
680.000	-4.579	-1.003	0.084
690.000	-4.548	-0.988	0.089
700.000	-4.548	-0.988	0.089
710.000	-4.548	-0.988	0.094
720.000	-4.548	-0.988	0.094
730.000	-4.548	-0.972	0.099
740.000	-4.517	-0.972	0.103
750.000	-4.517	-0.972	0.103
760.000	-4.517	-0.956	0.108
770.000	-4.517	-0.956	0.103
780.000	-4.517	-0.956	0.108
790.000	-4.517	-0.956	0.108
800.000	-4.517	-0.956	0.113
810.000	-4.517	-0.941	0.113
820.000	-4.485	-0.941	0.113
830.000	-4.485	-0.941	0.117
840.000	-4.485	-0.925	0.122
850.000	-4.454	-0.925	0.117
860.000	-4.454	-0.909	0.122

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SURFICIAL	DRAWDOW	N PHASE	
Elected			input 3
			E Lines Pom
			2010 (148)
870.000	-4.454	-0.909	0.122
880.000	-4.454	-0.909	0.127
890.000	-4.454	-0.909	0.127
900.000	-4.454	-0.909	0.127
910.000	-4.423	-0.909	0.127
920.000	-4.423	-0.909	0.127
930.000	-4.423	-0.909	0.127
940.000	-4.454	-0.909	0.127
950.000	-4.454	-0.909	0.132
960.000	-4.454	-0.909	0.132
970.000	-4.423	-0.894	0.136
980.000	-4.423	-0.894	0.132
990.000	-4.454	-0.894	0.132
1000.000	-4.454	-0.894	0.132
1010.000	-4.454	-0.894	0.132
1020.000	-4.454	-0.894	0.136
1030.000	-4.454	-0.894	0.132
1040.000	-4.454	-0.894	0.136
1050.000	-4.454	-0.894	0.136
1060.000	-4.423	-0.894	0.136
1070.000	-4.454	-0.894	0.141
1080.000	-4.423	-0.894	0.141
1090.000	-4.454	-0.894	0.146
1100.000	-4.423	-0.894	0.146
1110.000	-4.454	-0.894	0.146
1120.000	-4.454	-0.878	0.150
1130.000	-4.454	-0.894	0.150
1140.000	-4.454	-0.894	0.155
1150.000	-4.454	-0.894	0.155
1160.000	-4.423	-0.894	0.155
1170.000	-4.454	-0.894	0.160
1180.000	-4.423	-0.894	0.165
1190.000	-4.454	-0.894	0.169
1200.000	-4.485	-0.894	0.169
1210.000	-4.485	-0.894	0.174
1220.000	-4.454	-0.894	0.179
1230.000	-4.454	-0.894	0.184
1240.000	-4.454	-0.894	0.184
1250.000	-4.454	-0.894	0.188
1260.000	-4.454	-0.894	0.188
1270.000	-4.454	-0.894	0.188
1280.000	-4.548	-0.909	0.193
1290.000	-4.517	-0.909	0.193
1300.000	-4.517	-0.909	0.193
1310.000	-4.517	-0.909	0.193
1320.000	-4.517	-0.909	0.198
1330.000	-4.517	-0.909	0.198
1340.000	-4.517	-0.909	0.198
1350.000	-4.517	-0.909	0.198
1360.000	-4.517	-0.909	0.198
1370.000	-4.517	-0.909	0.198
1380.000	-4.517	-0.909	0.202

SURFICIAL		N PHASE	
P Chinadada		hour2	Input 3
			ar CopperPerm
			2010 8431
1390.000	-4.548	-0.909	0.207
1400.000	-4.548	-0.925	0.202
1410.000	-4.517	-0.925	0.207
1420.000	-4.548	-0.925	0.207
1430.000	-4.517	-0.925	0.207
1440.000	-4.517	-0.925	0.212
1450.000	-4.517	-0.925	0.212
1460.000	-4.517	-0.925	0.212
1470.000	-4.517	-0.925	0.212
1480.000	-4.517	-0.925	0.217
1490.000	-4.517	-0.925	0.217
1500.000	-4.548	-0.925	0.217
1510.000	-4.548	-0.941	0.217
1520.000	-4.548	-0.941	0.217
1530.000	-4.485	-0.925	0.221
1540.000	-4.485	-0.925	0.221
1550.000	-4.485	-0.925	0.221
1560.000	-4.485	-0.925	
1570.000	-4.485		0.221
1570.000	-4.405 -4.517	-0.925	0.221
1590.000		-0.925	0.221
1600.000	-4.517	-0.925	0.226
1610.000	-4.517	-0.925	0.226
1620.000	-4.485	-0.925	0.226
1620.000	-4.485 -4.485	-0.925 -0.941	0.226
1640.000	-4.455	-0.925	0.231
1650.000	-4.485	-0.925	0.231 0.231
1660.000	-4.517	-0.941	0.231
1670.000	-4.517	-0.941	0.231
1680.000	-4.517	-0.941	0.231
1690.000	-4.517	-0.941	0.231
1700.000	-4.517	-0.941	0.235
1710.000	-4.517	-0.941	0.235
1720.000	-4.517	-0.941	0.240
1730.000	-4.517	-0.941	0.240
1740.000	-4.517	-0.941	0.245
1750.000	-4.517	-0.941	0.245
1760.000	-4.517	-0.941 -0.941	0.249
1770.000	-4.517	-0.941	0.240
1780.000	-4.517	-0.941	0.240
1790.000	-4.517	-0.941	0.245
1800.000	-4.517	-0.941	0.245
1810.000	-4.517	-0.956	0.245
1820.000	-4.517	-0.956	0.250
1830.000	-4.517	-0.956	0.250
1840.000	-4.517	-0.956	0.250
1850.000	-4.517	-0.956	0.254
1860.000	-4.517	-0.956	0.254
1870.000	-4.517	-0.956	0.259
1880.000	-4.517	-0.956	0.259
1890.000	-4.517	-0.956	0.264
1900.000	-4.517	-0.956	0.264
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	DRAWDOWN	PHASE	
	ting 1	Incut 2	Input 3
		a Sorgan	8" Upper Perm
		CB	Zone (IAS)
1910.000	-4.517	-0.956	0.268
1920.000	-4.517	-0.956	0.273
1930.000	-4.517	-0.956	0.268
1940.000	-4.517	-0.956	0.273
1950.000	-4.517	-0.956	0.273
1960.000	-4.517	-0.972	0.268
1970.000	-4.548	-0.972	0.278
1980.000	-4.548	-0.972	0.278
1990.000	-4.517	-0.956	0.283
2000.000	-4.548	-0.972	0.283
2010.000	-4.548	-0.972	0.283
2020.000	-4.517	-0.972	0.287
2030.000	-4.548	-0.972	0.292
2040.000	-4.548	-0.972	0.292
2050.000	-4.517	-0.972	0.297
2060.000	-4.548	-0.972	0.297
2070.000	-4.548	-0.972	0.297
2080.000	-4.548	-0.972	0.297
2080.000		-0.972	
	-4.548	-	0.292
2100.000	-4.548	-0.988	0.297
2110.000	-4.548	-0.988	0.301
2120.000	-4.548	-0.988	0.301
2130.000	-4.548	-0.988	0.297
2140.000	-4.548	-0.972	0.306
2150.000	-4.548	-0.988	0.306
2160.000	-4.548	-0.988	0.311
2170.000	-4.579	-0.988	0.311
2180.000	-4.579	-0.988	0.311
2190.000	-4.579	-0.988	0.316
2200.000	-4.579	-0.988	0.311
2210.000	-4.579	-0.988	0.316
2220.000	-4.579	-0.988	0.320
2230.000	-4.579	-0.988	0.320
2240.000	-4.548	-0.988	0.316
2250.000	-4.579	-0.988	0.320
2260.000	-4.57 9	-0.988	0.320
2270.000	-4.579	-0.988	0.325
2280.000	-4.579	-0.988	0.325
2290.000	-4.579	-1.003	0.330
2300.000	-4.579	-1.003	0.330
2310.000	-4.579	-1.003	0.330
2320.000	-4.579	-1.003	0.335
2330.000	-4.611	-1.003	0.330
2340.000	-4.611	-1.003	0.330
2350.000	-4.611	-1.003	0.335
2360.000	-4.611	-1.019	0.339
2370.000	-4.611	-1.003	0.335
2380.000	-4.611	-1.019	0.339
2390.000	-4.611	-1.003	0.344
2400.000	-4.611	-1.019	0.339
2410.000	-4.611	-1.019	0.339
2420.000	-4.611	-1.019	0.339

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SURFICIAL	DRAWDOWI	N PHASE	
Elected Theory and	interst fill For Switched	indez :	biout 3 B ^{er} Lipper Perm
			Zoné (IAS)
2430.000	-4.611	-1.019	0.339
2440.000	-4.611	-1.019	0.339
2450.000	-4.611	-1.019	0.339
2460.000	-4.611	-1.019	0.344
2470.000	-4.611	-1.019	0.344
2480.000	-4.579	-1.019	0.349
2490.000	-4.611	-1.019	0.349
2500.000	-4.611	-1.019	0.353
2510.000	-4.611	-1.035	0.353
2520.000	-4.611	-1.035	0.358
2530.000	-4.611	-1.035	0.353
2540.000	-4.611	-1.035	0.358
2550.000	-4.579	-1.035	0.358
2560.000	-4.642	-1.035	0.363
2570.000	-4.642	-1.035	0.368
2580.000	-4.611	-1.035	0.368
2590.000	-4.642	-1.050	0.372
2600.000	-4.642	-1.050	0.372
2610.000	-4.642	-1.050	0.377
2620.000	-4.642	-1.050	0.382
2630.000	-4.642	-1.035	0.386
2640.000	-4.642	-1.035	0.391
2650.000	-4.642	-1.035	0.391
2660,000	-4.642	-1.035	0.396
2670.000	-4.642	-1.035	0.396
2680.000	-4.642	-1.035	0.401
2690.000	-4.642	-1.035	0.401
2700.000	-4.642	-1.050	0.405
2710.000	-4.642	-1.050	0.405
2720.000	-4.642	-1.035	0.410
2730.000	-4.642	-1.050	0.415
2740.000	-4.611	-1.035	0.415
2750.000	-4.611	-1.035	0.419
2760.000	-4.611	-1.035	0.419
2770.000	-4.611	-1.035	0.424
2780.000	-4.642	-1.050	0.424
2790.000	-4.642	-1.050	0.424
2800.000	-4.642	-1.050	0.429
2810.000	-4.642	-1.050	0.424
2820.000	-4.642	-1.050	0.424
2830.000	-4.642	-1.066	0.424
2840.000	-4.642	-1.050	0.429
2850.000	-4.674	-1.066	0.424
2860.000	-4.674	-1.050	0.429
2870.000	-4.674	-1.066	0.434
2880.000	-4.674	-1.066	0.434
2890.000	-4.674	-1.066	0.434
2900.000	-4.674	-1.066	0.434
2910.000	-4.674	-1.066	0.434
2920.000	-4.674	-1.066	0.438
2930.000	-4.674	-1.066	0.438
2940.000	-4.674	-1.066	0.438

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2950.000	-4.674	-1.066	0.443
2960.000	-4.611	-1.066	0.438
2970.000	-4.642	-1.066	0.443
2980.000	-4.611	-1.050	0.452
2990.000	-4.642	-1.050	0.462
3000.000	-4.642	-1.050	0.457
3010.000	-4.642	-1.066	0.452
3020.000	-4.674	-1.066	0.457
3030.000	-4.642	-1.066	0.457
3040.000	-4.674	-1.066	0.452
3050.000	-4.642	-1.066	0.457
3060.000	-4.642	-1.066	0.467
3070.000	-4.642	-1.066	0.462
3080.000	-4.642	-1.066	0.462
3090.000	-4.642	-1.066	0.471
3100.000	-4.642	-1.066	0.476
3110.000	-4.642	-1.066	0.481
3120.000	-4.642	-1.066	0.490
3130.000	-4.642	-1.066	0.495
3140.000	-4.579	-1.066	0.490
3150.000	-4.642	-1.066	0.500
3160.000	-4.642	-1.066	0.500
3170.000	-4.642	-1.066	0.500
3180.000	-4.674	-1.066	0.500
3190.000	-4.674	-1.082	0.495
3200.000	-4.674	-1.066	0.495
3210.000	-4.674	-1.082	0.490
3220.000	-4.674	-1.082	0.495
3230.000	-4.674	-1.082	0.495
3240.000	-4.674	-1.082	0.495
3250.000	-4.674	-1.082	0.500
3260.000	-4.674	-1.082	0.504
3270.000	-4.674	-1.082	0.504
3280.000	-4.674	-1.082	0.504
3290.000	-4.674	-1.082	0.509
3300.000	-4.674	-1.082	0.509
3310.000	-4.674	-1.082	0.514
3320.000	-4.674	-1.082	0.514
3330.000	-4.674	-1.082	0.519
3340.000 3350.000	-4.674 -4.674	-1.082	0.523
3360.000	-4.674 -4.674	-1.082 -1.082	0.523 0.523
3370.000	-4.674	-1.082	0.523
3380.000	-4.611	-1.082	0.528
3390.000	-4.674	-1.082	0.537
3400.000	-4.674	-1.082	0.537
3410.000	-4.674	-1.082	0.537
3420.000	-4.674	-1.082	0.537
3430.000	-4.674	-1.082	0.542
3440.000	-4.674	-1.082	0.542
3450.000	-4.674	-1.082	0.547
3460.000	-4.705	-1.082	0.547
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3470.000	-4.674	-1.097	0.552
3480.000	-4.674	-1.097	0.552
3490.000	-4.674	-1.097	0.552
3500.000	-4.674	-1.097	0.556
3510.000	-4.705	-1.097	0.556
3520.000	-4.705	-1.097	0.556
3530.000	-4.674	-1.097	0.561
3540.000	-4.674	-1.097	0.556
3550.000	-4.674	-1.097	0.561
3560.000	-4.674	-1.097	0.561
3570.000	-4.674	-1.097	0.566
3580.000	-4.674	-1.097	0.566
3590.000	-4.674	-1.097	0.570
3600.000	-4.674	-1.097	0.575
3610.000	-4.674	-1.097	0.570
3620.000	-4.674	-1.097	0.575
3630.000	-4.674	-1.097	0.575
3640.000	-4.705	-1.097	0.575
3650.000	-4.705	-1.097	0.580
3660.000	-4.674	-1.097	0.580
3670.000	-4.705	-1.097	0.580
3680.000	-4.705	-1.097	0.585
3690.000	-4.705	-1.097	0.580
3700.000	-4.705	-1.113	0.585
3710.000	-4.705	-1.097	0.585
3720.000	-4.705	-1.097	0.585
3730.000	-4,705	-1.097	0.585
3740.000	-4.705	-1.113	0.589
3750.000	-4.736	-1.113	0.589
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APPENDIX B

Data Logger Water Level Measurements for Upper Permeable Zone (IAS) APT.

UPIND-B.WB2

SE2000 Environmental Logger 01/22 09:17 Unit# 577 Test 1 Setups: INPUT 1 INPUT 2 INPUT 3 INPUT 4 INPUT 5 INPUT 6 INPUT 7 Туре Level (F) Level (F) Level (F) Level (F) Level (F) Level (F) Mode Surface Surface Surface Surface Surface Surface Reference 0.000 0.000 0.000 0.000 0.000 0.000 0.000 PSI at Ref. 37.215 23.412 22.720 3.160 3.281 2.523 10.644 SG 1.000 1.000 1.000 1.000 1.000 1.000 1.000 Linearity 0.036 -0.081 0.014 0.073 0.106 0.078 0.081 Scale factor 99.651 99.925 49.817 14.905 15.039 15.068 15.012 Offset -0.083 -0.112 -0.107 0.009 -0.040 0.040 -0.016 Delay mSEC 50.000 50.000 50.000 50.000 50.000 50.000 50.000 Step 0 01/06 22:27:16

UPPER PERMEABLE ZONE (INTERMEDIATE AQUIFER SYSTEM) DRAWDOWN PHASE

Barro storage					
ULUER KINDER II					
0	0	0	0	0.004	ß
0.0083	0	0	0	0.004	0
0.0166	0	0	0	0.004	0
0.025	0	0	0	0.004	0
0.0333	0	0	0	0.004	0
0.0416	0.031	0	0	0.004	0
0.05	0	0	a	0.004	0
0.0583	0	0	Q	0.004	0.004
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0.0833	0	0	0	0.004	0
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0.1333	-2.792	-0.031	0	0.004	0
			õ		
0.15	-3.482	-0.062		0	0
0.1583	-4.392	-0.062	0	0.004	0
0.1666	-5.239	-0.062	0	0.004	0
0.175	-5.866	-0.094	0	0.004	0
0.1833	-6.682	-0.094	0	0.004	Û.
0.1916	-7.31	-0.125	0	0.004	0
0.2	-8.031	-0.157	0	0.004	0
0.2083	-9.067	-0.157	0	0.004	0
0.2166	-9.318	-0.188	0	0.004	0
0.225	-9.725	-0.22	0	0.004	0
0.2333	-10.227	-0.251	0	0.004	0
0.2416	-10.761	-0.251	0	0.004	Ó
0.25	-11.2	-0.282	0	0	0
0.2583	-11.702	-0.314	0	0	0
0.2666	-12.11	-0.345	0	0	0
0.275	-12.643	-0.377	0	0.004	0
0.2833	-12.926	-0.377	0	0.004	0
0.2916	-13.365	-0.408	0	0	0
0.3	-13.835	-0.44	0	0	0
0.3083	-14.118	-0.44	0	0.004	ΰ
0.3166	-14.463	-0.471	0	0	0
0.325	-14.871	-0.471	0	0.004	0
0.3333	-15.153	-0.503	0	0.004	0
0.35	-15.718	-0.534	0	0.004	0
0.3666	-16.283	-0.565	0	0.004	0
0.3833	-16.816	-0.597	0	0.004	0
0.4	-17.286	-0.597	0	0.004	0
0.4166	-17.632	-0.628	0	0.004	0
0.4333	-18.134	-0.66	0	0.004	0
0.45	-18.51	-0.691	0	0.004	0
0.4666	-18.792	-0.723	0	0.004	0
0.4833	-19.169	-0.754	0	0.004	0
0.5	-19.514	-0.786	0	0.004	0
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SE2000
Environmental Logger
01/13 13:01
Unit# 577 Test 1
Setups: INPUT 1 INPUT 2 INPUT 3 INPUT 4 INPUT 5 INPUT 6 INPUT 7
Type Level (F) Level (F) Level (F) Level (F) Level (F) Level (F)
Mode Surface Surface Surface Surface Surface Surface
Reference 0.000 0.000 0.000 0.000 0.000 0.000 0.000
PSI at Ref. 37.215 23.412 22.720 3.160 3.281 2.523 10.644
SG 1.000 1.000 1.000 1.000 1.000 1.000 1.000
Linearity 0.036 -0.081 0.014 0.073 0.106 0.078 0.081
Scale factor 99.651 99.925 49.817 14.905 15.039 15.068 15.012
Offset -0.083 -0.112 -0.107 0.009 -0.040 0.040 -0.016
Delay mSEC 50.000 50.000 50.000 50.000 50.000 50.000 50.000
Step 1 01/08 12:24:53

UPPER PERMEABLE ZONE (INTERMEDIATE AQUIFER SYSTEM) RECOVERY PHASE

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0	-39.874	-16.035	0.156	-0.136	-0.071
0.0083	-39.937	-16.035	0.156	-0.136	-0.071
0.0166	-39.905	-16.035	0.156	-0.131	-0.066
0.025	-39.905	-16.035	0.156	-0.136	-0.071
0.0333	-39.937	-16.035	0.156	-0.136	-0.066
0.0416	-39.874	-16.035	0.156	-0.136	-0.071
0.05	-39.843	-16.035	0.156	-0.136	-0.071
0.0583 0.0666	-39.874 -39.874	-16.035	0.156	-0.136	-0.076 -0.071
0.0000	-39.905	-16.035 -16.035	0.156 0.156	-0.136 -0.136	-0.066
0.0833	-39.905	-16.035	0.156	-0.136	-0.071
0.0916	-39.905	-16.035	0.156	-0.136	-0.071
0.1	-39.937	-16.035	0.156	-0.136	-0.071
0.1083	-39.905	-16.035	0.156	-0.136	-0.066
0.1166	-39.905	-16.004	0.156	-0.136	-0.071
0.125	-39.905	-16.035	0.156	-0.136	-0.061
0.1333	-39.874	-16.035	0.156	-0.131	-0.076
0.1416	-36.674	-16.035	0.156	-0.136	-0.071
0.15	-37.71	-16.035	0.156	-0.136	-0.076
0.1583	-38.149	-16.004	0.156	-0.136	-0.066
0.1666	-37.459	-16.004	0.156	-0.136	-0.071
0.175	-36.643	-16.004	0.156	-0.136	-0.066
0.1833	-35.796	-16.004	0.156	-0.136	-0.071
0.1916	-35.043	-16.004	0.156	-0.136	-0.066
0.2	-34.321	-16.004	0.156	-0.136	-0.061
0.2083	-33.569	-16.004	0.156	-0.136	-0.066
0.2166	-32.878	-16.004	0.156	-0.136	-0.066
0.225	-32.22	-16.004	0.156	-0.136	-0.071
0.2333	-31.529	-15.972	0.156	-0.136	-0.071
0.2416	-30.902	-15.972	0.156	-0.136	-0.066
0.25	-30.275	-15.972	0.156	-0.131	-0.071
0.2583	-29.678	-15.972	0.156	-0.141	-0.066
0.2666	-29.114	-15.941	0.141	-0.131	-0.066
0.275	-28.549	-15.941	0.156	-0.136	-0.071
0.2833	-27.984	-15.941	0.156	-0.131	-0.061 -0.066
0.2916	-27.482	-15.909	0.141	-0.136 -0.136	-0.066
0.3 0.3083	-26.949 -26.447	-15.909 -15.878	0.141 0.141	-0.136	-0.066
0.3166	-25.977	-15.878	0.141	-0.136	-0.071
0.325	-25.506	-15.846	0.141	-0.136	-0.071
0.3333	-25.067	-15.646	0.156	-0.136	-0.066
0.35	-24.22	-15.815	0.156	-0.136	-0.061
0.3666	-23.404	-15.783	0.156	-0.131	-0.066
0.3833	-22.683	-15.721	0.156	-0.136	-0.071
0.4	-21.992	-15.689	0.156	-0.131	-0.066
0.4166	-21.365	-15.658	0.156	-0.131	-0.066
0.4333	-20.737	-15.626	0.156	-0.131	-0.066
0.45	-20.235	-15.595	0.156	-0.131	-0.071
0.4666	-19.734	-15.563	0.156	-0.131	-0.066
0.4833	-19.263	-15.5	0.141	-0.131	-0.071
0.5	-18.855	-15.469	0.141	-0.131	-0.066
0.5166	-18.479	-15.438	0.141	-0.136	-0.066
0.5333	-18.102	-15.406	0.156	-0.136	-0.066
0.55	-17.788	-15.343	0.156	-0.131	-0.071
0.5666	-17.475	-15.312	0.156	-0.131	-0.066

UPPER PER	MEABLE ZONE		TE AQUIFER S		WDOWN PHASE	IIPPER PER		E (INT <u>ERM</u> EDIA		SYSTEM \ RECA	
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0.5666	-20.581	-0.88	0	0.004	0	0.5833	-17.224	-15.28	0.156	-0.131	-0.066
0.5833	-20.894	-0.68	0	0.004	0	0.6	-16.973	-15.249	0.156	-0.131	-0.066
0.6	-21.239	-0.911	0	0.004	0	0.6166	-16.753	-15.217	0.156	-0.131	-0.071
0.6166 0.6333	-21.396 -21.679	-0.943 -0.943	0 0	0.004 0.004	0	0.6333 0.65	-16.565 -16.408	-15.186 -15.155	0.156 0.156	-0.131 -0.131	-0.066 -0.066
0.65	-21.93	-0.974	ő	0.004	0	0.6666	-16.251	-15.123	0.138	-0.131	-0.088
0.6666	-22.181	-0.974	0	0.004	Û	0.6833	-16.094	-15.092	0.141	-0.131	-0.066
0.6833	-22.432	-1.006	0	0.004	0	0.7	-15.969	-15.029	0.141	-0.131	-0.071
0.7 0.7166	-22.526 -22.683	-1.037 -1.037	0 0	0.004 0.004	0	0.7166 0.7333	-15.843 -15.749	-14.997 -14.966	0.141	-0.131	-0.066
0.7333	-22.871	-1.068	0	0.004	0	0.7333	-15.624	-14.966	0.141 0.141	-0.131 -0.131	-0.066 -0.066
0.75	-22.996	-1.068	0	0.004	0	0.7666	-15.561	-14.934	0.141	-0.131	-0.066
0.7666	-23.122	-1.1	0	0.004	0	0.7833	-15.467	-14.903	0.141	-0.131	-0,066
0.7833 0.8	-23.247 -23.404	-1.1 -1.131	0 0	0.004 0.004	0.004 0	0.8	-15.404	-14.872	0.156	-0.131	-0.066 -0.066
0.8166	-23.467	-1.163	õ	0.004	0	0.8166 0.8333	-15.373 -15.31	-14.872 -14.84	0.156 0.156	-0.131 -0.131	-0.066
0.8333	-23.592	-1.163	Ó	0.004	0	0.85	-15.279	-14.809	0.156	-0.131	-0.066
0.85	-23.718	-1.163	0	0.004	0	0.8666	-15.216	-14.809	0.141	-0.131	-0.071
0.8666	-23.843	-1.194	0	0.004	0	0.8833	-15.184	-14.777	0.141	-0.136	-0.066
0.8833 0.9	-23.906 -24.063	-1.194 -1.226	0	0.004	0	0.9 0.9166	-15.153 -15.122	-14.777 -14.746	0.156	-0.131 -0.136	-0.066 -0.071
0.9166	-24.003	-1.226	0	0.004	0	0.9333	-15.09	-14.746	0.141 0.141	-0.136	-0.071
0.9333	-24.251	-1.257	0	0.004	ō	0.95	-15.059	-14.746	0.141	-0.131	-0.071
0.95	-24.345	-1.257	0	0.004	0	0.9666	-15.028	-14.714	0.141	-0.136	-0.071
0.9666	-24.471	-1.257	0	0.004	0	0.9833	-14.996	-14.714	0.156	-0.131	-0.066
0.9833 1	-24.596 -24.69	-1.289 -1.289	0 0	0.004 0.004	0	1 1.2	-14.965 -14.745	-14.683 -14.526	0.156 0.141	-0.131 -0.136	-0.066 -0.071
1.2	-25.381	-1.414	0.015	0.004	õ	1.4	-14.62	-14.431	0.141	-0.136	-0.071
1.4	-25.914	-1.54	0.015	0.004	0	1.6	-14.494	-14.368	0.141	-0.136	-0.071
1.6	-26.228	-1.634	0.015	0.004	0	1.8	-14.369	-14.274	0.141	-0.136	-0.066
1.8	-26.447	-1.697	0.015	0.004	0.004	2	-14.275	-14.211	0.141	-0.136	-0.071 -0.071
2 2.2	-26.698 -26.855	-1.792 -1.854	0.015 0	0.004 0.004	0.004 0.004	2.2 2.4	-14.212 -14.118	-14.148 -14.085	0.141 0.141	-0.136 -0.136	-0.061
2.4	-26.981	-1.917	0.015	0.009	0	2.6	-14.055	-14.023	0.141	-0.136	-0.071
2.6	-27.106	-1.98	0.015	0.004	0.004	2.8	-13.992	-13.96	0.141	-0.141	-0.071
2.8	-27.2	-2.012	0.015	0.004	0.004	3	-13.93	-13.928	0.141	-0.136	-0.071
3 3.2	-27.263 -27.357	-2.075 -2.137	0.015 0.015	0.009 0.009	0.004 0.004	3.2 3.4	-13.867 -13.804	-13.865 -13.834	0.141	-0.136 -0.136	-0.071 -0.071
3.4	-27.357	-2.169	0.015	0.009	0	3.4	-13.741	-13.654	0.141 0.141	-0.136	-0.071
3.6	-27.482	-2.232	0.015	0.009	0.004	3.8	-13.71	-13.74	0.141	-0.136	-0.066
3.8	-27.545	-2.263	0.015	0.009	0.004	4	-13. 64 7	-13.677	0.141	-0.136	-0.066
4	-27.608	-2.326	0.015	0.004	0.004	4.2	-13.616	-13.645	0.141	-0.136	-0.061
4.2 4.4	-27.671 -27.733	-2.358 -2.389	0.015 0.015	0.009	0.004 0.004	4.4 4.6	-13.584 -13.522	-13.614 -13.551	0.141 0.156	-0.131 -0.136	-0.061 -0.066
4.6	-27.733	-2.42	0.015	0.009	0.004	4.8	-13.49	-13.519	0.141	-0.131	-0.071
4.8	-27.828	-2.483	0.015	0.009	0.004	5	-13.428	-13.488	0.141	-0.136	-0.066
5	-27.89	-2.515	0.015	0.009	0.004	5.2	-13.396	-13.457	0.141	-0.136	-0.071
5.2	-27.953	-2.546	0.015	0.009	0.004	5.4	-13.365	-13.425	0.141	-0.136	-0.066
5.4 5.6	-27.953 -28.016	-2.578 -2.641	0.015 0.015	0.009 0.009	0.004 0.004	5.6 5.8	-13.302 -13.271	-13.394 -13.362	0.141 0.141	-0.136 -0.136	-0.071 -0.071
5.8	-28.079	-2.672	0	0.009	0.004	6	-13.239	-13.331	0.141	-0.136	-0.066
6	-28.141	-2.703	0.015	0.009	0.004	6.2	-13.208	-13.299	0.141	-0.136	-0.066
6.2	-28.173	-2.735	0.015	0.009	0.004	6.4	-13.177	-13.268	0.141	-0.136	-0.071
6.4	-28.235	-2.766	0.015	0.009	0.004	6.6	-13.145	-13.237	0.141	-0.136 -0.136	-0.071 -0.066
6.6 6.8	-28.235 -28.267	-2.798 -2.829	0.015 0.015	0.009	0.004 0.004	6.8 7	-13.114 -13.082	-13.174 -13.174	0.156 0.141	-0.136	-0.086
7	-28.298	-2.861	0.015	0.009	0.004	7.2	-13.051	-13.142	0.141	-0.136	-0.071
7.2	-28.33	-2.892	0.015	0.009	0.009	7.4	-13.02	-13.111	0.156	-0.136	-0.066
7.4	-28.361	-2.923	0.015	0.009	0.004	7.6	-12.988	-13.079	0.156	-0.136	-0.061
7.6 7.8	-28.455 -28.424	-2.923 -2.986	0.015 0.015	0.009 0.009	0.009	7.8 8	-12.957 -12.926	-13.048 -12.985	0.156 0.156	-0.131 -0.136	-0.061 -0.061
8	-28.486	-2.986	0.015	0.009	0.004 0.009	8.2	-12.826	-12.985	0.156	-0.136	-0.061
8.2	-28.549	-3.018	0.015	0.009	0.004	8.4	-12.863	-12.954	0.156	-0.136	-0.071
8.4	-28.612	-3.049	0.015	0.009	0.009	8.6	-12.831	-12.954	0.141	-0.131	-0.066
8.6 8.8	-28.643 -28.612	-3.081 -3.112	0.015	0.014	0.009	8.8	-12.8 12.760	-12.922	0.156	-0.131	-0.066
9	-28.643	-3.112 -3.144	0.015 0.015	0.009	0.009 0.009	9 9.2	-12.769 -12.737	-12.891 -12.859	0.156 0.156	-0.136 -0.136	-0.066 -0.061
9.2	-28.706	-3.144	0.015	0.014	0.009	9.4	-12.706	-12.828	0.156	-0.131	-0.066
9.4	-28.737	-3.175	0.015	0.014	0.009	9.6	-12.675	-12.828	0.156	-0.131	-0.061
9.6	-28.737	-3.206	0.015	0.014	0.009	9.8	-12.643	-12.796	0.156	-0.126	-0.047
9.8 10	-28.8 -28.831	-3.238 -3.269	0.015 0.015	0.014 0.009	0.009	10	-12.643 -12.424	-12.796 -12.576	0.156	-0.126	-0.071
10	-20.001	-3.209	0.013	0.009	0.009	12	-12.424	-12.576	0.156	-0.136	-0.057

UP		ABLE ZONE		E AQUIFER S	YSTEM) DRAM	DOWN PHASE	UPPER PE	RMEABLE ZON	E (INTERMEDIA	TE AQUIFER :	SYSTEM) REC	OVERY PHASE
		5			同時 学校 時期	input 5	Cleaned	Trake.				input 6
					California Securit	12" Burnerson	Three grades				12 Land part	12 Suprime
	12	-29.082	-3.489	0.015	0.014	0.009	14	-12.204	-12.388	0.156	-0.136	-0.071
	14	-29.302	-3.71	0.015	0.014	0.014	16	-12.047	-12.23	0.156	-0.136	-0.071
	16	-29.553	-3.93	0.015	0.009	0.009	18	-11.859	-12.042	0.156	-0.136	-0.066
	18 20	-29.647 -29.804	-4.118 -4.275	0.015 0.015	0.009 0.009	0.009 0.009	20 22	-11.702 -11.577	-11.884 -11.727	0.156 0.156	-0.141 -0.131	-0.057 -0.061
	22	-29.992	-4.433	0.015	0.009	-0.009	24	-11.42	-11.633	0.156	-0.131	-0.066
	24	-30.118	-4.59	0.015	0.014	0.004	26	-11.294	-11.476	0.156	-0.131	-0.061
	26	-30.212	-4.716	0.015	0.014	0.009	28	-11.2	-11.381	0.156	-0.136	-0,061
	28 30	-30.369 -30.431	-4.841	0.015	0.014	0.014	30	-11.075	-11.256	0.156	-0.126	-0.061
	30 32	-30.526	-4.967 -5.093	0.015 0.015	0.014 0.014	0.014 0.014	32 34	-10.949 -10.855	-11.13 -11.035	0.156 0.156	-0.131 -0.131	-0.061 -0.057
	34	-30.651	-5.187	0.015	0.018	0.014	36	-10.761	-10.941	0.156	-0.131	-0.061
	36	-30.777	-5.313	0.015	0.014	0.014	38	-10.635	-10.815	0.156	-0.126	-0.057
	38	-30.839	-5.407	0.015	0.018	0.019	40	-10.541	-10.721	0.156	-0.126	-0.057
	40 42	-30.965 -31.09	-5.502 -5.627	0.015 0.015	0.023 0.018	0.023 0.019	42 44	-10.478 -10.384	-10.658 -10.564	0.156 0.156	-0.126 -0.117	-0.052 -0.052
	44	-31.059	-5.722	0.015	0.018	0.023	44	-10.384	-10.304	0.156	-0.112	-0.042
	46	-31.184	-5.816	0.015	0.018	0.023	48	-10.227	-10.375	0.156	-0.112	-0.047
	48	-31.278	-5.91	0.015	0.018	0.023	50	-10.133	-10.312	0.156	-0.108	-0.047
	50	-31.341	-5.942	0.015	0.028	0.028	52	-10.039	-10.187	0.156	-0.108	-0.042
	52 54	-31.373 -31.404	-6.036 -6.131	0.015 0.015	0.028	0.028	54 56	-9.976 -9.914	-10.155 -10.092	0.156 0.156	-0.117 -0.112	-0.047 -0.047
	56	-31.561	-6.225	0.015	0.028	0.028	58	-9.851	-9.998	0.156	-0.112	-0.042
	58	-31.592	-6.319	0.015	0.028	0.028	60	-9.757	-9.935	0.156	-0.112	-0.047
	60	-31.686	-6.382	0.015	0.028	0.028	62	-9.694	-9.872	0.156	-0.112	-0.042
	62	-31.718	-6.476	0.015	0.028	0.028	64	-9.631	-9.778	0.156	-0.112	-0.038
	64 66	-31.78 -31.875	-6.508 -6.602	0.015 0.015	0.028 0.028	0.033 0.028	66 68	-9.569 -9.506	-9.715 -9.652	0.156 0.156	-0.112 -0.108	-0.042 -0.038
	68	-31.937	-6.696	0.015	0.028	0.028	70	-9.443	-9.621	0.156	-0.112	-0.042
	70	-31.969	-6.759	0.015	0.028	0.033	72	-9.38	-9.526	0.156	-0.112	-0.042
	72	-31.969	-6.822	0.015	0.032	0.033	74	-9.318	-9.495	0.156	-0.112	-0.042
	74	-31.969 -32.031	-6.885	0.015	0.032	0.033	76	-9.255 -9.192	-9.432 -9.369	0.156 0.156	-0.108 -0.108	-0.033 -0.042
	76 78	-32.031	-6.948 -7.011	0.031 0.015	0.032 0.032	0.038 0.038	78 80	-9.162	-9.309	0.156	-0.108	-0.038
	80	-32.188	-7.074	0.015	0.032	0.033	82	-9.098	-9.243	0.156	-0.108	-0.038
	82	-32.251	-7.137	0.015	0.037	0.033	84	-9.035	-9.212	0.156	-0.112	-0.038
	84	-32.314	-7.2	0.015	0.032	0.033	86	-8.973	-9.149	0.156	-0.108	-0.033
	86	-32.376 -32.439	-7.262	0.031 0.015	0.037	0.033	88 90	-8.941 -8.878	-9.086 -9.023	0.156 0.156	-0.108 -0.108	-0.038 -0.033
	88 90	-32.439 -32.502	-7.325 -7.388	0.015	0.037 0.037	0.038 0.038	90	-8.816	-9.023	0.156	-0.103	-0.033
	92	-32.533	-7.42	0.031	0.042	0.038	94	-8.784	-8.929	0.156	-0.098	-0.023
	94	-32.565	-7.483	0.031	0.042	0.038	96	-8.722	-8.866	0.156	-0.094	-0.019
	96	-32.565	-7.545	0.031	0.042	0.042	98	-8.69	-8.835	0.156	-0.103	-0.023
	98 100	-32.627 -32.753	-7.608 -7.64	0.031 0.031	0.042 0.047	0.042 0.047	100 110	-8.627 -8.408	-8.772 -8.552	0.141 0.156	-0.098 -0.098	-9.763 -9.763
	110	-32.941	-7.891	0.031	0.047	0.047	120	-8.188	-8.331	0.156	-0.089	-9,763
	120	-33.098	-8.143	0.031	0.051	0.052	130	-8	-8.111	0.141	-0.079	-9.763
	130	-33.255	-8.363	0.031	0.061	0.061	140	-7.812	-7.891	0.141	-0.065	-9.763
	140	-33.412	-8.552	0.031	0.07	0.071	150	-7.655	-7.734	0.141	-0.065	-9.763
	150 160	-33.569 -33.757	-8.772 -8.929	0.031 0.031	0.065 0.075	0.066 0.076	160 170	-7.467 -7.31	-7.545 -7.42	0.141 0.141	-0.056 -0.051	-9.763 -9.763
	170	-33.882	-9.117	0.031	0.079	0.08	180	-7.153	-7.262	0.141	-0.047	-9.763
	180	-34.039	-9.306	0.031	0.089	0.09	190	-6.996	-7.105	0.141	-0.042	-9.763
	190	-34.165	-9.463	0.047	0.098	0.095	200	-6.87	-6.979	0.141	-0.037	-9.763
	200	-34.259	-9.621	D.047	0.103	0.099	210	-6.714	-6.822	0.141	-0.037	-9.763
	210 220	-34.416 -34.478	-9.746 -9.904	0.047 0.047	0.108 0.112	0.099 0.104	220 230	-6.588 -6.463	-6.696 -6.539	0.141 0.141	-0.032 -0.018	-9.763 -9.763
	230	-34.604	-10.029	0.047	0.117	0.114	240	-6.368	-6.445	0.141	-9.375	-9,763
	240	-34.667	-10.155	0.047	0.122	0.118	250	-6.243	-6.351	0.125	-9.375	-9.763
	250	-34.792	-10.281	0.047	0.131	0.123	260	-6.117	-6.225	0.125	-9.375	-9.763
	260	-34.98	-10.407	0.047	0.136	0.128	270	-6.023	-6.099	0.141	-9.375	-9.763
	270 280	-35.106 -35.137	-10.532 -10.627	0.047 0.047	0.141 0.141	0.133 0.133	260 290	-5.898 -5.804	-5.973 -5.91	0.125 0.125	-9.375 -9.375	-9.763 -9.763
	290	-35.137	-10.827	0.047	0.145	0.133	300	-5.71	-5.785	0.125	-9.375	-9.763
	300	-35.263	-10.847	0.047	0.15	0.137	310	-5.647	-5.722	0.125	-9.375	-9.763
	310	-35.388	-10.973	0.047	0.15	0.142	320	-5.521	-5.596	0.141	-9.375	-9.763
	320	-35.419 -35.514	-11.067	0.047	0.155	0.142	330	-5.427	-5.533	0.141	-9.375	-9.763
	330 340	-35.514 -35.639	-11.161 -11.256	0.062 0.062	0.159 0.164	0.147 0.147	340 350	-5.365 -5.27	-5.47 -5.344	0.141 0.141	-9.375 -9.375	-9.763 -9.763
	350	-35.702	-11.35	0.062	0.164	0.152	360	-5.27 -5.208	-5.344 -5.282	0.141	-9.375 -9.375	-9.763 -9.763
	360	-35.796	-11.444	0.062	0.169	0.152	370	-5.114	-5.187	0.141	-9.375	-9.763
	370	-35.827	-11.507	0.062	0.1 69	D.156	380	-5.051	-5.124	0.141	-9.375	-9.763

UPPER PER	MEABLE ZONE	(INTERMEDIA	TE AQUIFER (SYSTEM) DRAV	DOWN PHASE		RMEABLE ZONE	(INTERMEDIA	TE AQUIFER :	SYSTEM) REC	OVERY PHASE
				12 Lower page	ibiput 5 12* Scenarios		Status Conta				
										C. Serie Pro-	12 Currier
380	-35.89	-11.601	0.062	0.169	0.156	390	-4.957	-5.061	0.141	-9.375	-9.763
390 400	-35.953 -36.016	-11.696 -11.759	0.062 0.062	0.169 0.173	0.156 0.156	400	-4.894	-4.967	0.141	-9.375	-9.763
410	-36.141	-11.853	0.062	0.173	0.156	410 420	-4.831 -4.768	-4.904 -4.841	0.141 0.141	-9.375 -9.375	-9.763 -9.763
420	-36.172	-11.916	0.062	0.164	0.152	430	-4.706	-4.779	0.141	-9.375	-9.763
430	-36.298	-12.01	0.062	0.164	0.142	440	-4.643	-4.716	0.141	-9.375	-9.763
440	-36.298	-12.073	0.062	0.159	0.142	450	-4.58	-4.653	0.141	-9.375	-9.763
450 460	-36.361 -36.486	-12.105 -12.199	0.062 0.062	0.159 0.155	0.137 0.133	460 470	-4.517 -4.455	-4.59 -4.527	0.141	-9.375	-9.763
470	-36.517	-12.293	0.062	0.15	0.128	480	-4.392	-4.464	0.141 0.141	-9.375 -9.375	-9.763 -9.763
480	-36.549	-12.356	0.078	0.15	0.123	490	-4.329	-4.401	0.141	-9.375	-9.763
490	-36.58	-12.419	0.078	0.141	0.118	500	-4.298	-4.37	0.141	-9.375	-9.763
500 510	-36.643 -36.768	-12.482 -12.545	0.078 0.078	0.136 0.131	0.114 0.109	510 520	-4.235 -4.172	-4.307 -4.244	0.141	-9.375	-9.763
520	-36.768	-12.608	0.078	0.126	0.104	530	-4.141	-4.213	0.141 0.141	-9.375 -9.375	-9.763 -9.763
530	-36.831	-12.671	0.078	0.122	0.099	540	-4.078	-4.15	0.141	-9.375	-9.763
540	-36.863	-12.702	0.078	0.117	0.095	550	-4.047	-4.087	0.141	-9.375	-9.763
550	-36.894	-12.796	0.078	0.112	0.09	560	-3.984	-4.055	0.141	-9.375	-9.763
560 570	-36.988 -36.957	-12.859 -12.922	0.078 0.078	0.112 0.103	0.09	570	-3.921	-3.992	0.141	-9.375	-9.763
580	-30.907	-12.922	0.078	0.098	0.08 0.08	580 590	-3.89 -3.827	-3.961 -3.93	0.141 0.141	-9.375 -9.375	-9.763 -9.763
590	-37.082	-13.016	0.078	0.094	0.08	600	-3.796	-3.867	0.141	-9.375	-9.763
600	-37.145	-13.079	0.078	0.079	0.076	610	-3.764	-3.835	0.141	-9.375	-9.763
610	-37.176	-13.142	0.078	0.089	0.071	620	-3.702	-3.804	0.141	-9.375	-9.763
620 630	-37.27 -37.27	-13.174 -13.237	0.078 0.078	0.159 0.418	0.066 0.066	630 640	-3.67 -3.639	-3.741 -3.71	0.141 0.141	-9.375 -9.375	-9.763 -9.763
640	-37.302	-13.268	0.078	0.352	0.057	650	-3.608	-3.678	0.141	-9.375	-9.763
650	-37.427	-13.331	0.078	0.352	0.047	660	-3.545	-3.615	0.141	-9.375	-9.763
660	-37.49	-13.362	0.078	0.032	0.004	670	-3.513	-3.584	0.141	-9.375	-9.763
670 680	-37.49 -37.553	-13.425	0.078	0.216	-0.014	680	-3.482	-3.552	0.141	-9.375	-9.763
690	-37.553	-13.457 -13.519	0.078 0.078	0.253 0.23	-0.047 -0.061	690 700	-3.451 -3.388	-3.521 -3.458	0.141 0.141	-9.375 -9.375	-9.763 -9.763
700	-37.615	-13.551	0.078	-0.164	-0.085	710	-3.357	-3.427	0.141	-9.375	-9.763
710	-37.584	-13.614	0.078	-0.192	-0.099	720	-3.325	-3.395	0.141	-9.375	-9.763
720	-37.615	-13.645	0.078	-0.211	-0.114	730	-3.294	-3.364	0.141	-9.375	-9.763
730	-37.678	-13.677	0.078	-0.225	-0.118	740	-3.262	-3.332	0.141	-9.375	-9.763
740 750	-37.678 -37.772	-13.74 -13.771	0.078 0.094	-0.235 -0.249	-0.133 -0.137	750 760	-3.231 -3.168	-3.301 -3.269	0.141 0.141	-9.375 -9.375	-9.763 -9.763
760	-37.835	-13.802	0.078	-0.239	-0.152	770	-3.168	-3.238	0.141	-9.375	-9.763
770	-37.804	-13.834	0.078	-0.244	-0.161	780	-3.106	-3.206	0.141	-9.375	-9.763
780	-37.835	-13.865	0.078	-0.108	-0.166	790	-3.106	-3.175	0.141	-9.375	-9.763
790 800	-37.866 -37.866	-13.865 -13.897	0.076 0.078	0.117	-0.171	800	-3.043	-3.144	0.141	-9.375	-9.763
810	-38.023	-13.96	0.078	0.103 -0.272	-0.161 -0.166	810 820	-3.011 -3.011	-3.112 -3.081	0.141 0.141	-9.375 -9.375	-9.763 -9.763
820	-37.961	-13.991	0.078	-0.277	-0.175	830	-2.98	-3.049	0.141	-9.375	-9.763
830	-37.992	-14.023	0.078	-0.282	-0.171	840	-2.949	-3.018	0.141	-9.375	-9.763
840	-37.992	-14.054	0.078	-0.272	-0.175	850	-2.917	-2.986	0.141	-9.375	-9.763
850 860	-38.055 -38.149	-14.085 -14.117	0.094 0.078	-0.267 -0.282	-0.166 -0.175	660 870	-2.886 -2.855	-2.955 -2.923	0.141 0.141	-9.375 -9.375	-9.763 -9.763
870	-38.117	-14.148	0.078	-0.282	-0.166	880	-2.835	-2.892	0.141	-9.375	-9.763
880	-38.055	-14.117	0.078	-0.267	-0.161	890	-2.792	-2.861	0.141	-9.375	-9.763
890	-38.117	-14.211	0.078	-0.258	-0.166	900	-2.76	-2.829	0.141	-9.375	-9.763
900 910	-38.18	-14.211	0.094	-0.253	-0.156	910	-2.729	-2.829	0.141	-9.375	-9.763
910 920	-38.18 -38.211	-14.243 -14.274	0.094 0.078	-0.244 -0.239	-0.152 -0.152	920 930	-2.729 -2.698	-2.798 -2.766	0.141 0.141	-9.375 -9.375	-9.763 -9.763
930	-38.274	-14.306	0.094	-0.235	-0.147	940	-2.666	-2.735	0.141	-9.375	-9.763
940	-38.243	-14.337	0.078	-0.239	-0.152	950	-2.635	-2.703	0.141	-9.375	-9.763
950	-38.306	-14.368	0.094	-0.244	-0.156	960	-2.604	-2.672	0.141	-9.375	-9.763
960	-38.243	-14.4	0.078	-0.253	-0.175	970	-2.572	-2.672	0.141	-9.375	-9.763
970 960	-38.4 -38.306	-14.431 -14.431	0.078 0.078	-0.258 -0.258	-0.171 -0.171	960 990	-2.572 -2.541	-2.641 -2.609	0.141	-9.375	-9.763
990	-38.4	-14.463	0.078	-0.258	-0.175	1000	-2.541	-2.578	0.141 0.141	-9.375 -9.375	-9.763 -9.763
1000	-38.431	-14.494	0.078	-0.263	-0.185	1010	-2.478	-2.578	0.141	-9.375	-9.763
1010	-38.462	-14.526	0.094	-0.263	-0.18	1020	-2.478	-2.546	0.141	-9.375	-9.763
1020 1030	-38.4 -38.557	-14.526	0.078	-0.267	-0.18	1030	-2.447	-2.515	0.141	-9.375	-9.763
1030	-38.557 -38.494	-14.557 -14.589	0.094 0.094	-0.263 -0.239	-0.18 -0.166	10 40 1050	-2.415 -2.415	-2.515 -2. 483	0.141 0.141	-9.375 -9.375	-9.763 -9.763
1050	-38.588	-14.62	0.078	-0.202	-0.133	1050	-2.415	-2.463 -2.452	0.141	-9.375 -9.375	-9.763 -9.763
1060	-38.557	-14.62	0.078	-0.164	-0.095	1070	-2.353	-2.452	0.141	-9.375	-9.763
1070	-38.651	-14.651	0.094	-0.136	-0.071	1080	-2.353	-2.42	0.141	-9.375	-9.763
1080 1090	-38.557 -38.619	-14.683 -14.714	0.078	-0.117	-0.052	1090	-2.321	-2.42	0.141	-9.375	-9.763
1000	-00.018	-14.714	0.078	-0.098	-0.042	1100	-2.321	-2.389	0.141	-9.375	-9.763

UPPER PER	MEABLE ZONE		re aquifer s	SYSTEM) DRAW	DOWN PHASE	UF	PPER PEF	RMEABLE ZONE	(INTERMEDIA	TE AQUIFER :	SYSTEM) REC	OVERY PHASE
		Rolf (Annal S.	house 4 12 Losser prim	Input 5 12" Statemente	P					Talana an	anna 5
1100	-38.651	-14.714	0.094	-0.084	-0.028	300398	1110	-2.29	-2.389	0.141	-9.375	-9.763
1110	-38.682	-14.746	0.094	-0.075	-0.023		1120	-2.29	-2.358	0.141	-9.375	-9.763
1120	-38.682	-14.777	0.094	-0.07	-0.019		1130	-2.258	-2.358	0.141	-9.375	-9.763
1130 1140	-38.682 -38.713	-14.777 -14.809	0.094	-0.061	-0.014		1140	-2.258	-2.326	0.141	-9.375	-9.763
1140	-38.682	-14.809	0.094 0.094	-0.061 -0.051	-0.014 -0.009		1150 1160	-2.227 -2.227	-2.326 -2.295	0.141 0.141	-9.375 -9.375	-9.763 -9.763
1160	-38.713	-14.84	0.094	-0.051	-0.009		1170	-2.196	-2.263	0.141	-9.375	-9.763
1170	-38.745	-14.872	0.094	-0.051	-0.009		1180	-2.196	-2.263	0.125	-9.375	-9.763
1180	-38.808	-14.903	0.094	-0.051	-0.019		1190	-2.196	-2.232	0.141	-9.375	-9.763
1190	-38.839	-14.903	0.094	-0.051	-0.023		1200	-2.164	-2.232	0.141	-9.375	-9.763
1200 1210	-38.808 -38.902	-14.934 -14.966	0.094 0.094	-0.047 -0.051	-0.023		1210	-2.133	-2.232	0.141	-9.375	-9.763
1210	-38.902	-14.900	0.094	-0.051	-0.028 -0.033		1220 1230	-2.133 -2.133	-2.2 -2.2	0.125 0.125	-9.375 -9.375	-9.763 -9.763
1230	-38.87	-14.997	0.094	-0.056	-0.038		1240	-2.102	-2.169	0.125	-9.375	-9.763
1240	-38.964	-14.997	0.094	-0.056	-0.042		1250	-2.102	-2.169	0.125	-9.375	-9.763
1250	-39.027	-15.029	0.094	-0.061	-0.052		1260	-2.07	-2.169	0.125	-9.375	-9.763
1260	-38.964	-15.06	0.094	-0.065	-0.057		1270	-2.07	-2.137	0.125	-9.375	-9.763
1270	-39.058	-15.06	0.094	-0.07	-0.066		1280	-2.07	-2.137	0.125	-9.375	-9.763
1280 1290	-39.058 -38.964	-15.092 -15.092	0.094 0.094	-0.075 -0.084	-0.076 -0.076		1290 1300	-2.039 -2.039	-2.106 -2.106	0.125 0.125	-9.375 -9.375	-9.763 -9.763
1300	-39.027	-15.123	0.094	-0.084	-0.085		1300	-2.005	-2.106	0.125	-9.375	-9.763
1310	-39.027	-15.155	0.094	-0.089	-0.085		1320	-2.007	-2.075	0.125	-9.375	-9.763
1320	-39.027	-15.155	0.109	-0.094	-0.095		1330	-2.007	-2.075	0.125	-9.375	-9.763
1330	-39.058	-15.186	0.109	-0.103	-0.099		1340	-1.976	-2.075	0.125	-9.375	-9.763
1340	-39.09	-15.186	0.109	-0.103	-0.104		1350	-1.976	-2.043	0.125	-9.375	-9.763
1350 1360	-39.121 -39.09	-15.186 -15.217	0.109 0.109	-0.108 -0.112	-0.109 -0.118		1360 1370	-1.976 -1.945	-2.043 -2.043	0.125 0.125	-9.375 -9.375	-9.763 -9.763
1360	-39.121	-15.249	0.109	-0.112	-0.123		1370	-1.945	-2.043	0.125	-9.375	-9.763
1380	-39.121	-15.249	0.109	-0.126	-0.133		1390	-1.913	-2.012	0.109	-9.375	-9.763
1390	-39.184	-15.28	0.109	-0.126	-0.133		1400	-1.913	-1.98	0.109	-9.375	-9.763
1400	-39.184	-15.28	0.109	-0.131	-0.137		1410	-1.913	-1.98	0.125	-9.375	-9.763
1410	-39.247	-15.312	0.109	-0.136	-0.142		1420	-1.882	-1.949	0.109	-9.375	-9.763
1420 1430	-39.278 -39.247	-15.312 -15.343	0.109 0.10 9	-0.136 -0.141	-0.142 -0.147		1430 1440	- 1.882 -1.851	-1.949 -1.949	0.109 0.109	-9.375 -9.375	-9.763 -9.763
1440	-39.215	-15.343	0.109	-0.141	-0.152		1450	-1.851	-1.917	0.109	-9.375	-9.763
1450	-39.309	-15.375	0.109	-0.141	-0.147		1460	-1.851	-1.917	0.109	-9.375	-9.763
1460	-39.309	-15.375	0.109	-0.141	-0.152		1470	-1.819	-1.886	0.109	-9.375	-9.763
1470	-39.278	-15.406	0.109	-0.131	-0.142		1480	-1.819	-1.886	0.109	- 9 .375	-9.763
1480	-39.341	-15.406	0.109	-0.126	-0.133		1490	-1.788	-1.886	0.109	-9.375	-9.763
1490 1500	-39.309 -39.309	-15.406 -15.406	0.125 0.125	-0.122 -0.112	-0.128 -0.118		1500 1510	-1.788 -1.756	-1.854 -1.854	0.109 0.109	-9.375 -9.375	-9.763 -9.763
1510	-39.404	-15.375	0.125	-0.103	-0.114		1520	-1.756	-1.823	0.109	-9.375	-9.763
1520	-39.372	-15.438	0.125	-0.103	-0.109		1530	-1.756	-1.823	0.109	-9.375	-9.763
1530	-39.341	-15.438	0.125	-0.098	-0.104		1540	-1.725	-1.823	0.094	-9.375	-9.763
1540	-39.341	-15.438	0.125	-0.094	-0.099		1550	-1.725	-1.792	0.094	-9.375	-9.763
1550	-39.404	-15.469	0.125	-0.089	-0.09		1560	-1.725	-1.792	0.094	-9.375	-9.763
1560 1570	-39.404 -39.309	-15.469 -15.469	0.125 0.125	-0.079 -0.079	-0.085 -0.085		1570 1580	-1.725 -1.694	-1.792 -1.76	0.109 0.094	-9.375 -9.375	-9.763 -9.763
1580	-39.404	-15.469	0.125	-0.075	-0.08		1590	-1.694	-1.76	0.094	-9.375	-9.763
1590	-39.341	-15.469	0.125	-0.065	-0.071		1600	-1.694	-1.76	0.094	-9.375	-9.763
1600	-39.404	-15.5	0.125	-0.065	-0.071		1610	-1.662	-1.76	0.094	-9.375	-9.763
1610	-39.404	-15.532	0.125	-0.065	-0.066		1620	-1.662	-1.729	0.094	-9.375	-9.763
1620	-39.341	-15.532 -15.532	0.125	-0.061	-0.066		1630	-1.631	-1.729 -1.729	0.094 0.094	-9.375 -9.375	-9.763 -9.763
1630 1640	-39.404 -39.435	-15.532	0.125 0.125	-0.056 -0.051	-0.061 -0.052		1640 1650	-1.631 -1.631	-1.697	0.094	-9.375	-9.763
1650	-39.435	-15.563	0.125	-0.047	-0.047		1660	-1.631	-1.697	0.094	-9.375	-9.763
1660	-39.498	-15.563	0.125	-0.042	-0.047		1670	-1.631	-1.697	0.094	-9.375	-9.763
1670	-39.498	-15.563	0.125	-0.037	-0.038		1680	-1.6	-1.697	0.094	-9.375	-9.763
1680	-39.529	-15.563	0.125	-0.032	-0.033		1690	-1.6	-1.666	0.094	-9.375	-9.763
1690	-39.498	-15.595	0.125	-0.028	-0.028		1700	-1.6	-1.666	0.094	-9.375	-9.763
1700 1710	-39.498 -39.498	-15.595 -15.595	0.141 0.141	-0.018 -0.014	-0.023 -0.019		1710 1720	-1.6 -1.568	-1.666 -1.634	0.094 0.094	-9.375 -9.375	-9.763 -9.763
1720	-39.498	-15.626	0.141	-0.014	-0.019		1720	-1.568	-1.634	0.094	-9.375	-9.763
1730	-39.498	-15.626	0.141	-0.004	-0.004		1740	-1.568	1.634	0.094	-9.375	-9.763
1740	-39.498	-15.626	0.141	0	-0.004		1750	-1.568	-1.634	0.094	-9.375	-9.763
1750	-39.498	-15.626	0.141	0.004	0		1760	-1.537	-1.634	0.094	-9.375	-9.763
1760 1770	-39.529 -39.498	-15.658 -15.658	0.141	0.009	0.004		1770	-1.537	-1.603	0.094	-9.375	-9.763
1780	-39.495 -39.56	-15.658	0.141 0.141	0.014 0.018	0.014 0.014		1780 1790	-1.537 -1.537	-1.603 -1.603	0.094 0.094	-9.375 -9.375	-9.763 -9.763
1790	-39.56	-15.689	0.141	0.023	0.019		1800	-1.505	-1.603	0.094	-9.375	-9.763
1800	-39.56	-15.689	0.141	0.023	0.019		1810	-1.505	-1.572	0.078	-9.375	-9.763
1810	-39.56	-15.689	0.141	0.028	0.023		1820	-1.505	-1.603	0.078	-9.375	-9.763

					I ACTUAL MENTATO YOU TO	UPPER
					knoux 5	
the shall					12 Summon	
1920	-39.592	-15.689	0.4.44	0.000	0.022	1920
1820 1830	-39.655	-15.658	0.141 0.141	0.028 0.037	0.023 0.028	1830
						1840
1840 1850	-39.592 -39.592	-15.721 -15.721	0.141	0.032 0.032	0.023 0.023	1850
1860	-39.592 -39.623		0.141	0.032		1860
		-15.721	0.141		0.023	1870
1870	-39.655	-15.752	0.141	0.032	0.023	1880
1880	-39.592	-15.752	0.141	0.032	0.023	1890
1890	-39.686 -39.655	-15.752	0.141	0.028	0.019	1900
1900 1910	-39.686	-15.783	0.141	0.023	0.014	1910
1910	-39.666	-15.783	0.141	0.023	0.014	1920
		-15.783	0.141	0.018	0.009	1930
1930	-39.717	-15.815	0.141	0.014	0.004	1940
1940	-39.717	-15.815	0.141	0.009	0	1950
1950	-39.655	-15.783	0.141	0.004	0	1960
1960	-39.686	-15.783	0.141	0	-0.009	1970
1970	-39.749	-15.846	0.141	-0.009	-0.014	1980
1980	-39.686	-15.846	0.141	-0.014	-0.023	1990
1990	-39.717	-15.846	0.141	-0.023	-0.028	2000
2000	-39.717	-15.878	0.141	-0.028	-0.038	2010
2010	-39.717	-15.878	0.141	-0.037	-0.042	2020
2020	-39.811	-15.878	0.141	-0.042	-0.047	2030
2030	-39.749	-15.878	0.141	-0.042	-0.047	2040
2040	-39.78	-15.909	0.156	-0.047	-0.057	2050
2050	-39.717	-15.909	0.156	-0.051	-0.052	2060
2060	-39.78	-15.909	0.156	-0.051	-0.052	2070
2070	-39.749	-15.909	0.156	-0.065	-0.066	2080
2080	-39.749	-15.941	0.141	-0.075	-0.066	2090
2090	-39.78	-15.941	0.141	-0.084	-0.08	2100
2100	-39.811	-15.941	0.141	-0.094	-0.08	2110
2110	-39.811	-15. 9 72	0.141	-0.098	-0.085	2120
2120	-39.843	-15.972	0.141	-0.103	-0.09	2130
2130	-39.811	-15.972	0.141	-0.108	-0.09	2140
2140	-39.811	-15.941	0.156	-0.108	-0.09	2150
2150	-39.874	-15.972	0.156	-0.112	-0.095	2160
2160	-39.78	-16,004	0.156	-0.117	-0.095	2170
2170	-39.874	-16.004	0.141	-0.122	-0.095	2180
2180	-39.874	-16.004	0.156	-0.126	-0.099	2190
2190	-39.905	-16.004	0.156	-0.131	-0.095	2200
2200	-39.905	-15.972	0.156	-0.122	-0.095	2210
2210	-39.905	-16.035	0.156	-0.126	-0.095	2220
2220	-39.905	-16.035	0.156	-0.126	-0.099	2230
2230	-39.937	-16.035	0.156	-0.122	-0.085	2240
2240	-39.937	-16.035	0.156	-0.126	-0.085	2250
2250	-39.905	-16.066	0.141	-0.131	-0.085	2260
2260	-39.905	-16.066	0.156	-0.136	-0.08	2270
2270	-39.937	-16.066	0.156	-0.136	-0.076	2280
						0000

				WETEN DECO	
Repert	RMEABLE ZONE		IE AQUIFER	SYSTEM RECC	VERY PHASE
Time (min)		i dan peruhan 199	it fraginger		ST Simerano
1830	-1.505	-1.572	0.078	-9.375	-9.763
1840	-1.505	-1.572	0.094	-9.375	-9.763
1850 1860	-1.505 -1.505	-1.572 -1.572	0.094 0.094	-9.375 -9.375	-9.763 -9.763
1870	-1.505	-1.54	0.109	-9.375	-9.763
1880	-1.474	-1.54	0.109	-9.375	-9.763
1890 1900	-1.474 -1.443	-1.54 -1. 5 4	0.125 0.141	-9.375 -9.375	-9.763 -9.763
1910	-1.443	-1.54	0.156	-9.375	-9.763
1920	-1.443	-1.509	0.172	-9.375	-9.763
1930 1940	-1.443 -1.411	-1.509 -1.509	0.203 0.219	-9.375 -9.375	-9.763 -9.763
1950	-1.411	-1.477	0.235	-9.375	-9.763
1960	-1.411	-1.477	0.266	-9.375	-9.763
1970 1980	-1.411 -1.411	-1.477 -1.477	0.282 0.313	-9.375 -9.375	-9.763 -9.763
1990	-1.411	-1.446	0.345	-9.375	-9.763
2000	-1.38	-1.446	0.36	-9.375	-9.763
2010	-1.38	-1.477	0.392	-9.375	-9.763
2020 2030	-1.38 -1.38	-1.477 -1.446	0.407 0.423	- 9 .375 -9.375	-9.763 -9.763
2040	-1.38	-1.446	0.439	-9.375	-9.763
2050	-1.38	-1.446	0.454	-9.375	-9.763
2060 2070	-1.38 -1.38	-1.446 -1.446	0.47 0.486	-9.375 -9.375	-9.763 -9.763
2080	-1.349	-1.446	0.501	-9.375	-9.763
2090	-1.349	-1.414	0.517	-9.375	-9.763
2100 2110	-1.349 -1,349	-1.414 -1.414	0.517 0.533	-9.375 -9.375	-9.763 -9.763
2110	-1.349	-1.414	0.533	-9.375	-9.763
2130	-1.349	-1.414	0.548	-9.375	-9.763
2140	-1.317	-1.414	0.548	-9.375	-9.763
2150 2160	-1.317 -1.317	-1.383 -1.383	0.564 0.564	-9.375 -9.375	-9.763 -9.763
2170	-1.317	-1.383	0.564	-9.375	-9.763
2180	-1.317	-1.383	0.564	-9.375	-9.763
2190 2200	-1.317 -1.317	-1.383 -1.383	0.58 0.58	-9.375 -9.375	-9.763 -9.763
2210	-1.286	-1.383	0.58	-9.375	-9.763
2220	-1.286	-1.383	0.58	-9.375	-9.763
2230 2240	-1.286 -1.286	-1.383 -1.351	0.596 0.596	-9.375 -9.375	-9.763 -9.763
2250	-1.286	-1.351	0.596	-9.375	-9.763
2260	-1.286	-1.351	0.596	-9.375	-9.763
2270	-1.254	-1.351	0.596	-9.375 0.375	-9.763 -9.763
2280 2290	-1.254 -1.254	-1.351 -1.32	0.611 0.611	-9.375 -9.375	-9.763
2300	-1.254	-1.32	0.611	-9.375	-9.763
2310	-1.254	-1.32	0.611	-9.375	-9.763
2320 2330	-1.254 -1.223	-1.32 -1.32	0.611 0.611	-9.375 -9.375	-9.763 -9.763
2340	-1.223	-1.32	0.611	-9.375	-9.763
2350	-1.223	-1.289	0.611	-9.375	-9.763
2360 2370	-1.223 -1.223	-1.289 -1.289	0.611 0.611	-9.375 -9.375	-9.763 -9.763
2380	-1.223	-1.289	0.611	-9.375	-9.763
2390	-1.192	-1.289	0.611	-9.375	-9.763
2400 2410	-1.192 -1.192	-1.289 -1.289	0.611 0.627	-9.375 -9.375	-9.763 -9.763
2410	-1.192	-1.257	0.627	-9.375	-9.763
2430	-1.192	-1.289	0.611	-9.375	-9.763
2440	-1.192	-1.257	0.627	-9.375	-9.763
2450 2460	-1.192 -1.192	-1.257 -1.257	0.627 0.627	-9.375 -9.375	-9.763 -9.763
2470	-1.192	-1.257	0.627	-9.375	-9.763
2480	-1.192	-1.257	0.627	-9.375	-9.763
2490 2500	-1.16 -1.16	-1.257 -1.257	0.627 0.627	-9.375 -9.375	-9.763 -9.763
2500	-1.16	-1.257	0.627	-9,375 -9,375	-9.763 -9.763
2520	-1,16	-1.226	0.627	-9.375	-9.763
2530 2540	-1.16 -1.16	-1.257 -1.226	0.627	-9.375 -9.375	-9.763 -9.763
2040	-1.16	-1.226	0.627	-9.375	-9.763

UPPER PERMEABLE ZONE (INTERMEDIATE AQUIFER SYSTEM) DRAWDOWN PHASE

amogadi alba adistri dalamini dan sakit inggan Manaziri dan 1995 inggan	input5

UPPER PE	RMEABLE ZONI		re aquifer	SYSTEM) RECO	VERY PHASE
	A BURN SHORE				and the second s
2550	-1.16	-1.226	0.627	-9.375	-9.763
2560 2570	-1.16 -1.16	-1.226 -1.226	0.627 0.627	-9.375 -9.375	-9.763
2580	-1.16	-1.226	0.627	-9.375	-9.763 -9.763
2590	-1. 16	-1.226	0.627	-9.375	-9.763
2600	-1.16	-1.226	0.627	-9.375	-9.763
2610 2620	-1.16 -1.16	-1.226 -1.226	0.627 0.627	-9.375 -9.375	-9.763 -9.763
2630	-1.16	-1.226	0.627	-9.375	-9.763
2640	-1.129	-1.226	0.627	-9.375	-9.763
2650 2660	-1.16 -1.129	-1.226 -1.226	0.627 0.627	-9.375 -9.375	-9.763 -9.763
2670	-1.129	-1.226	0.627	-9.375	-9.763
2680	-1.129	-1.226	0.627	-9.375	-9.763
2690 2700	-1.129	-1.226	0.627	-9.375	-9.763
2700	-1.129 -1.129	-1.194 -1.194	0.627 0.627	-9.375 -9.375	-9.763 -9.763
2720	-1.129	-1.226	0.627	-9.375	-9.763
2730	-1.129	-1.226	0.627	-9.375	-9.763
2740	-1.129	-1.226	0.611	-9.375	-9.763
2750 2760	-1.129 -1.129	-1.194 -1.226	0.627 0.611	-9.375 -9.375	-9.763 -9.763
2770	-1.129	-1.194	0.627	-9.375	-9.763
2780	-1.129	-1.194	0.627	-9.375	-9.763
2790 2800	-1.129	-1.194	0.627	-9.375	-9.763
2810	-1.129 -1.129	-1.194 -1.194	0.627 0.627	-9.375 -9.375	-9.763 -9.763
2820	-1.129	-1.194	0.627	-9.375	-9.763
2830	-1.129	-1. 194	0.611	-9.375	-9.763
2840 2850	-1.129	-1.194	0.627	-9.375	-9.763
2860	-1.129 -1.129	-1.194 -1.194	0.627 0.627	-9.375 -9.375	-9.763 -9.763
2870	-1.129	-1.194	0.627	-9.375	-9.763
2880	-1.098	-1.194	0.611	-9.375	-9.763
2890 2900	-1.098	-1.194	0.627	-9.375	-9.763
2900	-1.098 -1.098	-1.194 -1.163	0.611 0.611	-9.375 -9.375	-9.763 -9.763
2920	-1.098	-1.163	0.611	-9.375	-9.763
2930	-1.098	-1.163	0.611	-9.375	-9.763
2940 2950	-1.098 -1.098	-1.163 -1.163	0.611 0.611	-9.375	-9.763
2960	-1.098	-1.163	0.611	-9.375 -9.375	-9.763 -9.763
2970	-1.098	-1.163	0.611	-9.375	-9.763
2980	-1.098	-1.163	0.611	-9.375	-9.763
2990 3000	-1.098 -1.098	-1.163 -1.163	0.611 0.611	-9.375 -9.375	-9.763 -9.763
3010	-1.098	-1.163	0.611	-9.375	-9.763
3020	-1.066	-1.163	0.611	-9.375	- 9 .763
3030	-1.098	-1.163	0.611	-9.375	-9.763
3040 3050	-1.098 -1.066	-1.163 -1.163	0.596 0.611	-9.375 -9.375	-9.763 -9.763
3060	-1.098	-1.163	0.596	-9.375	-9.763
3070	-1.098	-1.163	0.611	-9.375	-9.763
3080 3090	-1.066 -1.066	-1.163	0.596	-9.375	-9.763
3100	-1.066	-1.163 -1.163	0.596 0.596	-9.375 -9.375	-9.763 -9.763
3110	-1.066	-1.163	0.596	-9.375	-9.763
3120	-1.066	-1.131	0.596	-9.375	-9.763
3130 3140	-1.066 -1.066	-1.163	0.596 0.596	-9.375	-9.763
3150	-1.066	-1.131 -1.131	0.596	-9.375 -9.375	-9.763 -9.763
3160	-1.066	-1.131	0.596	-9.375	-9.763
3170	-1.066	-1.131	0.596	-9.375	-9.763
3180 3190	-1.066 -1.066	-1.131 -1.131	0.595	-9.375	-9.763 9.762
3200	-1.066	-1.131	0.596 0.596	-9.375 -9.375	-9.763 -9.763
3210	-1.066	-1.131	0.596	-9.375	-9.763
3220	-1.066	-1.131	0.596	-9.375	-9.763
3230 3240	-1.066 -1.066	-1.131 -1.131	0.596	-9.375	-9.763 0.763
3240	-1.066	-1.131 -1.131	0.596 0.596	-9.375 -9.375	-9.763 -9.763
3260	-1.066	-1.131	0.596	-9.375	-9.763

UPPER PERMEABLE ZONE	(INTERMEDIATE AQUIFER	SYSTEM) DRAWDOWN PHASE
Someric States and All	ilia cadia ili 2.9 References	12 Lover party 17 Storman

UPPER PER	MEABLE ZON	E (INTERMEDIA)	TE AQUIFER	SYSTEM) RECO	VERY PHASE
Circond	aput 1 27 Logice poleit				6 secol
Alter Street					THE SOLUTION
3270	-1.066	-1.131	0.596	-9.375	-9.763
3280 3290	-1.066 -1.066	-1.131 -1.131	0.596 0.58	-9.375	-9.763
3300	-1.066	-1.131	0.58	-9.375 -9.375	-9.763 -9.763
3310	-1.066	-1.131	0.58	-9.375	-9.763
3320	-1.066	-1.131	0.58	-9.375	-9.763
3330 3340	-1.066 -1.066	-1.131 -1.131	0.58 0.58	-9.375 -9.375	-9.763 -9.763
3350	-1.066	-1.131	0.58	-9.375	-9.763
3360	-1.098	-1.163	0.58	-9.375	-9.763
3370 3380	-1.066 -1.066	-1.131 -1.131	0.58 0.58	-9.375 -9.375	-9.763 -9.763
3390	-1.098	-1.131	0.58	-9.375	-9.763
3400	-1.066	-1.131	0.58	-9.375	-9.763
3410 3420	-1.098	-1.163	0.58	-9.375	-9.763
3420 3430	-1.066 -1.098	-1.163 -1.163	0.58 0.58	-9.375 -9.375	-9.763 -9.763
3440	-1.066	-1.131	0.58	-9.375	-9.763
3450	-1.098	-1.163	0.58	-9.375	-9.763
3460 3470	-1.098	-1.163	0.58	-9.375	-9.763
3480	-1.098 -1.098	-1.163 -1.163	0.58 0.58	-9.375 -9.375	-9.763 -9.763
3490	-1.098	-1.163	0.58	-9.375	-9.763
3500	-1.066	-1.163	0.58	-9.375	-9.763
3510 3520	-1.066 -1.098	-1.163	0.58 0.58	-9.375	-9.763
3530	-1.098	-1.163 -1.163	0.58	-9.375 -9.375	-9.763 -9.763
3540	-1.098	-1.163	0.58	-9.375	-9.763
3550	-1.098	-1.163	0.58	-9.375	-9.763
3560 3570	-1.098 -1.098	-1.163 -1.163	0.58 0.58	-9.375 -9.375	-9.763 -9.763
3580	-1.098	-1.163	0.58	-9.375	-9.763
3590	-1.098	-1.131	0.58	-9.375	-9.763
3600	-1.066	-1.131	0.58	-9.375	-9.763
3610 3620	-1.098 -1.098	-1.163 -1.131	0.58 0.58	-9.375 -9.375	-9.763 -9.763
3630	-1.098	-1.163	0.58	-9.375	-9.763
3640	-1.066	-1.131	0.58	-9.375	-9.763
3650 3660	-1.066 -1.066	-1.131	0.58	-9.375	-9.763
3670	-1.066	-1.131 -1.131	0.58 0.58	-9.375 -9.375	-9.763 -9.763
3680	-1.066	-1.131	0.58	-9.375	-9.763
3690	-1.066	-1.131	0.58	-9.375	-9.763
3700 3710	-1.066 -1.066	-1.131 -1.131	0.58 0.58	-9.375 -9.375	-9.763 -9.763
3720	-1.066	-1.131	0.58	-9.375	-9.763
3730	-1.066	-1.131	0.58	-9.375	-9.763
3740 3750	-1.066	-1.131	0.58	-9.375	-9.763
3750	-1.035 -1.066	-1.131 -1.131	0.58 0.58	-9.375 -9.375	-9.763 -9.763
3770	-1.066	-1.131	0.58	-9.375	-9.763
3780	-1.035	-1.1	0.564	-9.375	-9.763
3790 3800	-1.035 -1.035	-1.131 -1.131	0.58 0.58	-9.375 -9.375	-9.763 -9.763
3810	-1.035	-1.1	0.58	-9.375	-9.763
3820	-1.035	-1.1	0.58	-9.375	-9.763
3830	-1.035	-1.1	0.58	-9.375	-9.763
3840 3850	-1.035 -1.035	-1.1 -1.1	0.58 0.564	-9.375 -9.375	-9.763 -9.763
3860	-1.035	-1.1	0.564	-9.375	-9.763
3870	-1.035	-1.1	0.564	-9.375	-9.763
3880 3890	-1.035 -1.035	-1.1 -1.1	0.564 0.58	-9.375 -9.375	-9.763 -9.763
3900	-1.035	-1.1 -1.1	0.564	-9.375 -9.375	-9.763 - 9 .763
3910	-1.003	-1.1	0.564	-9.375	-9.763
3920	-1.035	-1.068	0.564	-9.375	-9.763
3930 3940	-1.003 -1.003	-1.068 -1.068	0.564 0.564	-9.375 -9.375	-9.763 -9.763
3950	-1.003	-1.068	0.564	-9.375 -9.375	-9.763 -9.763
3960	-1.003	-1.068	0.564	-9.375	-9.763
3970 3960	-1.003 -1.003	-1.068	0.564	-9.375	-9.763 0.763
3300	-1.003	-1.068	0.564	-9.375	-9.763

UPPER PERMEABLE ZONE (INTERMEDIATE AQUIFER SYSTEM) DRAWDOWN PHASE

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UPPER PERMEABLE ZONE (INTERMEDIATE AQUIFER SYSTEM) RECOVERY PHASE	

UPPER PER	MEABLE ZONE			<u>SYSTEM) RECO</u>	All search and and and an a search of the second se
Caping 1	Security 9 Coordina				12 Swamer
	and the second second	CO)	- CB		
3990 4000	-1.003 -1.003	-1.068 -1.068	0.564 0.564	-9.375 -9.375	-9.763 -9.763
4010	-1.003	-1.068	0.564	-9.375	-9.763
4020	-1.003	-1.068	0.564	-9.375	-9.763
4030 4040	-1.003 -1.003	-1.068 -1.068	0.564 0.564	-9.375 -9.375	-9.763 -9.763
4050	-0.972	-1.068	0.564	-9.375	-9.763
4060 4070	-0.972 -1.003	-1.037 -1.068	0.564 0.564	-9.375 -9.375	-9.763
4050	-0.972	-1.068	0.564	-9.375	-9.763 -9.763
4090	-1.003	-1.068	0.548	-9.375	-9.763
4100 4110	-1.003 -0.972	-1.037 -1.068	0.548 0.548	-9.375 -9.375	-9.763 -9.763
4120	-0.972	-1.068	0.548	-9.375	-9.763
4130	-0.972	-1.037	0.548	-9.375	-9.763
4140 4150	-0.972 -0.972	-1.068 -1.037	0.548 0.548	-9.375 -9.375	-9.763 -9.763
4160	-0.972	-1.068	0.548	-9.375	-9.763
4170 4180	-1.003 -1.003	-1.068 -1.037	0.548 0.548	-9.375 -9.375	-9.763 -9.763
4190	-0.972	-1.068	0.548	-9.375	-9.763
4200	-0.972	-1.037	0.548	-9.375	-9.763
4210 4220	-0.972 -0.972	-1.068 -1.037	0.548 0.533	-9.375 -9.375	-9.763 -9.763
4230	-0.972	-1.068	0.533	-9.375	-9.763
4240	-0.972	-1.037	0.548	-9.375	-9.763
4250 4260	-0.972 -0.972	-1.037 -1.037	0.533 0.533	-9.375 -9.375	-9.763 -9.763
4270	-0.972	-1.037	0.533	-9.375	-9.763
4280	-0.972	-1.037	0.533	-9.375	-9.763
4290 4300	-0.972 -0.972	-1.037 -1.037	0.533 0.533	-9.375 -9.375	-9.763 -9.763
4310	-0.972	-1.037	0.533	-9.375	-9.763
4320 4330	-0.972 -0.972	-1.037 -1.037	0.533 0.533	-9.375 -9.375	-9.763 -9.763
4340	-0.972	-1.037	0.533	-9.375	-9.763
4350	-0.972	-1.037	0.533	-9.375	-9.763
4360 4370	-0.972 -0.972	-1.037 -1.037	0.533 0.533	-9.375 -9.375	-9.763 -9.763
4380	-0.941	-1.037	0.533	-9.375	-9.763
4390	-0.972	-1.037	0.517	-9.375	-9.763
4400 4410	-0.941 -0.941	-1.037 -1.037	0.517 0.517	-9.375 -9.375	-9.763 -9.763
4420	-0.941	-1.037	0.517	-9.375	-9.763
4430 4440	-0.941 -0.941	-1.006 -1.006	0.517 0. 5 17	-9.375 -9.375	-9.763 -9.763
4450	-0.941	-1.006	0.517	-9.375	-9.763
4460	-0.941	-1.006	0.517	-9.375	-9.763
4470 4480	-0.941 -0.941	-1.006 -1.006	0.517 0.517	-9.375 -9.375	-9.763 -9.763
4490	-0.941	-1.006	0.517	-9.375	-9.763
4500	-0.941	-1.006	0.501	-9.375	-9.763
4510 4520	-0.941 -0.941	-1.006 -1.006	0.501 0.501	-9.375 -9.375	-9.763 -9.763
4530	-0.941	-1.006	0.501	-9.375	-9.763
4540 4550	-0.941 -0.941	-1.006 -1.006	0.501 0.501	-9.375 -9.375	-9.763 -9.763
4560	-0.941	-1.006	0.501	-9.375	-9.763
4570	-0.941	-1.006	0.501	-9.375	-9.763
4580 4590	-0.941 -0.909	-1.006 -1.006	0.501 0.501	-9.375 -9.375	-9.763 -9.763
4600	-0.941	-1.006	0.501	-9.375	-9.763
4610	-0.909	-1.006	0.501	-9.375	-9.763
4620 4630	-0.941 -0.909	-0.974 -0.974	0.501 0.501	-9,375 -9,375	-9.763 -9.763
4640	-0.909	-0.974	0.501	-9,375	-9.763
4650 4660	-0.909	-0.974 -0.974	0.501	-9.375 0.375	-9.763 8.763
4660 4670	-0.909 -0.909	-0.974 -0.974	0.486 0.486	-9.375 -9.375	-9.763 -9.763
4680	-0.909	-0.974	0.486	-9.375	-9.763
4690 4700	-0.909 -0.909	-0.974 -0.974	0.486 0.501	-9.375 -9.375	-9.763 -9.763
4,00	-0.500	-0.014	0.001	-9.570	-0.100

UPPER PERMEABLE ZONE	(INTERMEDIATE AQUIFER S)	YSTEM) DRAWDOWN PHASE

Converted in Second and the second of the	84.00
The low Charles of Control of Control of Control (Vilore parts - 2) Super	
in this provide the first set is the instant set in the set of the set of the density of the set of the set of the	

UPPER PER		(INTERMEDIA)		SYSTEN) RECO	2507EDCC.NullrungebroWegestatere
Terrer Dorden	Boost C.				ST Buenren
4710	-0.909	-0.974	0.486	-9.375	-9.763
4720	-0.909	-0.974	0.486	-9.375	-9.763
4730	-0.909	-0.974	0.486	-9.375	-9 763
4740	-0.909	-0.974	0.486	-9.375	-9.763
4750	-0.909	-0.974	0.486	-9.375	-9.763
4760	-0.909	-0.974	0.486	-9.375	-9.763
4770	-0.909	-0.974	0.486	-9.375	-9.763
4780	-0.909	-0.974	0.486	-9.375	-9.763
4790 4800	-0,909 -0,909	-0.974	0.486 0.486	-9.375 -9.375	-9.763
4810	-0,909	-0.974 -0.974	0.486	-9.375	-9.763 -9.763
4820	-0,909	-0.943	0.486	-9.375	-9.763
4830	-0.878	-0.943	0.486	-9.375	-9.763
4840	-0.878	-0.974	0.486	-9.375	-9.763
4850	-0.878	-0.943	0.486	-9.375	-9.763
4860	-0.878	-0.943	0.486	-9.375	-9.763
4870	-0.878	-0.943	0.486	-9.375	-9.763
4880	-0.878	-0.974	0.486	-9.375	-9.763
4890	-0.878	-0.943	0.486	-9.375	-9.763
4900	-0.878	-0.943	0.486	-9.375	-9.763
4910	-0.878	-0.943	0.486	-9.375	-9.763
4920	-0.878	-0.943	0.486	-9.375	-9.763
4930	-0.878	-0.943	0.486	-9.375	-9.763
4940	-0.878	-0.943	0.486	-9.375	-9.763
4950	-0.878	-0.943	0.486	-9.375	-9.763
4960	-0.878	-0.943	0.486	-9.375	-9.763
4970	-0.878	-0.943	0.496	-9.375	-9.763
4980	-0.878	-0.943	0.486	-9.375	-9.763
4990	-0.878	-0.943	0.486	-9.375	-9.763
5000	-0.878	-0.943	0.486	-9.375	-9.763
5010	-0.878	-0.943	0.486	-9.375	-9.763
5020	-0.878	-0.943	0.486	-9.375	-9.763
5030	-0.878	-0.943	0.486	-9.375	-9.763
5040 5050	-0.878 -0.878	-0.911 -0.943	0.486 0.486	-9.375 -9.375	-9.763 -9.763
5060	-0.847	-0.911	0.486	-9.375	-9.763
5070	-0.847	-0.911	0.486	-9.375	-9.763
5080	-0.847	-0.943	0.486	-9.375	-9.763
5090	-0.847	-0.911	0.486	-9.375	-9.763
5100	-0.847	-0.911	0.47	-9.375	-9.763
5110	-0.847	-0.911	0.486	-9.375	-9.763
5120	-0.847	-0.911	0.47	-9.375	-9.763
5130	-0.847	-0.911	0.486	-9.375	-9.763
5140	-0.847	-0.911	0.486	-9.375	-9.763
5150	-0.847	-0.911	0.47	-9.375	-9.763
5160	-0.847	-0.911	0.486	-9.375	-9.763
5170	-0.847	-0.911	0.486	-9.375	-9.763
5180	-0.847	-0.911	0.47	-9.375	-9.763
5190	-0.647	-0.911	0.486	-9.375	-9.763
5200	-0.847	-0.911	0.47	-9.375	-9.763
5210	-0.847	-0.911	0.47	-9.375	-9.763
5220	-0.847	-0.911	0.47	-9.375	-9.763
5230	-0.847	-0.911	0.47	-9.375	-9.763
5240	-0.815	-0.88	0.47	-9.375	-9.763
5250	-0.815	-0.88	0.486	-9.375	-9.763
5260 5270	-0.815	-0.88	0.47	-9,375	-9.763
5270 5290	-0.815	-0.911	0.47	-9.375	-9.763
5280	-0.815	-0.88	0.47	-9,375	-9.763

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UPPER PERMEABLE ZONE (INTERMEDIATE AQUIFER SYSTEM) DRAWDOWN PHASE

Connection and the second seco	NZ LONG PAR	Prote 5 12" Suenense

UPPER PERMEABLE ZONE (INTERMEDIATE AQUIFER SYSTEM) RI	ECOVERY PHASE

Cirpent				SYSTEM) RECO	inges 5
Time Bring				12 10 10 10 10	12 Sentities
5430	-0.784	-0.848	0.47	-9.375	-9.763
5440	-0.784	-0.848	0.47	-9.375	-9.763
5450	-0.784	-0.848	0.47	-9.375	-9.763
5460 5470	-0.784 -0.784	-0.848 -0.848	0.47 0.47	-9.375 -9.375	-9.763 -9.763
5480	-0.784	-0.848	0.454	-9.375	-9.763
5490	-0.784	-0.848	0.454	-9.375	-9.763
5500	-0.784	-0.848	0.454	-9.375	-9.763
5510 5520	-0.784 -0.784	-0.848 -0.848	0.454 0.454	-9.375 -9.375	-9.763 -9.763
5530	-0.784	-0.848	0.454	-9.375	-9.763
5540	-0.784	-0.848	0.454	-9.375	-9.763
5550	-0.784	-0.848	0.454	-9.375	-9.763
5560 5570	-0.784	-0.848	0.454	-9.375	-9.763
5570	-0.784 -0.784	-0.848 -0.848	0.454 0.454	-9.375 -9.375	-9.763 -9.763
5590	-0.784	-0.848	0.454	-9.375	-9.763
5600	-0,784	-0.848	0.454	-9.375	-9.763
5610	-0.784	-0.848	0.454	-9.375	-9.763
5620 5630	-0,784 -0,784	-0.848 -0.848	0.454 0.454	-9.375 -9.375	-9.763
5640	-0.784	-0.848	0.454	-9.375	-9.763 -9.763
5650	-0.784	-0.848	0.454	-9.375	-9.763
5660	-0.784	-0.848	0.454	-9.375	-9.763
5670	-0,784	-0.848	0.439	-9.375	-9.763
5680 5690	-0.784 -0.784	-0.848 -0.848	0.439 0.439	-9.375 -9.375	-9.763 -9.763
5700	-0.784	-0.848	0.439	-9.375	-9.763
5710	-0.784	-0.848	0.439	-9.375	-9.763
5720	-0.784	-0.848	0.439	-9.375	-9.763
5730 5740	-0.784 -0.752	-0.848 -0.848	0.439 0.439	-9.375 -9.375	-9.763 -9.763
5750	-0.752	-0.817	0.439	-9.375	-9.763
5760	-0.752	-0.817	0.439	-9.375	-9.763
577 0	-0.752	-0.817	0.439	-9.375	-9.763
5780	-0.752	-0.817	0.439	-9.375	-9.763
5790 5800	-0.752 -0.752	-0.817 -0.817	0.439 0.439	-9.375 -9.375	-9.763 -9.763
5810	-0.752	-0.817	0.439	-9.375	-9.763
5820	-0.752	-0.817	0.439	-9.375	-9.763
5830	-0.752	-0.817	0.439	-9.375	-9.763
5840 5850	-0.752 -0.752	-0.817 -0.817	0.423 0.423	-9.375 -9.375	-9.763 -9.763
5860	-0.752	-0.817	0.423	-9.375	-9.763
5870	-0.752	-0.817	0.423	-9.375	-9.763
5880	-0.752	-0.817	0.423	-9.375	-9.763
5890	-0.752	-0.817	0.423	-9.375	-9.763
5900 5910	-0.752 -0.752	-0.817 -0.817	0.423 0.423	-9.375 -9.375	-9.763 -9.763
5920	-0.752	-0.817	0.423	-9.375	-9.763
5930	-0.752	-0.817	0.423	-9.375	-9.763
5940	-0.752	-0.817	0.423	-9.375	-9.763
5950 5960	-0.752 -0.721	-0.817 -0.786	0.423 0.407	-9.375 -9.375	-9.763 - 9 .763
5970	-0.752	-0.817	0.423	-9.375	-9.763
5980	-0.721	-0.817	0.407	-9.375	-9.763
5990	-0.721	-0.786	0.407	-9.375	-9.763
6000 6010	-0.721 -0.721	-0.786 -0.786	0.407 0.407	-9.375 -9.375	-9.763 -9.763
6020	-0.721	-0.786	0.407	-9.375	-9.763
6030	-0.752	-0.786	0.407	-9,375	-9.763
6040	-0.721	-0.7 86	0.407	-9.375	-9.763
6050	-0.721	-0.786	0.407	-9,375	-9.763
6060 6070	-0.721 -0.721	-0.786 -0.786	0.407 0.407	-9.375 -9.375	-9.763 -9.763
6080	-0.721	-0.786	0.407	-9,375	-9.763
6090	-0.721	-0.786	0.407	-9.375	-9.763
6100	-0.721	-0.786	0.407	-9.375	-9.763
6110 6120	-0.721 -0.721	-0.786 -0.786	0.407 0.407	-9.375 -9.375	-9.763 -9.763
6130	-0.721	-0.786	0.407	-9.375 -9.375	-9.763 -9.763
6140	-0.721	-0.786	0.407	-9.375	-9.763

	EM) DRAWDOWN PHASE
Street (1997) . Steel 1. Store .	1945 - Hours
	Charles (15) Science (1998)

UPPER PE	RMEABLE ZONE		TE AQUIFER :	SYSTEM) RECO	VERY PHASE
Transmiss Three Spoight					Constanting of the second s
6150	-0.721	-0.786	0.407	-9.375	-9.763
6160 6170	-0.721	-0.786 -0.786	0.407	-9.375	-9,763
6170 6180	-0.721 -0.721	-0.786	0.407 0.392	-9.375 -9.375	-9.763 -9.763
6190	-0.721	-0.786	0.407	-9.375	-9,763
6200	-0.721	-0.786	0.407	-9.375	-9.763
6210	-0.721	-0.786	0.392	-9.375	-9,763
6220	-0.721	-0.786	0.392	-9.375	-9.763
6230	-0.721	-0.786	0.392	-9.375	-9,763
6240 6250	-0.721 -0.721	~0.786 -0.786	0.392	-9.375	-9,763 -9,763
6260	-0.721	-0.786	0.392	-9.375 -9.375	-9.763
6270	-0.721	-0.786	0.392	-9.375	-9.763
6280	-0.721	-0.786	0.392	-9.375	-9.763
6290	-0.721	-0.786	0.392	-9.375	-9.763
6300	-0.721	-0.786	0.392	-9.375	-9.763
6310	-0.721	-0.786	0.392	-9.375	-9.763 0.763
6320 6330	-0.721 -0.721	-0.786 -0.754	0.392 0.392	-9.375 -9.375	-9.763 -9.763
6340	-0.721	-0.786	0.392	-9.375	-9.763
6350	-0.721	-0.754	0.392	-9.375	-9.763
6360	-0.721	-0.754	0.392	-9.375	-9.763
6370	-0.721	-0.786	0.392	-9.375	-9.763
6380	-0.69	-0.754	0.392	-9.375	-9.763
6390	-0.721	-0.754	0.392	-9.375	-9.763
6400 6410	-0.69 -0.721	-0.754 -0.754	0.392 0.392	-9.375 -9.375	-9,763 -9,763
6420	-0.69	-0.754	0.392	-9.375	-9.763
6430	-0.69	-0.786	0.392	-9.375	-9.763
6440	-0.69	-0.754	0.392	-9.375	-9.763
6450	-0.69	-0.754	0.392	-9.375	-9.763
6460	-0.69	-0.754	0.392	-9.375	-9.763
6470	-0.69	-0.754	0.392	-9.375	-9.763
6480 6490	-0.69 -0.69	-0.754 -0.754	0.392 0.392	-9.375 -9.375	-9.763 -9.763
6500	-0.69	-0.754	0.392	-9.375	-9.763
6510	-0.69	-0.754	0.392	-9.375	-9.763
6520	-0.69	-0.754	0.392	-9.375	-9.763
6530	-0.69	-0.754	0.392	-9.375	-9.763
6540	-0.69	-0.754	0.392	-9.375	-9.763
6550 6560	-0.69 -0.69	-0.754 -0.754	0.392 0.392	-9.375 -9.375	-9.763 -9.763
6570	-0.69	-0.754	0.392	-9.375	-9.763
6580	-0.69	-0.754	0.392	-9.375	-9.763
6590	-0.658	-0.754	0.392	-9.375	-9.763
6600	-0.658	-0.754	0.392	-9.375	-9.763
6610	-0.658	-0.723	0.392	-9.375	-9.763
6620 6630	-0.658 -0.658	-0.723 -0.723	0.392 0.392	-9.375 -9.375	-9.763 -9.763
6640	-0.658	-0.723	0.392	-9.375	-9.763
6650	-0.658	-0.723	0.392	-9.375	-9.763
6660	-0.658	-0.723	0.392	-9.375	-9.763
6670	-0.658	-0.723	0.392	-9.375	-9.763
6680	-0.658	-0.723	0.392	-9.375	-9.763
6690	-0.658	-0.723	0.392	-9.375	-9.763 -9.763
6700 6710	-0.658 -0.658	-0.723 -0.723	0.392 0.392	-9.375 -9.375	-9.763
6720	-0.627	-0.723	0.392	-9.375	-9.763
6730	-0.627	-0.691	0.392	-9.375	-9.763
6740	-0.658	-0.691	0.392	-9.375	-9.763
6750	-0.627	-0.691	0.392	-9.375	-9.763
6760	-0.658	-0.691	0.392	-9.375	-9.763
6770 6790	-0.627	-0.691	0.392	-9.375	-9.763 0.763
6780 6790	-0.627 -0.627	-0.691 -0.691	0.392 0.376	-9.375 -9.375	-9.763 -9.763
6800	-0.627	-0.691	0.376	-9.375 -9.375	-9.763
6810	-0.627	-0.691	0.376	-9.375	-9.763
6820	-0.627	-0.691	0.376	-9.375	-9.763
6830	-0.627	-0.691	0.376	-9.375	-9.763
6840	-0.627	-0.691	0.376	-9.375	-9.763
6850	-0.627	-0.691	0.376	-9.375	-9.763
6860	-0.627	-0.691	0.376	-9.375	-9.763

UPPER PERMEABLE ZONE (INTI	ERMEDIATE AQUIFER SYSTEM) DRAWDOWN PHASE
Constant Constant State		na raid 6 Wom (2 Summe)

UPPER PERMEABLE ZONE (INTERMEDIATE AQUIFER SYSTEM) RECOVERY P	HASE

				SYSTEM RECC	
Elevend	10040	acced 2			Input 6
Time limbo			Restaure and	h fi mnel og i	tiz Summer
	DAMENTED ST	Rollins, Aberra	and catter		
6870	-0.627	-0.691	0.392	-9.375	-9.763
6880	-0.627	-0.66	0.376	-9.375	-9.763
6890	-0.627	-0.691	0.376	-9.375	-9.763
6900	-0.627	-0.691	0.376	-9.375	-9.763
6910	-0.627	-0.691	0.376	-9.375	-9.763
6920	-0.596	-0.691	0.376	-9.375	-9.763
6930	-0.596	-0.66	0.376	-9.375	-9.763
6940	-0.596	-0.66	0.376	-9.375	-9.763
6950	-0.596	-0.66	0.376	-9.375	-9.763
6960	-0.596	-0.66	0.376	-9.375	-9.763
6970	-0.596	-0.66	0.376	-9.375	-9.763
6980	-0.596	-0.66	0.376	-9.375	-9.763
6990	-0.596	-0.66	0.376	-9.375	-9.763
7000	-0.596	-0.66	0.376	-9.375	-9.763
7010	-0.596	-0.66	0.376	-9.375	-9.763
7020	-0.596	-0.66	0.376	-9.375	-9.763
7030	-0.596	-0.66	0.376	-9.375	-9.763
7040	-0.596	-0.66	0.36	-9.375	-9.763
7050	-0.596	-0.66	0.376	-9.375	-9.763
7060	-0.596	-0.66	0.36	-9.375	-9.763
7070	-0.596	-0.66	0.36	-9.375	-9.763
7080	-0.596	-0.66	0.376	-9.375	-9.763
7090	-0.5 96	-0.66	0.36	-9.375	-9.763
7100	-0.596	-0.66	0.36	-9.375	-9.763
7110	-0.596	-0.66	0.36	-9.375	-9.763
7120	-0.596	-0.66	0.36	-9.375	-9.763
7130	-0.596	-0.66	0.36	-9.375	-9.763
7140	-0.596	~0.66	0.36	-9.375	-9.763
7150	-0.596	-0.66	0.36	-9.375	-9.763
7160	-0.596	-0.66	0.36	-9.375	-9.763
7170	-0.596	-0.66	0.36	-9.375	-9,763
7180	-0.564	-0.66	0.36	-9.375	-9.763
7190	-0.596	-0.66	0.36	-9.375	-9.763
7200	-0.596	-0.691	0.36	-9.375	-9.763
7210	-0.596	-0.66	0.36	-9.375	-9.763
7220	-0.627	-0.691	0.345	-9.375	-9.763

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APPENDIX C

Data Logger Water Level Measurements for Lower Permeable Zone (IAS) APT.

SE2000	lint-c.wpd
Environmental Logger	
04/02 10:48	
Unit# 577 Test 0	
Setups: INPUT 1 INPUT 2 INPUT 3 INPUT 4 INPUT	5
Type Level (F) Level (F) Level (F) Level (F)	
Mode Surface Surface Surface Surface	
I.D. 100 15 15 15 15	
Reference 0.000 0.000 0.000 0.000 0.000	
PSI at Ref. 19.409 6.662 2.507 1.812 11.237	
SG 1.000 1.000 1.000 1.000 1.000	
Linearity 0.144 0.073 0.081 0.147 0.110	
Scale factor 99.286 14.989 15.012 14.930 15.035	
Offset -0.222 0.034 -0.016 0.116 -0.026	
Delay mSEC 50.000 50.000 50.000 50.000 50.000	
Step 0 04/02 09:43:06	
I OMER DEDMEARLE ZONE (IAO) ANT REAMENING MAL BUA	~=

				3.002-2- 7.000-25	
0	0.062	0.004	0.009	0.009	TAXABLE IN CONTRACTOR
0.0083	0	0.004	0.009	0.009	0.6
0.0166	0.031	0	0.009	0.009	0.0
0.025	0.031	0.004	0.009	0.009	0.
0.0333	0.156	0.004	0.009	0.009	0.0
0.0416	0.156	0.004	0.009	0.009	0.0
0.05	0.125	0.004	0.009	0.009	C
0.0583	0.062	0.004	0.009	0.009	0.0
0.0666	0	0.004	0.004	0.009	0.0
0.075	0.031	0.004	0.009	0.009	0.
0.0833	0.125	0.004	0.004	0.009	0.0
0.0916	-4.721	0.004	0.004	0.009	0.0
0.1	-2.814	0.004	0.004	0.009	(
0.1083	-4.158	0	0.009	0.009	0.1
0.1166	-3.689	0.004	0.009	0.009	0.1
0.125	-2.501	0.004	0.009	0.009	0.
0.1333	-1.876	0.004	0.009	0.009	0.1
0.1416	-1.313	0	0.009	0.009	0.1
0.15	-1.25	0	0.004	0.009	0
0.1583	-1.188	0.004	0.004	0.009	0,1
0.1666	-1.313	0	0.004	0.009	0.1
0.175	-1.282	0.004	0.004	0.009	0.
0.1833	-1.344	0	0	0.004	0.1
0.1916	-1.25	0.004	0	0.009	0.1
0.2	-1.219	0	0	0.009	(
0.2083	-1.156	0	0	0.009	0.:
0.2166	-1.25	0.004	-0.004	0.009	0.2
0.225	-1.063	0	-0.004	0.004	0.
0.2333	-1.219	0.004	-0.004	0.004	0.3
0.2416	-1.156	0	-0.004	0.009	0.3
0.25	-1.125	0.004	-0.009	0.009	0
0.2583	-25.23	0.004	-0.009	0.009	0.2
0.2666	-14.069	0.004	-0.014	0.009	0.2
0.275	-11.412	0.004	-0.014	0.009	0.
0.2833	-12.631	0.004	-0.018	0.004	0.2
0.2916	-12.412	0.004	-0.014	0.004	0.2
0.3	-11.818	0	-0.018	0.009	(
0.3083	-12.287	0	-0.018	0.009	0.3
0.3166	-12.944	0.004	-0.018	0.004	0.3
0.325	-13.319	0.004	-0.023	0.009	0.
0.3333	-13.444	0.004	-0.033	0.009	0.3

SE2000
Environmental Logger
05/05 07:49
Unit# 577 Test 0
Setups: INPUT 1 INPUT 2 INPUT 3 INPUT 4 INPUT 5
Type Level (F) Level (F) Level (F) Level (F) Level (F)
Mode Surface Surface Surface Surface Surface
I.D. 100 15 15 15 15
Reference 0.000 0.000 0.000 0.000 0.000
PSI at Ref. 32.777 6.360 2.496 1.669 11.065
SG 1.000 1.000 1.000 1.000 1.000
Linearity 0.144 0.073 0.081 0.147 0.110
Scale factor 99.286 14.989 15.012 14.930 15.035
Offset -0.222 0.034 -0.016 0.116 -0.026
Delay mSEC 50.000 50.000 50.000 50.000 50.000
Step 1 04/03 06:32:01

LOWER PERMEABLE ZONE (IAS) RECOVERY PHASE

				Si Angelani Si Angelani
		e og skop forsa fille Franklig dansk og ska		Laure - Carl
0	-18.915	-0.146	-1.902	-0.146
0.0083	-18.884	-0.146	-1.902	-0.146
0.0166	-16.602	-0.146	-1.902	-0.146
0.025	-16.383	-0.146	-1.902	-0.146
0.0333	-15.508	-0.146	-1.902	-0.146
0.0416	-13.945	-0.146	-1.902	-0.146
0.05	-12.475	-0.146	-1.902	-0.146
0.0583	-11.225	-0.146	-1.907	-0.146
0.0666	-9.568	-0.146	-1.907	-0.146
0.075	-8.755	-0.146	-1.902	-0.146
0.0833	-7.723	-0.146	-1.902	-0.146
0.0916	-5.222	-0.146	-1.907	-0.146
0.1	-1.063	-0.151	-1.902	-0.146
0.1083	23.581	-0.151	-1.902	-0.146
0.1166	-3.252	-0.151	-1.907	-0.146
0.125	-5.816	-0.151	-1.902	-0.146
0.1333	-3.283	-0.146	-1.902	-0.146
0.1416	-2.97	-0.151	-1.902	-0.146
0.15	-4.159	-0.151	-1.898	-0.146
0.1583	-4.409	-0.151	-1.898	-0.146
0.1666	-3.908	-0.151	-1.898	-0.146
0.175	1.657	-0.151	-1.893	-0.146
0.1833	-4.159	-0.151	-1.888	-0.146
0.1916	-1.313	-0.151	-1.888	-0.146
0.2	0.532	-0.151	-1.883	-0.145
0.2083	-2.157	-0.151	-1.883	-0.146
0.2166	-0.438	-0.151	-1.879	-0.146
0.225	-1.751	-0.151	-1.874	-0.146
0.2333	-2.22	-0.151	-1.869	-0.146
0.2416	-2.095	-0.151	-1.864	-0.146
0.25	-2.189	-0.151	-1.864	-0.146
0.2583	-2.72	-0.151	-1.855	-0.146
0.2666	-2.501	-0.151	-1.855	-0.146
0.275	-2.189	-0.151	-1.846	-0.146
0.2833	-2.095	-0.151	-1.846	-0.146
0.2916	-2.032	-0.151	-1.841	-0.146
0.3	-2.22	-0.151	-1.831	-0.146
0.3083	-2.251	-0.151	-1.831	-0.146
0.3166	-2.251	-0.151	-1.822	-0.146
0.325	-2.125	-0.151	-1.817	-0.146
0.3333	-1.939	-0.151	-1.812	-0.146

LOWER PER		(IAS) APT DRAW		F		MEARLE ZONE	(IAS) RECOVER	
			train 9	ingia 4	Berger			
		adhanna an suaraith	10' 999	6" Awan Pk	Time (mo).		and the second second	
				A CONTRACTOR		n an		
0.35	-14,194	0.004	-0.033	0.009	0.35	-1.407	-0.151	-1.803
0.3666	-14.851	0	-0.042	0.009	0.3666	-1.563	-0.151	-1.793
0.3833 0.4	-13.038 -15.945	0.004 0.004	-0.037 -0.066	0.009 0.009	0.3833 0.4	-2.126 -2.251	-0.151 -0.151	-1.784 -1.775
0.4166	-16.133	0	-0.066	0.009	0.4166	-2.231	-0.151	-1.765
0.4333	-16.664	0	-0.075	0.009	0.4333	1.939	-0.151	-1.751
0.45	-16.789	0.004	-0.08	0.009	0.45	0.688	-0.151	-1.741
0.4666	-16.445	0	-0.089	0.009	0.4666	0.469	-0.151	-1.732
0.4833	-16.914	0.004	-0.099	0.009	0.4833	-1.688	-0.151	-1.723
0.5	-16.695	0.004	-0.104	0.009	0.5	-1.376	-0.151	-1.708
0.5166	-16.758	0.004	-0.113	0.009	0.5166	-0.5	-0.151	-1.694
0.5333 0.55	-16.258	0.004	-0.123	0.009	0.5333	-1.563	-0.155	-1.689
0.55	-16.414 -15.007	0.004 0.004	-0.137 -0.137	0.014 0.014	0.55 0.5666	-1.657 -0.969	-0.151 -0.151	-1.675 -1.661
0.5883	-13.007	0.004	-0.157 -0.151	0.009	0.5833	-0.969 -0.563	-0.151	-1.652
0.6	-12.694	0.004	-0.16	0.009	0.5555	-0.875	-0.155	-1.642
0.6166	-11.537	0.004	-0.165	0.014	0.6166	-1.001	-0.155	-1.633
0.6333	-11.349	0.004	-0.175	0.009	0.6333	-0.875	-0.151	1.618
0.65	-10.005	0	-0.184	0.009	0.65	-0.625	-0.155	-1.609
0.6666	-8.817	0.009	-0.189	0.014	0.6666	-0.75	-0.155	-1.6
0.6833	-8.317	0.004	-0.198	0.014	0.6833	-0.875	-0.155	-1.59
0.7	-8.567	0.004	-0.203	0.014	0.7	-0.719	-0.155	-1.576
0.7166	-8.129	0.004	-0.213	0.014	0.7168	-0.625	-0.155	-1.586
0.7333	-9.724	0.004	-0.222	0.014	0.7333	-0.719	-0.155	-1.557
0.75	-10.755	0.004	-0.222 -0.231	0.014 0.014	0.75 0.7666	-0.719	-0.155	-1.547 -1.538
0.7666 0.7833	-11.756 -12.068	0.009 0.004	-0.231 -0.231	0.014	0.7833	-0.657 -0.594	-0.155 -0.165	-1.538
0.8	-12.537	0.004	-0.231	0.014	0.8	-0.657	-0.155	-1.519
0.8166	-13.382	0.009	-0.246	0.014	0.8166	-0.625	-0.155	-1.51
0.8333	-11.506	0.004	-0.246	0.014	0.8333	-0.594	-0.155	-1.505
0.85	-11.349	0.004	-0.255	0.014	0.85	-0.5	-0.155	-1.491
0.8666	-9,442	0.004	-0.26	0.009	0.8666	0.5	-0.155	-1. 485
0.8833	-5.034	0.004	-0.265	0.009	0.8833	-0.313	-0.155	-1.47 5
0.9	13.884	0.004	-0.269	0.014	0.9	-2.533	-0.155	-1.467
0.9166	-6 .878	0.004	-0.274	0.009	0.9166	-1. 344	-0.155	-1.458
0.9333	-16.821	0.009	-0.27 9	0.009	0.9333	-0.438	-0.155	-1.448
0.95	-11.474	0.009	-0.284	0.009	0.95	-0.156	-0.155	-1.443
0.9666	-13.694	0.004	-0.284	0.014 0.009	0.9666 0.9833	-0.531 -0.75	-0.155	-1.434
0.9833 †	-13.006 -13.663	0.004 0.004	-0.288 -0.293	0.009	0.9655	-0.75	-0.155 -0.155	-1.424 -1.415
1.2	-16.758	0.009	-0.295	0.009	1.2	-0.344	-0.155	-1.33
1.4	-17.727	0.009	-0.407	0.014	1.4	-0.281	-0.155	-1.259
1.6	-17.852	0.009	-0.463	0.014	1.6	-0.219	-0.155	-1.207
1.8	-17.977	0.009	-0.511	0.014	1.8	-0.188	-0.155	-1.155
2	-17.79	0.009	-0.563	0.018	2	-0.125	-0.16	-1.117
2.2	-17.758	0.009	-0.605	0.014	2.2	-0.062	-0.155	-1.079
2.4	-18.008	0.009	-0.643	0.014	2.4	-0.062	-0.16	-1.051
2.6	-17.977	0.014	-0.681	0.014	2.6	0	-0.16	-1.022
2.8	-18.071	0.009	-0.71	0.014	2.8	0.438	-0.16	-0.999
3	-18.415 18.301	0.009	-0.738	0.014	3	0.282	-0.16	-0.97
3.2 3.4	-18.321 -18.102	0.009 0.009	-0.766 -0.79	0.014 0.014	3.2 3.4	0.469 0.313	-0.16 -0.16	-0.951 -0.928
3.4	-18.102	0.014	-0.75	0.014	3.4 3.6	0.313	-0.16	-0.928
3.8	-18.509	0.014	-0.833	0.014	3.8	0.375	-0.16	-0.89
4	-18.227	0.014	-0.851	0.014	4	0.375	-0.16	-0.875
4.2	-18.571	0.009	-0.866	0.014	4.2	0.375	-0.16	-0.861
4.4	-18.602	0.014	-0.885	0.014	4.4	0.407	-0.16	-0.847
4.6	-18.259	0.009	-0.908	0.014	4.6	0.407	-0.165	-0.833

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		Field 2	light 2	Imput 4				Second second
	and the second	and the second se	12" Sane	S" Avon Pk		Tiene (min)	and a second second second	
4.8	-18.634	0.009	-0.913	0.009	-	4.8	0.407	-0.165
5	-18.634	0.014	-0.927	0.014		5	0.438	-0.165
5.2	-18.759	0.014	-0.941	0.014		5.2	0.438	-0.165
5.4	-18.571	0.014	-0.951	0.018		5.4	0.438	-0.165
5.6	-18.384	0.014	-0.965	0.014		5.6	0.469	-0.165
5.8	-18.634	0.009	-0.979	0.014		5.8	0.469	-0.165
6	-18.853	0.004	-0.984	0.014		6	0.469	-0.165
6.2	-18.602	0.009	-0.998	0.014		6.2	0.469	-0.165
6.4	-18.821	0.014	-1.008	0.014		6.4	0.5	-0.165
6.6	-18.415	0.014	-1.017	0.014		6.6	0.5	-0.165
6.8	-18,196	0.014	-1.031	0.014				
7	-18.415	0.014	-1.031	0.014		6.8	0.5	-0.165
, 7.2	-18.509	0.014				7	0.5	-0.165
			-1.046	0.014		7.2	0.5	-0.165
7.4	-18.509	0.014	-1.055	0.014		7.4	0.5	-0.165
7.6	-18.602	0.014	-1.064	0.014		7.6	0.688	-0.165
7.8	-18.696	0.014	-1.069	0.014		7.8	0.532	-0.165
8	-18.634	0.009	-1.079	0.014		8	0.532	-0.165
8.2	-19.134	0.009	-1.088	0.014		8.2	0.657	-0.165
8.4	-18.915	0.014	-1.093	0.014		8.4	0.563	-0.17
8.6	-18.602	0.014	-1.098	0.014		8.6	0.5	-0.17
8.8	-18.446	0.014	-1.112	0.014		8.8	0.563	-0.165
9	-19.009	0.014	-1.117	0.014		9	0.563	-0.17
9.2	-19.103	0.014	-1.121	0.014		9.2	0.563	-0.165
9.4	-19.04	0.014	-1.126	0.014		9.4	0.563	-0.17
9.6	-18.79	0.014	-1.135	0.014		9.6	0.594	-0.17
9.8	-18.759	0.014	-1.14	0.014		9.8	0.594	-0.17
10	-18.571	0.014	-1. 145	0.009		10	0.594	-0.17
12	-19.009	0.014	-1.202	0.009		12	0.594	-0.17
14	-18.634	0.014	-1.244	0.009		14	0.625	-0.17
16	-19.259	0.009	-1.273	0.009		16	0.625	-0.174
18	-18.978	0.014	-1.301	0.009		18	0.657	-0.174
20	-19.353	0.014	-1.329	0.009		20	0.688	-0.179
22	-18.946	0.014	-1.344	0.009		22	0.688	-0.179
24	-19.009	0.014	-1.367	0.009		24	0.719	-0.179
26	-19.353	0.014	-1.391	0.014		26	0.782	-0.179
28	-19.321	0.014	-1.405	0.009		28	0.782	-0.179
30	-19.54	0.014	-1.415	0.003		30		
32	-19.54	0.014	-1.415				0.782	-0.184
32 34				0.018		32	0.751	-0.184
	-19.071	0.014	-1.438	0.014		34	0.782	-0.184
36	-19.009	0.014	-1.452	0.014		36	0.782	-0.184
38	-19.572	0.014	-1.471	0.014		38	0.782	-0.184
40	-19.196	0.014	-1.476	0.014		40	0.782	-0.184
42	-19.415	0.014	-1.495	0.014		42	0.782	-0.189
44	-19.572	0.009	-1.495	0.014		44	0.813	-0.189
46 40	-19.572	0.014	-1.505	0.014		46	0.813	-0.189
48	-18.946	0.014	-1.509	0.014		48	0.813	-0.193
50	-19.259	0.014	-1.519	0.014		50	0.813	-0.193
52	-19.353	0.014	-1.528	0.014		52	0.813	-0.193
54	-19.259	0.009	-1.533	0.014		54	0.813	-0.193
56	-19.572	0.014	-1.542	0.018		56	0.844	-0.193
58	-19.728	0.014	-1.547	0.018		58	0.844	-0.193
60	-19.603	0.014	-1.552	0.014		60	0.844	-0.198
62	-19.134	0.014	-1.557	0.018		62	0.844	-0.198
64	-19.478	0.014	-1.561	0.018		64	0.844	-0.198
66	-19.603	0.014	-1.561	0.028		66	0.844	-0.198
68	-19.509	0.014	-1. 56 1	0.028		68	0.844	-0.203
70	-19.447	0.014	-1.571	0.028		70	0.844	-0.203
72	-19.478	0.014	-1.58	0.028		72	0.844	-0.203

LOWER PERMEABLE ZONE (IAS) RECOVERY PHASE

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Time intil		Of Cipper permi	12 604	6" Avon Pk	Time (min	and the second		2.02
74	-19.509	0.014	-1.58	0.028	74	0.844	-0.203	-0.322
76	-19.134	0.014	-1.585	0.028	76	0.876	-0.203	-0.317
78	-19.509	0.014	-1.59	0.032	78	0.876	-0.203	-0.317
80	-19.728	0.014	-1.59	0.032	80	0.876	-0.208	-0.312
82 84	-19.321	0.014	-1.594	0.028	82	0.876	-0.208	-0.308
86	-19.509 -19.103	0.014 0.014	-1.604 -1.604	0.028 0.032	84 86	0.876 0.876	-0.208 -0.208	-0.303 -0.303
88	-19.634	0.014	-1.609	0.032	88	0.876	-0.208	-0.303
90	-19.384	0.014	-1.618	0.028	90	0.876	-0.208	-0.298
92	-19.04	0.014	-1.613	0.032	92	0.876	-0.208	-0.303
94	-19.228	0.014	-1.618	0.032	94	0.876	-0.212	-0.298
96	-19.29	0.014	-1.623	0.032	96	0.876	-0.212	-0.298
98	-19.259	0.018	-1. 628	0.032	98	0.876	-0.212	-0.298
100	-18.978	0.018	-1.628	0.032	100	0.876	-0.212	-0.298
115	-19.384	0.014	-1.646	0.037	115	0.876	-0.217	-0.289
130	-19.196	0.014	-1.665	0.042	130	0.876	-0.222	-0.289
145	-19.634	0.014	-1.665	0.047	145	0.907	-0.231	-0.284
160	-19.29	0.018	-1.67	0.051	160	0.907	-0.236	-0.284
175 190	-19.384 -19.134	0.018 0.018	-1.67 -1.665	0.065 0.07	175 190	0.907 0.907	-0.241 -0.245	-0.274 -0.27
205	-19.29	0.023	-1.67	0.075	205	0.907	-0.25	-0.27
200	-19.353	0.028	-1.68	0.075	203	0.907	-0.255	-0.265
235	-19.103	0.023	-1.675	0.08	235	0.907	-0.255	-0.265
250	-18.978	0.023	-1.68	0.084	250	0.907	-0.26	-0.255
265	-19.54	0.028	-1.689	0.084	265	0.907	-0.26	-0.246
280	-19.228	0.023	-1. 694	0.08	280	0.938	-0.264	-0.246
295	-19.29	0.023	-1.694	0.089	295	0.938	-0.264	-0.237
310	-19.228	0.028	-1.703	0.08	310	0.938	-0.264	-0.227
325	-19.321	0.033	-1.699	0.089	325	0.969	-0.264	-0.222
340	-19.196	0.028	-1.703	0.089	340	0.938	-0.264	-0.213
355	-19.384	0.028	-1.713	0.08	355	0.969	-0.264	-0.203
370 385	-19.54	0.023 0.028	-1.713 -1.727	0.075 0.07	370 385	1.001 1.001	-0.264 -0.264	-0.184 -0.184
400	-19.478 -19.29	0.028	-1.722	0.061	400	1.001	-0.264	-0.184
415	-19.353	0.023	-1.722	0.051	415	1.032	-0.264	-0.17
430	-19.259	0.018	-1.722	0.042	430	1.032	-0.26	-0.156
445	-18.978	0.014	-1.727	0.037	445	1.032	-0.26	-0.132
460	-19.29	0.009	-1.746	0.028	460	1.063	-0.26	-0.118
475	-19.196	0.009	-1.76	0.014	475	1.063	-0.26	-0.109
490	-18.978	0.004	-1.774	0.004	490	1.032	-0.26	-0.137
505	-19.697	0	-1.788	-0.004	505	1.001	-0.26	-0.166
520	-19.04	0	-1.798	-0.009	520	0.969	-0.264	-0.189
535	-18.79	-0.004	-1.812	-0.023	535	0.969	-0.264	-0.203
550	-19.509	-0.009	-1.822	-0.032	550	0.938	-0.269	-0.218
565 580	-18.946 -19.259	-0.009 -0.014	-1.831 -1.84	-0.037 -0.047	565 580	0.938 0.907	-0.264 -0.269	-0.227 -0.241
595	-19.353	-0.014	-1.8 5	-0.047	595	0.907	-0.209	-0.241
610	-19.134	-0.028	-1.864	-0.065	610	0.876	-0.274	-0.284
625	-18.821	-0.033	-1.874	-0.08	625	0.876	-0.279	-0.293
640	-18.915	-0.033	-1.883	-0.084	640	0.876	-0.283	-0.298
655	-19.196	-0.037	-1.888	-0.089	655	0.907	-0.288	-0.274
670	-19.165	-0.042	-1.893	-0.094	670	0.938	-0.293	-0.255
685	-19.04	-0.042	-1.897	-0.098	685	0.938	-0.298	-0.241
700	-18.821	-0.047	-1.902	-0.103	700	0.938	-0.298	-0.237
715	-18.853	-0.052	-1.907	-0.103	715	0.969	-0.302	-0.237
730 745	-19.165	-0.052	-1.907	-0.103	730	0.969	-0.307	-0.232
760	-19.071 -19.196	-0.056 -0.056	-1.911 -1.911	-0.108 -0.103	745 760	0.938 0.938	-0.312 -0.316	-0.237 -0.241
700	-10.100	-0,000	-1.011	-0.100	700	0.890	-0.310	-0.241

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page 4

	RMEABLE ZONE	(IAS) APT DRAV	NDOWN PHAS	E
	1.60 2.060		inperi S	lopat 4
Million of the contract	Heren De Stationer de Stationer		12 604	6" Avon Pk
775	-18.978	-0.056	-1.907	-0.108
790	-18.728	-0.061	-1.907	-0.108
805	-18.602	-0.061	-1.907	-0.108
820	-18.946	-0.066	-1.907	-0.108
835	-19,134	-0.066	-1.902	-0.098
850	-19.353	-0.066	-1.893	-0.094
865	-18, 946	-0.066	-1.888	-0.089
880	-19.478	-0.071	-1.888	-0.089
895	-18,79	-0.071	-1.883	-0.089
910	-18.54	-0.071	-1.883	-0.089
925	-19.384	-0.071	-1.878	-0.084
940	-19,165	-0.071	-1.869	-0.075
955	-19,415	-0.071	-1.864	-0.075
970	-18.665	-0.071	-1.859	-0.07
985	-19.353	-0.075	-1.859	-0.075
1000	-19.259	-0.075	-1.855	-0.065
1015	-18.665	-0.08	-1.85	-0.065
1030	-18.946	-0.085	-1.85	-0.065
1045	-18.915	-0.085	-1.85	-0.065
1060	-18.853	-0.09	-1.845	-0.07
1075	-18.978	~0.09	-1.845	-0.075
1090	-18.853	-0.094	-1.85	-0.075
1105	-18.946	-0.099	-1.845	-0.075
1120	-18.29	-0.104	-1.859	-0.094
1135	-18.946	-0.113	-1.869	-0.103
1150	-19.071	-0.123	-1.878	-0.113
1165	-18.728	-0.123	-1.878	-0.117
1180	-18.446	-0.127	-1.883	-0.122
1195	-19.071	-0.132	-1.888	-0.127
1210	-18.853	-0.137	-1.897	-0.141

Elepted	RMEABLE ZONE	(IAS) RECOVER	S STATE CONTRACTOR OF STATES	tread 4
Time (mo)	12 LONGE Pare			di Ayon Pit
775	0.938	-0.326	-0.246	-0.146
790	0.938	-0.326	-0.251	-0.146
805	0.938	-0.335	-0.255	-0.146
820	0.938	-0.34	-0.265	-0.146
835	0.907	-0.345	-0.274	-0.146
850	0.907	-0.35	-0.279	-0.146
865 880	0.907	-0.354	-0.284 -0.293	-0.146
895	0.907 0.907	-0.359 -0.359	-0.293	-0.146 -0.146
910	0.876	-0.364	-0.298	-0.146
925	0.907	-0.364	-0.289	-0.146
940	0.907	-0.369	-0.284	-0.146
955	0.907	-0.369	-0.284	-0.146
970	0.907	-0.373	-0.279	-0.146
985	0.907	-0.373	-0.274	-0.146
1000	0.938	-0.378	-0.274	-0.146
1015	0.907	-0.378	-0.274	-0.146
1030	0.938	-0.378	-0.265	-0.146
1045	0.938	-0.378	-0.265	-0.146
1060	0.938	-0.383	-0.26	-0.146
1075	0.938	-0.383	-0.255	-0.146
1090	0.938	-0.378	-0.246	-0.146
1105	0.969	-0.378	-0.237	-0.146
1120	0.969	-0.378	-0.232	-0.146
1135 1150	0.969 0.969	-0.378 -0.378	-0.218 -0.218	-0.146 -0.146
1165	0.969	-0.378	-0.208	-0.146
1180	1.001	-0.373	-0.203	-0.146
1195	1.001	-0.373	-0.199	-0.146
1210	1.001	-0.373	-0.194	-0.146
1225	1.001	-0.373	-0.189	-0.146
1240	1.001	-0.373	-0.189	-0.146
1255	1.032	-0.373	-0.18	-0.146
1270	1.001	-0.369	-0.175	-0.146
1285	1.032	-0.373	-0.175	-0.146
1300	1.032	-0.373	-0.175	-0.146
1315	1.032	-0.373	-0.175	-0.146
1330	1.001	-0.373	-0.175	-0.146
1345	1.001	-0.378	-0.184	-0.146
1360	1.001	-0.378	-0.189	-0.146
1375 1390	1.001 1.001	-0.383 -0.388	-0.194 -0.199	-0.146 -0.146
1390	1.001	-0.388	-0.213	-0.146
1420	0.969	-0.392	-0.218	-0.146
1435	0.969	-0.402	-0.232	-0.146
1450	0.938	-0.407	-0.241	-0.146
1465	0.938	-0.407	-0.251	-0.146
1480	0.938	-0.411	-0.255	-0.146
1495	0.938	-0.411	-0.255	-0.146
1510	0.938	-0.416	-0.255	-0.146
1525	0.907	-0.421	-0.27	-0.146
1540	0.876	-0.425	-0.284	-0.146
1555	0.876	-0.425	-0.293	-0.146
1570	0.844	-0.43	-0.303	-0.146
1585	0.844	-0.43	-0.308	-0.146
1600	0.844	-0.44	-0.317	-0.146
1615 1630	0.844 0.782	-0.44 -0.444	-0.322	-0.146 -0.146
1000	U. 102	-0.444	-0.374	-0.140

Encode : Rept : moit 2 - Movi 2 - Input 4 Tene (of) 12 super parts 6 Bouverparts 17 Star 5 Aven Pa					
	intern (8	novi 2 Soni perit	input 3 HZ Stav	input 4 6" Avon Pic

LOWER PER	MEABLE ZON	E (IAS) RECOVER	Y PHASE	
Biggerday		te trèstique	10008	Input 4
Thing (min)	121 Logic Pen	C Supersonn	12 Sun	S. Awan Pk.
4045	0.740			0.140
1645 1660	0.719 0.688	-0.454 -0.459	-0.431 -0.459	-0.146 -0.146
1675	0.657	-0.454	-0.487	-0.146
1690	0.625	-0.459	-0.511	-0.146
1705	0.594	-0.463	-0.53	-0.146
1720	0.625	-0.459	-0.53	-0.146
1735	0.594	-0.454	-0.535	-0.146
1750	0.594	-0.449	-0.53	-0.146
1765 1780	0.594 0.594	-0.444 -0.444	-0.53	-0.146
1795	0.625	-0.444	-0.53 -0.521	-0.146 -0.146
1810	0.625	-0.44	-0.521	-0.146
1825	0.594	-0.44	-0.525	-0.146
1840	0.625	-0.435	-0.521	-0.146
1855	0.625	-0.435	-0.506	-0.146
1870	0.657	-0.435	-0.497	-0.146
1885	0.657	-0.43	-0.478	-0.145
1900	0.688	-0.425	-0.468	-0.146
1915 1930	0.688	-0.425	-0.459	-0.146 -0.146
1930	0.688 0.688	-0.425 -0.421	-0.454 -0.445	-0.146
1960	0.000	-0.421	-0.44	-0.146
1975	0.688	-0.425	-0.44	-0.146
1990	0.688	-0.421	-0.44	-0.146
2005	0.719	-0.421	-0.435	-0.146
2020	0.719	-0.421	-0.431	-0.146
2035	0.751	-0.425	-0.41 6	-0.146
2050	0.751	-0.425	-0.421	-0.146
2065	0.751	-0.425	-0.421	-0.146
2080	0.782	-0.425	-0.388	-0.146 -0.146
2095 2110	0.813 0.844	-0.43 -0.435	-0.355 -0.331	-0.146
2125	0.844	-0.435	-0.317	-0,146
2140	0.876	-0.435	-0.308	-0.146
2155	0.876	-0.44	-0.303	-0.146
2170	0.876	-0.444	-0.308	-0.146
2185	0.87 6	-0.449	-0.308	-0.146
2200	0.876	-0.454	-0.312	-0.146
2215	0.876	-0.459	-0.312	-0.146
2230	0.876	-0.459	-0.322	-0.146
2245 2260	0.844 0.844	-0.4 6 8 -0.473	-0.326 -0.331	-0.146 -0.146
2275	0.844	-0.478	-0.331	-0.146
2290	0.844	-0.482	-0.331	-0.146
2305	0.844	-0.492	-0.336	-0.146
2320	0.844	-0.492	-0.336	-0.146
2335	0.844	-0.497	-0.341	-0.146
2350	0.844	-0.501	-0.341	-0.146
2365	0.844	-0.501	-0.341	-0.146
2380	0.876	-0.506	-0.336	-0.146
2395 2410	0.876 0.844	-0.511 -0.515	-0.336 -0.336	-0.146 -0.146
2410	0.876	-0.515	-0.331	-0.146
2440	0.876	-0.52	-0.326	-0.146
2455	0.876	-0.52	-0.326	-0.146
2470	0.876	-0.525	-0.322	-0.146
2485	0.876	-0.525	-0.317	-0.146
2500	0.907	-0.525	-0.308	-0.146

omoposen. y/27283888983939696365	MEABLE ZONE	(IAS) RECOVER	Y PHASE	
Clapson		100/2		finad 4
Time (min)-	der Lonen Bern			6 Alon Pk
2515	0.907	-0.525	-0.298	-0.146
2530	0.938	-0.53	-0.289	-0.146
2545	0.938	-0.53	-0.279	-0.146
2560	0.938	-0,53	-0.265	-0.146
2575	0.938	-0.53	-0.255	-0.146
2590	0.969	-0.53	-0.246	-0.146
2605 2620	0.969	-0.53	-0.237	-0.146
2620	0.969 1.001	-0.534 -0.534	-0.227 -0.218	-0.146 -0.146
2650	1.001	-0.539	-0.213	-0.146
2665	1.001	-0.539	-0.208	-0.146
2680	1.001	-0.539	-0.199	-0.146
2695	1.032	-0.544	-0.194	-0.145
2710	1.032	-0.549	-0.194	-0.146
2725	1.032	-0.549	-0.189	-0.146
2740	1.032	-0.553	-0.184	-0.146
2755	1.032	-0.553	-0.18	-0.146
2770 2785	1.032 1.032	-0.563 -0.563	-0.18 -0.18	-0.146 -0.146
2800	1.032	-0.568	-0.184	-0.146
2815	1.032	-0.572	-0.189	-0.146
2830	1.032	-0.577	-0.194	-0.146
2845	1.001	-0.587	-0.203	-0.146
2860	1.001	-0.591	-0.208	-0.146
2875	1.001	-0.596	-0.218	-0.146
2890	0.969	-0.601	-0.222	-0.146
2905	0.969	-0.605	-0.232	-0.146
2920 2935	0.969	-0.615	-0.237	-0.146
2950 2950	0.969 0.969	-0.615 -0.62	-0.241 -0.246	-0.146 -0.146
2965	0.938	-0.629	-0.240	-0.146
2980	0.938	-0.634	-0.255	-0.146
2995	0.938	-0.634	-0.26	-0.146
3010	0.938	-0.643	-0.26	-0.146
3025	0.938	-0.643	-0.265	-0.146
3040	0.907	-0.648	-0.27	-0.146
3055	0.907	-0.653	-0.27	-0.146
3070	0.907	-0.658	-0.274	-0.146
3085 3100	0.907 0.907	-0.658 -0.658	-0.274 -0.27	-0.146 -0.146
3115	0.907	-0.658	-0.265	-0.146
3130	0.907	-0.658	-0.265	-0.146
3145	0.907	-0.662	-0.265	-0.146
3160	0.907	-0.667	-0.26	-0.146
3175	0.938	-0.662	-0.251	-0.146
3190	0.938	-0.662	-0.241	-0.146
3205	0.969	-0.658	-0.232	-0.146
3220	0.969	-0.662	-0.222	-0.146
3235	0.969	-0.662	-0.222	-0.146
3250 3265	0.969 0.969	-0.662 -0.662	-0.218 -0.208	-0.146 -0.146
3280	0.969	-0.662	-0.208	-0.146
3295	0.969	-0.662	-0.199	-0.146
3310	1.001	-0.662	-0.184	-0.146
3325	0.969	-0.662	-0.18	-0.146
3340	1.001	-0.653	-0.161	-0.146
3355	1.032	-0.653	-0.151	-0.146
3370	1.032	-0.648	-0.147	-0.146

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and the second second second second	Madding, State States	In the second	Statistics	
Statistic Statistics				
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Conversion and the local division of the loc	and the second second second			State Cale Cale State
	Million and a second state	A STATE OF A		

LOWER PE	RMEABLE ZONE	(IAS) RECOVER	YPHASE	
and the state of the	Fight 1	hde2		
Timin (min)				Staten R.
Contraction in the	- pompad			
3385	1.032	-0.648	-0.132	-0.146
3400	1.063	-0.643	-0.118	-0.146
3415	1.063	-0.643	-0.113	-0.146
3430	1.063	-0.643	-0.104	-0.146
3445	1.063	-0.643	-0.109	-0.146
3460	1.063	-0.648	-0.104	-0.146
3475 3490	1.063 1.063	-0.648 -0.648	-0.099 -0.099	-0.146 -0.146
3505	1.063	-0.648	-0.099	-0.146
3520	1.063	-0.653	-0.104	-0.146
3535	1.063	-0.653	-0.109	-0.146
3550	1.063	-0.658	-0.113	-0.146
3565	1.063	-0.658	-0.118	-0.146
3580	1.063	-0.662	-0.123	-0.146
3595	1.032	-0.662	-0.128	-0.146
3610	1.032	-0.667	-0.132	-0.146
3625	1.032	-0.672	-0.142	-0.146
3640	1.032	-0.677	-0.151	-0.146
3655	1.001	-0.681	-0.161	-0.146
3670	1.001	-0.681	-0.166	-0.146
3685	1.001	-0.686	-0.18	-0.146
3700	0.969	-0.691	-0.189	-0.146
3715	0.969	-0.699	-0.203	-0.146
3730	0.969	-0.699	-0.213	-0.146
3745	0.938	-0.704	-0.222	-0.146
3760	0.938	-0.709	-0.232	-0.146
3775	0.938	-0.709	-0.237	-0.146
3790	0.938	-0.713	-0.246	-0.146
3805	0.938	-0.713	-0.246	-0.146
3820	0.938	-0.713	-0.251	-0.146
3835	0.938	-0.713	-0.251	-0.146
3850	0.938	-0.713	-0.251	-0.146
3865	0.938	-0.713	-0.251	-0.146
3880	0.938	-0.718	-0.251	-0.146
3895	0.938	-0.718	-0.251	-0.146
3910	0.938	-0.713	-0.246	-0.146
3925	0.938	-0.718	-0.241	-0.146
3940	0.938	-0.713	-0.237	-0.146
3955	0.969	-0.713	-0.227	-0.146
3970	0.969	-0.709	-0.222	-0.146
3985	0.969	-0.709	-0.213	-0.146
4000	1.001	-0.709	-0.203	-0.146
4015	1.001	-0.709	-0.199	-0.146
4030	1.001	-0.704	-0.184	-0.146
4045	1.032	-0.704	-0.175	-0.146
4060	1.032	-0.699	-0.166	-0.146
4075	1.032	-0.699	-0.156	-0.146
4090	1.063	-0.699	-0.147	-0.146
4105	1.063	-0.695	-0.137	-0.146
4120	1.063	-0.695	-0.128	-0.146
4135	1.063	-0.695	-0.123	-0.146
4150	1.063	-0.695	-0.118	-0.146
4165	1.095	-0.695	-0.109	-0.146
4180	1.095	-0.695	-0.104	-0.146
4195 4210	1.095 1.095	-0.691	-0.099	-0.146 -0.146
4210 4225		-0.695	-0.104 -0.104	-0.146 -0.146
4225 4240	1.095 1.095	-0.695 -0.699	-0.104 -0.109	-0.146 -0.146
-2-10	1.090	-0.000	-0.108	-0.140

	ALL DES STATEMENT OF A	145075	
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		(IAS) RECOVER	Y PHASE	
Electron	- 4941	Husz -	Statt 3	11244
Time (min)	12" Lunior Point	C Chorrenn	12,818	ST Aven Pk
	PRINCIPAL PRINCI		of the state of the	dia de la constante
4255	1.095	-0.704	-0.109	-0.146
4270	1.095	-0.704	-0.113	-0.146
4285	1.095	-0.709	-0.123	-0.146
4300 4315	1.095 1.063	-0.709 -0.713	-0.128 -0.137	-0.146
4330	1.063	-0.713	-0.137	-0.146 -0.146
4345	1.063	-0.718	-0.142	-0.146
4360	1.063	-0.718	-0.142	-0.146
4375	1.063	-0.718	-0.142	-0.146
4390	1.063	-0.723	-0.142	-0.146
4405	1.032	-0.723	-0.142	-0.146
4420	1.032	-0.723	-0.147	-0.146
4435	1.032	-0.728	-0.151	-0.146
4450	1.032	-0.732	-0.161	-0.146
4465	1.032	-0.732	-0,166	-0.146
4480	1.001	-0.737	-0.18	-0.146
4495	1.001	-0.742	-0.175	-0.146
4510	1.001	-0.742	-0.184	-0.146
4525	1.001	-0.747	-0.194	-0.146
4540	0.969	-0.747	-0.194	-0.146
4555 4570	0.969 0.969	-0.747 -0.747	-0.194 -0.194	-0.146 -0.146
4585	0.969	-0.751	-0.199	-0.146
4600	0.969	-0.751	-0.189	-0.146
4615	0.969	-0.747	-0.184	-0.146
4630	1.001	-0.742	-0.175	-0.146
4645	1.001	-0.742	-0.166	-0.146
4660	1.001	-0.737	-0,161	-0.146
4675	1.032	-0.742	-0.156	-0.146
4690	1.001	-0.742	-0.151	-0.146
4705	1.063	-0.737	-0.132	-0.146
4720	1.032	-0.737	-0.132	-0.146
4735	1.063	-0.732	-0.118	-0.146
4750	1.032	-0.732	-0.113	-0.146
4765	1.063	-0.728	-0.099	-0.146
4780	1.063	-0.728	-0.08	-0.146
4795 4810	1.095 1.095	-0.723 -0.718	-0.066 -0.057	-0.146 -0.146
4825	1.126	-0.713	-0.038	-0.146
4840	1.126	-0.713	-0.024	-0.146
4855	1.126	-0.709	-0.015	-0.146
4870	1.157	-0.709	-0.006	-0.146
4885	1.157	-0.709	0.004	-0.146
4900	1.188	-0.709	0.013	-0.146
4915	1.157	-0.709	0.018	-0.146
4930	1.188	-0.709	0.023	-0.146
4945	1.188	-0.709	0.028	-0.146
4960	1.188	-0.709	0.028	-0.146
4975	1.188	-0.709	0.028	-0.146
4990	1.188	-0.713	0.023	-0.146
5005	1.188	-0.709	0.028	-0.146
5020 5025	1.188	-0.709	0.023	-0.146
5035 5050	1.188	-0.713 -0.713	0.018	-0.146
5050 5065	1.188 1.188	-0.713 -0.713	0.013 0.009	-0.146 -0.146
5085	1.166	-0.713	0.009	-0.146 -0.146
5095	1.157	-0.713	-0.001	-0.146
5110	1.157	-0.713	-0.006	-0.146

Margin and Margin					
BEE States a second a se	and a state of the	AND STREET	the second second second		Contraction of the second
Contraction of the second second					
Bartesicnasii Antos	A CONTRACTOR OF	Anthenin Statistics	The state of the s	Same Minister of States	1. 16 1 C
				The first second second	
	MAX REALES		ment i statute en la	Strate State State	den and the second

White the second s		(IAS) RECOVER	C DOCTORES SAVANA-A-Marine Beneral	
		E Uppercem		intrad 4
Time (min)	and the second states and	C Uppersonn-	12°808	8 Axon Pk
5125	1.157	-0.718	-0.01	-0.146
5140	1.157	-0.723	-0.024	-0.146
5155	1.157	-0.723	-0.033	-0.146
5170	1.126	-0.728	-0.042	-0.146
5185	1.126	-0.728	-0.052	-0.146
5200	1.126	-0.732	-0.066	-0.146
5215	1.095	-0.737	-0.076	-0.146
5230	1.095	-0.742	-0.095	-0.146
5245	1.063	-0.742	-0.099	-0.146
5260	1.063	-0.742	-0.109	-0.146
5275	1.063	-0.742	-0.113	-0.146
5290	1.063	-0.742	-0.113	-0.146
5305	1.063	-0.742	-0.113	-0.146
5320 5335	1.063	-0.737	-0.113	-0.146 -0.146
5350	1.063 1.063	-0.737 -0.732	-0.113 -0.113	-0.146
5365	1.063	-0.737	-0.113	-0.146
5380	1.063	-0.732	-0.109	-0.146
5395	1.063	-0.728	-0.104	-0.146
5410	1.095	-0.728	-0.095	-0.146
5425	1.095	-0.723	-0.09	-0.146
5440	1.095	-0.718	-0.08	-0.146
5455	1.095	-0.718	-0.076	-0.146
5470	1.126	-0.713	-0.066	-0.146
5485	1.126	-0.713	-0.061	-0.146
5500	1.157	-0.704	-0.042	-0.146
5515	1.157	-0.704	-0.033	-0.146
5530	1.157	-0.699	-0.028	-0.146
5545	1.157	-0.699	-0.015	-0.146
5560	1.188	-0.691	-0.001	-0.146
5575 5590	1.188 1.22	-0.686 -0.686	0.009 0.018	-0.146 -0.146
5605	1.22	-0.681	0.028	-0.146
5620	1.22	-0.677	0.037	-0.146
5635	1.22	-0.677	0.042	-0.146
5650	1.22	-0.681	0.042	-0.146
5665	1.22	-0.681	0.037	-0.146
5680	1.22	-0.681	0.037	-0.146
5695	1.251	-0.677	0.047	-0.146
5710	1.251	-0.681	0.037	-0.146
5725	1.22	-0.681	0.037	-0.146
5740	1.22	-0.681	0.032	-0.146
5755	1.22	-0.686	0.028	-0.146
5770	1.188	-0.686	0.009	-0.146
5785 5800	1.157	-0.686	-0.038	-0.146 -0.146
5815	1.095 1.063	-0.686 -0.686	-0.076 -0.099	-0.146
5830	1.032	-0.686	-0.132	-0.146
5845	1.032	-0.686	-0.151	-0.146
5860	1.001	-0.686	-0.175	-0.146
5875	0.969	-0.691	-0.189	-0.146
5890	0.938	-0.695	-0.213	-0.146
5905	0.938	-0.691	-0.232	-0.146
5920	0.938	-0.691	-0.251	-0.146
5935	0.876	-0.695	-0.265	-0.146
5950	0.907	-0.695	-0.279	-0.146
5965	0.844	-0.695	-0.293	-0.146
5980	0.844	-0.695	-0.312	-0.146



page 11

APPENDIX D

Data Logger Water Level Measurements for Suwannee/Upper Floridan aquifer APT.

SE2000	suwd-d.wpd
Environmental Logger	
04/09 06:47	
Unit# 577 Test 2	
Setups: INPUT 1 INPUT 2 INPUT 3 INPUT 4 INPUT 5	
Type Level (F) Level (F) Level (F) Level (F)	
Mode Surface Surface Surface Surface	
I.D. 100 15 15 15 15	
Reference 0.000 0.000 0.000 0.000 0.000	
PSI at Ref. 37.226 6.352 2.580 1.669 11.179	
SG 1.000 1.000 1.000 1.000 1.000	
Linearity 0.144 0.073 0.081 0.147 0.110	
Scale factor 99.286 14.989 15.012 14.930 15.035	
Offset -0.222 0.034 -0.016 0.116 -0.026	
Delay mSEC 50.000 50.000 50.000 50.000 50.000	
Step 0 04/09 06:31:30	
Suwannee/UFA APT Drawdown Phase	
2004 A Standard Street works - 100000 (ASA A SA A SA A SA A SA A SA A SA	

0	-0.125	0	0	0.004	-0.009	
0.0083	0.406	0	0.004	0.014	-0.009	
0.0166	0.125	0	0.009	0.004	0	
0.025	-1.188	0	0	0.009	-0.009	
0.0333	-3.472	0	0.004	0.009	0	
0.0416	1.251	0	0.004	0.009	0.009	
0.05	-0.782	0.004	0.009	0.009	0	
0.0583	-1.22	0	0.004	0.009	0	
0.0666	-0.312	0	0	0.004	0	
0.075	-0.938	0	0.004	0.009	-0.009	
0.0833	-1.313	0	0.009	0.009	0	
0.0916	-1.376	0	0	0.009	0.004	
0.1	-2.002	0	0	0.009	-0.004	
0.1083	-1.22	0	0.004	0.009	0	
0.1166	-1.626	0	0.004	0.004	-0.004	
0.125	-29.246	0	0	0.009	-0.004	
0.1333	-15.39	0	0	0.009	0.004	
0.1416	-12.7	0	0.004	0.009	-0.004	
0.15	-14.953	0	0.004	0.009	-0.004	
0.1583	-13.326	0	0	0.009	-0.009	
0.1666	-13.889	0	0.004	0.009	-0.004	
0.175	-13.701	O	-0.004	0.009	-0.009	
0.1833	-14.014	0	0	0.009	-0.014	
0.1916	-14.702	0	0	0.009	-0.014	
0.2	-14.859	0	-0.004	0.009	-0.023	
0.2083	-15.422	0	0	0.009	-0.028	
0.2166	-15.953	0	-0.004	0.009	-0.028	
0.225	-16.423	0	-0.009	0.009	-0.028	
0.2333	-16.923	0	0	0.009	-0.033	
0.2416	-17.142	0	-0.009	0.009	-0.043	
0.25	-17 893	0	-0.009	0.009	-0.047	
0.2583	-18.299	0	-0.004	0.009	-0.052	
0.2666	-18.831	0	-0.009	0.009	-0.052	
0.275	-19.019	0	-0.014	0.004	-0.067	
0.2833	-19.613	0	-0.009	0.009	-0.067	
0.2916	-19.957	0	-0.014	0.009	-0.081	
0.3	-20.52	0	-0.014	0.009	-0.086	
0.3083	-20.833	0	-0.014	0.009	-0.095	
0.3166 0.325	-21.052 -21.49	0	-0.018 -0.018	0.009	-0.1 -0.105	
0.325	-21.49	0	-0.018 -0.014	0.009		
0.3355	-21.771	0	-0.014	0.009	-0.114	
0.35	-22.365	0	-0.014	0.009	-0.134	
0.3666	-23.116 -23.679	0	-0.028	0.009	-0.148	
0.3833	-23.0/9 -24.148	0	-0.023	0.009	-0.167	
0.4	-24.146 -24.836	0	-0.023	0.009	-0.186	
0.4100	-24.030	v	-0.033	0.009	-0.201	

SE2000
Environmental Logger
05/05 08:34
Unit# 577 Test 2
Setups: INPUT 1 INPUT 2 INPUT 3 INPUT 4 INPUT 5
Type Level (F) Level (F) Level (F) Level (F)
Mode Surface Surface Surface Surface
I.D. 100 15 15 15 15
Reference 0.000 0.000 0.000 0.000 0.000
PSI at Ref. 37.228 6.352 2.580 1.669 11.179
SG 1.000 1.000 1.000 1.000 1.000
Linearity 0.144 0.073 0.081 0.147 0.110
Scale factor 99.286 14.989 15.012 14.930 15.035
Offset -0.222 0.034 -0.016 0.116 -0.026
Delay mSEC 50.000 50.000 50.000 50.000 50.000
Step 1 04/10 06:37:32
Suwannee/UFA APT Recovery Phase
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0	-60.326	0.071	-0.534	-0.089	-8.514
0.0083	-60.17	0.071	-0.53	-0.094	-8.514
0.0166	-60.264	0.071	-0.544	-0.094	-8.514
0.025	-60.545	0.071	-0.534	-0.094	-8.514
0.0333	-60.326	0.071	-0.534	-0.094	-8.514
0.0416	-60.451	0.071	-0.534	-0.094	-8.514
0.05	-59.982	0.071	-0.534	-0.094	-8.514
0.0583	-60.357	0.071	-0.544	-0.094	-8.514
0.0666	-57.669	0.071	-0.534	-0.094	-8.514
0.075	-56.637	0.071	-0.534	-0.094	-8.514
0.0833	-56.606	0.071	-0.539	-0.094	-8.514
0.0916	-54.855	0.071	-0.534	-0.094	-8.514
0.1	-52.948	0.071	-0.53	-0.094	-8.514
0.1083	-51.572	0.071	-0.534	-0.094	-8.514
0.1166	-50.134	0.071	-0.534	-0.094	-8.514
0.125	-49.134	0.071	-0.534	-0.094	-8.514
0.1333	-48.227	0.071	-0.534	-0.094	-8.514
0.1416	-47.258	0.071	-0.534	-0.094	-8.514
0.15	-46.757	0.071	-0.534	-0.094	-8.514
0.1583	-46.382	0.071	-0.534	-0.094	-8.514
0.1666	-45.882	0.071	-0.534	-0.094	-8.514
0.175	-45.6	0.071	-0.534	-0.094	-8.514
0.1833	-45.632	0.071	-0.534	-0.094	-8.514
0.1916	-45.35	0.071	-0.534	-0.094	-8.514
0.2	-45.131	0.071	-0.534	-0.094	-8.514
0.2083	-45.038	0.071	-0.534	-0.094	-8.514
0.2166	-44.788	0.066	-0.534	-0.094	-8.514
0.225	-44.631	0.066	-0.534	-0.094	-8.514
0.2333	-44.475	0.066	-0.534	-0.094	-8.514
0.2416	-44.193	0.071	-0.534	-0.094	-8.509
0.25	-43.912	0.066	-0.534	-0.094	-8.509
0.2583	-43.787	0.071	-0.534	-0.094	-8.509
0.2666	-43.38	0.066	-0.534	-0.094	-8.504
0.275	-43.224	0.071	-0.534	-0.094	-8.504
0.2833	-42.974	0.066	-0.534	-0.094	-8.499
0.2916	-42.599	0.071	-0.53	-0.094	-8.49
0.3	-42.474	0.066	-0.534	-0.094	-8.485
0.3083	-42.224	0.066	-0.53	-0.094	-8.48
0.3166	-41.911	0.066	-0.534	-0.094	-8.476
0.325	-41.755	0.066	-0.53	-0.094	-8.471
0.3333	-41.504	0.066	-0.53	-0.094	-8.471
0.35	-41.16	0.066	-0.53	-0.094	-8.461
0.3666	-40.785	0.066	-0.53	-0.094	-8.456
0.3833 0.4	-40.441 -40.222	0.066 0.066	-0.53 -0.525	-0.094	-8.447
0.4	-40.222 -39.941	0.066	-0.525	-0.094 -0.094	-8.437 -8.433
0.4100	-00.041	0.000	-0.00	-0.089	-0.433

Suwa	nnee/Ul	FA APT Dra	wdown Phase				Suwannee/U	FA APT Re	cover <u>y Pha</u>
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0.4	333	-25.43	0	-0.028	0.009	-0.22	0.4333	-39.566	0.066
0.4	45	-25.587	0	-0.028	0.009	-0.229	0.45	-39.284	0.066
0.4	666	-26.087	õ	-0.037	0.009	-0.248	0.4666	-39.097	0.068
0.4	833	-26.4	0	-0.033	0.009	-0.263	0.4833	-38.878	0.066
0.	.5	-26.869	0	-0.033	0.009	-0.282	0.5	-38.377	0.066
	166	-27,182	0	-0.042	0.009	-0.296	0.5166	-38.127	0.071
	333	-27.526	0	-0.042	0.009	-0.311	0.5333	-38.065	0.066
0.		-27,964	0	-0.037	0.009	-0.32	0.55	-37.783	0.066
	666	-28.12	0	-0.042	0.009	-0.335	0.5666	-37.283	0.066
	833	-28.433	0.004	-0.047	0.009	-0.344	0.5833	-37.064	0.066
	.6	-28.839	0.004	-0.047	0.009	-0.354	0.6	-36.908	0.066
	166	-29.308	0	-0.042	0.009	-0.363	0.6166	-36.532	0.066
	333	-29.559	0.004	-0.047	0.009	-0.378	0.6333	-36.282	0.066
	65	-30.059	0	-0.052	0.009	-0.387	0.65	-36.032	0.066
	666	-30.466	0.004	-0.052	0.009	-0.397	0.6666	-35.782	0.066
	833	-30.841	0	-0.047	0.009	-0.411	0.6833	-35.532	0.066
	.7	-30.966	0.004	-0.056	0.009	-0.421	0.7	-35.313	0.066
	168	-31.56	0.004	-0.056	0.009	-0.43	0.7166	-34.969	0.066
	333	-31.654	0.004	-0.052	0.009	-0.44	0.7333	-34.75	0.066
	75	-32.029	0.004	-0.052	0.009	-0.454	0.75	-34.469	0.066
	666	-32.154	0.004	-0.056	0.009	-0.469	0.7666	-34.25	0.066
	833	-32.623	0.004	-0.066	0.009	-0.473	0.7833	-33.999	0.066
	.8	-32.811	0.004	-0.061	0.009	-0.488	0.8	-33.749	0.066
0.8		-33.124	0.004	-0.056	0.009	-0.502	0.8166	-33.53	0.066
		-33.437	0.004		0.009		0.8333	-33.33	0.066
0.8				-0.056		-0.512		-33.061	0.066
	85 88	-33.593	0.004	-0.061	0.009	-0.526	0.85		0.066
	666	-33.906	0.004	-0.061	0.009	-0.536	0.8666	-32.842	
	833	-34.406	0.004	-0.066	0.009	-0.545	0.8833	-32.623	0.066
	.9 466	-34.437	0.004	-0.066	0.009	-0.564	0.9	-32.373	0.066
0.9		-34,719	0.004	-0.071	0.009	-0.574	0.9166	-32.154	0.066 0.066
0.9		-35.094	0.004	-0.071	0.009	-0.583	0.9333	-31.935	
0.9		-35.876	0.004	-0.071	0.009	-0.598	0.95	-31.717	0.066 0,066
	666 800	-36.314	0.004	-0.071	0.009	-0.607	0.9666 0.9833	-31.498 -31.279	0,066
0.9		-36.658	0.004 0.004	-0.075 -0.071	0.009	-0.622	0.9633	-31.279	0.066
1		-36.908 -40.66		-0.085	0.009 0.009	-0.631 -0.78		-28.652	0.066
	.2	-43.005	0.004 0.004	-0.094	0.009	-0.933	1.2	-26.65	0,066
	.4	-44.6		-0.104	0.009		1.4		0.066
	.6		0.004		0.009	-1.076	1.6	-24.711	
1.		-46.257 -46.538	0.004	-0.118		-1.224	1.8 2	-23.022	0.066 0.066
	2		0.004	-0.123	0.009	-1.368		-21.458	
2.		-47.695	0.004	-0.132	0.009	-1.512	2.2	-20.082	0.066
2.		48.133	0.004	-0.137	0.009	-1.65	2.4	-18.769	0.066
2.		-49.259	0.009	-0.142	0.009	-1.784	2.6	-17.611	0.066
2.		-49.978	0.004	-0.146	0.009	-1.913	2.8	-16.516	0.066
	3	-50,447	0.009	-0.151	0.009	-2.042	3	-15.516	0.061
3. 3.		-50.447	0.009	-0.156 -0.16	0.009 0.009	-2.162	3.2	-14.577	0.066 0.061
		-51.135	0.009			-2.282 -2.391	3.4	-13.733 -12.951	0.061
3.		-51.541	0.009	-0.17	0.009		3.6		
3.		-51.604	0.009	-0.17	0.009	-2.506	3.8	-11.95	0.061
	4	-52.01	0.009	-0.175	0.004	-2.611	4	-11.136	0.061
4.		-52.26	0.009	-0.175	0.009	-2.712	4.2	-10.448	0.061
4.		-52.698	0.009	-0.179	0.004	-2.812	4.4	-9.823	0.061
4.		-53.011	0.009	-0.184	0.009	-2.908	4.6	-9.259	0.061
4.		-52.792	0.009	-0.184	0.009	-3.003	4.8	-8.759	0.061
5		-53.542	0.009	-0.189	0.004	-3.094	5	-8.258	0.061
5. 5		-53.386	0.009	-0.194	0.004	-3.18	5.2	-7.727	0.061
5. 5.		-53.73	0.009 0.009	-0.194 -0.194	0.004	-3.266	5.4	-7.289	0.061
5. 5.		-53.917 -54.292	0.009	-0.194	0.004	-3.348	5.6 5.9	-6.913 -6.528	0.061
ວ. 6		-54.292 -54.105	0.009	-0.198 -0.198	0.004	-3.429	5.8	-6.538	0.061
6.1		-54.105 -54.292	0.009	-0.198	0.009	-3.505	6	-6.225	0.061
6.4 6.4		-94.292 -54.605	0.009	-0.203 -0.208	0.004	-3.582	8.2 6.4	-5.912	0.061
0.4	-	-94.009	0.008	-0.200	0.004	-3.658	6.4	-5.631	0.061

Suwannee/UFA APT Recovery Phase

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Suwannee		wdown Phas	9			Suv	vannee	UFA APT Rec	overy Phase
			an a	lipse a brance	1953 5 27 Star (95				
6.6	-54.574	0.009	-0.208	0.004	-3.725		6.6	-5.349	0.061
6.8	-54.793	0.009	-0.208	0.004	-3.797		6.8	-5.099	0.056
7	-54.73	0.009	-0.213	0.004	-3.864		7	-4.911	0.061
7.2	-55.074	0.009	-0.213	0.004	-3.926		7.2	-4.723	0.061
7.4	-55.23	0.009	-0.213	0.004	-3.993		7.4	-4.411	0.061
7.6	-54.918	0.009	-0.222	0.004	-4.05		7.6	-4.192	0.056
7.8	-55.105	0.009	-0.217	0.004	-4.112		7.8	-4.004	0.056
8	-55.074	0.009	-0.222	0.004	-4.174		8	-3.816	0.056
8.2	-55.574	0.009	-0.222	0.004	-4.227		8.2	-3.66	0.056
8.4	-55.262	0.009	-0.231	0	-4.284		8.4	-3.503	0.056
8.6	-55.699	0.009	-0.227	0	-4.342		8.6	-3.347	0.058
8.8 9	-55.574	0.009	-0.231	0	-4.389		8.8	-3.159	0.056
9.2	-55.637 -55.699	0.009 0.009	-0.227 -0.227	0.004 0.004	-4.437 -4.49		9 9.2	-3.003 -2.878	0.056 0.056
9.4	-55.574	0.009	-0.227	0.004	-4.533		9.4	-2.753	0.056
9.6	-55.605	0.014	-0.231	0.004	-4.585		9.6	-2.627	0.056
9.8	-55.824	0.009	-0.236	0.004	-4.628		9.8	-2.44	0.056
10	-56.012	0.009	-0.236	0.004	-4.671		10	-2.471	0.056
12	-56.512	0.009	-0.25	-0.004	-5.058		12	-1.626	0.056
14	-56.637	0.009	-0.265	-0.004	-5.364		14	-1.126	0.056
16	-56.981	0.009	-0.274	-0.004	-5.612		16	-0.844	0.056
18	-57.044	0.009	-0.274	٥	-5.808		18	-0.656	0.056
20	-57.106	0.009	-0.284	0.004	-5.961		20	-0.5	0.056
22	-57.294	0.009	-0.298	-0.004	-6.104		22	-0.406	0.056
24	-57.481	0.009	-0.302	-0.004	-6.238		24	-0.344	0.056
26	-57.669	0.009	-0.307	-0.004	-6.352		26	-0.281	0.052
28	-57.919	0.014	-0.307	0	-6.462		28	-0.25	0.052
30 32	-58.044 -57.669	0.009 0.009	-0.317 -0.321	-0.004 -0.009	-6.557 -6.648		30 32	-0.187 -0.156	0.052 0.052
32 34	-57.669	0.009	-0.321	-0.009	-6.734		32 34	-0.156	0.052
36	-58.075	0.009	-0.326	-0.009	-6.81		36	-0.125	0.052
38	-57.7	0.009	-0.331	-0.009	-6.877		38	-0.093	0.052
40	-57.731	0.009	-0.336	-0.009	-6.939		40	-0.062	0.052
42	-57.825	0.009	-0.336	-0.009	-7.001		42	-0.062	0.056
44	-58.075	0.009	-0.34	-0.009	-7.059		44	-0.062	0.052
46	-57.669	0.009	-0.34	-0.004	-7.106		46	-0.031	0.052
48	-57.638	0.009	-0.35	-0.014	-7.154		48	-0.031	0.052
50	-58.044	0.009	-0.35	-0.014	-7.197		50	0	0.052
52	-57.856	0.009	-0.35	-0.014	-7.24		52	0	0.052
54	-57.606	0.009	~0.355	-0.014	-7.273		54	0	0.052
56	-57.856	0.009	-0.359	-0.014	-7.312		56	0	0.052
58	-57.95	0.004	-0.364	-0.018	-7.35		58	0.031	0.052
60 62	-57.919 -57.575	0.004 0.004	-0.364 -0.364	-0.018 -0.018	-7.378 -7.407		60 62	0.031 0.031	0,052 0,052
62 64	-57.763	0.004	-0.373	-0.013	-7.436		64	0.031	0.052
66	-57.825	0.004	-0.373	-0.018	-7.459		66	0.031	0.052
68	-57.763	0.009	-0.369	-0.023	-7.483		68	0.031	0.052
70	-57.825	0.009	-0.373	-0.018	-7.507		70	0.062	0.052
72	-57.783	0.009	-0.373	-0.018	-7.531		72	0.031	0.052
74	-57.45	0.009	-0.369	-0.018	-7.55		74	0.062	0.047
76	-57.7	0.009	-0.378	-0.018	-7.569		76	0.062	0.047
78	-57.888	0.009	-0.373	-0.018	-7.588		78	0.062	0.047
80	-57.606	0.009	-0.383	-0.018	-7.603		80	0.062	0.047
82	-57.763	0.009	-0.373	-0.018	-7.622		82	0.062	0.047
84	-57.638	0.009	-0.373	-0.014	-7.636		84	0.062	0.047
86 88	-57.95 -57.889	0.009	-0.383	-0.018	-7.65		86 86	0.062	0.047
88 90	-57.669 -57.575	0.009 0.00 9	-0.383 -0.383	-0.018 -0.023	-7.665 -7.679		88 90	0.062	0.047
90 92	-57.575 -57.45	0.009	-0.388	-0.023	-7.679 -7.688		90 92	0.062 0.062	0.047 0.047
94	-57.638	0.009	-0.392	-0.023	-7.703		92 94	0.062	0.047
96	-57.95	0.009	-0.388	-0.023	-7.717		96	0.062	0.047
98	-57.95	0.004	-0.392	-0.023	-7.731		98	0.062	0.047

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Suwannee	/UFA APT	Drawdown	Phase
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Suwannee	/UFA APT Drav	wdown Phae	3e			Suwannee/L	JFA APT Rec	overy Phase	÷
and a state of the second s					1994 5 2' See 08				
				and the second	Contraction (Contraction)	and the second second	and an		1993
100	-57.45	0.009	-0.388	-0.023	-7.741	100	0.093	0.047	
115	-57.575	0.009	-0.397	-0.028	-7.812	115	0.093	0.047	
130	-57.512	0.009	-0.402	-0.028	-7.875	130	0.093	0.042	
145	-57.825	0.009 0.004	-0.421	-0.032 -0.047	-7.908	145	0.093	0.042	
160 175	-57.419 -57.669	0.004	-0.454	-0.047 -0.047	-7.956 -7.989	160	0.093	0.042	
190	-57.325	0.004	-0.511 -0.558	-0.056	-8.027	175 190	0.093 0.062	0.037 0.037	
205	-57.325	-0.004	-0.591	-0.061	-8.056	205	0.093	0.037	
220	-57.294	-0.004	-0.62	-0.07	-8.084	220	0.093	0.037	
235	-57.387	-0.004	-0.643	-0.07	-8.089	235	0.093	0.033	
250	-57.45	-0.004	-0.667	-0.075	-8.108	250	0.093	0.037	
265	-57.231	-0.004	-0.676	-0.07	-8.108	265	0.093	0.037	
280	-56.825	-0.009	-0.695	-0.084	-8.123	280	0.093	0.037	
295	-56.418	-0.009	-0.71	-0.08	-8.118	295	0.093	0.037	
310	-56.825	-0.009	-0.714	-0.084	-8.127	310	0.093	0.037	
325	-56.887	-0.004	-0.681	-0.08	-8.118	325	0.093	0.037	
340	-57.012	-0.004	-0.686	-0.075	-8.127	340	0.093	0.037	
355	-56.731	-0.004	-0.705	-0.08	-8.156	355	0.062	0.037	
370	-56.512	0	-0.714	-0.075	-8.118	370	0.062	0.037	
385	-56.043	0	-0.728	-0.07	-8.094	385	0.062	0.037	
400	-59.419	0	-0.728	-0.061	-8.323	400	0.062	0.037	
415	-60.076	0.004	-0.728	-0.056	-8.456	415	0.062	0.042	
430 445	-59.388 -59.92	0.004 0.009	-0.738 -0.71	-0.051 -0.037	-8.476 -8.504	430 445	0.062	0.047 0.042	
445	-59.92	0.009	-0.705	-0.037	-8.523	460	0.062	0.042	
400	-59.545	0.003	-0.691	-0.018	-8.528	475	0.062	0.042	
490	-59.857	0.009	-0.657	-0.023	-8.538	490	0.031	0.047	
505	-61.014	0.014	-0.605	-0.018	-8.58	505	0.031	0.052	
520	-61.733	0.033	-0.572	-0.028	-8.633	520	0.031	0.056	
535	-61.201	0.028	-0.568	-0.037	-8.652	535	0.031	0.056	
550	-61.483	0.047	-0.544	-0.042	-8.662	550	0.031	0.056	
565	-61.108	0.066	-0.525	-0.028	-8.657	565	0.031	0.056	
580	-61.139	0.071	-0.511	-0.023	-8.647	580	0.031	0.056	
595	-61.233	0.075	-0.501	-0.014	-8.609	595	0.031	0.056	
610	-61.264	0.08	-0.482	-0.014	-8.59	610	0.031	0.052	
625	-60.451	0.08	-0.478	-0.004	-8.571	625	0.031	0.052	
640	-60.795	0.08	-0.473	-0.004	-8.561	640	0.031	0.052	
655	-60.607	0.08	-0.463	0	-8.552	655	0.031	0.052	
670	-61.076	80.0	-0.459	0	-8.542	670	0.031	0.052	
685	-60.795	80.0	-0.463	-0.004	-8.528	685	0.031	0.052	
700	-60.482 -60.826	0.08 0.08	-0.463 -0.463	0 0	-8.523 -8.504	700 715	0.031 0.031	0.052 0.052	
715 730	-60.526 -60.514	0.085	-0.463 -0.449	o	-8.485	730	0.031	0.052	
730	-60.764	0.08	-0.444	-0.004	-8.49	745	0.031	0.032	
760	-60.607	0.08	-0.459	-0.009	-8.48	760	0.031	0.052	
775	-60.951	0.08	-0.444	-0.009	-8.504	775	0.031	0.047	
790	-60.639	0.08	-0.454	-0.018	-8.518	790	0.031	0.047	
805	-60.264	0.075	-0.459	-0.028	-8.509	805	0.031	0.047	
820	-60.138	0.075	-0.468	-0.037	-8.504	820	0	0.042	
835	-60.232	0.071	-0.478	-0.047	-8.504	835	0	0.042	
850	-60.482	0.071	-0.473	-0.056	-8.514	850	0	0.042	
865	-60.576	0.066	-0.478	-0.065	-8.49	865	0	0.037	
880	-60.857	0.061	-0.501	-0.08	-8.514	880	0	0.037	
895	-60.514	0.061	-0.501	-0.094	-8.528	895	-0.031	0.033	
910	-60.67	0.056	-0.515	-0.103	-8.538	910	-0.031	0.033	
925	-60.451	0.061	-0.52	-0.108	-8.542	925	-0.031	0.033	
940	-60.545	0.061	-0.515	-0.113	-8.547	940	-0.031	0.033	
955	-60.545	0.061	-0.539	-0.122	-8.552	955	-0.031	0.028	•
970	-60.639	0.056	-0.539	-0.127	-8.552	970	-0.031	0.028	-
985	-60.545	0.061	-0.534	-0.131	-8.557	985	-0.031	0.028	•
1000 1015	-60.545 -60.732	0.061	-0.549	-0.136 -0.145	-8.561 8.566	1000	-0.062	0.028	
CTUTS	-60.732	0.056	-0.549	-0.145	-8.566	1015	-0.062	0.028	•

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1030	-60.576	0.056	-0.553	-0.155	-8.576
1045	-60.67	0.052	-0.572	-0.16	-8.58
1060	-60.514	0.056	-0.563	-0.16	-8.576
1075	-60.764	0.056	-0.577	-0.164	-8.59
1090	-60.357	0.056	-0.577	-0.169	-8.59
1105	-60.732	0.052	-0.586	-0.174	-8.58
1120	-60.389	0.056	-0.577	-0.169	-8.58
1135	-60.795	0.061	-0.586	-0.169	-8.576
1150	-60.42	0.056	-0.586	-0.169	-8.58
1165	-60.389	0.056	-0.582	-0.164	-8.576
1180	-60.42	0.061	-0.586	-0.16	-8.576
1195	-60.295	0.061	-0,586	-0.155	-8.576
1210	-60.451	0.066	-0.572	-0.15	-8.571
1225	-59.982	0.066	-0.577	-0.145	-8.571
1240	-60.201	0.066	-0.572	-0.141	-8.566
1255	-60.795	0.066	-0.577	-0.131	-8.561
1270	-60.389	0.071	-0.563	-0.127	-8.561
1285	-60.732	0.071	-0.568	-0.122	-8.547
1300	-60.138	0.071	-0.558	-0.117	-8.552
1315	-60.482	0.071	-0.549	-0.117	-8.552
1330	-60.514	0.071	-0.549	-0.108	-8.552
1345	-60.639	0.071	-0.539	-0.103	-8.552
1360	-60.201	0.071	-0.539	-0.098	-8.538
1375	-60.795	0.071	-0.549	-0.094	-8.533
1390	-60.232	0.075	-0.534	-0.094	-8.523
1405	-60.295	0.071	-0.534	-0.094	-8.528
1420	-60.764	0.071	-0.534	-0.089	-8.509

					tiput 5 C Saw OR
1030	-0.062	0.028	-0.231	-0.23	-0.205
1045 1060	-0.062 -0.062	0.028 0.028	-0.231 -0.236	-0.23 -0.235	-0.21 -0.215
1075	-0.093	0.028	-0.230	-0.233	-0.215
1090	-0.093	0.023	-0.246	-0.244	-0.22
1105	-0.093	0.023	-0.25	-0.249	-0.22
1120	-0.093	0.023	-0.25	-0.249	-0.22
1135	-0.093	0.023	-0.25	-0.249	-0.224
1150 1165	-0.093 -0.093	0.023 0.023	-0.246 -0.246	-0.235 -0.235	-0.215 -0.215
1180	-0.093	0.023	-0.241	-0.23	-0.215
1195	-0.093	0.023	-0.241	-0.226	-0.21
1210	-0.093	0.018	-0.246	-0.23	-0.22
1225	-0.093	0.018	-0.246	-0.226	-0.215
1240	-0.093	0.018	-0.246	-0.226	-0.215
1255 1270	-0.093 -0.093	0.018 0.018	~0.241 ~0.236	-0.221 -0.216	-0.21 -0.21
1285	-0.093	0.018	-0.231	-0.207	-0.201
1300	-0.062	0.014	-0.227	-0.202	-0.201
1315	-0.062	0.014	-0.222	-0.193	-0.196
1330	-0.062	0.014	-0.203	-0.188	-0.186
1345	-0.031	0.014	-0.189	-0.183	-0.172
1360	-0.031	0.014	-0.175	-0.174	-0.162
1375	-0.031 0	0.009 0.00 9	-0.165 -0.16	-0.169 -0.164	-0.153 -0.148
1390 1405	0	0.009	-0.151	-0.16	-0.143
1420	Ō	0.004	-0.146	-0.155	-0.138
1435	0	0.004	-0.142	-0.15	-0.129
1450	0	0.004	-0.137	-0.145	-0.124
1465	0.031	0	-0.127	-0.141	-0.124
1480	0.031	0	-0.123	-0.136	-0.119
1495	0.031	0	-0.118	-0.131	-0.114
1510 1525	0.031 0.031	0 0	-0.113 -0.104	-0.122 -0.122	-0.105 -0.1
1540	0.031	-0.004	-0.094	-0.127	-0.095
1555	0.031	-0.004	-0.094	-0.127	-0.1
1570	0.031	-0.009	-0.094	-0.131	-0.1
1585	0.031	-0.009	-0.094	-0.131	-0.1
1600	0.031	-0.014	-0.094	-0.136	-0.1
1615 1630	0.031 0.031	-0.018 -0.023	-0.099 -0.099	-0.145 -0.145	-0.1 -0.11
1645	0.031	-0.023	-0.094	-0.145	-0.105
1660	0.031	-0.028	-0.099	-0.145	-0.11
1675	0	-0.033	-0.104	-0.15	-0.114
1690	0.031	-0.033	-0.104	-0.15	-0.119
1705	0.031	-0.033	-0.099	-0.145	-0.114
1720	0.031	-0.028	-0.094	-0.145	-0.11
1735	0.031	-0.028	-0.099	-0.145	-0.114
1750 1765	0.031 0.031	-0.033 -0.037	-0.099 -0.099	-0.145 -0.145	-0.114 -0.114
1780	0	-0.037	-0.104	-0.15	-0.114
1795	0	-0.037	-0.099	-0.145	-0.114
1810	0	-0.042	-0.104	-0.145	-0.124
1825	0	-0.042	-0.099	-0.145	-0.114
1840	0	-0.042	-0.099	-0.131	-0.114
1855	0	-0.042	-0.099	-0.136	-0.114
1870 1885	0 0.031	-0.047 -0.042	-0.094 -0.089	-0.131 -0.122	-0.114 -0.1
1900	0.031	-0.042	-0.085	-0.122	-0.1
1915	0.031	-0.042	-0.075	-0.113	-0.095
1930	0.031	-0.042	-0.075	-0.103	-0.09
1 94 5	0.031	-0.042	-0.066	-0.094	-0.081

Suwannee/UFA APT Recovery Phase



Suwannee/U	IFA APT Rec	overy Phase	TRUE CONTRACTOR		
			- Max win &		
	isonikou dii	a de la compañía de l Compañía de la compañía			
1960	0.031	-0.042	-0.061	-0.089	-0.076
1975	0.031	-0.042	-0.056	-0.084	-0.071
1990	0.031	-0.042	-0.052	-0.08	-0.062
2005	0.062	-0.047	-0.052	-0.075	-0.062
2020	0.062	-0.047	-0.047	-0.075	-0.057
2035	0.062	-0.052	-0.047	-0.07	-0.052
2050 2065	0.062	-0.052 -0.056	-0.047 -0.042	-0.07 -0.065	-0.047 -0.043
2080	0.062	-0.052	-0.033	-0.061	-0.033
2095	0.093	-0.052	-0.028	-0.051	-0.023
2110	0.093	-0.056	-0.023	-0.051	-0.019
2125	0.093	-0.056	-0.014	-0.042	-0.014
2140	0.093	-0.056	-0.009	-0.042	-0.009
2155	0.093	-0.056	0	-0.037 -0.037	0 0
2170 2185	0.093 0.125	-0.061 -0.052	0.014	-0.028	0.014
2200	0.125	-0.056	0.014	-0.028	0.019
2215	0.125	-0.056	0.014	-0.032	0.019
2230	0.125	-0.061	0.018	-0.028	0.023
2245	0.125	-0.061	0.014	-0.037	0.019
2260	0,125	-0.066	0.009	-0.042	0.014
2275	0.125	-0.061	0.018	-0.037	0.023
2290 2305	0,125 0,125	-0.056 -0.056	0.023 0.023	-0.032 -0.037	0.028 0.028
2305	0.125	-0.052	0.023	-0.023	0.043
2335	0.156	-0.052	0.042	-0.018	0.047
2350	0,156	-0.052	0.042	-0.023	0.047
2365	0,156	-0.056	0.047	-0.018	0.047
2380	0.156	-0.052	0.052	-0.023	0.052
2395	0.156	-0.058	0.052	-0.018	0.052
2410	0,156	-0.056	0.052	-0.023	0.052
2425 2440	0.156 0.156	-0.056 -0.056	0.052 0.047	-0.023 -0.028	0.057 0.052
2455	0.135	-0.061	0.042	-0,032	0.047
2470	0.156	-0.061	0.042	-0.032	0.047
2485	0,156	-0.061	0.042	-0.037	0.047
2500	0.125	-0.066	0.037	-0.042	0.043
2515	0.125	-0.066	0.028	-0.051	0.038
2530	0.125	-0.066	0.033	-0.047	0.038
2545 2560	0.125 0.125	-0.066 -0.066	0.033 0.033	-0.047 -0.047	0.038 0.038
2575	0,125	-0.061	0.033	-0.042	0.038
2590	0.125	-0,061	0.033	-0.042	0.043
2605	0,156	-0.056	0.033	-0.042	0.043
2620	0.125	-0.052	0.037	-0.032	0.047
2635	0.156	-0.052	0.042	-0.032	0.047
2650	0.156	-0.047	0.047	-0.023	0.052
2665 2680	0.156 0.156	-0.042 -0.033	0.052 0.061	-0.014 -0.004	0.062 0.067
2695	0.156	-0.037	0.061	-0,004	0.067
2710	0,156	-0.028	0.066	0.009	0.076
2725	0.187	-0.018	0.075	0.018	0.086
2740	0.187	-0.009	0.089	0.032	0.1
2755	0.187	-0.009	0.094	0.037	0.1
2770	0.218	-0.004	0.104	0.051	0.11
2785 2800	0.218 0.218	0 0.004	0.108 0.118	0.056 0.07	0.119 0.124
2800	0.218	0.004	0.123	0.075	0.124
2830	0.25	0.014	0.132	0.084	0.143
2845	0.25	0.014	0.142	0.098	0.153
2860	0.25	0.014	0.146	0.098	0.153
2875	0.25	0.014	0.151	0.103	0.157

Suwannee/l	JFA APT Ree	covery Phase			
	Sector And Andrews	TANGARA ATANG Talam tara terda		ner de la compañía d Entre de la compañía d	NEW CONTRACTOR
			alita da como de la com Como de la como de la co		
2890	0.25	0.018	0.16	0.113	0,162
2905	0.25	0.018	0.165	0.117	0.167
2920	0.281	0.023	0.175	0.131	0.177
2935	0.281	0.023	0.179	0.136	0.181
2950	0.281	0.023	0.189	0.141	0.177
2965	0.281	0.028	0.198	0.155 0.16	0.186
2980 2995	0.281 0.281	0.023 0.023	0.198 0.203	0,164	0.196 0.196
3010	0.281	0.023	0.208	0,169	0.191
3025	0.281	0.018	0.203	0.164	0.181
3040	0.281	0.018	0.203	0.169	0.191
3055	0.281	0.018	0.203	0.164	0.191
3070	0.281	0.018	0.198	0.16	0.177
3085	0.281	0.018	0.203	0.169	0.191
3100 3115	0.281 0.281	0.018 0.018	0.198 0.203	0.164 0.169	0.172 0.186
3130	0.281	0.023	0.208	0.178	0.201
3145	0.281	0.023	0.217	0.183	0.181
3160	0.312	0.028	0.227	0.197	0.229
3175	0.312	0.028	0.227	0.197	0.196
3190	0.312	0.037	0.241	0.211	0.239
3205	0.312	0.037	0.236	0.207	0.224
3220	0.312	0.037	0.241	0.211	0.215
3235 3250	0.312 0.312	0.033 0.037	0.241 0.246	0.207 0.216	0.196 0.224
3265	0.312	0.037	0.246	0.216	0.234
3280	0.312	0.042	0.25	0.221	0.224
3295	0.312	0.042	0.255	0.226	0.239
3310	0.312	0.037	0.255	0.221	0.224
3325	0.312	0.042	0.265	0.23	0.239
3340	0.312	0.042	0.26	0.235	0.244
3355 3370	0.312 0.312	0.042 0.052	0.265 0.269	0.24 0.244	0.244 0.239
3385	0.312	0.052	0.279	0.244	0.239
3400	0.344	0.052	0.284	0.254	0.253
3415	0.344	0.056	0.288	0.263	0.268
3430	0.344	0.056	0.293	0.268	0.272
3445	0.344	0.056	0.298	0.268	0.268
3460	0.375	0.061	0.303	0.277	0.277
3475	0.375 0.375	0.066	0.307	0.282	0.282 0.277
3490 3505	0.375	0.066 0.066	0.307 0.312	0.282 0.287	0.277
3520	0.375	0.071	0.317	0.291	0.301
3535	0.375	0.071	0.317	0.291	0.301
3550	0.375	0.075	0.331	0.301	0.306
3565	0.375	0.08	0.331	0.306	0.315
3580	0.375	0.08	0.336	0.306	0.315
3595	0.406 0.406	0.08	0.336	0.306 0.301	0.315
3610 3625	0.406	0.08 0.085	0.336 0.336	0.301	0.315 0.32
3640	0.406	0.085	0.336	0.301	0.32
3655	0.406	0.085	0.331	0.296	0.315
3670	0.406	0.085	0.331	0.291	0.315
3685	0.406	0.085	0.331	0.287	0.315
3700	0.406	0.09	0.331	0.301	0.32
3715	0.406	0.094	0.34	0.31	0.33
3730 3745	.0.406	0.094	0.336	0.301	0.33
3745 3760	0.406 0.406	0.099 0.099	0.336 0.34	0.301 0.301	0.33 0.335
3775	0.406	0.099	0.34	0.291	0.335
3790	0.406	0.104	0.321	0.291	0.33
3805	0.406	0.108	0.34	0.291	0.33

Suwannee/UFA APT Drawdown Phase

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3 3 2 0 0 0.24 0.291 0.335 3 3 0.408 0.113 0.34 0.291 0.335 3 3650 0.408 0.113 0.336 0.221 0.333 3 3660 0.406 0.112 0.336 0.227 0.333 3 3660 0.406 0.132 0.331 0.263 0.333 3 3610 0.406 0.142 0.321 0.249 0.332 3 3625 0.406 0.161 0.336 0.224 0.333 3 3655 0.406 0.165 0.336 0.263 0.339 3 3655 0.406 0.165 0.336 0.254 0.339 4 0.406 0.165 0.336 0.254 0.339 4 0.406 0.164 0.344 0.263 0.339 4 0.406 0.164 0.345 0.262 0.339 <tr< th=""><th>Suwannee/L</th><th>JFA APT Re</th><th>covery Phase</th><th></th><th></th><th></th></tr<>	Suwannee/L	JFA APT Re	covery Phase			
3820 0.406 0.108 0.34 0.291 0.335 3845 0.406 0.113 0.336 0.222 0.335 3865 0.406 0.122 0.336 0.268 0.339 3865 0.406 0.132 0.331 0.263 0.333 3910 0.406 0.137 0.331 0.263 0.333 3925 0.406 0.161 0.336 0.263 0.335 3955 0.406 0.161 0.336 0.263 0.335 3955 0.406 0.165 0.336 0.224 0.335 3955 0.406 0.165 0.336 0.224 0.335 4000 0.406 0.175 0.34 0.263 0.339 4045 0.406 0.175 0.34 0.263 0.339 4045 0.406 0.189 0.345 0.268 0.344 4050 0.406 0.203 0.35 0.277 0.554 <td< th=""><th></th><th></th><th></th><th></th><th></th><th></th></td<>						
3850 0.406 0.113 0.336 0.222 0.33 3865 0.406 0.132 0.334 0.228 0.33 3865 0.406 0.132 0.331 0.228 0.33 3910 0.406 0.137 0.331 0.228 0.33 3925 0.406 0.142 0.321 0.249 0.325 3940 0.406 0.161 0.336 0.263 0.335 3955 0.406 0.165 0.336 0.263 0.335 3950 0.406 0.165 0.336 0.263 0.339 4000 0.406 0.175 0.34 0.263 0.339 4015 0.406 0.184 0.336 0.227 0.334 4030 0.406 0.203 0.35 0.277 0.354 4105 0.406 0.203 0.355 0.287 0.354 4115 0.437 0.213 0.356 0.287 0.354 4	 3820	0.406		0.34	0.291	0.335
3865 0.406 0.123 0.336 0.277 0.335 3890 0.406 0.132 0.331 0.228 0.339 3910 0.406 0.137 0.331 0.229 0.33 3925 0.406 0.142 0.321 0.249 0.325 3940 0.406 0.161 0.336 0.223 0.335 3955 0.406 0.165 0.336 0.224 0.335 3965 0.406 0.165 0.336 0.224 0.339 4000 0.406 0.175 0.34 0.223 0.339 4015 0.406 0.18 0.336 0.225 0.334 4045 0.406 0.189 0.35 0.277 0.354 4060 0.406 0.203 0.35 0.277 0.354 4105 0.406 0.203 0.35 0.277 0.354 4105 0.437 0.213 0.356 0.277 0.354 4	3835	0.406	0.113	0.34	0.291	0.335
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44950.4370.2650.3970.40.37845100.4370.2650.3970.40.37845250.4370.2650.3970.3950.37345400.4370.270.4020.4050.37845550.4690.2740.4070.4090.38245700.4690.2740.4070.4090.38245850.4690.2790.4110.4140.39246000.4690.2840.4160.4190.39246150.4690.2840.4160.4190.39746450.4690.2880.4210.4190.39746450.4690.3030.4350.4330.40646750.4690.3030.4350.4330.40646750.4690.3120.4350.4370.40647050.50.3170.440.4370.40647200.50.3170.4490.4420.416						
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46000.4690.2840.4160.4190.39246150.4690.2840.4160.4140.38746300.4690.2880.4210.4190.39746450.4690.2930.430.4280.41146600.4690.3030.4350.4330.40646750.4690.3070.4350.4330.41146900.4890.3120.4350.4370.40647050.50.3170.440.4370.40647200.50.3170.4490.4420.416	4570	0.469	0.274	0.407	0.409	0.382
46150.4690.2840.4160.4140.38746300.4690.2880.4210.4190.39746450.4690.2930.430.4280.41146600.4690.3030.4350.4330.40646750.4690.3070.4350.4330.41146900.4690.3120.4350.4370.40647050.50.3170.440.4370.40647200.50.3170.4490.4420.416						
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46900.4690.3120.4350.4370.40647050.50.3170.440.4370.40647200.50.3170.4490.4420.416						
4720 0.5 0.317 0.449 0.442 0.416						
			0.317	0.44	0.437	0.406
4735 0.5 0.322 0.449 0.447 0.416						
	4735	0.5	0.322	0.449	0.447	0.416

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Suwannee/	UFA <u>APT Rec</u>	overy Phase	1		Commence (175.00 - 3. Julio Science of
4750	0.5	0.326	0.449	0.452	0.43
4765	0.5	0.326	0.449	0.452	0.426
4780	0.5	0.331	0.454	0.447	0.426
4795	0.5	0.331	0.454	0.452	0.43
4810	0.5	0.331	0.454	0.447	0.421
4825 4840	0.5 0.5	0.336 0.341	0.454 0.459	0.452 0.456	0.426 0.43
4855	0.5	0.345	0.468	0.466	0.43
4870	0.5	0.35	0.463	0.466	0.44
4885	0.5	0.35	0.468	0.466	0.445
4900	0.5	0.35	0.463	0.466	0.43
4915	0.5	0.355	0.468	0.47	0.44
4930	0.5	0.355	0.468	0.466	0.44
4945 4960	0.5 0.5	0.355 0.36	0.463 0.463	0.461 0.461	0.435 0.44
4975	0.5	0.364	0.468	0.466	0.445
4990	0.5	0.369	0.473	0.47	0.449
5005	0.531	0.369	0.473	0.47	0.449
5020	0.5	0.369	0.468	0,466	0.445
5035	0.5	0.374	0.468	0.466	0.445
5050	0.5	0.374	0.468	0.466	0.449
5065 5080	0.531 0.5	0.379 0.379	0.468 0.468	0.466 0.466	0.449 0.449
5095	0.531	0.379	0.468	0.466	0.449
5110	0.5	0.383	0.463	0.461	0,449
5125	0.5	0.379	0.459	0.452	0.44
5140	0.5	0,379	0.454	0.442	0.44
5155	0.5	0.383	0.454	0.442	0.435
5170	0.5	0.383	0.449	0.433	0.435
5185	0.5	0.388	0.454 0.449	0.437	0.435 0.435
5200 5215	0.5 0.5	0.393 0.393	0.449	0.433 0.423	0.435
5230	0.5	0.397	0.449	0.423	0,435
5245	0.5	0.402	0.449	0.423	0.435
5260	0.5	0.407	0.454	0.428	0.44
5275	0.5	0.412	0.454	0.428	0.445
5290	0.5	0.416	0,459	0.428	0.445
5305 5320	0.5 0.5	0.421 0.426	0.463 0.463	0.433 0.433	0.449 0.454
5320 5335	0.531	0.420	0.463	0.433	0.454
5350	0.531	0.435	0.468	0.428	0.454
5365	0.531	0.44	0.468	0.433	0.459
5380	0.531	0.45	0.478	0.437	0.464
5395	0.531	0.454	0.478	0.437	0.464
5410	0.531	0.459	0.482	0.442	0.473
5425 5440	0.531 0.531	0.464 0.469	0.482 0.482	0.442 0.437	0.473 0.473
5455	0.531	0.473	0.482	0.437	0.473
5470	0.531	0.478	0.487	0.437	0.473
5485	0.531	0,483	0.487	0.442	0.478
5500	0.531	0.487	0.487	0.442	0.478
5515	0.531	0.492	0.487	0.442	0.478
5530	0.531	0.492	0.482	0.433	0.473
5545 5560	0.531	0.492	0.478	0.433	0.469
5560 5575	0.531 0.531	0.497 0.502	0.482 0.478	0.433 0.428	0.473 0.469
5590	0.531	0.502	0.478	0.428	0.469
5605	0.531	0.506	0.468	0.428	0.469
5620	0.531	0.506	0.468	0.423	0.469
5635	0.531	0.506	0.473	0.423	0.464
5650 5665	0.531	0.511	0.468	0.433	0.464
5665	0.531	0.516	0.468	0.428	0.464

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uwannee/u	JFA APT Dra	wdown Phas	ie			
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Suwannee/	UFA APT Rec	overy Phase			
				Serge Contraction of the second s	
2000		an a			
5680	0.531	0.521	0.463	0.423	0.459
5695	0.531	0.521	0.468	0.423	0.459
5710	0.531	0.525	0.468	0.423	0.459
5725 5740	0.531 0.531	0.53 0.53	0.463 0.463	0.423 0.423	0,459 0,459
5755	0.531	0.53	0.463	0.423	0.459
5770	0.531	0.535	0.463	0.423	0.454
5785	0.5	0.535	0.459	0.419	0.449
5800	0.5	0.535	0.454	0.419	0.449
5815 5830	0.5 0.5	0.54 0.54	0.454 0.454	0.419 0.419	0.445 0.445
5845	0.5	0.544	0.454	0.423	0.445
5860	0.531	0.549	0.459	0.428	0.449
5875	0.5	0.549	0.463	0.428	0.445
5890	0.531	0.554	0.463	0.428	0.445
5905 5920	0.531 0.531	0.554	0.468	0.437 0.447	0.445 0.464
5920	0.531	0.563 0.568	0.473 0.478	0.447	0.464
5950	0.531	0.573	0.478	0.456	0.459
5965	0.531	0.573	0.482	0.461	0.469
5980	0.531	0.578	0.482	0.456	0.464
5995	0.531	0.578	0.478	0.452	0.459
6010 6025	0.531 0.531	0.578 0.582	0.478 0.478	0.452 0.452	0.454 0.459
6040	0.531	0.587	0.478	0.456	0.459
6055	0.531	0.587	0.478	0.452	0.459
6070	0.531	0.596	0.478	0.447	0.464
6085	0.531	0.601	0.478	0.452	0.469
6100 6115	0.531 0.531	0.601 0.606	0.482 0.482	0.452 0.452	0.469 0.473
6130	0.531	0.611	0.482	0.452	0.473
6145	0.531	0.615	0.478	0.442	0.473
6160	0.531	0.62	0.492	0.456	0.478
6175	0.531	0.62	0.487	0.452	0.483
6190	0.531	0.625	0.478	0.437 0.419	0.473
6205 6220	0.531 0.563	0.625 0.639	0.463 0.478	0.419	0.464 0.478
6235	0.531	0.634	0.463	0.414	0.464
6250	0.531	0.649	0.473	0.428	0.478
6265	0.531	0.649	0.468	0.419	0.469
6280	0.563	0.658	0.478	0.428	0.478
6295 6310	0.563 0.563	0.663 0.672	0.473 0.492	0.423 0.437	0.478 0.497
6325	0.563	0.682	0.497	0.447	0.497
6340	0.563	0.686	0.497	0.447	0.502
6355	0.563	0.691	0.501	0.447	0.502
6370	0.594	0.696	0.511	0.452	0.512
6385 6400	0.594 0.594	0.696 0.701	0.506 0.506	0.452 0.456	0.507 0.512
6415	0.563	0.696	0.492	0.455	0.493
6430	0.563	0.701	0.492	0.437	0.497
6445	0.563	0.71	0.501	0.442	0.507
6460	0.563	0.71	0.497	0.442	0.502
6475	0.563	0.715	0.497	0.437	0.502
6490 6505	0.563 0.563	0.715 0.72	0.492 0.501	0.437 0.442	0.497 0.502
6520	0.594	0.729	0.501	0.452	0.502
6535	0.594	0.729	0.506	0.452	0.507
6550	0.594	0.729	0.497	0.442	0.507
6565	0.563	0.734	0.492	0.437	0.502
6580 6595	0.563 0.563	0.739 0.734	0.497 0.482	0.442	0.507
0000	0.000	0.734	V.90Z	0.423	0.493

Suwannee/UFA APT Drawdown Phase

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Suwannee/UFA APT Recovery Phase

Suwannee/UFA APT Recovery Phase						
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6610	0.563	0.739	0.487	0.428	0.497	
6625	0.563	0.748	0.497	0.442	0.507	
6640	0.594	0.758	0.506	0.461	0.512	
6655	0.594	0.758	0.511	0.461	0.516	
6670	0.594	0.767	0.511	0.466	0.521	
6685 6700	0.594 0.594	0.772 0.777	0.516 0.516	0.475 0.475	0.526 0.531	
6715	0.594	0.777	0.516	0.475	0.526	
6730	0.625	0.786	0.525	0.485	0.54	
6745	0.625	0.791	0.52	0.48	0.54	
6760	0.625	0.8	0.539	0.489	0.545	
6775	0.625	0.805	0.535	0.485	0.55	
6790	0.625	0.814	0.549	0.499	0.56	
6805	0.625	0.819	0.549	0.494	0.56	
6820 6835	0.657 0.625	0.824 0.829	0.553 0.558	0.499 0.499	0.564 0.564	
6850	0.657	0.833	0.563	0.503	0.569	
6865	0.657	0.843	0.568	0.513	0.574	
6880	0.657	0.848	0.572	0.518	0.579	
6895	0.657	0.857	0.577	0.522	0.588	
6910	0.657	0.862	0.587	0.527	0.593	
6925	0.688	0.867	0.587	0.527	0.598	
6940 6055	0.657	0.871	0.587	0.527	0.593	
6955 6970	0.688 0.688	0.876 0.881	0.587 0.591	0.527 0.532	0.593 0.598	
6985	0.688	0.885	0.591	0.527	0.603	
7000	0.688	0.895	0.596	0.532	0.603	
7015	0.688	0.9	0.601	0.536	0.607	
7030	0.688	0.9	0.591	0.532	0.603	
7045	0.657	0.9	0.591	0.527	0.598	
7060	0.688	0.909	0.596	0.536	0.603	
7075	0.688	0.914	0.596	0.536	0.603	
7090 7105	0.688 0.688	0.919 0.919	0.601 0.601	0.541 0.541	0.607 0.607	
7120	0.688	0.919	0.591	0.532	0.598	
7135	0.688	0.923	0.591	0.532	0.593	
7150	0.657	0.923	0.587	0.527	0.593	
7165	0.657	0.919	0.577	0.518	0.584	
7180	0.657	0.919	0.568	0.508	0.574	
7195	0.657	0.919	0.563	0.503	0.569	
7210 7225	0.625 0.625	0.919 0.923	0.553 0.553	0.499 0.494	0.56 0.555	
7240	0.625	0.923	0.549	0.494	0.555	
7255	0.625	0.928	0.549	0.494	0.555	
7270	0.625	0.933	0.553	0.499	0.555	
7285	0.625	0.938	0.549	0.499	0.55	
7300	0.625	0.938	0.549	0.503	0.55	
7315	0.625	0.942	0.553	0.503	0.555	
7330	0.625	0.942	0.549	0.503	0.55	
7345 7360	0.625 0.625	0.947 0.952	0.553 0.558	0.503 0.513	0.55 0.555	
7375	0.625	0.952	0.558	0.513	0.555	
7390	0.625	0.961	0.563	0.527	0.564	
7405	0.625	0.961	0.563	0.527	0.56	
7420	0.625	0.961	0.553	0.518	0.55	
7435	0.625	0.966	0.563	0.527	0.56	
7450	0.657	0.971	0.568	0.532	0.56	
7465 7480	0.657 0.657	0.98	0.568	0.536	0.564	
7480 7495	0.657 0.657	0.98 0.99	0.577 0.582	0.541 0.546	0.569 0.579	
7510	0.657	0.99	0.587	0.551	0.579	
7525	0.657	0.994	0.587	0.551	0.579	

Suwannee/UFA APT Recovery Phase

Suwannee/	JFA APT Rec	overy Phase	a dati ya o ngana da ana ana ana ana ana		
	OPAL TRAD	Aligne en e			
7540	0.888	1.004	0.596	0.565	0.588
7555	0.688	1.004	0.606	0.565	0.593
7570	0.688	1.013	0.61	0.574	0.603
7585	0.688	1.013	0.61	0.574	0.603
7600	0.688	1.018	0.61	0.569	0.593
7615	0.688	1.023	0.615	0.574	0.603
7630 7645	0.688 0.688	1.023 1.028	0.61 0.615	0.574 0.579	0.603 0.607
7660	0.688	1.037	0.62	0.579	0.612
7675	0.688	1.037	0.624	0.579	0.612
7690	0.688	1.047	0.629	0.588	0.612
7705	0.688	1.051	0.629	0.588	0.622
7720	0.688	1.051	0.634	0.588	0.622
7735	0.688	1.056	0.629	0.588	0.627
7750 7765	0.688 0.688	1.061	0.624	0.584	0.617
7780	0.688	1.061 1.061	0.624 0.62	0.584 0.579	0.617 0.612
7795	0.688	1.066	0.62	0.574	0.612
7810	0.688	1.066	0.62	0.574	0.607
7825	0.688	1.07	0.61	0.569	0.607
7840	0.688	1.07	0.61	0.56	0.603
7855	0.688	1.075	0.61	0.56	0.603
7870	0.657	1.075	0.601	0.555	0.598
7885	0.688 0.657	1.08	0.601	0.555	0.598
7900 7915	0.688	1.08 1.085	0.601 0.596	0.555 0.551	0.598 0.593
7930	0.688	1.089	0.596	0.551	0.593
7945	0.657	1.089	0.591	0.541	0.588
7960	0.657	1.089	0.587	0.536	0.584
7975	0.657	1.089	0.582	0.536	0.579
7990	0.657	1.099	0.587	0.541	0.588
8005	0.657	1.099	0.582	0.541	0.584
8020 8035	0.657 0.657	1.099 1.099	0.577 0.572	0.536 0.532	0.579 0.579
8050	0.657	1.099	0.572	0.532	0.574
8065	0.657	1.108	0.582	0.541	0.584
8080	0.657	1.113	0.591	0.546	0.588
8095	0.657	1.118	0.587	0.546	0.588
8110	0.657	1.122	0.587	0.546	0.588
8125	0.688	1.132	0.596	0.555	0.603
8140 8155	0.688	1.137	0.606	0.565	0.607
8170	0.688 0.688	1.137 1.146	0.606 0.61	0.565 0.569	0.607 0.612
8185	0.688	1.151	0.62	0.579	0.622
8200	0.719	1.156	0.62	0.574	0.622
8215	0.688	1.156	0.62	0.574	0.627
8230	0.719	1.17	0.634	0.584	0.641
8245	0.719	1.17	0.634	0.588	0.641
8260	0.719	1.184	0.653	0.602	0.655
8275 8290	0.719 0.719	1.184 1.189	0.653 0.653	0.602 0.602	0.66 0.66
8305	0.713	1.194	0.658	0.602	0.66
8320	0.75	1.198	0.662	0.607	0.665
8335	0.75	1.203	0.662	0.612	0.67
8350	0.75	1.208	0.672	0.616	0.674
8365	0.782	1.217	0.681	0.626	0.689
8380	0.75	1.217	0.677	0.621	0.689
8395 8410	0.782	1.227	0.681	0.626	0.689
8410 8425	0.75 0.75	1.222 1.222	0.672 0.672	0.612 0.612	0.684 0.684
8440	0.782	1.241	0.691	0.635	0.698
8455	0.782	1.246	0.691	0.631	0.698

Suwannee/L	JFA APT Red	overy Phase			
8470	0.782	4.05	0.000	0.635	0.703
8470 8485	0.782	1.25 1.255	0.696 0.696	0.635	0.708
8500	0.782	1.25	0.686	0.621	0.698
8515	0.782	1.255	0.691	0.621	0.698
8530	0.75	1.25	0.672	0.607	0.684
8545	0.75	1.25	0.667	0.602	0.679
8560	0.75	1.26	0.677	0.612	0.689
8575 8590	0.75 0.75	1.26 1.265	0.672 0.672	0.602 0.607	0.679 0.679
8605	0.75	1.265	0.667	0.602	0.679
8620	0.75	1.265	0.653	0.588	0.665
8635	0.719	1.265	0.643	0.579	0.655
8650	0.75	1.269	0.643	0.579	0.655
8665	0.719	1.269	0.639	0.574	0.646
8680	0.719	1.269	0.639	0.574	0.646
8695	0.719	1.279	0.643	0.579	0.651
8710 8725	0.719 0.719	1.279	0.639 0.634	0.579	0.641 0.646
8725 8740	0.719	1.279 1.288	0.634	0.574 0.588	0.651
8755	0.75	1.303	0.662	0.607	0.665
8770	0.719	1.298	0.653	0.598	0.66
8785	0.719	1.298	0.653	0.598	0.655
8800	0.719	1.298	0.658	0.607	0.651
8815	0.75	1.307	0.662	0.616	0.66
8830	0.75	1.307	0.662	0.616	0.66
8845	0.75	1.312	0.662	0.616	0.655
8860 8875	0.75 0.75	1.312 1.321	0.667 0.672	0.621 0.631	0.665 0.66
8890	0.75	1.321	0.681	0.645	0.67
8905	0.75	1.331	0.696	0.664	0.684
8920	0.782	1.34	0.71	0.682	0.694
8935	0.782	1.345	0.719	0.697	0.708
8950	0.782	1.345	0.714	0.692	0.703
8965	0.813	1.355	0.733	0.711	0.713
8980	0.813	1.355	0.733	0.711	0.718
8995 9010	0.813 0.813	1.359	0.738 0.743	0.715	0.727 0.732
9010	0.813	1.369 1.374	0.743	0.72 0.72	0.732
9040	0.844	1.393	0.757	0.72	0.756
9055	0.844	1.402	0.767	0.725	0.761
9070	0.844	1.407	0.771	0.73	0.765
9085	0.844	1.412	0.781	0.739	0.77
9100	0.844	1.416	0.781	0.739	0.775
9115	0.844	1.421	0.785	0.744	0.775
9130	0.875	1.43	0.795	0.753	0.789
9145 9160	0.875 0.875	1.428 1.435	0.79 0.795	0.748 0.753	0.78 0.789
9175	0.875	1.435	0.795	0.733	0.789
9190	0.875	1.44	0.795	0.748	0.785
9205	0.875	1.445	0.8	0.753	0.789
9220	0.844	1.445	0.795	0.748	0.785
9235	0.875	1.454	0.804	0.753	0.794
9250	0.875	1.459	0.804	0.758	0.799
9265	0.875	1.459	0.804	0.758	0.799
9280	0.875	1.459	0.804	0.753	0.799
9295 9310	0.875 0.875	1.464 1. 464	0.804 0.8	0.753 0.748	0.799 0.794
9325	0.875	1.464	0.8	0.748	0.794
9340	0.875	1.464	0.785	0.734	0.785
9355	0.875	1.468	0.785	0.73	0.78
9370	0.844	1.468	0.781	0.725	0.77
9385	0.844	1.473	0.785	0.73	0.785

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B		ever Phone			
Suwannee/	UFA APT Rec	overy Phase		CHURSE WARREN	
9400	0.875	1.478	0.781	0.73	0.78
9415	0.875	1.478	0.776	0.725	0.775
9430	0.844	1.478	0.776	0.72	0.775
9445	0.844	1.483	0.771	0.72	0.775
9460 9475	0.844 0.844	1.483 1.483	0.767 0.767	0.711 0.711	0.77 0.77
9490	0.844	1.487	0.762	0.711	0.765
9505	0.844	1.487	0.767	0.711	0.77
9520	0.844	1.492	0.767	0.715	0.77
9535	0.844	1.492	0.767	0.715	0.765
9550	0.844	1.497	0.767	0.72	0.775
9565	0.844	1.502	0.781	0.73	0.78
9580	0.875	1.511	0.785	0.739	0.789
9595	0.875	1.516	0.79	0.744	0.794
9610	0.875	1.521	0.795	0.748	0.799
9625	0.907	1.525	0.809	0.763 0.763	0.809
9640 9655	0.907 0.907	1.53 1.535	0.809 0.819	0.763	0.813 0.818
9655	0.907	1.539	0.823	0.781	0.818
9685	0.907	1.544	0.833	0.786	0.837
9700	0.907	1.549	0.838	0.791	0.842
9715	0.938	1.554	0.842	0.796	0.847
9730	0.938	1.563	0.852	0.805	0.856
9745	0.938	1,568	0.861	0.814	0.866
9760	0.938	1,577	0.871	0.824	0.876
9775	0.969	1.582	0.88	0.833	0.88
9790	0.969	1,587	0.89	0.838	0.89
9805	1.001	1.592	0.894	0.847	0.895
9820	1.001	1.596	0.899	0.847	0.9
9835	1.001	1.601	0.904	0.852	0.904
9850 9865	1.001 1.001	1.601 1.606	0.909 0.909	0.852 0.857	0.909 0.914
9880	1.001	1.615	0.918	0.861	0.923
9895	1.001	1.615	0.918	0.861	0.919
9910	1.001	1.82	0.918	0.861	0.928
9925	1.001	1.625	0.923	0.861	0.928
9940	1.001	1.625	0.923	0.861	0.928
9955	1.001	1.63	0.923	0.861	0.928
9970	1.001	1.634	0.923	0.861	0.928
9985	1.001	1.634	0.918	0,852	0.923
10000	1.001	1.634	0.918	0.847	0.923
10015	1.001	1.634	0.913	0.843	0.919
10030 10045	1.001 1.001	1.634 1.634	0.909 0.899	0.838	0.914 0.909
10045	1.001	1.634	0.695	0.828 0.824	0.909
10075	0.969	1.639	0.89	0.819	0.895
10090	0.969	1.644	0.89	0.819	0.9
10105	0.969	1.644	0.89	0.819	0.89
10120	0.969	1.644	0.88	0.814	0.89
10135	0.969	1.648	0.885	0.814	0.88
10150	0.969	1.648	0.88	0.814	0.885
10165	0.969	1.653	0.88	0.814	0.88
10180	0,969	1.653	0.88	0.819	0.876
10195	0.969	1.663	0.89	0.828	0.88
10210 10225	0.969 0.969	1.663	0.899	0.843	0.88
10225	0.969	1.667 1.672	0.904 0.909	0.861 0.871	0.895 0.89
10255	0.969	1.672	0.913	0.876	0.89
10270	1,001	1.677	0.918	0.885	0.914